

Angle-dependent operating device or method for obtaining a pseudo-stereophonic audio signal

The invention relates to audio signals (particularly
5 sound transducer signals) and to apparatuses and
methods for the obtainment, transmission,
transformation and reproduction thereof.

Generally, such systems attempt to depict or suggest
10 three-dimensional information which the human ear is
able to break down. This can be achieved by the
reproduction of two or more differently constituted
final signals, by the addition of artificial early
reflections or artificial diffuse sound or by the
15 simulation of audio circumstances relating to the human
head by means of HRTF, alternatively. These approaches
to a solution are used particularly in order to convert
monophonic audio signals into audio signals which
convey to the ear an actual or fictitious
20 three-dimensionality. Such methods are referred to as
"pseudo-stereophonic".

In comparison with conventional stereo signals,
pseudo-stereophonic signals usually exhibit
25 deficiencies. In particular, physico-acoustic reasons
mean that the localizability of the sound sources, for
example in the case of methods which distribute the
frequency spectrum with different phase shifts over the
final signals, is restricted. The application of
30 propagation time differences also normally results in
inconsistent localization for the same reasons.
Artificial reverberation, likewise for physico-acoustic
reasons, prompts fatigue phenomena in the listener. A
series of proposals have been made, particularly by
35 Gerzon (see below), which are intended to eliminate
such inconsistencies in the stereophonic depiction of
sound sources. Reproduction of the original
three-dimensional circumstances, as conventional stereo

signals aim to depict, does not usually occur even in complex applications, however.

In particular, pseudo-stereophony based on the simulation of intensity-stereophonic methods has the particular problem that a monophonic audio signal based on a figure-of-eight directivity pattern cannot be stereophonized, on account of the nondepiction of sound which is incident from the side.

The prior art is formed by the following documents:

US 5173944 considers signals, obtained at constant azimuth of 90 degrees, 120 degrees, 240 degrees and 270 degrees by means of HRTF from the differently delayed but uniformly amplified fundamental signal, which are overlaid on the fundamental signal. In this case, level and propagation time corrections remain independent of the original recording situation.

US 6636608 proposes phase shifts, determined on the basis of frequency, in the mono signal to be stereophonized which are overlaid on the original monophonic audio signal both in the left-hand and in the right-hand channel with different gains - which are likewise independent of the recording situation!

The aforementioned document US 5671287 (Gerzon) improves a method proposed by Orban (which takes a monophonic audio signal and obtains a summed signal and a difference signal which have frequency-dependent phase shifts - regardless of the recording situation!), these improvements likewise being based on frequency-dependent phase shifts or on a gain - regardless of the recording situation! - given slightly altered formation of the summed and difference signals.

The applicant's own European application No. 06008455.5 proposes methodical consideration of the manually or metrologically ascertained angle φ between principal axis and sound source using propagation time and level differences which are dependent on the angle φ . If the angle φ is equal to zero, however, compatible stereophonic depiction is not possible.

The invention explained below is intended to be a significant improvement in the stereophonic reproduction of a monophonic depicted sound source, taking account of the recording situation. In addition, a reliable method of stereophonization is intended to be provided for the aforementioned figure-of-eight directivity pattern, which has to date been problematical for intensity-stereophonic simulations. Subsequently, the aim is to allow compatible stereophonic depiction even for the case in which the angle φ between principal axis and sound source is equal to zero.

The subject matter of the invention can be presented as follows:

The technical solution-proposed in the applicant's own European application No. 06008455.5 - of methodical consideration of the angle φ between principal axis and sound source using propagation time and level differences which are dependent on the angle φ involves MS matrixing, where the following relationships apply to input signals M and S and resultant signals L and R:

$$(1) \quad L = (M + S) * \frac{1}{\sqrt{2}}$$

$$(2) \quad R = (M - S) * \frac{1}{\sqrt{2}}$$

The classic S signal—which is specific to MS engineering—has a figure-of-eight directivity pattern, said signal being offset from the M signal by 90
5 degrees to the left. If the level of the S signal is now increased in comparison with the M signal, what is known as the opening angle 2α (which is obtained from the points of intersection of the overlapping polar diagrams for the M system and the S system and—like
10 the figure-of-eight directivity pattern of the S system—is always situated symmetrically with respect to the principal axis of the M signal) is reduced to an increasing extent.

15 In a first step, it is possible to parameterize a fictitious opening angle 2α even in an arrangement or a method which takes account of the angle φ between the principal axis of the monophonic signal and the sound source. The calculated simulated side signal is then
20 dependent both on the angle φ and on half the fictitious opening angle α .

In a second step, gain factors are applied only to the signals which produce the side signal when summed.

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In a third step, the angle-dependent polar interval describing the directivity pattern of the M signal is parameterized. It is therefore now possible to stereophonize monophonic signals of arbitrary
30 directivity pattern taking account of a fictitious opening angle 2α .

Disclosure of the Invention

35 The invention involves the parameterization of a fictitious opening angle $\alpha + \beta$. In this case, α is the fictitious left-hand opening angle (situated to the left of the principal axis of the monophonic audio

signal to be stereophonized), β is the fictitious right-hand opening angle (situated to the right of the principal axis of the monophonic audio signal to be stereophonized), where it may be that $\alpha \neq \beta$. Thus, we are looking at the case - which does not arise in classic MS matrixing - of possible fictitious opening angles $\alpha + \beta$ which are *asymmetric* with respect to the principal axis of the monophonic audio signal to be stereophonized.

Accordingly, the trigonometrically ascertained level and propagation time differences for the simulated side signal are made dependent not only on φ and f but also on the fictitious left-hand opening angle α and on the fictitious right-hand opening angle β , wherein - if the sound source can be classified as being to the left of the principal axis - the relationship $\varphi \leq \alpha$ must apply or - if the sound source can be classified as being to the right of the principal axis - the relationship $\varphi \leq \beta$ must apply. In all cases, zero or a region around zero must be ruled out for α and β , since the level and propagation time differences calculated by parameterizing α and β converge toward infinity, that is to say are technically infeasible.

Suitable selection of α and β can therefore be used to attain stereophonic depiction of a monophonic audio signal, which usually affords more favorable conditions than methods which omit parameterization of a fictitious opening angle α and β . In particular, a compatible stereophonic resolution is also possible for the case in which φ is equal to zero. α and β can be chosen as desired subject to the above conditions or can be determined by a suitable algorithm as appropriate.

Trigonometrically, the following delay times $L(\alpha)$, $L(\beta)$ and gain factors $P(\alpha)$, $P(\beta)$ (which, in order to allow

unrestricted selection of φ , f and α and β , can be applied to the signals $S(\alpha)$ and $S(\beta)$ which produce the simulated side signal S) are obtained for the angle φ , the angle-dependent polar interval f describing the directivity pattern of the M signal and the angles α and β :

$$(3) \quad L_{\alpha} = -\frac{f(\alpha)}{2\sin\alpha} + \sqrt{\frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi}$$

$$(4) \quad L_{\beta} = -\frac{f(\beta)}{2\sin\beta} + \sqrt{\frac{f^2(\beta)}{4\sin^2\beta} + f^2(\varphi) + \frac{f(\beta)}{\sin\beta} * f(\varphi) * \sin\varphi}$$

$$(5) \quad P_{\alpha} = \frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi$$

$$(6) \quad P_{\beta} = \frac{f^2(\beta)}{4\sin^2\beta} + f^2(\varphi) + \frac{f(\beta)}{\sin\beta} * f(\varphi) * \sin\varphi$$

A simplification for apparatuses and methods which make use of the subject matter of the invention is the suggestion that the discriminants of $L(\alpha)$ and $L(\beta)$ can be used directly for ascertaining $P(\alpha)$ and $P(\beta)$. This significantly simplifies schematic diagrams and algorithms, which means miniaturization of the relevant hardware at the highest efficiency.

Particularly for the aforementioned problems of stereophonization of a monophonic audio signal with a figure-of-eight directivity pattern, the following solution is derived, on the basis of the polar interval $f(\psi) = \cos\psi$, which describes the figure-of-eight directivity pattern of the M signal and which is dependent on the polar angle ψ :

$$(7) \quad L_{\alpha} = -\frac{\cos \alpha}{2 \sin \alpha} + \sqrt{\frac{\cos^2 \alpha}{4 \sin^2 \alpha} + \cos^2 \varphi - \frac{\cos \alpha}{\sin \alpha} * \cos \varphi * \sin \varphi}$$

$$(8) \quad L_{\beta} = -\frac{\cos \beta}{2 \sin \beta} + \sqrt{\frac{\cos^2 \beta}{4 \sin^2 \beta} + \cos^2 \varphi + \frac{\cos \beta}{\sin \beta} * \cos \varphi * \sin \varphi}$$

$$(9) \quad P_{\alpha} = \frac{\cos^2 \alpha}{4 \sin^2 \alpha} + \cos^2 \varphi - \frac{\cos \alpha}{\sin \alpha} * \cos \varphi * \sin \varphi$$

$$(10) \quad P_{\beta} = \frac{\cos^2 \beta}{4 \sin^2 \beta} + \cos^2 \varphi + \frac{\cos \beta}{\sin \beta} * \cos \varphi * \sin \varphi$$

For the subject matter of the invention, it remains characteristic that the resultant MS signals finally
 5 need to be subjected to stereo conversion in accordance with formulae (1) and (2). A classic stereo signal is the result.

With the inclusion of apparatuses and methods which
 10 represent the prior art, it is otherwise possible to use the subject matter of the invention to obtain signals which provide stereophonic information via more than two loudspeakers (such as the surround-sound systems which are part of the prior art).

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Brief Description of the Figures

Embodiments and exemplary applications of the present invention are explained by way of example with
 20 reference to the following figures:

Figure 1 shows the operating principle of European Application No. 06008455.5.

Figure 2 shows a circuit which, in line with European Application No. 06008455.5, converts a monophonic audio signal into MS signals which can be stereophonized.

5 Figure 3 depicts the internal signals in the circuit shown in figure 2.

Figure 4 shows a classic MS arrangement for the half opening angle $\alpha = 135$ degrees, comprising an M system
10 with a cardioid directivity pattern and an S system with a figure-of-eight pattern.

Figure 5 shows a classic MS arrangement for the half opening angle $\alpha = 90$ degrees, comprising an M system
15 with an omnidirectional directivity pattern and an S system with a figure-of-eight directivity pattern.

Figure 6 shows a classic MS arrangement for the half opening angle $\alpha = 53$ degrees, comprising an M system
20 with a cardioid directivity pattern and an S system with a figure-of-eight directivity pattern.

Figure 7 shows a classic MS arrangement for the half opening angle $\alpha = 45$ degrees, comprising an M system
25 with a figure-of-eight directivity pattern and an S system with a figure-of-eight directivity pattern.

Figure 8 shows a classic MS arrangement for the half opening angle $\alpha = 33.5$ degrees, likewise comprising an M
30 system with a figure-of-eight directivity pattern and an S system with a figure-of-eight directivity pattern.

Figure 9 shows an extension of the operating principle of European Application No. 06008455.5, in which a
35 fictitious half opening angle α is also taken into account.

Figure 10 shows a circuit which converts a monophonic audio signal into MS signals, which can be stereophonized, taking account of a fictitious half opening angle α .

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Figure 11 shows an example of the operating principle of the invention for a signal with an omnidirectional directivity pattern which also takes account of a left-hand fictitious opening angle α and a right-hand fictitious opening angle β , which cannot arise in a classic MS arrangement on account of the use of a system with 90 degrees rotation to the left which is symmetrical with respect to the principal axis and which has a figure-of-eight directivity pattern for the S signal.

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Figure 12 shows an example of the operating principle of the invention for a signal having a cardioid pattern.

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Figure 13 shows an example of the operating principle of the invention for a signal having a hypercardioid pattern.

Figure 14 shows an example of the operating principle of the invention for a signal having a figure-of-eight directivity pattern.

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Figure 15 shows a circuit based on the subject matter of the invention which takes account of the recording angle φ , of a left-hand fictitious opening angle α , of a right-hand fictitious opening angle β and of an angle-dependent polar interval f describing the directivity pattern of the M signal in order to convert a monophonic audio signal into MS signals which can be stereophonized.

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Figure 16 shows a variant for the circuit in figure 15,
 wherein for the recording angle φ , the left-hand
 fictitious opening angle α and the angle-dependent
 polar interval f describing the directivity pattern of
 5 the M signal it must be true that the expression

$$(11) \quad \frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi$$

is not equal to zero or an element of a region around
 10 zero.

Figure 17 shows a further variant for the circuit in
 figure 15, wherein for the recording angle φ , the
 right-hand fictitious opening angle β and the
 15 angle-dependent polar interval f describing the
 directivity pattern of the M signal it must be true
 that the expression

$$(12) \quad \frac{f^2(\beta)}{4\sin^2\beta} + f^2(\varphi) + \frac{f(\beta)}{\sin\beta} * f(\varphi) * \sin\varphi$$

20 is not equal to zero or an element of a region around
 zero.

Figure 18 shows the parameters t_i , $P_i(t_i)$ from figure
 25 19.

Figure 19 shows the flowchart for a method based on the
 subject matter of the invention which takes account of
 the recording angle φ , of a left-hand fictitious
 30 opening angle α , of a right-hand fictitious opening
 angle β and of an angle-dependent polar interval f
 describing the directivity pattern of the M signal,
 given sufficiently small intervals $[t_i, t_{i+1}]$,
 in order to convert a monophonic audio signal into MS
 35 signals which can be stereophonized.

Detailed Embodiments and Exemplary Applications of the Invention

5 The prior art for the operating principle of an apparatus or a method for stereophonizing a monophonic signal having an omnidirectional directivity pattern is outlined in figure 1: a sound source 101 is recorded beneath position 102 by a microphone having an
10 omnidirectional directivity pattern, with the principal axis 103 and the directional axis 104 of the sound source forming the angle φ (105). 108 and 109 illustrate the geometric positioning of those two simulated signals which produce the simulated side
15 signal when summed. The propagation time difference in comparison with the principal signal for the simulated left-hand signal is 110, and the level of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from
20 101 and 112 (level correction taking account of the sound intensity, which decreases as the distance is squared). The propagation time difference in comparison with the principal signal for the simulated right-hand signal is 111, and the level of the simulated signal is
25 ascertained from the level of the principal signal, multiplied by the square of the distance from 101 and 113.

Reweightings the levels, which involves the input signal
30 being associated directly with the simulated left-hand signal, produces the circuit diagram in figure 2 for a circuit which converts a monophonic input signal into MS signals which can be stereophonized. Ascertained trigonometrically, the following are obtained in this
35 case for the propagation time differences L_A and L_B and the gain factors P_A and P_M :

$$(13) \quad L_A = \sqrt{\frac{5}{4} - \sin\varphi} - \frac{1}{2}$$

$$(14) \quad L_B = \sqrt{\frac{5}{4} + \sin\varphi} - \frac{1}{2}$$

$$(15) \quad P_M = \frac{1}{\frac{5}{4} - \sin\varphi}$$

$$(16) \quad P_B = \frac{\frac{5}{4} + \sin\varphi}{\frac{5}{4} - \sin\varphi}$$

The nature of the internally processed signals is shown in figure 3. The principal signal 316 is contrasted therein by two simulated signals 317 (with the delay time 310) and 318 (with the delay time 311) (where 314 is the time axis and 315 is the level axis). The maximum level point 302 is calculated from the maximum level point 312 on the basis of formula (15), and the maximum level point 313 is calculated on the basis of formula (16).

In order to derive apparatuses or methods operating on the basis of angle for the purpose of obtaining a pseudostereophonic audio signal, first of all the classic MS matrixing is considered for various half opening angles 2α and various directivity patterns of the M system. The symmetry of the S system with 90-degree rotation to the left with respect to the principal axis of the M system means that an inherent feature of all methods is an opening angle 2α which is likewise arranged symmetrically with respect to the principal axis and which is calculated from the points of intersection of the overlapping polar diagrams of the M system and the S system.

Thus, by way of example, figure 4 shows a classic MS arrangement for the half opening angle α (406) equal to 135 degrees, comprising an M system having a cardioid directivity pattern and an S system having a figure-of-eight directivity pattern. Figure 5 shows a classic MS arrangement for the half opening angle α (506) equal to 90 degrees, comprising an M system having an omnidirectional directivity pattern and an S system having a figure-of-eight directivity pattern. Figure 6 shows a classic MS arrangement for the half opening angle α (606) equals 53 degrees, comprising an M system having a cardioid directivity pattern and an S system having a figure-of-eight directivity pattern. Figure 7 shows a classic MS arrangement for the half opening angle α (706) equals 45 degrees, comprising an M system having a figure-of-eight directivity pattern and an S system having a figure-of-eight directivity pattern. Figure 8 shows a classic MS arrangement for the half opening angle α (806) equals 33.5 degrees, likewise comprising an M system having a figure-of-eight directivity pattern and an S system having a figure-of-eight directivity pattern.

An extension of the operating principle derived from figure 1 is the additional consideration of a fictitious half opening angle α , as shown in figure 9: in this case, a sound source 901 is recorded by a mono microphone 902 having an omnidirectional directivity pattern, where the principal axis 903 and the directional axis 904 of the sound source form the angle φ (905). Fresh consideration is given to the fictitious half opening angle α (906). This and the directivity pattern of the principal signal are used to directly derive the geometric positioning 908 of the simulated left-hand signal S_A and the geometric positioning 909 of the simulated right-hand signal S_B , which produce the simulated side signal when summed. The propagation time difference in comparison with the

principal signal for the simulated left-hand signal is 910, and the level of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 901 and 912 (level correction taking account of the sound intensity, which decreases as the distance is squared). The propagation time difference in comparison with the principal signal for the simulated right-hand signal is 911, and the level of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 901 and 913.

The associated circuit, which has been slightly modified in comparison with the circuit in figure 2, is provided by figure 10, which takes account of the fictitious half opening angle α in order to convert a monophonic audio signal into MS signals which can be stereophonized. In this case, the following relationships apply to the propagation time differences L_A and L_B and the gain factors P_A and P_B :

$$(17) \quad L_A = -\frac{1}{2\sin\alpha} + \sqrt{\frac{1}{4\sin^2\alpha} + 1 - \frac{\sin\varphi}{\sin\alpha}}$$

$$(18) \quad L_B = -\frac{1}{2\sin\alpha} + \sqrt{\frac{1}{4\sin^2\alpha} + 1 + \frac{\sin\varphi}{\sin\alpha}}$$

$$(19) \quad P_A = \frac{1}{4\sin^2\alpha} + 1 - \frac{\sin\varphi}{\sin\alpha}$$

$$(20) \quad P_B = \frac{1}{4\sin^2\alpha} + 1 + \frac{\sin\varphi}{\sin\alpha}$$

Application of the subject matter of the invention to a principal signal having an omnidirectional directivity pattern:

5 A first exemplary application of the invention, based on a monophonic audio signal having an omnidirectional directivity pattern, is shown in figure 11. In this case, in line with the invention, a fictitious opening angle $\alpha + \beta$ is parameterized, where α is the fictitious
 10 left-hand opening angle 1106 (situated to the left of the principal axis of the monophonic audio signal to be stereophonized), β is the fictitious right-hand opening angle 1107 (situated to the right of the principal axis of the monophonic audio signal to be
 15 stereophonized) - that is to say angles which cannot arise at all in a classic MS arrangement on account of the use of an S system having a figure-of-eight directivity pattern which has 90-degree rotation to the left and which is symmetrical with respect to the
 20 principal axis.

The subject matter of the invention accordingly leads to the consideration regarding the principal axis of the monophonic audio signal to be stereophonized with
 25 possibly *asymmetric* fictitious opening angles $\alpha + \beta$.

Considered in detail, the arrangement comprises a sound source 1101 which is recorded by a mono microphone 1102 having an omnidirectional directivity pattern, wherein
 30 the microphone principal axis 1103 and the directional axis 1104 of the sound source form the angle φ (1105). Subsequently, a fictitious left-hand opening angle α is parameterized (1106) and also a fictitious right-hand opening angle β (1107), wherein - if the sound source
 35 can be classified as being to the left of the principal axis - the relationship $\varphi \leq \alpha$ must apply or - if the sound source can be classified as being to the right of the principal axis - the relationship $\varphi \leq \beta$ must apply.

Furthermore, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time differences calculated trigonometrically by parameterizing α and β converge toward infinity, that is to say are technically infeasible).

Alpha, together with the directivity pattern of the principal signal, now determines exactly the geometric positioning 1108 of the simulated left-hand signal $S(\alpha)$, and β , together with the directivity pattern of the principal signal, determine exactly the geometric positioning 1109 of the simulated right-hand signal $S(\beta)$, which produce the simulated side signal when summed. The propagation time difference $L(\alpha)$ in comparison with the principal signal for the simulated left-hand signal is 1110, and the level $P(\alpha)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1101 and 1112 (level correction taking account of the sound intensity, which decreases as the distance is squared). The propagation time difference $L(\beta)$ in comparison with the principal signal for the simulated right-hand signal is 1111, and the level $P(\beta)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1101 and 1113.

Trigonometrically, the following delay times $L(\alpha)$, $L(\beta)$ and gain factors $P(\alpha)$, $P(\beta)$ (which, in order to allow unrestricted selection of φ , α and β , can be applied to the signals $S(\alpha)$ and $S(\beta)$ which produce the simulated side signal S , are accordingly obtained:

$$(21) \quad L_{\alpha} = -\frac{1}{2\sin\alpha} + \sqrt{\frac{1}{4\sin^2\alpha} + 1 - \frac{\sin\varphi}{\sin\alpha}}$$

$$(22) \quad L_{\beta} = -\frac{1}{2\sin\beta} + \sqrt{\frac{1}{4\sin^2\beta} + 1 + \frac{\sin\varphi}{\sin\beta}}$$

$$(23) \quad P_{\alpha} = \frac{1}{4\sin^2\alpha} + 1 - \frac{\sin\varphi}{\sin\alpha}$$

$$(24) \quad P_{\beta} = \frac{1}{4\sin^2\beta} + 1 + \frac{\sin\varphi}{\sin\beta}$$

Application of the subject matter of the invention to a principal signal having a cardioid pattern (figure 12):

5 The arrangement under consideration in the present case comprises a sound source 1201, which is recorded by a mono microphone 1202 having a cardioid directivity pattern, wherein the microphone principal axis 1203 and the directional axis 1204 of the sound source form the angle φ (1205). Subsequently, a fictitious left-hand opening angle α is parameterized (1206), and a fictitious right-hand opening angle β (1207), wherein again-if the sound source can be classified as being to the left of the principal axis-the relationship $\varphi \leq \alpha$ must apply or-if the sound source can be classified as being to the right of the principal axis-the relationship $\varphi \leq \beta$ must apply. Furthermore, in all cases, zero or a region around zero can again be ruled out for α and β (since the levels and propagation time differences trigonometrically calculated by parameterizing α and β likewise converge toward infinity, that is to say are technically infeasible).

α , together with the present directivity pattern for the principal signal, determines exactly the geometric positioning 1208 of the simulated left-hand signal

$S(\alpha)$, and β , likewise together with the directivity pattern under consideration here, determines exactly the geometric positioning 1209 of the simulated right-hand signal $S(\beta)$, which produce the simulated side signal when summed. The propagation time difference $L(\alpha)$ in comparison with the principal signal for the simulated left-hand signal is 1210, and the level $P(\alpha)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1201 and 1212 (level correction taking account of the sound intensity, which decreases as the distance is squared). The propagation time difference $L(\beta)$ in comparison with the principal signal for the simulated right-hand signal is 1211, and the level $P(\beta)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1201 and 1213.

Again, the following delay times $L(\alpha)$, $L(\beta)$ and gain factors $P(\alpha)$, $P(\beta)$ can be trigonometrically calculated taking account of the polar interval

$$f(\psi) = \frac{1}{2}(1 + \cos \Psi)$$

which describes the cardioid directivity pattern of the M signal and which is dependent on the polar angle Ψ (wherein the gain factors - in order to allow unrestricted selection of φ , α and β in relation to the directivity pattern - can be applied to the signals $S(\alpha)$ and $S(\beta)$ which produce the simulated side signal S):

$$(25) \quad L_{\alpha} = -\frac{(1 + \cos \alpha)}{4 \sin \alpha} + \sqrt{\frac{(1 + \cos \alpha)^2}{16 \sin^2 \alpha} + \frac{1}{4}(1 + \cos \varphi)^2 - \frac{(1 + \cos \alpha)}{4 \sin \alpha} * (1 + \cos \varphi) * \sin \varphi}$$

$$(26) \quad L_{\beta} = -\frac{(1 + \cos \beta)}{4 \sin \beta} + \sqrt{\frac{(1 + \cos \beta)^2}{16 \sin^2 \beta} + \frac{1}{4}(1 + \cos \varphi)^2 + \frac{(1 + \cos \beta)}{4 \sin \beta} * (1 + \cos \varphi) * \sin \varphi}$$

$$(27) \quad P_{\alpha} = \frac{(1 + \cos \alpha)^2}{16 \sin^2 \alpha} + \frac{1}{4}(1 + \cos \varphi)^2 - \frac{(1 + \cos \alpha)}{4 \sin \alpha} * (1 + \cos \varphi) * \sin \varphi$$

$$(28) \quad P_{\beta} = \frac{(1 + \cos \beta)^2}{16 \sin^2 \beta} + \frac{1}{4}(1 + \cos \varphi)^2 + \frac{(1 + \cos \beta)}{4 \sin \beta} * (1 + \cos \varphi) * \sin \varphi$$

Application of the subject matter of the invention to a signal having a hypercardioid pattern (figure 13):

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The arrangement comprises a sound source 1301 which is recorded by a mono microphone 1302 having a hypercardioid directivity pattern, wherein the microphone principal axis 1303 and the directional axis 1304 of the sound source form the angle φ (1305). Subsequently, a fictitious left-hand opening angle α is again parameterized (1306) and also a fictitious right-hand opening angle β (1307), wherein again-if the sound source can be classified as being to the left of the principal axis-the relationship $\varphi \leq \alpha$ must apply or-if the sound source can be classified as being to the right of the principal axis-the relationship $\varphi \leq \beta$ must apply. Again, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time differences trigonometrically calculated by parameterizing α and β converge toward infinity, that is to say are technically infeasible).

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α , again together with the hypercardioid pattern of the principal signal, determines exactly the geometric positioning 1308 of the simulated left-hand signal $S(\alpha)$, β , together with the hypercardioid directivity
 5 pattern, determines exactly the geometric positioning 1309 of the simulated left-hand signal $S(\beta)$, which produce the simulated side signal when summed. The propagation time difference $L(\alpha)$ in comparison with the principal signal for the simulated left-hand signal is
 10 1310, and the level $P(\alpha)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1301 and 1312 (level correction taking account of the sound intensity, which decreases as the distance is squared).
 15 The propagation time difference $L(\beta)$ in comparison with the principal signal for the simulated right-hand signal is 1311, and the level $P(\beta)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from
 20 1301 and 1313.

The delay times $L(\alpha)$, $L(\beta)$ and gain factors $P(\alpha)$, $P(\beta)$ can be (taking account of the polar interval

25 (28a)
$$f(\psi) = 1 - \frac{n}{2} + \frac{n}{2} * \cos \psi,$$

(where n assumes the value 1.5), which describes the hypercardioid directivity pattern of the M signal and which is dependent on the polar angle ψ)
 30 trigonometrically calculated (wherein the gain factors - in order to allow unrestricted selection of φ , α and β in relation to the directivity pattern - can be applied to the signals $S(\alpha)$ and $S(\beta)$, which produce the simulated side signal S):

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$$\begin{aligned}
 L_{\alpha} = & -\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \alpha)}{2 \sin \alpha} \\
 (29) \quad & + \sqrt{\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \alpha)^2}{4 \sin^2 \alpha} + (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi)^2} \\
 & \left[-\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \alpha)}{\sin \alpha} * (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi) * \sin \varphi \right]
 \end{aligned}$$

$$\begin{aligned}
 L_{\beta} = & -\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \beta)}{2 \sin \beta} \\
 (30) \quad & + \sqrt{\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \beta)^2}{4 \sin^2 \beta} + (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi)^2} \\
 & \left[+\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \beta)}{\sin \beta} * (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi) * \sin \varphi \right]
 \end{aligned}$$

$$\begin{aligned}
 P_{\alpha} = & \frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \alpha)^2}{4 \sin^2 \alpha} + (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi)^2 \\
 (31) \quad & -\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \alpha)}{\sin \alpha} * (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi) * \sin \varphi
 \end{aligned}$$

$$\begin{aligned}
 P_{\beta} = & \frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \beta)^2}{4 \sin^2 \beta} + (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi)^2 \\
 (32) \quad & +\frac{(1 - \frac{n}{2} + \frac{n}{2} * \cos \beta)}{\sin \beta} * (1 - \frac{n}{2} + \frac{n}{2} * \cos \varphi) * \sin \varphi
 \end{aligned}$$

Application of the subject matter of the invention to signals having further special forms of a cardioid pattern:

5 If the input signal to be stereophonized has special forms of the cardioid pattern, the relevant propagation time differences $L(\alpha)$ and $L(\beta)$ and gain factors $P(\alpha)$ and $P(\beta)$ can easily be calculated from formulae (29) to (32). In this case, the following applies for n:
10 $0 \leq n \leq 2$.

If n assumes the value 1, the gain factors and propagation time differences for an input signal having a classic cardioid directivity pattern are obtained,
15 for the value 0 the gain factors and propagation time differences for an input signal having an omnidirectional directivity pattern are obtained, for the value 2 the gain factors and propagation time differences for an input signal having a classic
20 figure-of-eight directivity pattern are obtained. If n assumes the value 1.25, the propagation time differences and gain factors for an input signal having a supercardioid pattern are obtained.

25 The application of formula (28a) to the polar interval f , resulting in the set of formulae (29) to (32), is accordingly found to be particularly favorable. Only the parameter n needs to be stipulated in order to describe almost all possible directivity patterns for
30 the M signal, expressed in polar coordinates (apart from the directional pattern, which, as frequency rises, increasingly has polar coordinates other than it (28a) is able to represent).

35 Application of the subject matter of the invention to a signal having a figure-of-eight pattern:

Figure 14 again shows a detailed illustration of the instance of application for an input signal having a figure-of-eight directivity pattern, which has already been discussed more than once above. The arrangement

5 comprises a sound source 1401 which is recorded by a mono microphone 1402 having a figure-of-eight directivity pattern, wherein the microphone principal axis 1403 and the directional axis 1404 of the sound source form the angle φ (1405). A fictitious left-hand

10 opening angle α is parameterized (1406) and also a fictitious right-hand opening angle β (1407), wherein again-if the sound source can be classified as being to the left of the principal axis-the relationship $\varphi \leq \alpha$ must apply or-if the sound source can be

15 classified as being to the right of the principal axis-the relationship $\varphi \leq \beta$ must apply. Subsequently, in all cases, zero or a region around zero can likewise be ruled out for α and β (since the levels and propagation time differences trigonometrically

20 calculated by parameterizing α and β likewise converge toward infinity, that is to say are technically infeasible).

α , together with the figure-of-eight directivity

25 pattern of the principal signal, determines exactly the geometric positioning 1408 of the simulated left-hand signal $S(\alpha)$, and β , together with the figure-of-eight directivity pattern, determines exactly the geometric positioning 1409 of the simulated right-hand signal

30 $S(\beta)$, which produce the simulated side signal when summed. The propagation time difference $L(\alpha)$ in comparison with the principal signal for the simulated left-hand signal is 1410, and the level $P(\alpha)$ of the simulated signal is ascertained from the level of the

35 principal signal, multiplied by the square of the distance from 1401 and 1412 (level correction taking account of the sound intensity, which decreases as the distance is squared). The propagation time difference

$L(\beta)$ in comparison with the principal signal for the simulated right-hand signal is 1411, and the level $P(\beta)$ of the simulated signal is ascertained from the level of the principal signal, multiplied by the square of the distance from 1401 and 1413. The associated set of formulae for the delay times $L(\alpha)$, $L(\beta)$ and the gain factors $P(\alpha)$, $P(\beta)$ can be taken from equations (7) to (10), and from equations (29) to (32), if n is equal to 2 (where the gain factors - in order to allow unrestricted selection of φ , α and β in relation to the directivity pattern - can be applied to the signals $S(\alpha)$ and $S(\beta)$ which produce the simulated side signal S).

Application of the subject matter of the invention to a circuit for stereophonizing a mono signal:

Figure 15 shows a circuit based on the subject matter of the invention which generalizes the directivity pattern of the input signal and which takes account of the recording angle φ , of a left-hand fictitious opening angle α , of a right-hand fictitious opening angle β and of an angle-dependent polar interval f describing the directivity pattern of the M signal in order to convert a monophonic audio signal into MS signals which can be stereophonized. In this case, formulae (3) to (6) can be used for the propagation time differences $L(\alpha)$ and $L(\beta)$ and the gain factors $P(\alpha)$ and $P(\beta)$. The input signal is used directly as the M signal in this case. The S signal is added up from the input signal delayed by the delay time $L(\alpha)$, which input signal is subsequently amplified by the gain factor $P(\alpha)$, and a further signal which represents the input signal delayed by the delay time $L(\beta)$, subsequently amplified by the gain factor $P(\beta)$. Again, the relationship $\varphi \leq \alpha$ must apply - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Similarly, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time

differences trigonometrically calculated by parameterizing α and β converge toward infinity, that is to say are technically infeasible).

- 5 Derivations of circuits which deliver equivalent signals under slight restrictions:

Figure 15 can be used to infer a slightly restrictedly operating circuit of the form in figure 16 when the gain factors are reweighted. In this case, the restriction is the condition that for the recording angle φ , the left-hand fictitious opening angle α and the angle-dependent polar interval f describing the directivity pattern of the M signal it must be true
15 that the expression

$$(33) \quad \frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi$$

is not equal to zero or an element of a region around zero. The propagation time differences $L(\alpha)$ and $L(\beta)$ cited in figure 16 directly represent equations (3) and (4) in this case; for the gain factors P_M and $P(\beta)$, the relationships

$$(34) \quad P_M = \frac{1}{\frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi}$$

$$(35) \quad P_\beta = \frac{\frac{f^2(\beta)}{4\sin^2\beta} + f^2(\varphi) + \frac{f(\beta)}{\sin\beta} * f(\varphi) * \sin\varphi}{\frac{f^2(\alpha)}{4\sin^2\alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin\alpha} * f(\varphi) * \sin\varphi}$$

25

apply.

In addition, the relationship $\varphi \leq \alpha$ must apply - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Again, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and
 5 propagation time differences trigonometrically calculated by parameterizing α and β converge to some extent toward infinity, that is to say are technically infeasible).

10 A second derivation from figure 15 given a change in the reweighting of the gain factors produces a likewise slightly restrictedly operating circuit in the form from figure 17, wherein it must be true for the recording angle φ , the right-hand fictitious opening
 15 angle β and the angle-dependent polar interval f describing the directivity pattern of the M signal that the expression

$$(36) \quad \frac{f^2(\beta)}{4 \sin^2 \beta} + f^2(\varphi) + \frac{f(\beta)}{\sin \beta} * f(\varphi) * \sin \varphi$$

20 is not equal to zero or an element of a region around zero. The propagation time differences $L(\alpha)$ and $L(\beta)$ cited in figure 17 are again equations (3) and (4) in this case; for the gain factors P_M and $P(\alpha)$, however,
 25 the relationships

$$(37) \quad P_M = \frac{1}{\frac{f^2(\beta)}{4 \sin^2 \beta} + f^2(\varphi) + \frac{f(\beta)}{\sin \beta} * f(\varphi) * \sin \varphi}$$

$$(38) \quad P_\alpha = \frac{\frac{f^2(\alpha)}{4 \sin^2 \alpha} + f^2(\varphi) - \frac{f(\alpha)}{\sin \alpha} * f(\varphi) * \sin \varphi}{\frac{f^2(\beta)}{4 \sin^2 \beta} + f^2(\varphi) + \frac{f(\beta)}{\sin \beta} * f(\varphi) * \sin \varphi}$$

now apply.

Again, the relationship $\varphi \leq \alpha$ must apply - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Similarly, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time differences trigonometrically calculated by parameterizing α and β converge to some extent toward infinity, that is to say are technically infeasible).

Application of the subject matter of the invention to a computation method for stereophonizing a mono signal:

A monophonic input signal can be arithmetically represented using a coordinate system in the form in figure 18, where 1814 is the time axis and 1815 is the level axis. 1819 is the time t_i , and 1820 is the level point $P_i(t_i)$ correlated to t_i . For sufficiently small intervals $[t_i, t_{i+1}]$, that is to say a sufficient sampling rate, it is now possible to depict the sound event with sufficient accuracy.

Figure 19 shows the associated flowchart for a method based on the subject matter of the invention which takes account of the recording angle φ , of a left-hand fictitious opening angle α , of a right-hand fictitious opening angle β and of an angle-dependent polar interval f describing the directivity pattern of the M signal, given sufficiently small intervals $[t_i, t_{i+1}]$, in order to convert a monophonic audio signal into MS signals which can be stereophonized (under the simplifying assumption that the propagation time difference $L(\alpha)$ or the propagation time difference $L(\beta)$ remains unequal to zero).

For the propagation time differences $L(\alpha)$ and $L(\beta)$ and the gain factors $P(\alpha)$ and $P(\beta)$, equations (3) to (6) again subsequently apply.

An M signal (the array $[M_i(t_i)]$) and an S signal (the array $[S_i(t_i)]$), which is actually added up from the input signal delayed by the delay time $L(\alpha)$, which input signal is subsequently amplified by the gain factor $P(\alpha)$, and a further signal, which is the input signal actually delayed by the delay time $L(\beta)$, subsequently amplified by the gain factor $P(\beta)$. The algorithm rules out inadmissible values of α and β . In general, the relationship $\varphi \leq \alpha$ must apply for such algorithms - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Similarly, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time differences trigonometrically calculated by parameterizing α and β converge toward infinity, that is to say are technically infeasible).

Derivations of two computation methods which deliver equivalent signals under slight restrictions:

20

Method 1: If it remains algorithmically assured that (33) is not equal to zero or an element of a region around zero, a computation method similar to figure 19 can be applied to a monophonic input signal for sufficiently small intervals $[t_i, t_{i+1}]$ in a manner shown in figure 16, but with the M signal (the array $[M_i(t_i)]$) now appearing amplified by the factor (34). The S signal (the array $[S_i(t_i)]$) is the result of the addition of the input signal (the array $[P_i(t_i)]$) actually delayed by the delay time $L(\alpha)$ (see formula (3)) to the input signal (again the array $[P_i(t_i)]$) actually delayed by the delay time $L(\beta)$ (see formula (4)) and then amplified by the factor $P(\beta)$ ' (see formula (35)). The algorithm must rule out inadmissible values of α and β : the relationship $\varphi \leq \alpha$ must apply - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Similarly, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and

propagation time differences trigonometrically calculated by parameterizing α and β converge to some extent toward infinity, that is to say remain technically infeasible).

5

Method 2: If it remains algorithmically assured that (36) is not equal to zero or an element of a region around zero, a computation method similar to figure 19 can likewise be applied to a monophonic input signal for sufficiently small intervals $[t_i, t_{i+1}]$ in the manner of figure 17, with the M signal (the array $[M_i(t_i)]$) now appearing amplified by the factor (37). The S signal (the array $[S_i(t_i)]$) is the result of the addition of the input signal (the array $[P_i(t_i)]$) actually delayed by the delay time $L(\alpha)$ (see formula (3)) and subsequently amplified by the gain factor $P(\alpha)'$ (see formula (38)) to the input signal (again the array $[P_i(t_i)]$) actually delayed by the delay time $L(\beta)$ (see formula (4)). The algorithm must rule out inadmissible values of α and β . The relationship $\varphi \leq \alpha$ must apply - if $\varphi > 0$ - or the relationship $|\varphi| \leq \beta$ must apply - if $\varphi < 0$. Similarly, in all cases, zero or a region around zero can be ruled out for α and β (since the levels and propagation time differences trigonometrically calculated by parameterizing α and β converge to some extent toward infinity, that is to say remain technically infeasible).

Observed overall, the apparatuses and methods described naturally also permit the amplification of the respective input signal before a subsequent delay is executed.

Examples of areas of application for the invention

35

The three-dimensional breakdown of a sound source recorded at a particular angle φ has great practical significance particularly for telephone signals. In the

case of hands-free devices, such as are used in automobiles or for internet telephony, the monophonic signal emitted is perceived as not corresponding to the real call situation; the opposite appears
 5 "omnipresent". If, however, metrological methods associated with the prior art are used to ascertain the angle φ or to functionally interpolate the polar coordinates (possible by virtue of algorithmic consideration of the maxima and minima in the polar
 10 diagram of the input signal), and if the fictitious left-hand opening angle α and the fictitious right-hand opening angle β are subsequently matched algorithmically or manually to the recording and listening situation, it is possible to use a
 15 (miniaturizable!) circuit in the form in figure 15, for example, to attain a stereophonic signal, during final MS matrixing, which takes much greater account of a call situation under natural conditions.

20 The procedure may be similar with monophonic sound recordings in which sound sources need to be reproduced stereophonically.

Similarly, if the direction of depiction of a sound
 25 source - insulated by means of signal processing - within a stereo image is perceived as being too acute, the direction of depiction can be gradually dispersed by applying the subject matter of the invention.

30 The shaping of the directivity pattern of the input signal (possible point by point by varying the polar coordinates which describe the directivity pattern of the input signal, comprehensively possible, by way of example, by means of the application - associated with
 35 the prior art - of comb filters in conjunction with methods based on fast Fourier transformation (FFT)) before it passes through an arrangement or a method in accordance with the subject matter of the invention can

sometimes improve the result further or ensure that the directivity pattern of the input signal is normalized.

5 The invention can achieve an overall significant contribution to the retrospective multidimensional consideration of signal paths. The application thereof is therefore not limited to the examples above.

Patent Claims

1. An apparatus for stereophonizing a mono signal,
characterized by
- 5 (a) the evaluation of the manually or metrologically
ascertained angle φ between sound source and microphone
principal axis in combination with
- 10 (aa) an arbitrarily or algorithmically determined
fictitious opening angle α , which adjoins the
microphone principal axis on the left, is not an
element of a region around zero or equal to zero, and
for which, if the angle φ is positive, the condition is
15 satisfied that the angle φ is less than or equal to the
angle α ;
- (bb) an arbitrarily or algorithmically determined
fictitious opening angle β , which adjoins the
20 microphone principal axis on the right, is not an
element of a region around zero or equal to zero, and
for which, if the angle φ is negative, the condition is
satisfied that the magnitude of the angle φ is less
than or equal to the angle β ;
- 25 (cc) the manually or metrologically determined
directivity pattern of the mono signal to be
stereophonized, representable in polar coordinates;
- 30 (b) the calculation of the gain factor $P(\alpha)$, which is
dependent on the angle φ , on the angle α and on the
directivity pattern of the mono signal to be
stereophonized (representable in polar coordinates);
- 35 (c) the calculation of the gain factor $P(\beta)$, which is
dependent on the angle φ , on the angle β and on the
directivity pattern of the mono signal to be
stereophonized (representable in polar coordinates);

(d) the calculation of the delay time $L(\alpha)$, which is dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(e) the calculation of the delay time $L(\beta)$, which is dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(f) the direct use of the mono signal to be stereophonized as the principal signal;

(g) the delay of the mono signal to be stereophonized by the delay time $L(\alpha)$ and amplification of the delayed signal by the gain factor $P(\alpha)$; or alternatively: the amplification of the mono signal to be stereophonized by the gain factor $P(\alpha)$ and the delay of the amplified signal by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized by the delay time $L(\beta)$ and amplification of the delayed signal by the gain factor $P(\beta)$; or alternatively: the amplification of the mono signal to be stereophonized by the gain factor $P(\beta)$ and the delay of the amplified signal by the delay time $L(\beta)$;

(i) the addition of the signals obtained under (g) and (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side signals into a stereo signal.

(Figure 15)

2. A method for stereophonizing a mono signal, characterized by

(a) the evaluation of the manually or metrologically ascertained angle φ between sound source and microphone principal axis in combination with

5

(aa) an arbitrarily or algorithmically determined fictitious opening angle α , which adjoins the microphone principal axis on the left, is not an element of a region around zero or equal to zero, and
 10 for which, if the angle φ is positive, the condition is satisfied that the angle φ is less than or equal to the angle α ;

(bb) an arbitrarily or algorithmically determined
 15 fictitious opening angle β , which adjoins the microphone principal axis on the right, is not an element of a region around zero or equal to zero, and for which, if the angle φ is negative, the condition is satisfied that the magnitude of the angle φ is less
 20 than or equal to the angle β ;

(cc) the manually or metrologically determined directivity pattern of the mono signal to be stereophonized, representable in polar coordinates;

25

(b) the calculation of the gain factor $P(\alpha)$, which is dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

30

(c) the calculation of the gain factor $P(\beta)$, which is dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

35

(d) the calculation of the delay time $L(\alpha)$, which is dependent on the angle φ , on the angle α and on the

directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(e) the calculation of the delay time $L(\beta)$, which is
 5 dependent on the angle φ , on the angle β and on the
 directivity pattern of the mono signal to be
 stereophonized (representable in polar coordinates);

(f) the direct use of the mono signal to be
 10 stereophonized as the principal signal;

(g) the delay of the mono signal to be stereophonized
 by the delay time $L(\alpha)$ and amplification of the delayed
 signal by the gain factor $P(\alpha)$; or alternatively: the
 15 amplification of the mono signal to be stereophonized
 by the gain factor $P(\alpha)$ and the delay of the amplified
 signal by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized
 20 by the delay time $L(\beta)$ and amplification of the delayed
 signal by the gain factor $P(\beta)$; or alternatively: the
 amplification of the mono signal to be stereophonized
 by the gain factor $P(\beta)$ and the delay of the amplified
 signal by the delay time $L(\beta)$;

25 (i) the addition of the signals obtained under (g) and
 (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side
 30 signals into a stereo signal.

(Figures 19.1 and 19.2)

3. The apparatus for stereophonizing a mono signal as
 35 claimed in claim 1, characterized by

(a) the gain factor $P(\alpha)$ equal to the squared polar
 interval for the angle α , divided by the squared sine

of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

5

(b) the gain factor $P(\beta)$ equal to the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β ;

10

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the gain factor $P(\alpha)$ described in (a);

15

(d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the gain factor $P(\beta)$ described in (b).

20

4. The method for stereophonizing a mono signal as claimed in claim 2, characterized by

25

(a) the gain factor $P(\alpha)$ equal to the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

30

(b) the gain factor $P(\beta)$ equal to the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β ;

35

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the gain factor $P(\alpha)$
5 described in (a);

(d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the gain factor $P(\beta)$
10 described in (b).

5. An apparatus for obtaining an equivalent stereo signal for the stereo signal obtained in accordance with claim 1 from a mono signal,
15 characterized by

(a) the evaluation of the manually or metrologically ascertained angle φ between sound source and microphone principal axis in combination with
20

(aa) an arbitrarily or algorithmically determined fictitious opening angle α , which adjoins the microphone principal axis on the left, is not an element of a region around zero or equal to zero, and
25 for which, if the angle φ is positive, the condition is satisfied that the angle φ is less than or equal to the angle α ;

(bb) an arbitrarily or algorithmically determined fictitious opening angle β , which adjoins the microphone principal axis on the right, is not an element of a region around zero or equal to zero, and
30 for which, if the angle φ is negative, the condition is satisfied that the magnitude of the angle φ is less
35 than or equal to the angle β ;

(cc) the manually or metrologically determined directivity pattern of the mono signal to be stereophonized, representable in polar coordinates;

5 (dd) the satisfaction of the condition that the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for
 10 the angle φ and the sine of φ divided by the sine of α is not an element of a region around zero or equal to zero;

(b) the calculation of the gain factor P_M' , which is
 15 dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(c) the calculation of the gain factor $P(\beta)'$, which is
 20 dependent on the angle φ , on the angle α , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(d) the calculation of the delay time $L(\alpha)$, which is
 25 dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(e) the calculation of the delay time $L(\beta)$, which is
 30 dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(f) the amplification of the mono signal to be
 35 stereophonized by the gain factor P_M , in order to obtain a principal signal;

(g) the delay of the mono signal to be stereophonized by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized by the delay time $L(\beta)$ and amplification of the delayed signal by the gain factor $P(\beta)'$; or alternatively: the amplification of the mono signal to be stereophonized by the gain factor $P(\beta)'$ and the delay of the amplified signal by the delay time $L(\beta)$;

10

(i) the addition of the signals obtained under (g) and (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side signals into a stereo signal.

15

(Figure 16)

6. A method for obtaining an equivalent stereo signal for the stereo signal obtained in accordance with claim 2 from a mono signal, characterized by

20

(a) the evaluation of the manually or metrologically ascertained angle φ between sound source and microphone principal axis in combination with

25

(aa) an arbitrarily or algorithmically determined fictitious opening angle α , which adjoins the microphone principal axis on the left, is not an element of a region around zero or equal to zero, and for which, if the angle φ is positive, the condition is satisfied that the angle φ is less than or equal to the angle α ;

30

(bb) an arbitrarily or algorithmically determined fictitious opening angle β , which adjoins the microphone principal axis on the right, is not an

35

element of a region around zero or equal to zero, and for which, if the angle φ is negative, the condition is satisfied that the magnitude of the angle φ is less than or equal to the angle β ;

5

(cc) the manually or metrologically determined directivity pattern of the mono signal to be stereophonized, representable in polar coordinates;

10 (dd) the satisfaction of the condition that the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for
15 the angle φ and the sine of φ divided by the sine of α is not an element of a region around zero or equal to zero;

(b) the calculation of the gain factor P_M , which is
20 dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(c) the calculation of the gain factor $P(\beta)'$, which is
25 dependent on the angle φ , on the angle α , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(d) the calculation of the delay time $L(\alpha)$, which is
30 dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(e) the calculation of the delay time $L(\beta)$, which is
35 dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(f) the amplification of the mono signals to be stereophonized by the gain factor P_M , in order to obtain a principal signal;

5 (g) the delay of the mono signal to be stereophonized by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized by the delay time $L(\beta)$ and amplification of the delayed
10 signal by the gain factor $P(\beta)'$; or alternatively: the amplification of the mono signal to be stereophonized by the gain factor $P(\beta)'$ and the delay of the amplified signal by the delay time $L(\beta)$;

15 (i) the addition of the signals obtained under (g) and (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side signals into a stereo signal.

20

7. The apparatus for stereophonizing a mono signal as claimed in claim 5, characterized by

(a) the gain factor P_M equal to the reciprocal value
25 of the result which is calculated from the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for
30 the angle φ and the sine of φ divided by the sine of α ;

(b) the gain factor $P(\beta)'$ equal to the product of the gain factor P_M described in (a) and the gain factor $P(\beta)$ described in claim 3(b);

35

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the result which is

calculated from the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

(d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β .

8. The method for stereophonizing a mono signal as claimed in claim 6, characterized by

(a) the gain factor P_M equal to the reciprocal value of the result which is calculated from the squared polar interval for the angle α , divided by the square sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

(b) the gain factor $P(\beta)'$ equal to the product of the gain factor P_M described in (a) and the gain factor $P(\beta)$ described in claim 3(b);

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the result which is calculated from the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ ,

minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

- 5 (d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by
 10 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β .

- 15 9. An apparatus for obtaining an equivalent stereo signal for the stereo signal obtained in accordance with claim 1 from a mono signal, characterized by

- 20 (a) the evaluation of the manually or metrologically ascertained angle φ between sound source and microphone principal axis in combination with

- (aa) an arbitrarily or algorithmically determined
 25 fictitious opening angle α , which adjoins the microphone principal axis on the left, is not an element of a region around zero or equal to zero, and for which, if the angle φ is positive, the condition is satisfied that the angle φ is less than or equal to the
 30 angle α ;

- (bb) an arbitrarily or algorithmically determined
 fictitious opening angle β , which adjoins the
 microphone principal axis on the right, is not an
 35 element of a region around zero or equal to zero, and for which, if the angle φ is negative, the condition is satisfied that the magnitude of the angle φ is less than or equal to the angle β ;

(cc) the manually or metrologically determined directivity pattern of the mono signal to be stereophonized, representable in polar coordinates;

5

(dd) the satisfaction of the condition that the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β is not an element of a region around zero or equal to zero;

15 (b) the calculation of the gain factor $P_{M'}$, which is dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

20 (c) the calculation of the gain factor $P(\alpha)'$, which is dependent on the angle φ , on the angle α , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

25 (d) the calculation of the delay time $L(\alpha)$, which is dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

30 (e) the calculation of the delay time $L(\beta)$, which is dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

35 (f) the amplification of the mono signal to be stereophonized by the gain factor $P_{M'}$ in order to obtain a principal signal;

(g) the delay of the mono signal to be stereophonized by the delay time $L(\alpha)$ and amplification of the delayed signal by the gain factor $P(\alpha)'$; or alternatively: the amplification of the mono signal to be stereophonized
 5 by the gain factor $P(\alpha)'$ and the delay of the amplified signal by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized by the delay time $L(\beta)$;

10

(i) the addition of the signals obtained under (g) and (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side
 15 signals into a stereo signal.

(Figure 17)

10. A method for obtaining an equivalent stereo signal
 20 for the stereo signal obtained in accordance with claim 2 from a mono signal,
 characterized by

(a) the evaluation of the manually or metrologically
 25 ascertained angle φ between sound source and microphone principal axis in combination with

(aa) an arbitrarily or algorithmically determined fictitious opening angle α , which adjoins the
 30 microphone principal axis on the left, is not an element of a region around zero or equal to zero, and for which, if the angle φ is positive, the condition is satisfied that the angle φ is less than or equal to the angle α ;

35

(bb) an arbitrarily or algorithmically determined fictitious opening angle β , which adjoins the microphone principal axis on the right, is not an

element of a region around zero or equal to zero, and for which, if the angle φ is negative, the condition is satisfied that the magnitude of the angle φ is less than or equal to the angle β ;

5

(cc) the manually or metrologically determined directivity pattern of the mono signal to be stereophonized, representable in polar coordinates;

10 (dd) the satisfaction of the condition that the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β is
15 not an element of a region around zero or equal to zero;

(b) the calculation of the gain factor P_M , which is
20 dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(c) the calculation of the gain factor $P(\alpha)$, which is
25 dependent on the angle φ , on the angle α , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(d) the calculation of the delay time $L(\alpha)$, which is
30 dependent on the angle φ , on the angle α and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(e) the calculation of the delay time $L(\beta)$, which is
35 dependent on the angle φ , on the angle β and on the directivity pattern of the mono signal to be stereophonized (representable in polar coordinates);

(f) the amplification of the mono signal to be stereophonized by the gain factor P_M , in order to obtain a principal signal;

5 (g) the delay of the mono signal to be stereophonized by the delay time $L(\alpha)$ and amplification of the delayed signal by the gain factor $P(\alpha)'$; or alternatively: the amplification of the mono signal to be stereophonized by the gain factor $P(\alpha)'$ and the delay of the amplified
10 signal by the delay time $L(\alpha)$;

(h) the delay of the mono signal to be stereophonized by the delay time $L(\beta)$;

15 (i) the addition of the signals obtained under (g) and (h) in order to obtain a side signal;

(j) the stereo conversion of the principal and side signals into a stereo signal.

20

11. The apparatus for stereophonizing a mono signal as claimed in claim 9, characterized by

(a) the gain factor P_M , equal to the reciprocal value
25 of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the
30 angle φ and the sine of φ divided by the sine of β ;

(b) the gain factor $P(\alpha)'$ equal to the product of the gain factor P_M , described in (a) and the gain factor $P(\alpha)$ described in claim 3(a);

35

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the result which is

calculated from the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ , minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

(d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β .

12. The method for stereophonizing a mono signal as claimed in claim 10, characterized by

(a) the gain factor P_M , equal to the reciprocal value of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β ;

(b) the gain factor $P(\alpha)'$ equal to the product of the gain factor P_M , described in (a) and the gain factor $P(\alpha)$ described in claim 3(a);

(c) the delay time $L(\alpha)$ equal to the negative polar interval for the angle α , divided by the doubled sine of α , plus the square root of the result which is calculated from the squared polar interval for the angle α , divided by the squared sine of α multiplied by 4, plus the squared polar interval for the angle φ ,

minus the product of the polar interval for the angle α , the polar interval for the angle φ and the sine of φ divided by the sine of α ;

5 (d) the delay time $L(\beta)$ equal to the negative polar interval for the angle β , divided by the doubled sine of β , plus the square root of the result which is calculated from the squared polar interval for the angle β , divided by the squared sine of β multiplied by
 10 4, plus the squared polar interval for the angle φ , plus the product of the polar interval for the angle β , the polar interval for the angle φ and the sine of φ divided by the sine of β .

15 13. The extended apparatus as claimed in claim 1 or claim 3 or claim 5 or claim 7 or claim 9 or claim 11, characterized by the additional transformation of the respectively obtained stereo signal into stereophonic signals which are reproduced by more than two
 20 loudspeakers.

14. The extended method as claimed in claim 2 or claim 4 or claim 6 or claim 8 or claim 10 or claim 12, characterized by the additional transformation of the
 25 respectively obtained stereo signal into stereophonic signals which are reproduced by more than two loudspeakers.