

DESCRIPTION

HEAT CONDUCTIVITY IMPROVING AGENT

5 TECHNICAL FIELD

The present invention relates to a heat conductivity improving agent, a resin composition comprising the same and a molded article of the composition. The present invention also relates to a method of improving the heat conductivity
10 of a resin composition.

BACKGROUND ART

Magnesium oxide, aluminum oxide and silica have been used as agents for improving the heat conductivities of
15 synthetic resins, rubbers and ceramics (patent document 1). Silica has low heat conductivity. Aluminum oxide has a defect that it wears a molding machine or a mold at the time of molding as it has high hardness though it has high heat conductivity. Therefore, magnesium oxide which has low
20 hardness and about 3 times higher heat conductivity than that of alumina has been attracting attention as a heat conductivity improving agent. However, magnesium oxide is gradually eroded by water or vapor and changes into magnesium hydroxide, thereby losing its physical properties.
25 Therefore, various improvements have been made on magnesium oxide to achieve higher heat conductivity. Magnesium oxide having a coating layer of silicon and/or aluminum-magnesium double oxide on the surface (patent document 2) and magnesium oxide coated with a phosphorus compound (patent document 3)
30 are such examples. Technology for using magnesium hydroxide as a heat conductivity improving agent has also been proposed (patent document 4). However, all of these do not obtain satisfactory results.

(Patent Document 1) JP-A 7-324146

(Patent Document 2) JP-A 2004-27177
(Patent Document 3) JP-A 2006-282783
(Patent Document 4) JP-A 9-176368

5 DISCLOSURE OF THE INVENTION

It is an object of the present invention to provide a heat conductivity improving agent capable of improving the heat conductivity of a resin. It is another object of the present invention to provide a resin composition having
10 excellent mechanical strength such as tensile strength and elongation and high heat conductivity as well as a molded article obtained therefrom. It is still another object of the present invention to provide a method for improving the heat conductivity of a resin composition.

15 The inventors of the present invention conducted studies on the improvement of a heat conductivity improving agent comprising a magnesium hydroxide particle as an effective component. As a result, they found that a magnesium hydroxide particle having a high aspect ratio has
20 an excellent effect as a heat conductivity improving agent. The present invention was accomplished based on this finding.

That is, the present invention is a heat conductivity improving agent which comprises a magnesium hydroxide particle as an effective component, having a thickness of
25 10 nm to 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

Further, the invention is the above resin composition comprising (i) 100 parts by weight of a resin and (ii) 20 to 300 parts by weight of a heat conductivity improving agent
30 which is a magnesium hydroxide particle having a thickness of 10 nm to 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

The present invention is also a molded article of the

above resin composition.

Further, the present invention is a method of improving the heat conductivity of a resin composition comprising a resin and a magnesium hydroxide particle, comprising mixing
5 100 parts by weight of the resin with 20 to 300 parts by weight of the magnesium hydroxide particle having a thickness of 10 nm to 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

10 BEST MODE FOR CARRYING OUT THE INVENTION

<heat conductivity improving agent>

The heat conductivity improving agent of the present invention comprises a magnesium hydroxide particle as an effective component, having a thickness of 10 nm to 0.2 μm
15 and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

The thickness of the magnesium hydroxide particle when measured by the SEM method is 10 nm to 0.2 μm , preferably 10 nm to 0.15 μm and more preferably 10 nm to 0.08 μm . The
20 lower limit of the thickness of the magnesium hydroxide particle may be 20 nm. The thickness of the magnesium hydroxide particle is the arithmetic average of the thickness measurement values of 10 arbitrary crystallites in a SEM photomicrograph (20,000 magnifications) (average
25 thickness).

The aspect ratio (long diameter/thickness) of the magnesium hydroxide particle is not less than 10, preferably not less than 15, more preferably 10 to 100 and much more preferably 50 to 200. The aspect ratio of the magnesium
30 hydroxide particle is a value obtained by dividing the average long diameter obtained from the arithmetic average of the long diameter measurement values of 10 arbitrary crystallites by the average thickness in a SEM photomicrograph (20,000 magnifications).

The BET specific surface area of the magnesium hydroxide particle is preferably 5 to 30 m²/g, more preferably 10 to 30 m²/g, much more preferably 10 to 25 m²/g and most preferably 10 to 20 m²/g.

5 Preferably, the magnesium hydroxide particle has a CaO content of not more than 0.01 wt%, a Cl content of not more than 0.05 wt%, an Na content of not more than 0.01 wt% and a total content of an iron compound, manganese compound, cobalt compound, chromium compound, copper compound,
10 vanadium compound and nickel compound of not more than 0.02 wt% in terms of metals.

 The magnesium hydroxide particle has a Mg(OH)₂ content of preferably not less than 99.0 wt%, more preferably not less than 99.5 wt% and much more preferably not less than
15 99.8 wt%.

(process for producing magnesium hydroxide particle)

 The magnesium hydroxide particle of the present invention having a high aspect ratio is obtained when a
20 monovalent organic acid is existent in the production of a magnesium hydroxide particle by hydrothermally processing slurry coprecipitated by adding an alkali to a water-soluble magnesium salt.

 Examples of the water-soluble magnesium salt include
25 magnesium chloride, magnesium nitrate, magnesium acetate and magnesium sulfate. Examples of the alkali include caustic soda, calcium hydroxide, potassium hydroxide and ammonia water. Examples of the monovalent organic acid include acetic acid, propionic acid, butyric acid and formic acid.
30 Sodium salts, potassium salts, magnesium salts and calcium salts thereof are also included.

 The amount of the alkali is preferably 20 to 200 moles, more preferably 30 to 100 moles and much more preferably 40 to 90 moles based on 1 mole of the water-soluble magnesium

salt. The amount of the monovalent organic acid is preferably 0.001 to 10 moles, more preferably 0.01 to 5.0 moles and much more preferably 0.05 to 3.0 moles based on 1 mole of the water-soluble magnesium salt.

5 The hydrothermal processing temperature is preferably 100 to 300°C, more preferably 110 to 250°C and much more preferably 130 to 200°C.

(surface treating agent)

10 The magnesium hydroxide particle is preferably surface treated with a surface treating agent. The surface treating agent is at least one selected from the group consisting of higher fatty acids, anionic surfactants, phosphoric acid esters, coupling agents (silane-based, titanate-based and
15 aluminum-based), esters of a polyhydric alcohol and a fatty acid, acrylic polymers and silicone treating agents.

 The higher fatty acids include higher fatty acids having 10 or more carbon atoms such as stearic acid, erucic acid, palmitic acid, lauric acid and behenic acid. Alkali
20 metal salts of these higher fatty acids may also be used.

 The anionic surfactants include sulfuric acid ester salts of a higher alcohol such as stearyl alcohol or oleyl alcohol, sulfuric acid ester salts of polyethylene glycol ether, amide-linked sulfuric acid ester salts, ester-linked
25 sulfuric acid ester salts, ester-linked sulfonates, amide-linked sulfonic acid salts, ether-linked sulfonic acid salts, ether-linked alkyl aryl sulfonic acid salts, ester-linked alkyl aryl sulfonic acid salts and amide-linked alkyl aryl sulfonic acid salts.

30 The phosphoric acid esters include monoesters and diesters of orthophosphoric acid and oleyl alcohol or stearyl alcohol and mixtures thereof. Acid and alkali metal salts and amine salts of these esters may also be used.

 The coupling agents include silane coupling agents

such as vinyl ethoxysilane,
vinyl-tris(2-methoxy-ethoxy)silane,
gamma-methacryloxypropyltrimethoxysilane,
gamma-aminopropyltrimethoxysilane,
5 beta-(3,4-epoxycyclohexyl)ethyltrimethoxysilane,
gamma-glycidoxypropyltrimethoxysilane and
gamma-mercaptopropyltrimethoxysilane; titanate-based
coupling agents such as isopropyl triisostearoyl titanate,
isopropyl tris(dioctylpyrophosphate)titanate, isopropyl
10 tri(N-aminoethyl-aminoethyl)titanate and isopropyl
tridecylbenzene sulfonyl titanate; and aluminum-based
coupling agents such as acetoalkoxyaluminum diisopropylate.

The esters of a polyhydric alcohol and a fatty acid
include glycerin monostearate and glycerin monooleate.

15 To coat the surface of the magnesium hydroxide particle
with the above surface treating agent, a wet or dry process
known per se may be employed. For example, in the wet process,
the surface treating agent in a liquid or emulsion form is
added to magnesium hydroxide slurry and mechanically fully
20 mixed with the slurry at a temperature up to about 100°C.
In the dry process, the surface treating agent in a liquid,
emulsion or solid form is added to a magnesium hydroxide
powder while it is fully stirred by means of a mixer such
as a Henschel mixer to be fully mixed with the powder under
25 heating or non-heating. The amount of the surface treating
agent to be added is preferably not more than 10 wt%, more
preferably 1.0 to 8.0 wt%, much more preferably 1.0 to 3.0
wt% based on the weight of the magnesium hydroxide particle.

30 Rinsing, dehydration, granulation, drying, milling
and classification are suitably selected as required and
carried out on the surface treated magnesium hydroxide
particle to produce a final product.

(coating layer)

To enhance the acid resistance of the magnesium hydroxide particle, the surface of the magnesium hydroxide particle may be coated with a coating agent having acid resistance. The coating agent is an oxide or hydroxide of at least one element selected from the group consisting of silicon, aluminum, titanium, zirconia, zinc and boron. The magnesium hydroxide particle preferably has a coating layer made of silicon oxide or hydroxide formed by making silicic acid or a soluble salt thereof act thereon.

The amount of the coating agent is preferably not more than 2 wt%, more preferably 0.01 to 1.5 wt%, much more preferably 0.01 to 1.0 wt% based on the magnesium hydroxide particle.

Further, the surface of the coating layer may be treated with at least one surface treating agent selected from the group consisting of higher fatty acids, anionic surfactants, phosphoric acid esters, coupling agents and esters of a polyhydric alcohol and a fatty acid.

<resin composition>

The resin composition of the present invention comprises (i) 100 parts by weight of a resin and (ii) 20 to 300 parts by weight of a heat conductivity improving agent, wherein the heat conductivity improving agent is a magnesium hydroxide particle having a thickness of 20 nm to 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

The resin composition of the present invention may be used as a sealing material for the heat generating parts of semiconductors, resistors and condensers and a material for parts for which heat radiation property is required, such as substrates, housings, heat exchangers and bearings.

Any resin is acceptable if it is generally used as a molded article. Examples of the resin include thermoplastic

resins such as olefin (α -olefin) polymers and copolymers having 2 to 8 carbon atoms including polyethylene, polypropylene, ethylene-propylene copolymer, polybutene and poly-4-methylpentene-1, copolymers of these olefins and
5 dienes, ethylene-acrylate copolymer, polystyrene, ABS resin, AAS resin, AS resin, MBS resin, ethylene-vinyl chloride copolymer resin, ethylene-vinyl acetate copolymer resin, ethylene-vinyl chloride-vinyl acetate graft polymer resin, vinylidene chloride, polyvinyl chloride, chlorinated
10 polyethylene, chlorinated polypropylene, vinyl chloride-propylene copolymer, vinyl acetate resin, phenoxy resin, polyacetal, polyamide, polyimide, polycarbonate, polysulfone, polyphenylene oxide, polyphenylene sulfide, polyethylene terephthalate, polybutylene terephthalate and
15 methacrylic resin.

Preferred examples of the thermoplastic resin include polyolefins and copolymers thereof. Specific examples thereof include polypropylene-based resins such as polypropylene homopolymer and ethylene-propylene copolymer,
20 polyethylene-based resins such as high-density polyethylene, low-density polyethylene, linear low-density polyethylene ultralow-density polyethylene, EVA (ethylene vinyl acetate resin), EEA (ethylene ethyl acrylate resin), EMA (ethylene methyl acrylate copolymer resin), EAA (ethylene acrylic acid
25 copolymer resin) and super high molecular weight polyethylene, and polymers and copolymers of an olefin (α -ethylene) having 2 to 6 carbon atoms such as polybutene and poly4-methylpentene-1.

Further, thermosetting resins such as epoxy resin,
30 phenolic resin, melamine resin, unsaturated polyester resin, alkyd resin and urea resin, and synthetic rubbers such as EPDM, butyl rubber, isoprene rubber, SBR, NBR, chlorosulfonated polyethylene, NIR, urethane rubber, butadiene rubber, acrylic rubber, silicone rubber and

fluorine rubber may also be used.

The content of the magnesium hydroxide particle in the resin composition is preferably 10 to 300 parts by weight, more preferably 25 to 200 parts by weight based on 100 parts by weight of the resin.

The resin composition of the present invention may comprise a heat conductivity improving aid. As the heat conductivity improving aid may be used a fibrous or chain inorganic substance which may be natural or synthetic. Examples of the aid include fibrous inorganic substances such as basic magnesium sulfate, carbon fibers, wollastonite, aluminum borate, potassium titanate, sepiolite and xonotlite, and chain inorganic substances such as acetylene black. The content of the heat conductivity improving aid in the resin composition is preferably not more than 200 parts by weight, more preferably 0.01 to 150 parts by weight, much more preferably 0.1 to 100 parts by weight based on 100 parts by weight of the resin.

Various additives, reinforcing material and filler may be added to the resin composition of the present invention. Examples of these include additives such as a vulcanizing agent, antioxidant, ultraviolet absorbent, flame retardant, optical stabilizer, metal inactivating agent, crosslinking agent, colorant, curing agent, lubricant, nucleating agent, foaming agent, deodorant, lithopone, clay, pieces of wood, glass fibers, ferrite, carbon black, talc, mica, calcium carbonate, red phosphorus, tin and inorganic salts thereof, metal fibers and metal powders, reinforcing materials and fillers.

<molded article>

The present invention includes molded articles formed from the above resin composition. The molded articles include heat radiation sheets, heat radiation plates, heat

radiation cases and heat radiation covers.

<method of improving the heat conductivity of resin composition>

5 The present invention includes a method of improving the heat conductivity of a resin composition comprising a resin and a magnesium hydroxide particle, comprising mixing 20 to 300 parts by weight of the magnesium hydroxide particle having a thickness of 10 nm to 0.2 μ m and an aspect ratio
10 (long diameter/thickness) measured by a SEM method of not less than 10 with 100 parts by weight of the resin. The resin and the magnesium hydroxide particle are as described above.

EXAMPLES

15 The properties of the magnesium hydroxide particle and the resin composition were measured by the following methods.

(a) Heat conductivity: based on ISO/CD 22007-2.

Apparatus: TPA-501 hot disk method thermophysical property measuring device (manufactured by Kyoto Electronics
20 Manufacturing Co., Ltd.), using the RTK-7 sensor having a diameter of 7 mm

(b) BET specific surface area: This was measured in accordance with the method described in "Catalyst" (Vol. 2 No. 4, p. 473, 1960, Tokuji Takagi).

25 (c) Aspect ratio:

SEM method: This was obtained from the arithmetic averages of long-diameter and thickness measurement values of 10 arbitrary crystallites in a SEM photomicrograph (20,000 magnifications) of the magnesium hydroxide particle.

30 Atomic force microscope method: This was measured by means of the OLS3500 of Olympus Corporation.

(d) CaO, Cl, Na: fluorescent X-ray method (base: atomic absorption method)

(e) Analysis of Fe, Mn, Cu, V, Co, Ni and Cr: ICP-MS method

(Inductively Coupled Plasma-Mass Spectrometry)

(f) $\text{Mg}(\text{OH})_2$: chelate titration method

(g) Tensile strength: JIS K6301 (vulcanized rubber physical method)

5 (h) Elongation: JIS K6301 (vulcanized rubber physical method)

(i) Hardness: JIS K6253 (spring type A)

Example 1

10 213 liters of a sodium hydroxide aqueous solution having a concentration of 3.0 mol/L was added to 400 liters of a mixed aqueous solution of magnesium chloride and sodium acetate ($\text{Mg} = 1.0$ mol/L, sodium acetate = 1.5 mol/L, 30°C) under agitation to carry out a co-precipitation reaction.
15 The whole amount of this reaction product was hydrothermally processed in a 1.0 kL autoclave at 160°C for 5 hours. After the reaction product was cooled to 100°C or lower, it was taken out from the autoclave, filtered, rinsed, dried and ground.

20 The obtained magnesium hydroxide was observed through a SEM, a photomicrograph thereof was taken, and the long diameters and thicknesses of 10 crystallites were measured to be averaged. As a result, the long diameter was $2.6\ \mu\text{m}$, the thickness was $0.12\ \mu\text{m}$ and therefore the aspect ratio was
25 21. The aspect ratio measured through an atomic force microscope was 46.

Example 2

30 1.8 liters of an ammonia water solution (30°C) having a concentration of 8 mol/L was added to 4 liters of a mixed aqueous solution of magnesium chloride and sodium acetate both of which are extra pure reagents ($\text{Mg} = 2.0$ mol/L, sodium acetate = 2.0 mol/L, 30°C) under agitation to carry out a co-precipitation reaction. 1 liter of this reaction product

was collected and put into an autoclave to be hydrothermally processed at 250°C for 3 hours. After the reaction product was cooled to 100°C or lower, it was taken out from the autoclave, filtered, rinsed, dried and ground.

5 The obtained magnesium hydroxide was observed through a SEM, a photomicrograph thereof was taken, and the widths and thicknesses of 10 crystallites were measured to be averaged. As a result, the width was 4.5 μm , the thickness was 0.06 μm and therefore the aspect ratio was 75. The aspect
10 ratio measured through an atomic force microscope was 130.

Example 3

1.6 liters of caustic soda having a concentration of 8.0 mol/L (35°C) was added to 5 liters of a mixed aqueous
15 solution of magnesium nitrate and sodium propionate both of which are extra pure reagents (Mg = 1.5 mol/L, sodium propionate = 1.0 mol/L, 30°C) under agitation to carry out a co-precipitation reaction. 1 liter of this reaction product was collected, hydrothermally processed in an
20 autoclave at 180°C for 4 hours and then treated in the same manner as in Example 1.

When the obtained magnesium hydroxide was observed through a SEM, the width of a crystal was 3.8 μm , the thickness thereof was 0.09 μm and therefore the aspect ratio was 42.
25 The aspect ratio measured through an atomic force microscope was 73.

Example 4

240 liters of ammonia water having a concentration of 4.0 mol/L (35°C) was added to 400 liters of a mixed aqueous
30 solution of magnesium nitrate and ammonium acetate (Mg = 1.5 mol/L, ammonium acetate = 1.5 mol/L, 35°C) under agitation to carry out a co-precipitation reaction. The whole amount of this reaction product was hydrothermally processed in a

1.0 kL autoclave at 200°C for 4 hours and then treated in the same manner as in Example 1. When the obtained magnesium hydroxide was observed through a SEM and a photomicrograph thereof was taken to be measured, the crystallites had a long diameter of 3.5 μm , a thickness of 0.11 μm and therefore an aspect ratio of 31. The aspect ratio measured through an atomic force microscope was 78.

Example 5 (surface treatment)

500 g of the magnesium hydroxide particle obtained in Example 1 was put into a Henschel mixer, and 5 g of vinylsilane corresponding to 1 wt% based on the weight of the magnesium hydroxide particle was diluted with 50 mL of ethanol under high-speed agitation and added to the magnesium hydroxide particle so as to treat the surface of the particle. This was dried at 120°C.

Comparative Example 1

The procedure of Example 1 was repeated except that sodium acetate was not used. The crystallite of the obtained magnesium hydroxide particle had a long diameter of 0.77 μm , a thickness of 0.14 μm and an aspect ratio of 5.5. The aspect ratio measured by an atomic force microscope was 10.

The characteristic properties of magnesium hydroxide particles obtained in Examples 1 to 4 and Comparative Example 1 are shown in Table 1.

Table 1

	Example 1	Example 2	Example 3	Example 4	Comparative Example 1
Aspect ratio ¹⁾	21	75	42	31	5.5
Aspect ratio ²⁾	46	130	73	78	10
BET specific surface area (m ² /g)	9.5	17.0	12.1	13.5	6.5
CaO(wt%)	0.001>	0.001>	0.001>	0.001>	0.011
Cl(wt%)	0.005	0.011	0.010	0.010	0.037
Na(wt%)	0.001	0.001	0.002	0.001	0.013
Fe(wt%)	0.001	0.003	0.002	0.003	0.005
Mn(wt%)	0.001	0.001	0.001	0.001	0.001
Cu(wt%)	0.0001≥	0.0001≥	0.0001≥	0.0001≥	0.0001≥
V(wt%)	0.0001≥	0.0001≥	0.0001≥	0.0001≥	0.0001≥
Co(wt%)	0.0001≥	0.0001≥	0.0001≥	0.0001≥	0.0001≥
Ni(wt%)	0.0001≥	0.0001≥	0.0001≥	0.0001≥	0.0001≥
Cr(wt%)	0.0001≥	0.0001≥	0.0001≥	0.0001≥	0.0001≥
Mg(OH) ₂ (wt%)	99.91	99.90	99.87	99.90	99.58

1) Aspect ratio measured by SEM method

2) Aspect ratio measured by atomic force microscope method

Example 6

100 parts by weight of dimethyl vinyl silicone rubber (TSE201 of Momentive Performance Materials Japan Inc.) and 100 parts by weight of the magnesium hydroxide particle
5 obtained in Example 1 as a heat conductivity filler were fed to a kneader to be kneaded together. A dimethyl vinyl silicone rubber compound which had been fully kneaded was collected and uniformly mixed with 1.0 part by weight of 2,5-dimethyl-2,5-t-butyl peroxyhexane (TC-8 of Momentive
10 Performance Materials Japan Inc.) as a crosslinking agent to prepare a composition.

The obtained composition was formed into a 2 mm-thick sheet which was then press vulcanized at 160°C for 10 minutes and secondarily vulcanized at 200°C for 4 hours. 24 hours
15 after the vulcanized sheet was returned to normal temperature, the hardness, tensile strength and elongation of the sheet were measured in accordance with JIS-K6301 (vulcanized rubber physical method). Further, the heat conductivity of the sheet was measured by using the TPA-501 hot disk method
20 thermophysical property measuring device (of Kyoto Electronics Manufacturing Co., Ltd.) in accordance with ISO/CC22007-2. The evaluation results are shown in Table 2.

25 Example 7

A sheet was manufactured in the same manner as in Example 6 except that the magnesium hydroxide particle obtained in Example 2 was used in place of the magnesium hydroxide particle obtained in Example 1 to measure its heat
30 conductivity. The evaluation results are shown in Table 2.

Example 8

A sheet was manufactured in the same manner as in Example 6 except that the magnesium hydroxide particle

obtained in Example 3 was used in place of the magnesium hydroxide particle obtained in Example 1 to measure its heat conductivity. The evaluation results are shown in Table 2.

5 Example 9

A sheet was manufactured in the same manner as in Example 6 except that the magnesium hydroxide particle obtained in Example 4 was used in place of the magnesium hydroxide particle obtained in Example 1 to measure its heat
10 conductivity. The evaluation results are shown in Table 2.

Comparative Example 2

A sheet was manufactured in the same manner as in Example 6 except that the magnesium hydroxide particle
15 obtained in Comparative Example 1 was used in place of the magnesium hydroxide particle obtained in Example 1 to measure its heat conductivity. The evaluation results are shown in Table 2.

Table 2

Specimen	Magnesium hydroxide particle in use	Temperature	Output	Time	Heat conductivity (W/m · K)				Hardness (JIS A)	Tensile strength (MPa)	Elongation (%)
		(°C)	(W)	(sec)	r=1	r=2	r=3	Average			
Ex. 6	Ex. 1	23	0.12	10	0.953	0.945	0.941	0.946	41	1.57	350
Ex. 7	Ex. 2	23	0.12	10	0.959	0.952	0.948	0.953	46	2.26	210
Ex. 8	Ex. 3	23	0.12	10	0.948	0.941	0.939	0.942	45	2.15	220
Ex. 9	Ex. 4	23	0.12	10	1.010	0.987	0.981	0.992	46	2.30	190
C. Ex. 2	C. Ex. 1	23	0.07	20	0.548	0.548	0.542	0.545	39	1.35	425

Ex.: Example, C.Ex.: Comparative Example

Example 10-1 (production of heat radiation sheet)

100 parts by weight of dimethyl vinyl silicone rubber (TSE201 of Momentive Performance Materials Japan Inc.) and 25 parts by weight of the magnesium hydroxide particle
5 obtained in Example 4 were kneaded together by means of a double-screw open roll. In this case, the magnesium hydroxide particle having a high aspect ratio was gradually injected while the crude dimethyl vinyl silicone rubber was wound round a roll to a roll width scale mark of 10. At a
10 roll width scale mark of 13, the kneaded product was scraped off from the roll and re-kneaded 10 times, 2.5-dimethyl-2,5-t-butyl peroxyhexane (TC-8 of Momentive Performance Materials Japan Inc.) as a vulcanizing agent was added, and the kneaded product was scraped off from the roll
15 and re-kneaded 10 times again. After the kneaded product was scraped off from the roll and re-kneaded 10 times at a roll width scale mark of 15, the resulting silicone rubber compound was collected.

This silicone rubber compound was formed into a 2
20 mm-thick sheet which was then press vulcanized at 160°C for 10 minutes and then secondarily vulcanized at 200°C for 4 hours to produce a heat radiation sheet. 24 hours after the sheet was returned to normal temperature, the tensile strength, elongation, hardness and heat conductivity of the
25 sheet were measured. The evaluation results are shown in Table 3.

Examples 10-2 to 10-4 (production of heat radiation sheet)

Heat radiation sheets were produced in the same manner
30 as in Example 10-1 except that the amount of the magnesium hydroxide particle obtained in Example 4 was changed as shown in Table 3. The evaluation results are shown in Table 3.

Example 10-5

300 g of magnesium hydroxide obtained in Example 2 was ground and dispersed in isopropyl alcohol by using a stirrer, and 9 g of methyl hydrogen silicone (KF-9901 of Shin-Etsu Chemical Co., Ltd.) was added to the resulting dispersion to surface treat the magnesium hydroxide. Thereafter, the surface treated magnesium hydroxide was filtered, dried and ground. 100 parts by weight of the obtained powder and a crosslinking agent (peroxide) were added to and mixed with 100 parts by weight of dimethyl vinyl silicone rubber by means of an open roll and crosslinked at 160°C for 10 minutes by using a press molding machine to pressure form a specimen having a diameter of 50 mm and a thickness of 3.0 mm. This specimen was used to measure its heat conductivity in accordance with a steady heat flow method (based on ASTM E1530). The results are shown in Table 3.

Example 10-6

After magnesium hydroxide obtained in Example 3 was ground and surface treated with silicone in the same manner as in Example 5, 100 parts by weight thereof was added to and kneaded with 100 parts by weight of dimethyl vinyl silicone rubber, and the kneaded product was molded to produce a test specimen. The measurement result of the heat conductivity of this test specimen is shown in Table 3.

Comparative Example 3

A heat radiation sheet was produced in the same manner as in Example 10-1 to measure its heat conductivity except that 100 parts by weight of KISUMA 8 (magnesium hydroxide manufactured by Kyowa Chemical Industry Co., Ltd. and having an aspect ratio measured by a SEM method of 4.8) was used in place of 25 parts by weight of the magnesium hydroxide particle obtained in Example 4. The evaluation results are shown in Table 3.

Table 3

	Ex. 10-1	Ex. 10-2	Ex. 10-3	Ex. 10-4	Ex. 10-5	Ex. 10-6	C. Ex.3
Amount of dimethyl vinyl silicone rubber	100	100	100	100	100	100	100
Amount of magnesium hydroxide obtained in Example 4	25	45	70	100	-	-	-
Amount of magnesium hydroxide obtained in Example 2	-	-	-	-	100	-	-
Amount of magnesium hydroxide obtained in Example 3	-	-	-	-	-	100	-
Amount of KISMA 8	-	-	-	-	-	-	100
Tensile strength (Mpa)	1.12	1.46	1.81	2.13	1.07	0.89	0.81
Elongation (%)	347	340	418	351	210	215	428
Hardness (JIS A)	22	27	38	46	46	49	29
Heat conductivity (W/m·K)	0.35	0.50	0.65	0.80	0.85	0.91	0.54

Ex.: Example

C.Ex.: Comparative Example

- 5 KISUMA 8: magnesium hydroxide manufactured by Kyowa Chemical Industry Co., Ltd. (aspect ratio measured by SEM method: 4.8)

Effect of the Invention

- 10 Since the heat conductivity improving agent of the present invention comprises a magnesium hydroxide particle having a high aspect ratio as an effective component, it can provide high heat conductivity to a resin. A resin composition comprising the heat conductivity improving agent of the present invention has high heat conductivity.
- 15 According to the method of improving heat conductivity of

the present invention, the heat conductivity of a resin composition can be improved without deteriorating the physical properties of the resin composition.

CLAIMS

1. A heat conductivity improving agent comprising a magnesium hydroxide particle having a thickness of 10 nm to 5 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.
2. The heat conductivity improving agent according to claim 1, wherein the aspect ratio of the magnesium hydroxide 10 particle is not less than 15.
3. The heat conductivity improving agent according to claim 1, wherein the BET specific surface area of the magnesium hydroxide particle is 10 to 30 m^2/g . 15
4. The heat conductivity improving agent according to claim 1, wherein the magnesium hydroxide particle has a CaO content of not more than 0.01 wt%, a Cl content of not more than 0.05 wt%, a Na content of not more than 0.01 wt%, a total 20 content of an iron compound, manganese compound, cobalt compound, chromium compound, copper compound, vanadium compound and nickel compound of not more than 0.02 wt% in terms of metals, and a $\text{Mg}(\text{OH})_2$ content of not less than 99.5 wt%. 25
5. The heat conductivity improving agent according to claim 1 which is surface treated with at least one surface treating agent selected from the group consisting of higher fatty acids, anionic surfactants, phosphoric acid esters, 30 coupling agents, esters of a polyhydric alcohol and a fatty acid and silicone oil.
6. The heat conductivity improving agent according to claim 1 which has a coating layer made of an oxide or hydroxide

of at least one element selected from the group consisting of silicon, aluminum, titanium, zirconia, zinc and boron.

7. The heat conductivity improving agent according to claim 1 which has a coating layer made of silicon oxide or hydroxide formed by making silicic acid or a soluble salt thereof act thereon.

8. The heat conductivity improving agent according to claim 6 or 7, wherein the surface of the coating layer is further treated with at least one surface treating agent selected from the group consisting of higher fatty acids, anionic surfactants, phosphoric acid esters, coupling agents and esters of a polyhydric alcohol and a fatty acid.

9. A heat dissipation agent comprising the heat conductivity improving agent of claim 1 as an effective component.

10. A resin composition comprising (i) 100 parts by weight of a resin and (ii) 20 to 300 parts by weight of a heat conductivity improving agent which is a magnesium hydroxide particle having a thickness of 10 nm to 0.2 μ m and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.

11. The resin composition according to claim 10, wherein the resin is silicone rubber.

12. A molded article formed from the resin composition of claim 10.

13. A heat radiation sheet formed from the resin composition of claim 10.

14. A method of improving the heat conductivity of a resin composition comprising a resin and a magnesium hydroxide particle, comprising mixing 100 parts by weight of the resin with 20 to 300 parts by weight of the magnesium hydroxide particle having a thickness of 10 nm to 0.2 μm and an aspect ratio (long diameter/thickness) measured by a SEM method of not less than 10.