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DESCRIPTION

REFRIGERATING MACHINE OIL COMPOSITION

Technical Field

5 The present invention relates to a refrigerating machine oil composition, and specifically it relates to a refrigerating machine oil composition comprising an alicyclic dicarboxylic acid ester compound.

Background Art

10 In recent years, the issues of refrigerant substitution and refrigerating system efficiency improvement have been studied from the standpoint of minimizing ozone layer destruction and global warming. In the area of refrigerant substitutes, progress is being made in the substitution of HFCs
15 (hydrofluorocarbons) for chlorine-containing refrigerants such as CFCs (chlorofluorocarbons) and HCFCs (hydrochlorofluorocarbons). On the other hand, since HFC refrigerants could be subject to restrictions in light of the problem of global
20 warming, natural refrigerants such as carbon dioxide, ammonia and hydrocarbons are also being researched for applied use.

25 Efforts toward such refrigerant substitution are advancing in parallel with development of refrigerating machine oils for these substitute refrigerants. Refrigerating machine oils must satisfy



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a number of performance requirements including lubricity, miscibility with refrigerants, heat and hydrolytic stability, electric insulating property and low hygroscopicity, and therefore compounds satisfying these requirements are selected to match the type and purpose of use of each refrigerant. Examples of refrigerating machine oils used for HFCs include oxygen-containing compounds such as esters, ethers and carbonates that are miscible with the refrigerants, and alkylbenzenes which have inferior miscibility with the refrigerants but have excellent lubricity and heat and hydrolytic stability.

At the same time, efforts are being made to lower the viscosity of refrigerating machine oils with the goal of achieving higher efficiency of refrigerating systems. Known ester-based refrigerator machine oils include polyol esters obtained by reaction of aliphatic polyhydric alcohols and fatty acids, as disclosed in Japanese Translation Publication No. HEI 3-505602 (JP-A 3-505602) of International Publication for Patent Application and Japanese Patent Kokai (Laid-Open) Publication No. HEI 3-128991 (JP-A 3-128991), and for reduction of the viscosity of such ester-based refrigerating machine oils it has been found effective to select fatty acids with low carbon number alkyl groups for use in the raw material.

However, fatty acids with lower alkyl groups generally produce the undesirable situation of low heat and hydrolytic stability of the obtained esters.

There are also known alicyclic polycarboxylic acid esters, such as disclosed in Japanese Patent Kokai (Laid-Open) Publication No. HEI 9-221690 (JP-A 9-221690), as ester-based refrigerating machine oils with excellent heat and hydrolytic stability, but those with a large number of carbon atoms in the terminal alkyl group at the ester site have insufficient miscibility with refrigerants, while those with a small number of carbon atoms in the terminal alkyl group have inferior heat and hydrolytic stability, as well as insufficient lubricity.

There has yet to be developed, therefore, an ester-based refrigerating machine oil that has low viscosity and high lubricity for high efficiency, together with heat and hydrolytic stability and miscibility with refrigerants, while also satisfying the other required aspects of performance.

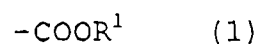
Disclosure of the Invention

It is an object of the present invention, which has been accomplished in light of the aforementioned problems of the prior art, to provide a refrigerating machine oil composition which has excellent lubricity, refrigerant miscibility, heat and hydrolytic stability

and electrical insulating property and which also increases the efficiency of refrigerating systems, when used together with HFC refrigerants or natural refrigerants such as carbon dioxide and hydrocarbons.

5 As a result of diligent research aimed at achieving this object, the present inventors have completed the present invention upon finding that the aforementioned problems are solved by a refrigerant oil composition comprising an alicyclic dicarboxylic
10 acid ester compound with two ester groups bonded to mutually adjacent carbon atoms on the alicyclic ring, wherein the ratio of cis-forms and trans-forms for the orientation of the two ester groups of the alicyclic dicarboxylic acid ester compound is controlled to be
15 within a specific range.

Namely, the refrigerating machine oil composition of the invention is a refrigerating machine oil composition comprising an alicyclic dicarboxylic acid ester compound containing an alicyclic ring and two
20 ester groups represented by the following general formula (1):



where R^1 represents a hydrocarbon group of 1-30 carbons,

25 the two ester groups bonded to mutually adjacent carbon atoms on the alicyclic ring,

wherein the molar ratio of cis-forms and trans-forms for the orientation of the two ester groups of the alicyclic dicarboxylic acid ester compound is from 20/80 to 80/20.

5 Moreover, in the refrigerating machine oil composition of the present invention, the molar ratio of cis-forms and trans-forms for the orientation of the two ester groups of the alicyclic dicarboxylic acid ester compound is preferably from 25/75 to 75/25,
10 more preferably from 30/70 to 70/30.

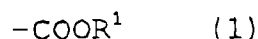
 In addition, the refrigerating machine oil composition of the present invention preferably also comprises at least one selected from the group consisting of phosphoric acid esters, acidic
15 phosphoric acid esters, amine salts of acidic phosphoric acid ester, chlorinated phosphoric acid esters and phosphorous acid esters.

 In addition, the refrigerating machine oil composition of the present invention preferably also
20 comprises at least one selected from the group consisting of phenylglycidyl ether-type epoxy compounds, alkylglycidyl ether-type epoxy compounds, glycidyl ester-type epoxy compounds, allyloxirane compounds, alkyloxirane compounds, alicyclic epoxy
25 compounds, epoxidized fatty acid monoesters and epoxidized vegetable oils.

Best Mode for Carrying Out the Invention

A preferred mode for the present invention will now be explained in detail.

The refrigerating machine oil composition of the invention is a refrigerating machine oil composition comprising an alicyclic dicarboxylic acid ester compound containing an alicyclic ring and two ester groups represented by the following general formula (1):



where R^1 represents a hydrocarbon group of 1-30 carbons,

the two ester groups bonded to mutually adjacent carbon atoms on the alicyclic ring,

wherein the molar ratio of cis-forms and trans-forms for the orientation of the two ester groups of the alicyclic dicarboxylic acid ester compound is from 20/80 to 80/20.

The alicyclic ring referred to here may be a cyclopentane ring, cyclopentene ring, cyclohexane ring, cyclohexene ring, cycloheptane ring, cycloheptene ring or the like, but is preferably a cyclohexane ring or cyclohexene ring. A cyclohexane ring is preferred among these because of its low rise in viscosity during use under prolonged and severe conditions, while a cyclohexene ring is even more

preferred because of its low rise in total acid value during use under prolonged and severe conditions.

An alicyclic dicarboxylic acid ester compound according to the invention comprises the
5 aforementioned alicyclic ring and two ester groups represented by formula (1) above. If only one ester group is present, the miscibility with refrigerants and the heat and hydrolytic stability are insufficient, whereas if three ester groups are
10 present, the low temperature flow properties are insufficient.

The two ester groups represented by formula (1) must also be bonded to mutually adjacent carbon atoms on the alicyclic ring. If they are not bonded to
15 mutually adjacent carbon atoms on the alicyclic ring, the heat and hydrolytic stability and the lubricity are inadequate.

An alicyclic dicarboxylic acid ester compound according to the invention includes both the cis- and
20 trans- forms for the orientation of the two adjacent ester groups represented by formula (1), but according to the invention, the molar ratio of the cis-forms and trans-forms is from 20/80 to 80/20, preferably from 25/75 to 75/25 and more preferably from 30/70 to
25 70/30. If the molar ratio of cis-forms and trans-forms is smaller than 20/80 it is not possible to

obtain high lubricity, whereas if it is greater than 80/20 it is not possible to obtain high heat and hydrolytic stability. As will be explained hereunder, one alicyclic dicarboxylic acid ester compound according to the invention may be used alone, or a mixture of two or more thereof may be used; however, when a refrigerating machine oil composition of the invention comprises two or more different types of alicyclic dicarboxylic acid esters, the molar ratio of the cis-forms and trans-forms refers to the molar ratio of the total cis-forms and total trans-forms in the composition.

R^1 in formula (1) represents a hydrocarbon group of 1-30, preferably 2-24 and more preferably 3-18 carbons. The hydrocarbon group referred to here may be an alkyl group, alkenyl group, cycloalkyl group, alkylcycloalkyl group, aryl group, alkylaryl group, arylalkyl group or the like. Preferred among these are alkyl group, cycloalkyl group and alkylcycloalkyl group from the standpoint of heat and hydrolytic stability.

The alkyl group may be straight or branched chain alkyl group, and as specific examples there may be mentioned straight or branched chain propyl group, straight or branched chain butyl group, straight or branched chain pentyl group, straight or branched

chain hexyl group, straight or branched chain heptyl group, straight or branched chain octyl group, straight or branched chain nonyl group, straight or branched chain decyl group, straight or branched chain undecyl group, straight or branched chain dodecyl group, straight or branched chain tridecyl group, straight or branched chain tetradecyl group, straight or branched chain pentadecyl group, straight or branched chain hexadecyl group, straight or branched chain heptadecyl group and straight or branched chain octadecyl group.

Among these, preferred straight chain alkyl groups are those with 4 or more carbons from the standpoint of heat and hydrolytic stability, and those with no more than 18 carbons from the standpoint of refrigerant miscibility. Preferred branched alkyl groups are those with 3 or more carbons from the standpoint of heat and hydrolytic stability, and those with no more than 18 carbons from the standpoint of refrigerant miscibility.

As cycloalkyl group there may be mentioned cyclopentyl group, cyclohexyl group, cycloheptyl group and the like, with cyclohexyl group being preferred from the standpoint of heat and hydrolytic stability. An alkylcycloalkyl group is one having an alkyl group bonded to a cycloalkyl group, and those with alkyl

groups bonded to cyclohexyl group are preferred from the standpoint of heat and hydrolytic stability. Preferred alkylcycloalkyl groups are also those with a total of 6 or more carbons from the standpoint of heat and hydrolytic stability, and those with no more than a total of 10 carbons from the standpoint of refrigerant miscibility and low temperature flow properties.

An alicyclic dicarboxylic acid ester compound according to the invention can be obtained by the production process described below, using a monohydric alcohol (R^1OH , where R^1 has the same definition as R^1 in formula (1) above) and an alicyclic dicarboxylic acid or its acid anhydride with two carboxyl groups on mutually adjacent carbon atoms on the alicyclic ring. According to the invention, the two R^1 groups of the alicyclic dicarboxylic acid ester compound may be the same or different, but the alcohol component used preferably includes

(a) at least one type of alcohol selected from the group consisting of aliphatic alcohols of 1-5 carbons, and

(b) at least one type of alcohol selected from the group consisting of aliphatic alcohols of 6-18 carbons,

in order to obtain adequate heat and hydrolytic

stability and lubricity, as well as excellent refrigerant miscibility. When only one type of alcohol from (a) above is used, the obtained alicyclic dicarboxylic acid ester compound tends to have inferior heat and hydrolytic stability as well as insufficient lubricity. When only one type of alcohol from (b) above is used, the obtained alicyclic dicarboxylic acid ester compound tends to have insufficient refrigerant miscibility.

While the alicyclic dicarboxylic acid ester compound according to the invention is preferably obtained using two or more different alcohols, it is particularly preferred to use both an alcohol from (a) and an alcohol from (b) above. Even if two or more different alcohols from (a) alone are used, the obtained alicyclic dicarboxylic acid ester compound tends to have inferior heat and hydrolytic stability, and insufficient lubricity. Also, even if two or more different alcohols from (b) alone are used, the obtained alicyclic dicarboxylic acid ester compound tends to have insufficient miscibility with refrigerants.

In an alicyclic dicarboxylic acid ester compound obtained using the aforementioned alcohol components (a) and (b), the R^1 derived from the aliphatic alcohol (a) is an alkyl group of 1-5 carbons, but is

preferably an alkyl group of 3-5 carbons from the standpoint of heat and hydrolytic stability. The alkyl group of 1-5 carbons may be straight or branched chain alkyl group, but straight chain alkyl group is preferred from the standpoint of lubricity, while branched chain alkyl group is preferred from the standpoint of refrigerant miscibility and heat and hydrolytic stability.

As specific examples of alkyl groups of 1-5 carbons derived from the alcohol component (a) there may be mentioned methyl group, ethyl group, straight or branched chain propyl group, straight or branched chain butyl group, straight or branched chain pentyl group and the like, among which n-butyl group and n-pentyl group are preferred from the standpoint of lubricity, while iso-butyl group and iso-pentyl group are preferred from the standpoint of heat and hydrolytic stability.

Furthermore, in an alicyclic dicarboxylic acid ester compound obtained using alcohol components (a) and (b), the R^1 derived from the aliphatic alcohol (b) is an alkyl group of 6-18 carbons but is preferably an alkyl group of 6-12 carbons, and more preferably an alkyl group of 7-9 carbons, from the standpoint of miscibility. The alkyl group of 6-18 carbons may be straight or branched chain alkyl group, but straight

chain alkyl group is preferred from the standpoint of lubricity, while branched chain alkyl group is preferred from the standpoint of miscibility and heat and hydrolytic stability. Alkyl group with more than 18 carbons is not preferred because they result in inferior refrigerant miscibility and low temperature flow properties.

As specific examples of alkyl group of 6-18 carbons derived from the alcohol component (b) there may be mentioned straight or branched chain hexyl group, straight or branched chain heptyl group, straight or branched chain octyl group, straight or branched chain nonyl group, straight or branched chain decyl group, straight or branched chain undecyl group, straight or branched chain dodecyl group, straight or branched chain tridecyl group, straight or branched chain tetradecyl group, straight or branched chain pentadecyl group, straight or branched chain hexadecyl group, straight or branched chain heptadecyl group and straight or branched chain octadecyl group, among which n-heptyl group, n-octyl group, n-nonyl group and n-decyl group are preferred from the standpoint of lubricity and miscibility, while iso-heptyl group, 2-ethylhexyl group and 3,5,5-trimethylhexyl group are preferred from the standpoint of both miscibility and heat and hydrolytic stability.

Preferred alicyclic dicarboxylic acid ester compounds according to the invention are ester compounds obtained using alcohols of the aforementioned (a) components and alcohols of the aforementioned (b) components, and they include the following.

(A) Esters wherein one of the two ester groups represented by general formula (1) in the same molecule is a group derived from an (a) component, and the other is a group derived from a (b) component;

(B) Mixtures of esters wherein the two ester groups represented by general formula (1) present in the same molecule are both groups derived from (a) components, and esters wherein the two ester groups represented by general formula (1) present in the same molecule are both groups derived from (b) components;

(C) Mixtures of (A) and (B).

Any of (A) to (C) above may be used as preferred alicyclic dicarboxylic acid ester compounds according to the invention, but (A) or (C) is particularly preferred from the standpoint of heat and hydrolytic stability.

In the case of (C), the proportion of (A) and (B) is not particularly restricted, but (A) is present at preferably 5% by mass or greater, more preferably 10% by mass or greater, even more preferably 15% by mass

or greater and most preferably 20% by mass or greater, with respect to the total of (A) and (B) from the standpoint of heat and hydrolytic stability.

For the R^1 components of formula (1) for the preferred alicyclic dicarboxylic acid ester compound of the invention, the ratio (molar ratio) of R^1 derived from an alcohol of (a) component and R^1 derived from an alcohol of (b) component is not particularly restricted, but it is preferably in the range of 1/99 to 99/1 since this will allow the lubricity, heat and hydrolytic stability and refrigerant miscibility to all be satisfied.

From a standpoint focused on the miscibility, the ratio (molar ratio) of R^1 derived from an (a) alcohol and R^1 derived from a (b) alcohol is preferably in the range of 60/40 to 99/1, more preferably in the range of 70/30 to 99/1 and most preferably in the range of 80/20 to 99/1. From a standpoint more focused on the heat and hydrolytic stability and lubricity, the aforementioned ratio is preferably in the range of 1/99 to 60/40, more preferably in the range of 1/99 to 50/50 and most preferably in the range of 1/99 to 40/60.

The alicyclic dicarboxylic acid ester compound may of course contain one or more than one hydrocarbon groups on the carbon atoms of the alicyclic ring.

Alkyl groups are preferred as such hydrocarbon groups, with methyl group being particularly preferred from the standpoint of miscibility.

5 An alicyclic dicarboxylic acid ester compound according to the invention has the structure described above, and such ester compounds are prepared by esterification of the prescribed acid component and alcohol component by a common process, preferably in an inert gas atmosphere such as nitrogen and with
10 heating in the presence of an esterifying catalyst or without a catalyst.

As acid components for the alicyclic dicarboxylic acid ester compound there may be mentioned cycloalkanedicarboxylic acids, cycloalkenedicarboxylic
15 acids and their acid anhydrides, wherein two ester groups are bonded to mutually adjacent carbon atoms on the alicyclic ring, and any one or mixture of two or more of these may be used. Specifically there may be mentioned 1,2-cyclohexanedicarboxylic acid, 4-
20 cyclohexene-1,2-dicarboxylic acid, 1-cyclohexene-1,2-dicarboxylic acid, 3-methyl-1,2-cyclohexanedicarboxylic acid, 4-methyl-1,2-cyclohexanedicarboxylic acid, 3-methyl-4-cyclohexene-1,2-dicarboxylic acid, 4-methyl-4-cyclohexene-1,2-
25 dicarboxylic acid and their acid anhydrides. Of these, 1,2-cyclohexanedicarboxylic acid, 3-methyl-

1,2,-cyclohexanedicarboxylic acid, 4-methyl-1,2-cyclohexanedicarboxylic acid and their acid anhydrides are preferred from the standpoint of minimizing rise in viscosity of the prepared ester compound during its use under prolonged and severe conditions, with 1,2-cyclohexanedicarboxylic acid being most preferred for its excellent miscibility. On the other hand, 4-cyclohexene-1,2-dicarboxylic acid, 1-cyclohexene-1,2-dicarboxylic acid, 4-methyl-1,2-cyclohexanedicarboxylic acid, 3-methyl-4-cyclohexene-1,2-dicarboxylic acid and 4-methyl-4-cyclohexene-1,2-dicarboxylic acid and their acid anhydrides are preferred from the standpoint of minimizing rise in the total acid value during use under prolonged and severe conditions, with 4-cyclohexene-1,2-dicarboxylic acid being most preferred for its excellent miscibility and heat and hydrolytic stability. According to the invention, when one of the aforementioned alicyclic dicarboxylic acids is used as the acid component, the molar ratio of cis-forms and trans-forms in the alicyclic dicarboxylic acid must be between 20/80 and 80/20, preferably between 25/75 and 75/25, and more preferably between 30/70 and 70/30.

There are no particular restrictions on the production process for these alicyclic dicarboxylic acids and their anhydrides, and any conventional

publicly known process may be employed. As a specific example, 4-cyclohexene-1,2-dicarboxylic acid may be obtained by reacting butadiene and maleic anhydride in a benzene solvent at 100°C.

5 The alcohol component of the alicyclic dicarboxylic acid ester compound of the invention may be a straight chain alcohol of 3-18 carbons, a branched chain alcohol of 3-18 carbons or a cycloalcohol of 5-10 carbons. Specifically there may
10 be mentioned straight or branched chain propanol (including n-propanol, 1-methylethanol, etc.), straight or branched chain butanol (including n-butanol, 1-methylpropanol, 2-methylpropanol, etc.), straight or branched chain pentanol (including n-
15 pentanol, 1-methylbutanol, 2-methylbutanol, 3-methylbutanol, etc.), straight or branched chain hexanol (including n-hexanol, 1-methylpentanol, 2-methylpentanol, 3-methylpentanol, etc.), straight or branched chain heptanol (including n-heptanol, 1-
20 methylhexanol, 2-methylhexanol, 3-methylhexanol, 4-methylhexanol, 5-methylhexanol, 2,4-dimethylpentanol, etc.), straight or branched chain octanol (including n-octanol, 2-ethylhexanol, 1-methylheptanol, 2-methylheptanol, etc.), straight or branched chain
25 nonanol (including n-nonanol, 1-methyloctanol, 3,5,5-trimethylhexanol, 1-(2'-methylpropyl)-3-methylbutanol,

etc.), straight or branched chain decanol (including n-decanol, iso-decanol, etc.), straight or branched chain undecanol (including n-undecanol, etc.), straight or branched chain dodecanol (including n-dodecanol, iso-dodecanol, etc.), straight or branched chain tridecanol, straight or branched chain tetradecanol (including n-tetradecanol, iso-tetradecanol, etc.), straight or branched chain pentadecanol, straight or branched chain hexadecanol (including n-hexadecanol, iso-hexadecanol, etc.), straight or branched chain heptadecanol, straight or branched chain octadecanol (including n-octadecanol, iso-octadecanol, etc.), cyclohexanol, methylcyclohexanol, dimethylcyclohexanol, and the like.

As mentioned above, a preferred alcohol component used according to the invention is

(a) at least one type of alcohol selected from the group consisting of aliphatic alcohols of 1-5 carbons, and

(b) at least one type of alcohol selected from the group consisting of aliphatic alcohols of 6-18 carbons.

As alcohols of (a) above there may be mentioned straight chain alcohols of 1-5 carbons and branched chain alcohols of 3-5 carbons. As specific examples

there may be mentioned methanol, ethanol, n-propanol, n-butanol, n-pentanol, iso-propanol, iso-butanol, sec-butanol and iso-pentanol, among which n-butanol and n-pentanol are preferred from the standpoint of lubricity, while iso-butanol and iso-pentanol are preferred from the standpoint of heat and hydrolytic stability.

On the other hand, as alcohols of (b) above there may be mentioned straight chain alcohols of 6-18 carbons and branched chain alcohols of 6-18 carbons. As specific examples there may be mentioned n-hexanol, n-heptanol, n-octanol, n-nonanol, n-decanol, n-undecanol, n-dodecanol, n-tetradecanol, n-hexadecanol, n-octadecanol, iso-hexanol, 2-methylhexanol, 1-methylheptanol, 2-methylheptanol, iso-heptanol, 2-ethylhexanol, 2-octanol, iso-octanol, 3,5,5-trimethylhexanol, iso-decanol, iso-tetradecanol, iso-hexadecanol, iso-octadecanol and 2,6-dimethyl-4-heptanol, with n-heptanol, n-octanol, n-nonanol and n-decanol being preferred from the standpoint of both lubricity and miscibility, and iso-heptanol, 2-ethylhexanol and 3,5,5-trimethylhexanol being preferred from the standpoint of both miscibility and heat and hydrolytic stability.

When the aforementioned acid component and alcohol component are used for esterification

reaction, the alcohol component is used at 1.0-1.5 equivalents and preferably 1.05-1.2 equivalents to 1 equivalent of the acid component, for example.

Furthermore, instead of the aforementioned acid components and alcohol components, lower alcohol esters of these acid components and/or acetic acid esters and propionic acid esters of these alcohols may be used to obtain alicyclic dicarboxylic acid ester compounds according to the invention by ester exchange reaction.

Specific examples of esterifying catalysts to be used for the invention include Lewis acids such as aluminum derivatives, tin derivatives and titanium derivatives; alkali metal salts such as sodium alkoxides and potassium alkoxides; and sulfonic acids such as para-toluenesulfonic acid, methanesulfonic acid and sulfuric acid. The amount of esterifying catalyst used may be, for example, about 0.1-1% by mass with respect to the total of the acid component and alcohol component raw materials. In consideration of the effect on the heat and hydrolytic stability of the obtained alicyclic dicarboxylic acid ester compound, a Lewis acid such as an aluminum derivative, tin derivative or titanium derivative is preferred, and tin derivatives are particularly preferred from the standpoint of reaction efficiency.

The temperature for the esterification is typically 150-230°C, and the reaction is usually complete by 3 to 30 hours.

After completion of the esterification reaction, the excess raw materials are distilled off under reduced pressure or under ordinary pressure, and then a common purification method such as liquid/liquid extraction, reduced pressure distillation, adsorption purification treatment with active carbon or the like, may be employed to purify the ester compound.

By using as the acid component of the raw material for the esterification reaction an alicyclic dicarboxylic acid with a molar ratio of 20/80 to 80/20 for cis-forms and trans-forms, it is possible to obtain an alicyclic dicarboxylic ester with a molar ratio of 20/80 to 80/20 for cis-forms and trans-forms. When an alicyclic dicarboxylic anhydride is used as the acid component of the raw material, the reaction may also be carried out under prescribed conditions to obtain an alicyclic dicarboxylic acid ester with the cis-form/trans-form molar ratio within the range specified above. An already prepared cis-form alicyclic dicarboxylic acid ester and trans-form alicyclic dicarboxylic acid ester may also be mixed with their molar ratios within the range specified above.

There are no particular restrictions on the content of the alicyclic dicarboxylic acid ester compound in the refrigerating machine oil composition of the invention, but it is preferably present at 5% by mass or greater, more preferably 10% by mass or greater, even more preferably 30% by mass or greater and most preferably 50% by mass or greater based on the total of the refrigerating machine oil composition, in order to bring out the excellent performance of the alicyclic dicarboxylic acid ester compound.

The alicyclic dicarboxylic acid ester compound in the refrigerating machine oil composition of the invention is used primarily as a base oil. While the alicyclic dicarboxylic acid ester compound may be used alone as the base oil for the refrigerating machine oil composition of the invention, it may also be used in combination with oxygen-containing synthetic oils including esters other than the alicyclic dicarboxylic acid ester compound specified by the invention, such as polyol esters and complex esters, polyglycols, polyvinyl ethers, ketones, polyphenyl ethers, silicones, polysiloxanes and perfluoroethers.

There are no particular restrictions on the amount of oxygen-containing synthetic oils included. From the standpoint of achieving improvement in

thermal efficiency as well as heat and hydrolytic stability of the refrigerating machine oil, however, other oxygen-containing synthetic oils are preferably present at no greater than 150 parts by weight, and
5 more preferably no greater than 100 parts by weight, to 100 parts by weight of the alicyclic dicarboxylic acid ester compound.

The refrigerating machine oil composition of the invention comprises an alicyclic dicarboxylic acid
10 ester compound and if necessary oxygen-containing synthetic oils, and these are used primarily for the base oil. The refrigerating machine oil composition of the invention may also be suitably used with no further additives, or if necessary, it may be used in
15 a form combined with various additives.

For further enhancement of the abrasion resistance and load resistance of the refrigerating machine oil composition of the invention, it may further include at least one type of phosphorus
20 compound selected from the group consisting of phosphoric acid esters, acidic phosphoric acid esters, amine salts of acidic phosphoric acid ester, chlorinated phosphoric acid esters and phosphorous acid esters. These phosphorus compounds are esters of
25 phosphoric acid or phosphorous acid with alkanols and polyether alcohols, or derivatives thereof.

As specific examples of phosphoric acid esters there may be mentioned tributyl phosphate, tripentyl phosphate, trihexyl phosphate, triheptyl phosphate, trioctyl phosphate, trinonyl phosphate, tridecyl phosphate, triundecyl phosphate, tridodecyl phosphate, 5 tritridecyl phosphate, tritetradecyl phosphate, tripentadecyl phosphate, trihexadecyl phosphate, triheptadecyl phosphate, trioctadecyl phosphate, trioleyl phosphate, triphenyl phosphate, tricresyl phosphate, trixylenyl phosphate, cresyldiphenyl phosphate and xylenyldiphenyl phosphate. As acidic phosphoric acid esters there may be mentioned monobutyl acid phosphate, monopentyl acid phosphate, monohexyl acid phosphate, monoheptyl acid phosphate, 15 monooctyl acid phosphate, monononyl acid phosphate, monodecyl acid phosphate, monoundecyl acid phosphate, monododecyl acid phosphate, monotridecyl acid phosphate, monotetradecyl acid phosphate, monopentadecyl acid phosphate, monohexadecyl acid phosphate, 20 monoheptadecyl acid phosphate, mono-octadecyl acid phosphate, monooleyl acid phosphate, dibutyl acid phosphate, dipentyl acid phosphate, dihexyl acid phosphate, diheptyl acid phosphate, dioctyl acid phosphate, dinonyl acid phosphate, 25 didecyl acid phosphate, diundecyl acid phosphate, didodecyl acid phosphate, ditridecyl acid

phosphate, ditetradecyl acid phosphate, dipentadecyl
acid phosphate, dihexadecyl acid phosphate,
diheptadecyl acid phosphate, dioctadecyl acid
phosphate and dioleyl acid phosphate. As amine salts
5 of acidic phosphoric acid ester there may be mentioned
amine salts of the above acidic phosphoric esters and
amines such as methylamine, ethylamine, propylamine,
butylamine, pentylamine, hexylamine, heptylamine,
octylamine, dimethylamine, diethylamine,
10 dipropylamine, dibutylamine, dipentylamine,
dihexylamine, diheptylamine, dioctylamine,
trimethylamine, triethylamine, tripropylamine,
tributylamine, tripentylamine, trihexylamine,
triheptylamine and trioctylamine. As chlorinated
15 phosphoric acid esters there may be mentioned tris
dichloropropyl phosphate, tris chloroethyl phosphate,
tris chlorophenyl phosphate and polyoxyalkylene
bis[di(chloroalkyl)] phosphate. As phosphorous acid
esters there may be mentioned dibutyl phosphite,
20 dipentyl phosphite, dihexyl phosphite, diheptyl
phosphite, dioctyl phosphite, dinonyl phosphite,
didecyl phosphite, diundecyl phosphite, didodecyl
phosphite, dioleyl phosphite, diphenyl phosphite,
dicresyl phosphite, tributyl phosphite, tripentyl
25 phosphite, trihexyl phosphite, triheptyl phosphite,
trioctyl phosphite, trinonyl phosphite, tridecyl

phosphite, triundecyl phosphite, tridodecyl phosphite, trioleyl phosphite, triphenyl phosphite and tricresyl phosphite. Mixtures of these may also be used.

When such phosphorus compounds are added to the refrigerating machine oil composition of the invention there are no particular restrictions on their content, but such phosphorus compounds will usually be added to a content of 0.01-5.0% by mass and preferably 0.02-3.0% by mass, based on the total of the refrigerating machine oil composition (based on the total of the base oil and all additives).

For enhanced heat and hydrolytic stability of the refrigerating machine oil composition of the invention, there may also be included one or more epoxy compounds selected from the group consisting of the following (i) to (viii):

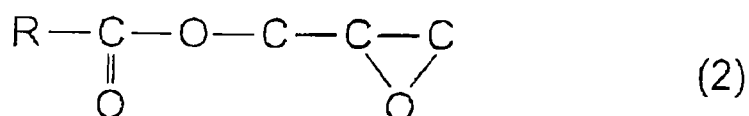
- (i) phenylglycidyl ether-type epoxy compounds
- (ii) alkylglycidyl ether-type epoxy compounds
- (iii) glycidyl ester-type epoxy compounds
- (iv) allyloxirane compounds
- (v) alkyloxirane compounds
- (vi) alicyclic epoxy compounds
- (vii) epoxidized fatty acid monoesters
- (viii) epoxidized vegetable oils

Specific examples of (i) phenylglycidyl ether-type epoxy compounds include phenylglycidyl ethers and

alkylphenylglycidyl ethers. Here, the alkylphenylglycidyl ethers may have 1-3 alkyl groups of 1-13 carbons, among which preferred examples include those with one alkyl group of 4-10 carbons, such as n-butylphenylglycidyl ether, i-butylphenylglycidyl ether, sec-butylphenylglycidyl ether, tert-butylphenylglycidyl ether, pentylphenylglycidyl ether, hexylphenylglycidyl ether, heptylphenylglycidyl ether, octylphenylglycidyl ether, nonylphenylglycidyl ether and decylphenylglycidyl ether.

Specific examples of (ii) alkylglycidyl ether-type epoxy compounds include decylglycidyl ether, undecylglycidyl ether, dodecylglycidyl ether, tridecylglycidyl ether, tetradecylglycidyl ether, 2-ethylhexylglycidyl ether, neopentylglycoldiglycidyl ether, trimethylolpropane triglycidyl ether, pentaerythritol tetraglycidyl ether, 1,6-hexanediol diglycidyl ether, sorbitolpolyglycidyl ether, polyalkyleneglycol monoglycidyl ether and polyalkyleneglycol diglycidyl ether.

Specific examples of (iii) glycidyl ester-type epoxy compounds include compounds represented by the following general formula (2):



where R represents a hydrocarbon group of 1-18 carbons.

In formula (2) above, R represents a hydrocarbon group of 1-18 carbons, and as such hydrocarbon groups there may be mentioned alkyl groups of 1-18 carbons, alkenyl groups of 2-18 carbons, cycloalkyl groups of 5-7 carbons, alkylcycloalkyl groups of 6-18 carbons, aryl groups of 6-10 carbons, alkylaryl groups of 7-18 carbons and arylalkyl groups of 7-18 carbons. Preferred among these are alkyl groups of 5-15 carbons, alkenyl groups of 2-15 carbons, phenyl groups and alkylphenyl groups with alkyl groups of 1-4 carbons.

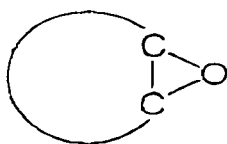
Specific preferred examples among these glycidyl ester epoxy compounds include glycidyl-2,2-dimethyl octanoate, glycidyl benzoate, glycidyl-tert-butyl benzoate, glycidyl acrylate, glycidyl methacrylate and the like.

Specific examples of (iv) allyloxirane compounds include 1,2-epoxystyrene and alkyl-1,2-epoxystyrene.

Specific examples of (v) alkyloxirane compounds include 1,2-epoxybutane, 1,2-epoxypentane, 1,2-epoxyhexane, 1,2-epoxyheptane, 1,2-epoxyoctane, 1,2-

epoxynonane, 1,2-epoxydecane, 1,2-epoxyundecane, 1,2-
 epoxydodecane, 1,2-epoxytridecane, 1,2-
 epoxytetradecane, 1,2-epoxypentadecane, 1,2-
 epoxyhexadecane, 1,2-epoxyheptadecane, 1,1,2-
 5 epoxyoctadecane, 2-epoxynonadecane and 1,2-
 epoxyeicosane.

As (vi) alicyclic epoxy compounds there may be
 mentioned compounds wherein carbon atoms composing the
 epoxy group are directly part of the alicycle, such as
 10 compounds represented by the following general formula
 (3):



(3)

Specific examples of such alicyclic epoxy
 compounds include 1,2-epoxycyclohexane, 1,2-
 15 epoxycyclopentane, 3,4-epoxycyclohexylmethyl-3,4-
 epoxycyclohexane carboxylate, bis(3,4-
 epoxycyclohexylmethyl) adipate, exo-2,3-
 epoxynorbornane, bis(3,4-epoxy-6-
 methylcyclohexylmethyl) adipate, 2-(7-
 20 oxabicyclo[4.1.0]hept-3-yl)-spiro(1,3-dioxane-5,3'-
 [7]oxabicyclo[4.1.0]heptane, 4-(1'-methylepoxyethyl)-
 1,2-epoxy-2-methylcyclohexane, 4-epoxyethyl-1,2-
 epoxycyclohexane.

Specific examples of (vii) epoxidized fatty acid

monoesters include esters of epoxidized fatty acids of 12-20 carbons and alcohols of 1-8 carbons, phenols or alkylphenols. Particularly preferred for use are butyl, hexyl, benzyl, cyclohexyl, methoxyethyl, octyl, phenyl and butylphenyl esters of epoxystearic acid.

Specific examples of (viii) epoxidized vegetable oils include epoxy compounds of vegetable oils such as soybean oil, linseed oil and cottonseed oil.

Among the aforementioned epoxy compounds, phenylglycidyl ether epoxy compounds, glycidyl ester epoxy compounds, alicyclic epoxy compounds and epoxidized fatty acid monoesters are preferred for further improved heat and hydrolytic stability, with glycidyl ester epoxy compounds and alicyclic epoxy compounds being even more preferred.

When these epoxy compounds are incorporated in a refrigerating machine oil composition according to the invention, there are no particular restrictions on their addition content but the epoxy compound is added to a content of preferably 0.1-5.0% by mass and more preferably 0.2-2.0% by mass, based on the total amount of the refrigerating machine oil composition (the total amount of the base oil and all incorporated additives).

Two or more different types of the aforementioned phosphorus compounds and epoxy compounds may, of

course, be used in combination.

In order to further improve performance, the refrigerating machine oil composition of the invention may be incorporated, as required, with hitherto publicly known additives for refrigerating machine oils, for example, phenol-type antioxidants such as di-tert-butyl-p-cresol and bisphenol A; amine-type antioxidants such as phenyl- α -naphthylamine and N,N-di(2-naphthyl)-p-phenylenediamine; wear resistance agents such as zinc dithiophosphate; extreme pressure agents such as chlorinated paraffin and sulfur compounds; oiliness improvers such as fatty acids; antifoaming agents such as silicone types; metal inactivators such as benzotriazole; viscosity index improvers; pour-point depressants; detergent dispersants and the like, either alone or in combinations of more than one type. The total amount of the additives added into the refrigerating machine oil is not particularly limited, but in general the content is preferably not more than 10% by mass and more preferably not more than 5% by mass, of the total amount of the refrigerating machine oil composition (i.e., the total amount of the base oil and all incorporated additives).

The kinematic viscosity of the refrigerating machine oil of the invention is not particularly

limited, but the kinematic viscosity at 40°C is preferably within a range of 3 to 100 mm²/s, more preferably 4 to 50 mm²/s and most preferably 5 to 40 mm²/s. Further, the kinematic viscosity at 100°C is within a range of 1 to 20 mm²/s and more preferably 2 to 10 mm²/s. One of the effects achieved by the invention is that satisfactory heat and hydrolytic stability can be obtained even when the viscosity is low, and this effect is more notably achieved in the case where the kinematic viscosity at 40°C is within a range of preferably 5 to 35 mm²/s, more preferably 5 to 25 mm²/s, even more preferably 5 to 20 mm²/s, and most preferably 5 to 15 mm²/s.

Also, the volume resistivity of the refrigerating machine oil composition of the invention is not particularly limited, but is preferably at least $1.0 \times 10^{11} \Omega \cdot \text{cm}$, more preferably at least $1.0 \times 10^{12} \Omega \cdot \text{cm}$ and most preferably at least $1.0 \times 10^{13} \Omega \cdot \text{cm}$. Particularly, when the refrigerating machine oil composition is used for a hermetic type refrigerating machine, a high electric insulating property tends to be requisite. According to the present invention, the volume resistivity is represented by the value [$\Omega \cdot \text{cm}$] at 25°C measured in accordance with JIS C 2101 "Electric Insulating Oil Testing Method."

The moisture content of the refrigerating machine

oil composition of the invention is not particularly limited, but is preferably no greater than 200 ppm, more preferably no greater than 100 ppm, and most preferably no greater than 50 ppm, of the total amount of the refrigerating machine oil composition. A low moisture content is particularly required when the refrigerating machine oil composition is used for a hermetic type refrigerating machine, because of its effects on the heat and hydrolytic stability and the electric insulating property of the oil.

The total acid value of the refrigerating machine oil composition of the invention is also not particularly limited, but when the oil composition is used in a refrigerating machine or in pipes to prevent metals from corrosion, the total acid value is preferably no greater than 0.1 mgKOH/g, and more preferably no greater than 0.05 mgKOH/g. According to the invention, the total acid value is represented as the total acid value measured in accordance with JIS K 2501 "Petroleum Products and Lubricating Oils -- Neutralization Value Testing Method".

The ash content of the refrigerating machine oil composition of the invention is not particularly limited, but in order to improve the heat and hydrolytic stability of the oil and reduce generation of sludge and the like, it is preferably no greater

than 100 ppm, and more preferably no greater than 50 ppm. According to the invention, the ash content is represented by the ash content value [ppm] as measured in accordance with JIS K 2272 "Testing Method for Ash
5 Content and Sulfuric Acid Ash Content in Crude Oils and Petroleum Products".

Refrigerants that may be used in refrigerating machines that employ refrigerating machine oil compositions according to the invention include HFC
10 refrigerants, fluorine-containing ether refrigerants such as perfluoroethers; fluorine-free ether refrigerants such as dimethyl ethers; and natural refrigerants such as carbon dioxide, hydrocarbons and the like, and these refrigerants can be used alone or
15 in combinations including two or more kinds of the refrigerants.

As HFC refrigerants there may be mentioned hydrofluorocarbons having 1-3 and preferably 1 or 2 carbon atoms. Specific examples include HFCs such as
20 difluoromethane (HFC-32), trifluoromethane (HFC-23), pentafluoroethane (HFC-125), 1,1,2,2-tetrafluoroethane (HFC-134), 1,1,1,2-tetrafluoroethane (HFC-134a), 1,1,1-trifluoroethane (HFC-143a), 1,1-difluoroethane (HFC-152a), and mixtures of two or more kinds of these
25 HFCs. The refrigerant is selected in accordance with the intended use and the required performance, and as

preferred examples there may be mentioned HFC-32 alone; HFC-23 alone; HFC-134a alone; HFC-125 alone; a mixture of HFC-134a/HFC-32 = 60-80% by mass/40-20% by mass; a mixture of HFC-32/HFC-125 = 40-70% by mass/60-30% by mass; a mixture of HFC-125/HFC-143a = 40-60% by mass/60-40% by mass; a mixture of HFC-134a/HFC-32/HFC-125 = 60% by mass/30% by mass/10% by mass; a mixture of HFC-134a/HFC-32/HFC-125 = 40-70% by mass/15-35% by mass/5-40% by mass; and a mixture of HFC-125/HFC-134a/HFC-143a = 35-55% by mass/1-15% by mass/40-60% by mass. More specific examples include a mixture of HFC-134a/HFC-32 = 70/30% by mass; a mixture of HFC-32/HFC-125 = 60/40% by mass; a mixture of HFC-32/HFC-125 = 50/50% by mass (R410A); a mixture of HFC-32/HFC-125 = 45/55% by mass (R410B); a mixture of HFC-125/HFC-143a = 50/50% by mass (R507C); a mixture of HFC-32/HFC-125/HFC-134a = 30/10/60% by mass; a mixture of HFC-32/HFC-125/HFC-134a = 23/25/52% by mass (R407C); a mixture of HFC-32/HFC-125/HFC-134a = 25/15/60% by mass (R407E); and a mixture of HFC-125/HFC-134a/HFC-143a = 44/4/52% by mass (R404A).

Examples of natural refrigerants include carbon dioxide, hydrocarbons and the like. A hydrocarbon refrigerant referred to here is preferably a gas at 25°C under 1 atm. Specifically such gases include alkanes, cycloalkanes and alkenes of 1 to 5 carbons

and preferably 1 to 4 carbons, as well as mixtures thereof. Specific examples of such hydrocarbon refrigerants include methane, ethylene, ethane, propylene, propane, cyclopropane, butane, isobutane
5 (i-butane), cyclobutane, methylcyclopropane and mixtures of two or more of these compounds. Propane, butane, isobutane and mixtures thereof are preferred among these.

The refrigerating machine oil composition of the
10 invention normally exists in the form of a refrigerating machine fluid composition mixed with a refrigerant as describe above when it is used in the refrigerating machine. According to the fluid composition, the mixing ratio of the refrigerating
15 machine oil composition to the refrigerant is not particularly limited, but the amount of the refrigerating machine oil composition is preferably within a range of 1 to 500 parts by weight and more preferably within a range of 2 to 400 parts by weight
20 to 100 parts by weight of the refrigerant.

The refrigerating machine oil composition of the invention can be used as a lubricating oil for refrigerant compressors in all types of refrigerating machines, because of its excellent electric properties
25 and low hygroscopicity. The refrigerating machines in which the composition may be used include,

specifically, an air conditioner for rooms, a package
air conditioner, a cold-storage chest (refrigerator),
an automotive air conditioner, a dehumidifier, a
freezer, a freeze and refrigeration warehouse, an
5 automatic vending machine, a showcase, a cooling
apparatuses in chemical plants, etc. The
refrigerating machine oil composition of the invention
is most preferably used in refrigerating machines
equipped with hermetic compressors. The refrigerating
10 machine oil composition of the invention may be used
with all types of compressors including reciprocating
types, rotary types and centrifugal types.

The construction of the preferred refrigerating
cycle in which the composition of the invention is
15 used will typically be equipped with a compressor, a
condenser, an expander and an evaporator, and if
necessary a drier.

The compressor may be, for example, a high-
pressure container-system compressor wherein a motor
20 comprising a rotator and a stator, a rotating shaft
fitted in the rotator, and a compressor section
connected to the motor are housed in a sealed
container holding a refrigerating machine oil, and
high-pressure refrigerant gas ejected from the
25 compressor section is collected in the sealed
container, or a low-pressure container-system

compressor wherein a motor comprising a rotator and a stator, a rotating shaft fitted in the rotator, and a compressor section connected to the motor are housed in a sealed container holding a refrigerating machine oil, and high-pressure refrigerant gas ejected from the compressor section is directly ejected out of the sealed container.

An insulating film used as the electric insulating system material for the motor section may be a crystalline plastic film with a glass transition point of 50°C or higher, specific preferred examples of which include one or more types of insulating films selected from the group consisting of polyethylene terephthalate, polybutylene terephthalate, polyphenylene sulfide, polyether-ether-ketone, polyethylene naphthalate, polyamideimide and polyimide, or composite films prepared by laminating high glass transition point resin layers on low glass transition point films, because of their resistance to deterioration in tensile strength and electric insulating property. The magnet wire which is used for the motor section is preferably one with an enamel coating having a glass transition point of 120°C or higher, such as a monolayer of a polyester, polyester imide, polyamide or polyamideimide, or an enamel coating which is a composite coating of a high glass

transition point upper layer on a low glass transition point underlayer. As composite coated enamel wires there may be mentioned those with a polyamideimide upper layer coated on a polyester imide underlayer (AI/EI), and those with a polyamideimide upper layer coated on a polyester underlayer (AI/PE). The drying agent packed in the drier is preferably synthetic zeolite comprising an alkali metal silicate/aluminate compound salt with a carbon dioxide gas absorption volume of no greater than 1.0% at a pore size of 3.3 Angstroms or smaller and a carbon dioxide gas partial pressure of 250 mmHg at 25°C. Specific examples include the trade names XH-9, XH-10, XH-11 and XH-600 by Union Showa Co., Ltd.

Examples

The present invention will now be explained in further detail by way of examples and comparative examples, with the understanding that the invention is in no way limited thereby.

Examples 1-32 and Comparative Examples 1-32

Sample oils were prepared for Examples 1-32 and Comparative Examples 1-32, using each of the following base oils and additives. The contents (% by mass) of the additives in the examples (based on the total sample oil weight) and the properties of each of the obtained sample oils (kinematic viscosity at 40°C and

100°C, total acid value) are shown in Tables 1-11.

[Base Oil]

Base Oil 1: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-heptanol

5 (Ester 1: 100% by mass, cis-form/trans-form ratio (molar ratio) = 55/45)

Base Oil 2: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 2-ethylhexanol

10 (Ester 2: 100% by mass, cis-form/trans-form ratio (molar ratio) = 58/42)

Base Oil 3: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 3,5,5-trimethylhexanol

15 (Ester 3: 100% by mass, cis-form/trans-form ratio (molar ratio) = 39/61)

Base Oil 4: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-nonanol

(Ester 4: 100% by mass, cis-form/trans-form ratio (molar ratio) = 66/34)

20 Base Oil 5: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-decanol

(Ester 5: 100% by mass, cis-form/trans-form ratio (molar ratio) = 49/51)

25 Base Oil 6: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and i-heptanol

(Ester 6: 100% by mass, cis-form/trans-form ratio

(molar ratio) = 35/65)

Base Oil 7: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and 2-ethylhexanol

(Ester 7: 100% by mass, cis-form/trans-form ratio

5 (molar ratio) = 45/55)

Base Oil 8: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and 3,5,5-trimethylhexanol

(Ester 8: 100% by mass, cis-form/trans-form ratio

(molar ratio) = 67/33)

10 Base Oil 9: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and n-heptanol

(Ester 9: 24% by mass, ester 10: 1% by mass, ester 11: 73% by mass, cis-form/trans-form ratio (molar ratio) = 53/47)

15 Base Oil 10: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and 2-ethylhexanol

(Ester 2: 51% by mass, ester 9: 36% by mass, ester 12: 13% by mass, cis-form/trans-form ratio (molar ratio) = 37/63)

20 Base Oil 11: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol

25 (Ester 3: 27% by mass, ester 9: 18% by mass, ester 13: 55% by mass, cis-form/trans-form ratio (molar ratio) = 62/38)

Base Oil 12: Ester obtained from 1,2-cyclohexanedicarboxylic acid, n-butanol and i-decanol
(Ester 5: 36% by mass, ester 14: 19% by mass, ester
15: 45% by mass, cis-form/trans-form ratio (molar
ratio) = 46/56)

Base Oil 13: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and n-heptanol
(Ester 16: 25% by mass, ester 17: 2% by mass, ester
18: 73% by mass, cis-form/trans-form ratio (molar
ratio) = 56/44)

Base Oil 14: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 2-ethylhexanol
(Ester 7: 51% by mass, ester 16: 39% by mass, ester
19: 10% by mass, cis-form/trans-form ratio (molar
ratio) = 37/63)

Base Oil 15: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol
(Ester 8: 26% by mass, ester 16: 17% by mass, ester
20: 57% by mass, cis-form/trans-form ratio (molar
ratio) = 42/58)

Base Oil 16: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, n-butanol and i-decanol
(Ester 21: 22% by mass, ester 22: 46% by mass, ester
23: 32% by mass, cis-form/trans-form ratio (molar
ratio) = 40/60)

Base Oil 17: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-heptanol
(Ester 1: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

5 Base Oil 18: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-heptanol
(Ester 1: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

10 Base Oil 19: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 2-ethylhexanol
(Ester 2: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

15 Base Oil 20: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 2-ethylhexanol
(Ester 2: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

20 Base Oil 21: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 3,5,5-trimethylhexanol
(Ester 3: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

25 Base Oil 22: Ester obtained from 1,2-cyclohexanedicarboxylic acid and 3,5,5-trimethylhexanol
(Ester 3: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

Base Oil 23: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-nonanol

(Ester 4: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

5 Base Oil 24: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-nonanol

(Ester 4: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

10 Base Oil 25: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-decanol

(Ester 5: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

Base Oil 26: Ester obtained from 1,2-cyclohexanedicarboxylic acid and i-decanol

15 (Ester 5: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

Base Oil 27: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and i-heptanol

20 (Ester 6: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

Base Oil 28: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and i-heptanol

(Ester 6: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

25 Base Oil 29: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid and 2-ethylhexanol

(Ester 7: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

Base Oil 30: Ester obtained from 4-cyclohexene-
1,2-dicarboxylic acid and 2-ethylhexanol

5 (Ester 7: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

Base Oil 31: Ester obtained from 4-cyclohexene-
1,2-dicarboxylic acid and 3,5,5-trimethylhexanol

10 (Ester 8: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 90/10)

Base Oil 32: Ester obtained from 4-cyclohexene-
1,2-dicarboxylic acid and 3,5,5-trimethylhexanol

(Ester 8: 100% by mass, cis-form/trans-form ratio
(molar ratio) = 10/90)

15 Base Oil 33: Ester obtained from 1,2-
cyclohexanedicarboxylic acid, i-butanol and n-heptanol
(Ester 9: 25% by mass, ester 10: 2% by mass, ester 11:
73% by mass, cis-form/trans-form ratio (molar ratio) =
90/10)

20 Base Oil 34: Ester obtained from 1,2-
cyclohexanedicarboxylic acid, i-butanol and n-heptanol
(Ester 9: 24% by mass, ester 10: 2% by mass, ester 11:
72% by mass, cis-form/trans-form ratio (molar ratio) =
10/90)

25 Base Oil 35: Ester obtained from 1,2-
cyclohexanedicarboxylic acid, i-butanol and 2-

ethylhexanol

(Ester 2: 50% by mass, ester 9: 38% by mass, ester 12: 12% by mass, cis-form/trans-form ratio (molar ratio) = 90/10)

5 Base Oil 36: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and 2-ethylhexanol

10 (Ester 2: 51% by mass, ester 9: 38% by mass, ester 12: 11% by mass, cis-form/trans-form ratio (molar ratio) = 10/90)

Base Oil 37: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol

15 (Ester 3: 26% by mass, ester 9: 18% by mass, ester 13: 56% by mass, cis-form/trans-form ratio (molar ratio) = 90/10)

Base Oil 38: Ester obtained from 1,2-cyclohexanedicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol

20 (Ester 3: 27% by mass, ester 9: 16% by mass, ester 13: 57% by mass, cis-form/trans-form ratio (molar ratio) = 10/90)

Base Oil 39: Ester obtained from 1,2-cyclohexanedicarboxylic acid, n-butanol and i-decanol

25 (Ester 5: 33% by mass, ester 14: 20% by mass, ester 15: 47% by mass, cis-form/trans-form ratio (molar

ratio) = 90/10)

5 Base Oil 40: Ester obtained from 1,2-cyclohexanedicarboxylic acid, n-butanol and i-decanol
(Ester 5: 34% by mass, ester 14: 20% by mass, ester
15: 46% by mass, cis-form/trans-form ratio (molar
ratio) = 10/90)

10 Base Oil 41: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and n-heptanol
(Ester 16: 26% by mass, ester 17: 2% by mass, ester
18: 72% by mass, cis-form/trans-form ratio (molar
ratio) = 90/10)

15 Base Oil 42: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and n-heptanol
(Ester 16: 27% by mass, ester 17: 2% by mass, ester
18: 71% by mass, cis-form/trans-form ratio (molar
ratio) = 10/90)

20 Base Oil 43: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 2-ethylhexanol
(Ester 7: 52% by mass, ester 16: 40% by mass, ester
19: 8% by mass, cis-form/trans-form ratio (molar
ratio) = 90/10)

25 Base Oil 44: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 2-ethylhexanol
(Ester 7: 50% by mass, ester 16: 41% by mass, ester
19: 9% by mass, cis-form/trans-form ratio (molar
ratio) = 10/90)

Base Oil 45: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol

5 (Ester 8: 26% by mass, ester 16: 18% by mass, ester 20: 56% by mass, cis-form/trans-form ratio (molar ratio) = 90/10)

Base Oil 46: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, i-butanol and 3,5,5-trimethylhexanol

10 (Ester 8: 27% by mass, ester 16: 17% by mass, ester 20: 56% by mass, cis-form/trans-form ratio (molar ratio) = 10/90)

Base Oil 47: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, n-butanol and i-decanol

15 (Ester 21: 20% by mass, ester 22: 47% by mass, ester 23: 33% by mass, cis-form/trans-form ratio (molar ratio) = 90/10)

Base Oil 48: Ester obtained from 4-cyclohexene-1,2-dicarboxylic acid, n-butanol and i-decanol

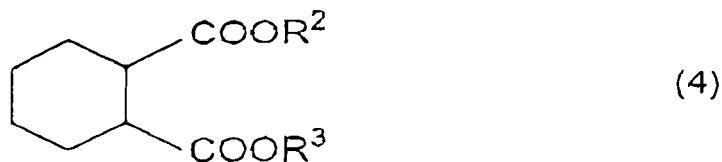
20 (Ester 21: 21% by mass, ester 22: 46% by mass, ester 23: 33% by mass, cis-form/trans-form ratio (molar ratio) = 10/90).

[1,2-cyclohexanedicarboxylic acid esters 1-5, 9-15]

25 The 1,2-cyclohexanedicarboxylic acid esters of the above base oils 1-5, 9-12, 17-26 and 33-40 have a

structure represented by the following general formula

(4):



where R^2 and R^3 of each ester are the following.

5 Ester 1 R^2 : i-heptyl group, R^3 : i-heptyl group

Ester 2 R^2 : 2-ethylhexyl group, R^3 : 2-ethylhexyl
group

Ester 3 R^2 : 3,5,5-trimethylhexyl group, R^3 :
3,5,5-trimethylhexyl group

10 Ester 4 R^2 : i-nonyl group, R^3 : i-nonyl group

Ester 5 R^2 : i-decyl group, R^3 : i-decyl group

Ester 9 R^2 : i-butyl group, R^3 : i-butyl group

Ester 10 R^2 : i-butyl group, R^3 : n-heptyl group

Ester 11 R^2 : n-heptyl group, R^3 : n-heptyl group

15 Ester 12 R^2 : i-butyl group, R^3 : 2-ethylhexyl
group

Ester 13 R^2 : i-butyl group, R^3 : 3,5,5-
trimethylhexyl group

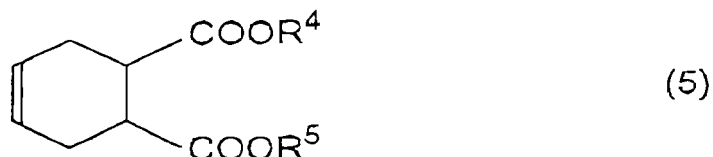
Ester 14 R^2 : n-butyl group, R^3 : n-butyl group

20 Ester 15 R^2 : n-butyl group, R^3 : i-decyl group.

[4-cyclohexene-1,2-dicarboxylic acid esters 6-8, 16-
23]

The 4-cyclohexene-1,2-dicarboxylic acid esters of

the above base oils 6-8, 13-16, 27-32 and 41-48 have a structure represented by the following general formula (5):



5 where R^4 and R^5 of each ester are the following.

Ester 6 R^4 : i-heptyl group, R^5 : i-heptyl group

Ester 7 R^4 : 2-ethylhexyl group, R^5 : 2-ethylhexyl group

Ester 8 R^4 : 3,5,5-trimethylhexyl group, R^5 : 3,5,5-trimethylhexyl group

Ester 16 R^4 : i-butyl group, R^5 : i-butyl group

Ester 17 R^4 : i-butyl group, R^5 : n-heptyl group

Ester 18 R^4 : n-heptyl group, R^5 : n-heptyl group

Ester 19 R^4 : i-butyl group, R^5 : 2-ethylhexyl group

Ester 20 R^4 : i-butyl group, R^5 : 3,5,5-trimethylhexyl group

Ester 21 R^4 : n-butyl group, R^5 : n-butyl group

Ester 22 R^4 : n-butyl group, R^5 : i-decyl group

Ester 23 R^4 : i-decyl group, R^5 : i-decyl group

[Additives]

Additive 1: Phenylglycidyl ether

Additive 2: Glycidyl-2,2-dimethyloctanoate

Additive 3: Cyclohexene oxide

The following tests were then carried out for each of the sample oils of Examples 1-32 and Comparative Examples 1-32.

5 (Refrigerant Miscibility Test)

10 In accordance with the "Refrigerant Miscibility Testing Method" of JIS-K-2211 "Refrigerating machine oils", 1 g of each of the sample oils was blended with 29 g of HFC134a refrigerant to observe whether the sample oils and the refrigerant were miscible with each other at 0°C, or whether they separated or formed a turbid state. The results are shown in Tables 1 to 11.

(Electric Insulating Property Test)

15 The volume resistivity of each of the sample oils at 25°C was measured in accordance with JIS-C-2101 "Electric Insulating Oil Testing Method." The results are shown in Tables 1 to 11.

(Heat/Hydrolytic stability Test I)

20 A 90 g portion of each of the sample oils prepared with a moisture content of 1000 ppm by mass was weighed out into an autoclave which was sealed after addition of 10 g of HFC134a refrigerant and catalysts (iron, copper and aluminum wires). The autoclave was then heated at 200°C for 2 weeks, after which the appearance of each of the sample oils and

25

the catalysts was observed, and the volume resistivity and total acid value of each of the sample oils was measured. The results are shown in Tables 1 to 11.

(Lubricity Test)

5 A wear tester employing a vane (SKH-51) as the upper test specimen and a disk (FC250 HRC40) as the lower test specimen was mounted inside a sealed container. A 600 ml portion of the sample oil was introduced into the wear testing zone, and after
10 evacuating the air from the system, HFC134a refrigerant was introduced and the system was heated. After adjustment of the system temperature to 100°C and the refrigerant pressure to 1.5 MPa, a stepwise load was applied up to 100 kgf at a load step of 10
15 kgf (2 minute steps). After a 60 minute test for each sample oil, the wear width of the vane and the wear depth of the disk were measured. The results are shown in Tables 1 to 8.

(Heat/Hydrolytic stability Test II)

20 A 90 g portion of each of the sample oils prepared with a moisture content of 1000 ppm by mass was weighed out into an autoclave which was sealed after addition of 10 g of HFC134a refrigerant and catalysts (iron, copper and aluminum wires). The
25 autoclave was then heated at 200°C for 2000 hours, after which the appearance of each of the sample oils

and the catalysts was observed, and the volume resistivity and total acid value of each of the sample oils was measured. The results are shown in Tables 9 to 11.

(Table 1)

		Example 1	Example 2	Example 3	Example 4	Example 5	Example 6
Base oil		Base oil 1	Base oil 2	Base oil 3	Base oil 4	Base oil 5	Base oil 6
Additive	Type	-	-	-	-	-	-
	Content (% by mass)	-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C	12.3	18.2	28.5	25.6	29.5	12.7
	100° C	2.8	3.5	4.7	4.5	4.7	2.8
Total acid value (mgKOH/g)		0.01	0.01	0.01	0.01	0.01	0.01
Miscibility		miscible	miscible	miscible	miscible	miscible	miscibl e
Volume resistivity (Ω·cm)		3.3 x 10 ¹³	4.9 x 10 ¹³	8.1 x 10 ¹³	7.9 x 10 ¹³	9.2 x 10 ¹²	3.5 x 10 ¹²
Heat / hydrolyti c stability I	Appearance of sample oil	no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)	4.9 x 10 ¹²	6.3 x 10 ¹²	1.9 x 10 ¹³	3.5 x 10 ¹³	4.4 x 10 ¹²	1.7 x 10 ¹¹
	Total acid value (mgKOH/g)	0.60	0.65	0.55	0.49	0.61	0.48
Lubricity test	Wear width (μm)	335	320	320	315	340	295
	Wear depth (μm)	1.3	1.4	1.1	1.5	1.4	1.1

(Table 2)

		Example 7	Example 8	Example 9	Example 10	Example 11	Example 12
Base oil		Base oil 7	Base oil 8	Base oil 9	Base oil 10	Base oil 11	Base oil 12
Additive	Type	-	-	-	-	-	-
	Content (% by mass)	-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C	16.5	29.5	10.8	12.7	12.7	12.6
	100° C	3.3	4.7	2.6	2.7	2.7	2.8
Total acid value (mgKOH/g)		0.01	0.01	0.00	0.00	0.00	0.00
Miscibility		miscible	miscible	miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)		2.2 × 10 ¹³	3.2 × 10 ¹³	7.5 × 10 ¹²	3.2 × 10 ¹³	3.7 × 10 ¹³	3.6 × 10 ¹³
Heat / hydrolytic stability I	Appearance of sample oil	no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)	4.7 × 10 ¹²	9.3 × 10 ¹¹	1.3 × 10 ¹²	5.2 × 10 ¹²	3.6 × 10 ¹²	5.8 × 10 ¹²
	Total acid value (mgKOH/g)	0.52	0.63	0.79	0.31	0.41	0.48
Lubricity test	Wear width (μm)	300	270	250	295	285	320
	Wear depth (μm)	1.2	1	0.8	1.1	1.2	1.2

(Table 3)

		Example 13	Example 14	Example 15	Example 16	Comp- Example 1	Comp. Example 2
Base oil		Base oil 13	Base oil 14	Base oil 15	Base oil 16	Base oil 17	Base oil 18
Additive	Type	-	-	-	-	-	-
	Content (% by mass)	-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C	10.3	12.9	15.2	11.7	12.5	12.0
	100° C	2.5	2.7	3.0	2.6	2.9	2.7
Total acid value (mgKOH/g)		0.00	0.00	0.00	0.00	0.01	0.00
Miscibility		miscible	miscible	miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)		1.9 x 10 ¹²	1.2 x 10 ¹²	1.9 x 10 ¹³	2.6 x 10 ¹³	2.7 x 10 ¹³	1.5 x 10 ¹³
Heat / hydrolyti c stability I	Appearance of sample oil		no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	partiall y blackene d
		Al	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		5.6 x 10 ¹¹	3.4 x 10 ¹¹	2.3 x 10 ¹²	4.5 x 10 ¹²	5.4 x 10 ¹²
	Total acid value (mgKOH/g)		0.86	0.35	0.39	0.61	0.60
Lubricity test	Wear width (μm)		275	295	305	290	390
	Wear depth (μm)		1.0	0.9	1.2	0.9	2.6
							1.3

(Table 4)

		Comp. Example 3	Comp. Example 4	Comp. Example 5	Comp. Example 6	Comp. Example 7	Comp. Example 8
Base oil		Base oil 19	Base oil 20	Base oil 21	Base oil 22	Base oil 23	Base oil 24
Additive	Type	-	-	-	-	-	-
	Content (% by mass)	-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C	18.2	18.2	28.5	28.5	25.6	25.6
	100° C	3.5	3.5	4.7	4.7	4.5	4.5
Total acid value (mgKOH/g)		0.01	0.01	0.01	0.01	0.01	0.01
Miscibility		miscible	miscible	miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)		4.6 x 10 ¹³	4.6 x 10 ¹³	7.4 x 10 ¹³	7.4 x 10 ¹³	8.1 x 10 ¹³	8.1 x 10 ¹³
Heat / hydrolytic stability I	Appearance of sample oil		no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change
		Fe	no change	partially blackened	no change	partially blackened	partially blackened
		Al	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		6.3 x 10 ¹²	2.1 x 10 ¹¹	2.2 x 10 ¹³	9.8 x 10 ¹⁰	2.8 x 10 ¹³
	Total acid value (mgKOH/g)		0.74	0.91	0.52	0.89	0.56
Lubricity test	Wear width (μm)		400	340	395	330	385
	Wear depth (μm)		2.9	1.5	2.5	1.0	2.4

(Table 5)

			Comp. Example 9	Comp. Example 10	Comp. Example 11	Comp. Example 12	Comp. Example 13	Comp. Example 14
Base oil			Base oil 25	Base oil 26	Base oil 27	Base oil 28	Base oil 29	Base oil 30
Additive	Type		-	-	-	-	-	-
	Content (% by mass)		-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C		29.5	29.5	12.8	12.5	18.9	17.7
	100° C		4.7	4.7	2.8	2.8	3.6	3.4
Total acid value (mgKOH/g)			0.01	0.01	0.01	0.01	0.01	0.01
Miscibility			miscible	miscible	miscibl e	miscible	miscible	miscible
Volume resistivity (Ω·cm)			8.3 x 10 ¹²	8.3 x 10 ¹²	3.1 x 10 ¹²	3.1 x 10 ¹²	6.1 x 10 ¹²	6.1 x 10 ¹²
Heat / hydrolytic stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	partiall y blackene d	no change	partially blackened	no change	partially blackened
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		3.1 x 10 ¹²	7.9 x 10 ¹⁰	1.1 x 10 ¹¹	1.0 x 10 ¹⁰	4.6 x 10 ¹¹	1.5 x 10 ¹⁰
	Total acid value (mgKOH/g)		0.63	0.86	0.51	0.78	0.55	0.79
Lubricity test	Wear width (μm)		390	350	380	300	410	290
	Wear depth (μm)		2.6	1.4	2.2	1.2	2.5	1.1

(Table 6)

			Comp. Example 15	Comp. Example 16	Comp. Example 17	Comp. Example 18	Comp. Example 19	Comp. Example 20
Base oil			Base oil 31	Base oil 32	Base oil 33	Base oil 34	Base oil 35	Base oil 36
Additive	Type	-	-	-	-	-	-	
	Content (% by mass)	-	-	-	-	-	-	
Kinematic viscosity (mm ² /s)	40° C	29.5	29.3	10.9	10.8	12.7	12.8	
	100° C	4.7	4.7	2.6	2.6	2.7	2.7	
Total acid value (mgKOH/g)			0.01	0.01	0.00	0.00	0.00	0.00
Miscibility			miscible	miscible	miscible	miscible	miscibl e	miscible
Volume resistivity (Ω·cm)			6.3 x 10 ¹²	6.3 x 10 ¹³	7.0 x 10 ¹²	7.8 x 10 ¹²	2.9 x 10 ¹³	3.5 x 10 ¹³
Heat / hydrolytic stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearanc e of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	partiall y blackene d	no change	partiall y blackene d	no change	partiall y blackene d
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		3.8 x 10 ¹¹	7.5 x 10 ¹⁰	1.1 x 10 ¹²	1.6 x 10 ¹⁰	4.9 x 10 ¹²	8.7 x 10 ¹⁰
	Total acid value (mgKOH/g)		0.64	0.85	0.81	1.12	0.29	0.87
Lubricity test	Wear width (µm)		375	260	365	265	390	285
	Wear depth (µm)		2.1	0.8	1.9	0.9	2.3	1.0

(Table 7)

			Comp. Example 21	Comp. Example 22	Comp. Example 23	Comp. Example 24	Comp. Example 25	Comp. Example 26
Base oil			Base oil 37	Base oil 38	Base oil 39	Base oil 40	Base oil 41	Base oil 42
Additive	Type		-	-	-	-	-	-
	Content (% by mass)		-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C		12.6	12.6	12.5	12.5	10.3	10.2
	100° C		2.7	2.7	2.8	2.8	2.5	2.5
Total acid value (mgKOH/g)			0.00	0.00	0.00	0.00	0.00	0.00
Miscibility			miscible	miscible	miscibl e	miscible	miscible	miscible
Volume resistivity (Ω·cm)			2.8 x 10 ¹³	3.9 x 10 ¹³	3.5 x 10 ¹³	3.7 x 10 ¹³	1.0 x 10 ¹²	2.1 x 10 ¹²
Heat / hydrolyti c stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	partiall y blackene d	no change	partially blackened	no change	partially blackened
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		4.5 x 10 ¹²	1.1 x 10 ¹¹	6.7 x 10 ¹²	8.4 x 10 ¹⁰	5.5 x 10 ¹¹	9.4 x 10 ⁹
	Total acid value (mgKOH/g)		0.39	0.76	0.53	0.93	0.90	1.35
	Lubricity test	Wear width (μm)		405	290	410	310	370
Wear depth (μm)		2.7	1.1	2.5	1.1	2.1	0.9	

(Table 8)

			Comp. Example 27	Comp. Example 28	Comp. Example 29	Comp. Example 30	Comp. Example 31	Comp. Example 32
Base oil			Base oil 43	Base oil 44	Base oil 45	Base oil 46	Base oil 47	Base oil 48
Additive	Type		-	-	-	-	-	-
	Content (% by mass)		-	-	-	-	-	-
Kinematic viscosity (mm ² /s)	40° C		12.8	12.7	15.3	15.4	11.9	11.8
	100° C		2.7	2.7	3.0	3.1	2.7	2.7
Total acid value (mgKOH/g)			0.00	0.00	0.00	0.00	0.00	0.00
Miscibility			miscible	miscible	miscibl e	miscible	miscible	miscible
Volume resistivity (Ω·cm)			1.0 x 10 ¹²	1.5 x 10 ¹²	9.9 x 10 ¹²	2.3 x 10 ¹³	1.8 x 10 ¹³	3.4 x 10 ¹³
Heat / hydrolytic stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	partiall y blackene d	no change	partially blackened	no change	partially blackened
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		4.2 x 10 ¹¹	4.7 x 10 ¹⁰	1.8 x 10 ¹²	1.6 x 10 ¹¹	3.6 x 10 ¹²	1.2 x 10 ¹¹
	Total acid value (mgKOH/g)		0.32	0.84	0.45	0.78	0.69	1.15
Lubricity test	Wear width (μm)		405	300	395	310	410	265
	Wear depth (μm)		2.8	1.0	2.4	1.3	2.8	0.8

(Table 9)

			Example 17	Example 18	Example 19	Example 20	Example 21	Example 22
Base oil			Base oil 1	Base oil 2	Base oil 3	Base oil 4	Base oil 5	Base oil 6
Additive	Type		Additive 1	Additive 1	Additive 2	Additive 2	Additive 3	Additive 2
	Content (% by mass)		0.2	0.2	0.2	0.2	0.2	0.2
Kinematic viscosity (mm ² /s)	40° C		12.3	18.2	28.5	25.6	29.5	12.7
	100° C		2.8	3.5	4.7	4.5	4.7	2.8
Total acid value (mgKOH/g)			0.01	0.01	0.01	0.01	0.01	0.01
Miscibility			miscible	miscible	miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)			3.3 × 10 ¹³	4.9 × 10 ¹³	8.1 × 10 ¹³	7.9 × 10 ¹³	9.2 × 10 ¹²	3.5 × 10 ¹²
Heat / hydrolytic stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearanc e of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change	no change
			no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		1.0 × 10 ¹³	1.1 × 10 ¹³	5.2 × 10 ¹³	6.7 × 10 ¹³	6.3 × 10 ¹²	6.8 × 10 ¹¹
	Total acid value (mgKOH/g)		0.47	0.32	0.19	0.25	0.21	0.18
Heat / hydrolytic stability II	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearanc e of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		8.7 × 10 ¹²	8.3 × 10 ¹²	3.2 × 10 ¹³	4.3 × 10 ¹³	5.3 × 10 ¹²	8.7 × 10 ¹²
	Total acid value (mgKOH/g)		0.97	0.82	0.34	0.38	0.29	0.41

(Table 10)

			Example 23	Example 24	Example 25	Example 26	Example 27	Example 28
Base oil			Base oil 7	Base oil 8	Base oil 9	Base oil 10	Base oil 11	Base oil 12
Additive	Type		Additive 2	Additive 3	Additive 1	Additive 2	Additive 2	Additive 2
	Content (% by mass)		0.2	0.2	0.2	0.2	0.2	0.2
Kinematic viscosity (mm ² /s)	40° C		16.5	29.5	10.8	12.7	12.7	12.6
	100° C		3.3	4.7	2.6	2.7	2.7	2.8
Total acid value (mgKOH/g)			0.01	0.01	0.00	0.00	0.00	0.00
Miscibility			miscible	miscible	miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)			2.2 x 10 ¹³	3.2 x 10 ¹³	7.5 x 10 ¹²	3.2 x 10 ¹³	3.7 x 10 ¹³	3.6 x 10 ¹³
Heat / hydrolyti c stability I	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		7.9 x 10 ¹²	4.2 x 10 ¹²	4.6 x 10 ¹²	7.8 x 10 ¹²	9.4 x 10 ¹²	8.6 x 10 ¹²
	Total acid value (mgKOH/g)		0.29	0.31	0.43	0.12	0.15	0.22
Heat / hydrolyti c stability II	Appearance of sample oil		no change	no change	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change	no change	no change	no change
		Fe	no change	no change	no change	no change	no change	no change
		Al	no change	no change	no change	no change	no change	no change
	Volume resistivity (Ω·cm)		4.7 x 10 ¹²	4.6 x 10 ¹²	2.1 x 10 ¹²	8.3 x 10 ¹²	7.9 x 10 ¹²	9.2 x 10 ¹²
	Total acid value (mgKOH/g)		0.36	0.39	0.78	0.31	0.40	0.42

(Table 11)

		Example 29	Example 30	Example 31	Example 32
Base oil		Base oil 13	Base oil 14	Base oil 15	Base oil 16
Additive	Type	Additive 1	Additive 3	Additive 3	Additive 3
	Content (% by mass)	0.2	0.2	0.2	0.2
Kinematic viscosity (mm ² /s)	40° C	10.3	12.9	15.2	11.7
	100° C	2.5	2.7	3.0	2.6
Total acid value (mgKOH/g)		0.00	0.00	0.00	0.00
Miscibility		miscible	miscible	miscible	miscible
Volume resistivity (Ω·cm)		1.9 x 10 ¹²	1.2 x 10 ¹²	1.9 x 10 ¹³	2.6 x 10 ¹³
Heat / hydrolytic stability I	Appearance of sample oil	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change
		Fe	no change	no change	no change
		Al	no change	no change	no change
	Volume resistivity (Ω·cm)	8.4 x 10 ¹¹	8.5 x 10 ¹¹	5.9 x 10 ¹²	7.3 x 10 ¹²
	Total acid value (mgKOH/g)	0.61	0.11	0.09	0.29
Heat / hydrolytic stability II	Appearance of sample oil	no change	no change	no change	no change
	Appearance of catalyst	Cu	no change	no change	no change
		Fe	no change	no change	no change
		Al	no change	no change	no change
	Volume resistivity (Ω·cm)	8.9 x 10 ¹¹	6.9 x 10 ¹¹	7.9 x 10 ¹²	9.3 x 10 ¹²
	Total acid value (mgKOH/g)	0.83	0.38	0.42	0.36

As shown in Tables 1 to 11, all of the sample oils of Examples 1 to 32 representing refrigerator machine oil compositions of the invention exhibited sufficiently low viscosity and satisfactory balance
5 between refrigerant miscibility, electric insulating property, heat and hydrolytic stability and lubricity, thus confirming their usefulness for providing high efficiency to refrigeration systems. Of the sample oils, those of Examples 17 to 32 using epoxy compounds
10 (additives 1-3) exhibited very excellent heat and hydrolytic stability.

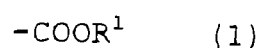
In contrast, the sample oils of Comparative Examples 1 to 32 were inadequate in any aspect including the refrigerant miscibility, electric
15 insulating property, heat and hydrolytic stability and lubricity.

Industrial Applicability

As explained above, the present invention can be used together with HFC refrigerants and natural
20 refrigerants such as carbon dioxide and hydrocarbons, to give a refrigerant machine oil composition with excellent lubricity, miscibility with refrigerants, heat and hydrolytic stability and electric insulating property, which can also provide high efficiency to
25 refrigeration systems.

CLAIMS

1. A refrigerating machine oil composition comprising an alicyclic dicarboxylic acid ester compound containing an alicyclic ring and two ester groups represented by the following general formula (1):



where R^1 represents a hydrocarbon group of 1-30 carbons,

said two ester groups bonded to mutually adjacent carbon atoms on the alicyclic ring,

wherein the molar ratio of cis-forms and trans-forms for the orientation of said two ester groups of said alicyclic dicarboxylic acid ester compound is from 20/80 to 80/20.

2. A refrigerating machine oil composition according to claim 1, wherein the molar ratio of cis-forms and trans-forms for the orientation of said two ester groups of said alicyclic dicarboxylic acid ester compound is from 25/75 to 75/25.

3. A refrigerating machine oil composition according to claim 1, wherein the molar ratio of cis-forms and trans-forms for the orientation of said two ester groups of said alicyclic dicarboxylic acid ester compound is from 30/70 to 70/30.

4. A refrigerating machine oil composition

according to claim 1, which further comprises at least one selected from the group consisting of phosphoric acid esters, acidic phosphoric acid esters, amine salts of acidic phosphoric acid ester, chlorinated phosphoric acid esters and phosphorous acid esters.

5 5. A refrigerating machine oil composition according to claim 1, which further comprises at least one selected from the group consisting of phenylglycidyl ether-type epoxy compounds,
10 alkylglycidyl ether-type epoxy compounds, glycidyl ester-type epoxy compounds, allyloxirane compounds, alkyloxirane compounds, alicyclic epoxy compounds, epoxidized fatty acid monoesters and epoxidized vegetable oils.

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