

HIGH POWER LASER DEVICES

Related Applications

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This application claims the benefit of U.S. Provisional Application No. 60/041,185, filed March 21, 1997, the contents of which are incorporated herein by reference.

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Background of the Invention

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Semiconductor lasers in common use today include edge-emitting diode lasers and vertical cavity surface emitting lasers (VCSELs). In an edge-emitting laser, a semiconductor gain medium, for example a quantum-well semiconductor structure, is formed on a surface of a semiconductor substrate. Cavity mirrors are formed or otherwise positioned on opposite sides of the substrate, perpendicular to the substrate surfaces, to form a resonant cavity which includes the gain medium. Electrical or optical pumping of the gain medium generates a laser beam which propagates in a direction along the plane of the substrate.

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Edge-emitting lasers are among the most common semiconductor laser devices. Available commercially as individual units and in linear bar arrays, they are used, for example, as an optical pump source for pumping solid state lasers. High power, typically greater than a few hundred milliwatts, adaptations of edge-emitting lasers commonly operate in high order spatial modes and at multiple frequencies. This prevents their use in applications which require high power laser output in a single spatial mode and/or at a single frequency. Edge emitters also have a significant degree of astigmatism and a beam aspect ratio which is generally large, making it difficult to focus the beam to a small spot, which prevents their use in those applications which require a focused output beam. Poor beam quality in edge-emitting lasers also makes frequency doubling of the laser output using nonlinear optical materials difficult and inefficient.

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In conventional VCSEL lasers, cavity mirrors are formed or otherwise positioned on opposite faces of a semiconductor gain medium grown on a semiconductor substrate. Electrical or optical pumping generates a laser beam emitted in a direction orthogonal to the plane of the substrate.

5 Conventional VCSELs find application in optical communications and optical interconnect systems. VCSEL lasers are characterized by generally low fundamental spatial mode TEM_{00} output powers, limited to about 8 milliwatts (mW) continuous wave (cw), and are further characterized by small fundamental spatial mode beam diameters, on the order of several micrometers (μm). Larger area VCSEL emitters, with beam
10 diameters on the order of 100 μm can produce output beams having a few hundred mW of cw output power. However, operation of conventional VCSELs at high power and large diameter generally carries with it the penalty of an output beam having high-order spatial modes and multiple frequencies. In an external cavity VCSEL configuration, referred to in the art as a vertical external cavity surface emitting laser (VECSEL), an
15 external reflector serves as the output coupler. External cavity VECSEL devices can provide higher fundamental spatial mode output power than VCSEL devices.

 Previous work on external cavity vertically emitting semiconductor lasers typically resulted in low output power. The work of Sandusky and Brueck, for example, produced low output power and used optical pumping to excite the semiconductor. See
20 J. V. Sandusky and S. R. J. Brueck, "A cw external cavity surface-emitting laser", Photonics Technology Letters, vol. 8 pp. 313-315, 1996. In a study by Hadley et al., an electrically excited VCSEL in an external cavity produced 2.4 mW cw and 100 mW pulsed in a fundamental spatial mode. In this case, an emitting area up to 120 μm was used. See M. A. Hadley, G. C. Wilson, K. Y. Lau and J. S. Smith, "High single-traverse mode output from external cavity surface emitting laser diodes", Applied Phys. Letters, vol. 63, pp. 1607-1609, 1993.
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 For various laser applications, a beam generated by the laser is subjected to frequency conversion or frequency doubling. This is accomplished by introducing a non-linear material, for example KTP, KTN, $KNbO_3$, and $LiNbO_3$ into the laser path.
30 The frequency of a beam incident on the non-linear material is converted to a second frequency. The non-linear materials are referred to as "doubling crystals" where the

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property of the material is such that it serves to double the frequency of a beam traversing the crystal. Efficient frequency conversion by the material generally requires a high-intensity, single mode incident beam.

Frequency doubling of semiconductor lasers has been demonstrated in the past to varying degrees of success using a doubling crystal mounted external to an edge-emitting diode laser cavity. The output beams from edge-emitting diode lasers are usually highly divergent and have significant aspect ratios as well as some degree of astigmatism which degrades the optical field intensity and phase front from that which is ideally required for efficient frequency doubling. Experiments have been carried out in which the light from a diode laser is launched into an optical waveguide fabricated in a non-linear material in order to maintain the optical field intensity over some relatively long path length. This technique is generally complicated and uses relatively low power diode lasers which have sufficient beam quality to launch the laser light into the external waveguide.

Various techniques in the past have attempted to harness beam power to enable efficient conversion. A first technique by Gunter, P. Gunter et al. "Nonlinear optical crystals for optical frequency doubling with laser diodes", Proc. of SPIE, vol. 236, pages 8-18, 1980, demonstrated low efficiency frequency doubling of diode laser radiation using potassium niobate KNbO_3 in a single-pass doubling configuration. In another technique, Koslovsky et al., Optics Letters 12, 1014, 1987, employed a single spatial mode, edge-emitting diode laser and KNbO_3 in an external ring resonator to increase the circulating power to achieve frequency conversion. The Koslovsky configuration required frequency-locking of the single-frequency laser to the Fabry-Perot resonance of the ring cavity as well as matching the temperature of the non-linear crystal to both frequencies. This required complicated crystal alignment and wavelength control circuitry to maintain frequency locking.

Summary of the Invention

The present invention is directed to an apparatus and method for generating high power laser radiation in a single fundamental spatial mode, in a manner which overcomes the aforementioned limitations. The laser of the present invention, when configured in an external cavity, is especially amenable to frequency conversion of the

output beam, as it provides beam power densities over suitable path lengths for efficient frequency conversion.

In a first embodiment of the present invention, the apparatus comprises a resonant cavity defined between first and second partial reflectors. The geometry of the resonant cavity defines a fundamental spatial or transverse cavity mode. A gain medium is disposed within the resonant cavity, and an energy source energizes the gain medium within a first volume. This causes spontaneous and stimulated energy emission to propagate in the gain medium in a direction transverse to the fundamental cavity mode. The transverse emission, in turn, optically pumps a second volume of the gain medium about the first volume. When the intensity of the spontaneous emission is sufficiently high, inversion and gain are produced in the second volume. The energy within the first and second volumes is coupled into the fundamental cavity mode laser beam.

By optimizing the geometry of the cavity such that the fundamental cavity mode is coupled to both the first and second volumes, the energy of the first volume transversely-directed into the second volume, which would otherwise be wasted, is instead captured by the fundamental beam, improving the overall power efficiency of the laser. To effect this, in a preferred embodiment, the cavity mirrors are selected to match the fundamental cavity mode to the cross-sectional diameter of the second volume. In this manner, the laser energy in the fundamental spatial mode is efficiently extracted from both first and second volumes of the gain medium. Similar results apply where the output energy is in a higher order spatial mode.

In a preferred embodiment, the first volume is substantially cylindrical and of cross sectional diameter D_1 , and the second volume is substantially an annulus of outer cross-sectional diameter D_2 and inner cross-sectional diameter D_1 , the first and second volumes being substantially cross-sectionally concentric.

The gain medium is preferably formed of a semiconductor material in a vertical cavity configuration. Alternatively, the gain medium may be formed of a solid state material having an active ion which has absorption in the spectral region of the gain transition. Examples of such solid state materials include Er:glass, Yb:glass, and Yb:YAG. In the case of solid state materials, pump energy would be preferably generated by optical means, for example a diode laser.

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A nonlinear crystal may be placed in the optical cavity or external to the laser to change the laser output frequency. Suitable materials for nonlinear conversion include KTP, KTN, KNbO₃, and LiNbO₃ and periodically-poled materials such as periodically-poled LiNbO₃.

5 A preferred embodiment of the present invention, described in detail below, is capable of generating intracavity circulating power levels in excess of 100 kW in a fundamental spatial mode for a 1 mm diameter beam. These levels are sufficient for producing harmonic conversion of the fundamental radiation in a non-linear material. As an example, frequency doubling in a semiconductor configuration using GaInAs gain
10 media provides a fundamental wavelength of 900 nm to 1100 nm and a frequency doubled output in the blue to green wavelengths.

Brief Description of the Drawings

15 The foregoing and other objects, features and advantages of the invention will be apparent from the more particular description of preferred embodiments of the invention, as illustrated in the accompanying drawings in which like reference characters refer to the same parts throughout the different views. The drawings are not necessarily to scale, emphasis instead being placed upon illustrating the principles of the invention.

20 FIG. 1 is a perspective view of a VECSEL laser configuration in accordance with the present invention.

FIG. 2 is a cutaway side view of the configuration of FIG. 1 illustrating transverse propagation of spontaneous and stimulated emission from the first pumped volume into the second annular volume in accordance with the present invention.

25 FIG. 3 is a perspective view of a VCSEL laser configuration illustrating the relationship of the first pumped volume and the second annular volume in accordance with the present invention.

FIG. 4 is a perspective illustration of an optical amplifier configuration in accordance with the present invention.

30 FIG. 5 is a side view of a coupling configuration for coupling output energy into a fiber-optic.

Detailed Description of Preferred Embodiments

FIG. 1 is a perspective view of a preferred embodiment of the present invention, in a VECSEL configuration. The laser of FIG. 1 includes a semiconductor substrate 20, upon a first face of which is formed a semiconductor quantum-well gain region 22. A first reflector 26, for example a p-Bragg reflector, is formed on the quantum-well region 22. A second external reflector 30 is positioned opposite the first reflector 26. The distance between the first and second reflectors 26, 30 and their respective curvatures define a fundamental cavity mode 60. The second reflector 30 is illustrated as an external cavity mirror in FIG. 1 in accordance with a VECSEL configuration; however, the second reflector 30 may alternatively be layered directly adjacent the second face of the substrate to provide a VCSEL configuration. Note that for purposes of the present invention, the term "reflector" as used herein includes partially and/or fully reflective materials and/or surfaces. The surface 42 of the substrate 20 facing the second reflector 30 preferably is treated with an anti-reflection coating 42, such that any beam energy 60 traversing that interface will pass with minimal reflection, a desirable feature as is well known in the prior art.

As shown in the cross-sectional illustration of FIG. 2, the resonant cavity is pumped electrically through an annular electrical contact 28, causing current 38 to flow between annular contact 28 and circular contact 40 on opposite faces of the substrate 20. The resulting current flow 38 is generally conical in shape, the base 39A of the cone being at the annular contact 28 and the peak of the cone 39B being near contact 40. The flow in the peak 39B is generally circular in cross section and energizes a first substantially cylindrical volume 44 of the gain region 22, the first volume 44 being of a cross-sectional diameter D_1 . The diameter D_1 is preferably substantially greater than the thickness of the gain region 22.

The excited gain region 22 of diameter D_1 generates stimulated and spontaneous emission, represented by arrows 48, which travels in a direction transverse to the propagation of the cavity laser beam. In standard prior-art VCSEL or VECSEL lasers, such energy would escape out the sides of the device or would otherwise be wasted as energy not contributing to the output beam 32. In the configuration of the present invention, this transverse energy 48 is absorbed in a second annular volume 46

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surrounding the first pumped volume. This absorbed energy serves to pump the second volume 46, providing gain and therefore power into the fundamental laser mode 60.

When the electrical or optical pumping of the first region D_1 produces gain, this gain occurs for both the transverse and longitudinal directions. Since the traverse gain length is larger than the longitudinal gain length, more stimulated emission can occur in that direction. The larger the dimension D_1 , the greater the net gain for stimulated emission in the transverse direction. Higher output power requires larger area devices because of thermal dissipation and the limit set by catastrophic degradation by the optical power density on the surface of the semiconductor in the longitudinal direction. For such large area devices, significant power can be lost by the occurrence of the transverse stimulated emission thereby reducing the overall power conversion efficiency.

Spontaneous emission also occurs but becomes less important for the larger area devices. If the adjacent region is designed to absorb the stimulated emission (and also to a lesser extent the spontaneous emission), then the energy that otherwise would have been lost can be used to optically pump the second region D_2 to the extent that it will produce gain. The energy pumped into the second region D_2 can be extracted in the orthogonal direction by adjusting the external mirror 30 to produce a mode waist equal to D_2 on the gain medium. The external cavity mirror 30 will fix or "clamp" the gain in the total area defined by D_1 and D_2 . There is a limit to the extent of the second region D_2 , as the degree of transverse pumping decreases with decreasing intensity away from the center of the pumped region. This limit is related to the dimension D_1 and the pumping intensity (electrical or optical) in the area defined by D_1 .

Given the mode waist diameter D_2 , the technique for designing a cavity which would provide a suitable radius of curvature R for the second reflector 30 and the suitable optical cavity length L is well known in the art. See, for example, Herwig Kogelnik and Tingye Lee, "Beams, Modes, and Resonators", CRC Handbook of Lasers, CRC Press, 1971, pg. 421-441. The second diameter D_2 is a function of the excitation level and the diameter D_1 . The design would be optimized for maximum output power limited by the circulating power density, which is limited by catastrophic degradation of the semiconductor, and the thermal power dissipation from the second diameter D_2 . The

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mode waist diameter for the cavity could be matched, for example, by adjusting the cavity length L for a fixed radius of curvature R for the second reflector 30.

FIG. 3 is a perspective view of a laser in a VSCEL configuration in accordance with the present invention illustrating the relationship of the first pumped volume 44 and the second output volume 46. The pumped first volume 44 is of diameter D_1 in the region of the gain medium 22. The transverse propagation of spontaneous and stimulated emission represented by arrows 48 optically pumps or otherwise energizes an annular volume 46 characterizing a second volume 46 surrounding the first volume 44. The annular volume 46 has an inner diameter of D_1 and an outer diameter of D_2 and is substantially cross-sectionally concentric with the first volume 44 assuming a Gaussian beam distribution. The fundamental cavity mode is optimized to have a diameter approximately equal to the outer diameter D_2 of the second volume 46, such that energy in both first and second volumes is captured and therefore contributes to the output beam 32. Excitation of the first volume 44, may occur by electrical or optical means.

The laser cavity parameters are preferably adjusted to set the mode waist substantially equal to the diameter D_2 at the maximum operating power levels. In a laser cavity comprising a single flat mirror 26 and a single concave spherical mirror 30 having a radius of curvature R as shown in FIG. 2, the mode beam diameter on the laser chip w_1 and at the output mirror w_2 is characterized by:

$$w_1^2 = 4\lambda L / \pi [(R - L)/L]^{1/2} \quad (1)$$

$$w_2^2 = 4\lambda L / \pi [L/(R - L)]^{1/2} \quad (2)$$

where L is the cavity length and λ is the wavelength of the output laser beam 32 as described in Kogelnik et al. cited above. It is clear from these equations that the diameter of the fundamental laser mode can be made equal to the outer diameter D_2 of the second volume 46, for example by adjusting the cavity length L for a specific radius of curvature R . Alternatively, the radius of curvature R may be selected for a specific range of cavity lengths L . Instead of curved mirrors, a flat output coupler 30 may be

employed with a lens in the cavity, of appropriate geometry to achieve the same results. A physical lens or thermal lens may be used for this purpose.

A preferred embodiment of a semiconductor laser device may comprise a multiple-element quantum-well structure or a single gain region having a total gain thickness equivalent to that of a multiple-quantum well-structure. In order to achieve sufficient single pass gain, a 900 nanometer (nm) to 1100 nm wavelength laser structure formed in a semiconductor material such as GaInAs preferably has at least five quantum wells or an equivalent thickness. For more efficient operation, at least ten quantum wells are used in order to effectively overcome the optical losses due to free carrier absorption at the laser wavelength in the conductive substrate layer 20. A typical thickness for a single quantum well is approximately 8 nm. Note that the optical bandgap is dependent on the thickness of the quantum well and therefore an equivalent thickness for a single layer of gain material would have its wavelength somewhat shifted from the same compositional structure for the narrow quantum well material. The total thickness or the number of quantum wells can be increased to increase the gain to overcome all intracavity losses for efficient operation. This is limited only by the ability to uniformly grow such structures and by the practical threshold current density for such structures. Conventional VCSELs typically operate with only one or a few quantum wells between very high reflectivity mirrors. Such devices exhibit low optical gain and therefore would not operate as efficiently as the apparatus of the present invention.

The electrical current or optical pump energy injected into the laser device can be provided by any of the well-known methods, for example in G.P. Agarwal, "Semiconductor Lasers", The American Institute of Physics Press, pages 146-157. In a preferred embodiment of the present invention, most of the injection current 38 is directed into a circular region of a diameter equal to or less than the diameter D_1 of the fundamental spatial mode as defined by equations (1) and (2) above.

As described above, low efficiency frequency doubling of diode laser radiation using edge-emitting diode lasers has been demonstrated in the past by Gunter and Koslovsky et al. In contrast, the preferred embodiment of the present invention employs a VCSEL or VECSEL vertical cavity laser structure in which the total single pass gain is significantly lower than in edge-emitting lasers. In addition, the output from the vertical

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cavity device of the present invention is distributed over a much larger circular beam area than in edge-emitting devices, for example several hundred times greater in area. The achievable intracavity circulating power density in a fundamental circular spatial mode can exceed several MW/cm², limited only by catastrophic degradation at the semiconductor surface. While similar power densities can be achieved in edge-emitting lasers, the beam is confined to the waveguide of the diode cavity which makes frequency doubling difficult. Since the efficiency of frequency conversion is dependent on both the optical intensity and the length of the interaction region, frequency doubling of diode lasers is complicated and has been carried out in waveguide structures to maintain the field intensity of a sufficient interaction distance. A high conversion efficiency can be achieved in the present invention since high optical field intensities can be maintained over a sufficiently long interaction length because the beam is substantially non-divergent within the optical laser cavity. A high quality beam provides a more favorable frequency conversion situation for any conversion configuration outside of the cavity such as in the recently-studied periodically-poled nonlinear materials. Furthermore, the present invention can be operated in a pulsed, gain-switched, or mode-locked configuration to increase the optical power and therefore the nonlinear conversion efficiency. The present invention applies not only to harmonic frequency conversion, but also to sum and difference frequency generation. In a preferred embodiment, the non-linear material includes Fabry-Perot resonances such that the laser operates in a single frequency. An exemplary configuration is illustrated in FIG. 2, which includes an intracavity non-linear crystal 58 between the substrate 20 and external mirror 30.

Each prior art configuration mentioned above, for example the Sandusky et al. and Hadley et al. configuration, was limited by matching the cavity geometry to the extent of the pumped volume only, unlike the present invention which extracts energy from the first pumped volume in addition to the second volume energized by transverse energy emission generated in the first volume.

The output power in the present invention can be magnified by increasing the diameter of the mode volume, as described above. Peak output power levels, for example in excess of 10 kW, can be generated from a gain area of one millimeter in

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diameter. Continuous cw output power levels may exceed 10 Watts from a single element device, limited only by thermal considerations.

A second harmonic radiation which propagates in the backward direction can additionally be absorbed in a semiconductor laser structure in such a way as to produce electrons and holes which migrate to the active gain region, thereby increasing the power of the fundamental laser radiation. This also has the effect of increasing efficiency of the second harmonic output as well as producing a single-ended output of harmonic radiation. In an alternative embodiment, a three-mirror cavity could be used in which the nonlinear material is disposed in a position in which the harmonic radiation does not reflect back into the gain medium but exits through the middle mirror. A ring resonator configuration may also be employed.

Typical frequency doubling materials appropriate for conversion of infrared wavelengths into the visible include periodically-poled LiNbO₃, KTP, and KNbO₃. For example KTP can be phase matched to convert 1 μ m radiation into green wavelengths and KNbO₃ can convert infrared radiation into blue wavelengths using GaInAs diode lasers operating in the 900 nm wavelength range.

Many configurations for intracavity frequency doubling that are well known in the field can be used in the present invention. For example, a focusing lens can be positioned within the laser resonator defined by the mirrors 24 and 30 to increase the power density. The technique would allow use of very short lengths of nonlinear materials or nonlinear materials with lower nonlinear figures-of-merit.

For doubling materials such as KTP and KNbO₃, active crystal lengths can be significantly less than 1 cm for the circulating power levels possible in the present configurations. Shorter nonlinear material lengths provide wider temperature and wavelength phase matching conditions. For KNbO₃ for example, a crystal length of 1 mm or less can provide a temperature phase matching bandwidth of more than several degrees Celsius and a wavelength bandwidth of several nanometers. Such broad acceptance ranges make the manufacture and operation of such devices significantly more practical. The wavelength may be controlled by the selection of the alloy composition of the gain medium material, while precision wavelength control is

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achievable with intracavity etalons or other wavelength controlling techniques well known in the art. Similar results apply to other non-linear materials, including KTP.

The semiconductor gain region 22 preferably comprises a multiple-element quantum well structure. Alternatively, a single gain region whose total gain thickness is equal to that of the multiple quantum well structure may be employed. In order to achieve sufficient single pass gain, the number of quantum wells typical for a 900 nm to 1100 nm wavelength laser structure made from GaInAs should be more than 5 with a typical range of between 10 and 25 wells. For a high-peak-power device operating under pulsed conditions using either electrical or optical excitation, the number of wells may be more than 50. The limit is governed by the practical ability to grow large numbers of strain-free quantum well layers. In this case, a heterostructure may be a more effective choice. High-peak-power devices could be made, for example, by using high-power Q-switched solid state lasers as pump sources.

Conventional vertical cavity semiconductor lasers typically operate with only one or a few quantum wells and very-high-reflectivity cavity mirrors. Such devices may not operate as efficiently in the present invention because of inherently low optical gain. The net gain must be sufficient to overcome losses in the external cavity including the free carrier loss in the substrate material 22 and the optical losses in the nonlinear material and associated anti-reflection coating on the intracavity optical elements.

FIG. 2 illustrates a typical quantum-well device 22 formed on a semiconductor substrate 20. A highly reflective mirror 26 is grown on the back surface of the device to provide one of the mirrors of the laser resonator. The top cladding layer serves as a conductive contact which can be antireflection coated 42 and which has low optical absorption at the laser wavelength. In an alternative embodiment, a layer of electrically-conductive material with an optical bandgap greater than the second harmonic radiation serves as the conductive layer with a second layer, of thickness less than the diffusion length of carriers, transparent to the fundamental laser radiation and absorbing the second harmonic radiation grown between the active material and the thick wide-bandgap material, would allow the optically excited carriers to diffuse into the gain region. The thick conductive material may comprise for example, deposited tin oxide.

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Single frequency operation may be achieved, for example, by introducing an etalon in the cavity. Alternatively, the non-linear crystal 58 may also serve as a frequency selective element.

5 The ability to generate visible wavelengths in high-power output makes the present invention attractive to a range of applications including projection display, optical disc read and write, optical holographic memory storage, and bio-fluorescence sensors. For the case of projection display, three primary colors could be generated. For example, the blue wavelength and green wavelength could be produced by frequency doubling the output of GaInAs semiconductor lasers whose outputs could be selected in the
10 wavelength range from 900 nm to more than 1100 nm. Appropriate frequency doubling materials include KTP for the green wavelength and KNbO₃ for the blue wavelength. Power may be scaled using arrays of such devices. Output power levels of several tens of Watts may be generated. Since the output from such an array would lack coherence between elements of the array, the effects of speckle would be significantly reduced so as
15 not to affect the quality of the projected image in the display system. In the case of an array device, the output couplers may comprise an array of lithographically-produced binary optical mirrors or micromirrors whose positions are precisely aligned with the center of the diode laser emitting areas.

20 A projection display system employing the present invention could be operated using various light valve devices such as liquid crystal spatial light modulators, micro-mirrors such as those sold by Texas Instruments, and grating deflector light valves such as those developed by Silicon Light Machines of Sunnyvale, California. For an array of laser sources, all elements of the light valve could be illuminated by every laser source by
25 allowing the individual laser beams to expand so they overlap in the far field. In this way, the failure of one element would not significantly degrade the operation of the system. Binary optical lenses may be used to focus the laser light in a top-hat distribution onto each pixel of the light valve to make efficient use of all available laser radiation.

30 While this invention has been particularly shown and described with references to preferred embodiments thereof, it will be understood by those skilled in the art that

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various changes in form and details may be made therein without departing from the spirit and scope of the invention as defined by the appended claims.

As an example of an alternative embodiment, FIG. 4 is a perspective illustration of the present invention configured as an optical amplifier 70. As in the laser configuration, the optical amplifier 70 configuration includes a semiconductor substrate 20, a semiconductor gain medium 22, and a first reflector 26. Note that a second reflector is not required as the optical amplifier 70 does not include a resonant cavity. A first volume 44 of the gain medium 22 is pumped with electrical or optical energy 56. The first volume 44 is generally cross-sectionally circular, having a diameter D_1 . As described above, this causes transverse stimulated and spontaneous propagation of energy 48 into a second volume 46 about the first volume 44. In a preferred embodiment, the second volume 46 is substantially circular in cross-section, the diameter being D_2 . An incident beam 50 of diameter D_2 and of a first amplitude is directed at the pumped region 46, overlapping with and being energized by both the first volume 44 and second volume 46. The incident beam 50 reflects at mirror 26 and is released as an output beam 52 of similar diameter D_2 . The output beam 52 is amplified by the energized gain region 46 and is therefore of higher intensity than the incident beam 50. A plurality of such gain elements may be used to increase the total gain of the system.

A second alternative embodiment is illustrated in FIG. 5, representative of a side view of an optical coupling configuration. A single mirror/lens element 70 includes a first concave face 72 which operates as a resonator mirror for VECSEL laser 78, and a second convex face 74 which operates as a focusing element for directing laser radiation 32 into fiber-optic 76. The fiber-optic 76 may comprise single-mode or multi-mode fiber, and is positioned at the focus of the laser radiation 32 such that the laser energy is directed substantially within the numerical aperture of the fiber. The reflectivity of the first surface 72 is optimized to maximize output power from the laser device 78, while the second surface 74 and the input surface 75 of fiber optic 76 are anti-reflection coated at the laser wavelength to minimize reflectivity.

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During assembly, the mirror/lens element 70 is aligned and positioned to maximize laser output power coupling, and is fixed using well-known techniques, including soldering, epoxying and/or laser welding. The fiber is then positioned to accept the focused radiation 32 and is set accordingly by any of the above techniques.

- 5 This embodiment offers the advantage of a reduction of the number of optical elements required to focus energy into a fiber by incorporating the function of a cavity mirror and an output lens into a single element.



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Claims

I claim:

1. A laser comprising:

5 a resonant cavity between first and second reflectors, said resonant cavity defining a fundamental cavity mode;

a gain medium disposed within said resonant cavity; and

an energy source for energizing said gain medium within a first volume, said energy source causing optical energy emission to propagate in said gain medium in a direction substantially transverse to said fundamental cavity mode, said

10 transverse energy emission optically pumping a second volume of said gain medium about said first volume, said energy within said first and second volumes being coupled into said fundamental cavity mode.

15 2. The laser of Claim 1 wherein said first volume is substantially cylindrical and of cross-sectional diameter D_1 and said second volume is substantially an annulus of outer cross-sectional diameter D_2 and inner cross-sectional diameter D_1 , said first and second volumes being substantially cross-sectionally concentric.

20 3. The laser of Claim 1 wherein the gain medium comprises a material selected from the group consisting of semiconductor, multiple-quantum-well semiconductor and solid state.

25 4. The laser of Claim 1 wherein the energy source energizes the gain medium with electrically pumped current.

5. The laser of Claim 1 wherein the energy source energizes the gain medium by optical excitation.

30 6. The laser of Claim 1 further comprising an annular electrode and a circular electrode disposed on opposite sides of the gain medium which, when energized, pump a first cylindrical volume of the laser.

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7. The laser of Claim 1 further comprising a non-linear material disposed in the path of the laser beam for adjusting the frequency of the beam.
8. The laser of Claim 7 wherein the non-linear material is disposed within the laser cavity.
9. The laser of Claim 7 wherein the non-linear material is disposed external to the laser cavity.
10. The laser of Claim 7 wherein the non-linear material is selected from the group consisting of KTP, LiNbO₃, periodically-poled LiNbO₃, KTN, and KNbO₃.
11. The laser of Claim 7 wherein the non-linear material includes Fabry-Perot resonances such that the laser operates in a single frequency.
12. The laser of Claim 1 further comprising an intracavity tuning element selected from the group consisting of an etalon, a birefringent element, a prism, and a grating.
13. The laser of Claim 1 further comprising a conductive material transparent to the fundamental wavelength and absorbent of second harmonic radiation grown adjacent to the gain region such that second harmonic light is absorbed in said conductive material and electrons and holes diffuse into the gain region to increase the efficiency of second harmonic radiation emitted in a forward direction.
14. The laser of Claim 1 operated in a pulsed or mode-locked configuration.
15. Multiple lasers of Claim 1 configured as an array of addressable elements.

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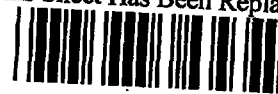




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16. The laser of Claim 1 further comprising an optic element having a first reflective surface and a second transmissive surface, said first surface operating as said first cavity reflector, said second transmissive surface for focusing energy output from said element.
17. The laser of Claim 16 wherein the first reflective surface is concave, and wherein the second reflective surface is convex.
18. The laser of Claim 16 further comprising a fiber-optic having an input surface aligned to receive said focused energy output.
19. An optical device comprising:
a semiconductor substrate;
a semiconductor gain medium on a first face of said substrate; and
an energy source for energizing said gain medium within a first volume, said energy source causing optical energy emission to propagate in said gain medium in a direction substantially transverse to said first volume, said transverse emission optically pumping a second volume of said gain medium about said first volume, such that an input beam of a width approximately equivalent to the cross-sectional width of said second volume and directed at said second volume is amplified by energy in said first and said second volumes.

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20. A laser comprising:

a semiconductor substrate;

a semiconductor gain medium on said substrate;

first and second reflectors defining a resonant cavity including said substrate

and said gain medium, said resonant cavity defining a fundamental cavity mode;
and

an energy source for energizing said gain medium within a first volume, said energy source causing optical energy emission to propagate in said gain medium in a direction substantially transverse to said fundamental cavity mode, said transverse emission optically pumping a second volume of said gain medium about said first volume, said energy within said first and second volumes being coupled into said fundamental cavity mode.

21. The laser of Claim 20 wherein said first volume is substantially cylindrical and of cross-sectional diameter D_1 and said second volume is substantially an annulus of outer cross-sectional diameter D_2 and inner cross-sectional diameter D_1 , said first and second volumes being substantially cross-sectionally concentric.

22. The laser of Claim 20 further comprising an annular electrode and a circular electrode disposed on opposite sides of the gain medium which, when energized, pump a first cylindrical volume of the laser.

23. The laser of Claim 20 further comprising a non-linear material disposed in the path of the laser beam for adjusting the frequency of the beam.

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