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SPECIFICATION



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APPARATUS FOR SPRAYING MICROPARTICLES AND SPRAYING METHOD USING
5 THE APPARATUS, AND METHOD FOR MANUFACTURING LIQUID CRYSTAL
DISPLAY

TECHNICAL FIELD

The present invention relates to a microparticle spraying
10 apparatus and to a microparticle spraying method and a method
of manufacturing a liquid crystal display device, which utilize
said apparatus.

BACKGROUND ART

15 With advances in electronics, microfine microparticles
are used in a variety of applications. Among such
microparticles are electrically conductive microparticles in
use in anisotropic films, conductive microparticles in use in
the field of bonding technology, and microparticles applied as
20 spacers in liquid crystal display devices.

As one of the applications of such microparticles, the
liquid crystal display devices have been broadly used in
personal computers and portable electronic appliances. The
liquid crystal display device generally comprises a pair of
25 substrates 1, a liquid crystal layer 7 sandwiched therebetween,
a color filter layer 4, a black matrix layer 5, a transparent
electrode layer 3, alignment layers 9, etc. as illustrated in
Fig. 12. Here, it is a spacer layer 8 that defines the interval
of two substrates 1, i.e. the proper thickness of the liquid
30 crystal layer.

In the conventional method of manufacturing a liquid
crystal display device which comprises spraying spacer
microparticles randomly and uniformly over a substrate carrying
pixel electrodes, the spacer microparticles are inevitably
35 disposed as well on the pixel electrodes, i.e. the display areas

of the liquid crystal display, as can be seen from Fig. 12, with the result that the aperture rate is substantially decreased. The spacer microparticles are generally composed of synthetic resin, glass or the like and when the spacer is disposed on pixel electrodes, light leaks occur in the spacer region owing to a depolarization effect. In addition, the orientation of liquid crystals on the spacer surface is disturbed to cause escape of light, resulting in decreases in contrast and tone to aggravate the display quality.

10 In order to overcome the above disadvantages, the spacer microparticles should be disposed exclusively in the light-shielding black matrix areas formed in the color filter layer. The black matrix layer is provided for improved contrast of display in the liquid crystal display device and, in the case
15 of a TFT liquid crystal device, for preventing the optically erratic action of the cell due to external light.

As the technology directed to disposing a spacer selectively in the black matrix areas, i.e. in the areas other than pixel electrodes of a liquid crystal display device,
20 Japanese Kokai Publication Hei-4-256925 discloses a method which comprises holding the gate electrode group and drain electrode group at the same electric potential during application of the spacer microparticles. Japanese Kokai Publication Hei-5-53121 discloses a method which comprises
25 applying a voltage to the wiring electrodes during application of the spacer microparticles. Moreover, Japanese Kokai Publication Hei-5-61052 discloses a dry microparticle spraying method which comprises applying a positive voltage to the wiring electrodes and a negative charge to the spacer microparticles.

30 However, any method as mentioned above invariably depends on the use of wiring electrodes and, therefore, are only applicable to TFT liquid crystal display devices. In STN liquid crystal display devices, there are no electrodes corresponding to said wiring electrodes but stripe electrodes are disposed
35 in orthogonal relation between the two substrates to form pixel

electrodes, with the areas corresponding to the black matrix forming the electrode gaps (spaces), with the result that the above technologies cannot be utilized.

Meanwhile, Japanese Kokai Publication Hei-4-204417
5 discloses a technology wherein the spacer is selectively disposed in the electrode-free areas by charging the electrodes on one of the insulating substrates and spraying the spacer charged to the same polarity as the electrodes over the insulating substrate and, in addition, a conductor is disposed
10 under the electrode substrate in a microparticle spraying apparatus so that a plus voltage may be applied so as to control the falling speed of the negatively charged spacer while the housing comprises a conductive material to which a minus voltage may be applied for avoiding attraction of the negatively charged
15 spacer microparticles to the apparatus wall.

However, there is some variation in the charging amount of the spacer due to the intrinsic variation of the spacer material itself, with a portion of the spacer being charged to the opposite polarity, and such reversely (positively) charged
20 spacer microparticles are disposed on the electrodes (which are negatively charged) on the insulating substrate to substantially reduce the aperture rate.

Japanese Kokai Publication Sho-63-77025 discloses a spacer spraying apparatus wherein the ceiling and bottom of the
25 apparatus are constituted as a pair of electrodes so that an electric field may be generated by applying a direct-current voltage across said ceiling and bottom and the spacer equalized to the ceiling in electric potential is sprayed. Because, with this apparatus, the spacer is caused to fall through the
30 electric field, the falling speed of the spacer can be controlled so that the spacer microparticles can be uniformly dispersed and deposited on a substrate.

However, with this spacer spraying apparatus, the falling speed of spacer microparticles can be controlled in some measure
35 by exploiting the influence of an electric field but since lines

of electric force are formed between the top and bottom electrodes, selective control of spacer falling position is difficult. Moreover, when a voltage is applied to the stripe electrode array for use as bottom electrodes, no selectivity
5 is obtained but a uniform electric field prevails because of the narrow electrode gaps in the liquid display device. Thus, it is even more difficult to dispose the spacer selectively in the electrode gaps where no pixels exist.

Japanese Kokai Publication Hei-1-187533 discloses a
10 spacer spraying apparatus wherein a spraying chamber is connected to a spacer supply tank through a pipeline and, using a gas as the vehicle, the spacer is fed from the spacer supply tank to the spraying chamber.

However, this spacer spraying apparatus is not designed
15 for selective control of spacer falling position and incapable of preventing disposition of spacer microparticles on the display areas of the liquid crystal display device.

SUMMARY OF THE INVENTION

20 The present invention has for its object to overcome the above-mentioned disadvantages and provide a microparticle spraying apparatus with which the disposition of microparticles on a substrate carrying electrodes can be accurately controlled, particularly a microparticle spraying apparatus capable of
25 selectively disposing spacer microparticles in electrode gaps where no pixels are present even on a substrate carrying an array of stripe electrodes in use for the STN liquid crystal display device, to a microparticle spraying method and a method of manufacturing a liquid crystal display device which utilize
30 said apparatus.

The first aspect of the present invention relates to a microparticle spraying apparatus for selective disposition of a charged microparticle on a substrate carrying a plurality of electrodes

35 which comprises a spraying chamber adapted to accommodate

said substrate, a microparticle supply means for supplying said microparticle into said spraying chamber and spraying it on said substrate, and a voltage application means for applying voltages to the electrodes disposed on said substrate,

5 said voltage application means being capable of applying different levels of voltages to said electrodes respectively.

The second aspect of the present invention relates to a microparticle spraying method

10 comprising applying an electric potential to a plurality of electrodes on a substrate, charging a microparticle electrostatically, and spraying and disposing said microparticle selectively on said substrate,

 wherein a microparticle spraying apparatus includes a means for eliminating an oppositely charged microparticle.

15 The third aspect of the present invention relates to a microparticle spraying method

 comprising applying an electric potential to a plurality of electrodes formed on a substrate, charging a microparticle electrostatically, selectively spraying and disposing said microparticle on the substrate,

20 wherein a charged element with an electric potential of the same polarity as said charged microparticles being applied is disposed in at least a domain of the surface extending from the nozzle orifice of a microparticle delivery nozzle duct to the periphery of said substrate.

25 The fourth aspect of the present invention relates to a microparticle spraying method

 comprising spraying plural kinds of microparticles constituted by dissimilar constituent material or surface composition from the corresponding microparticle tanks with a pressurized gas as the vehicle using a microparticle spraying apparatus,

30 wherein said microparticle spraying apparatus comprises a spraying chamber for accommodating a substrate, a microparticle supply means comprising at least one

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microparticle delivery nozzle duct and at least one microparticle tank, both for supplying a microparticle into said spraying chamber and spraying it onto said substrate, and a voltage application means for applying voltages to a plurality of electrodes formed on said substrate,

said voltage application means being capable of applying dissimilar levels of voltages to each of said electrodes.

The fifth aspect of the present invention relates to a method of manufacturing a liquid crystal display device

which comprises using the above-mentioned microparticle spraying apparatus,

disposing a spacer selectively on a substrate carrying a stripe electrode array constituted by a plurality of linear transparent electrodes arranged in parallel, and

applying a relatively high level of voltage to an even number of linear transparent electrodes arranged in parallel and a relatively low level of voltage to an even number of linear transparent electrodes neighboring said even number of linear transparent electrodes to thereby produce a region with a relatively high potential (+ (positive)) and a region with a relatively low potential (- (negative)) in an alternate pattern and, in this condition,

further spraying either a positively (+) charged spacer or a negatively (-) charged spacer onto said substrate or

further spraying a positive (+) charged spacer and a negatively (-) charged spacer alternately or in succession onto the substrate.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a schematic view showing a microparticle spraying apparatus embodying the principles of the invention.

Fig. 2 is a schematic view showing a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region as formed on a stripe electrode array as viewed from above said array.

Fig. 3 is a schematic view showing the lines of electric force formed in the region of potential difference shown in Fig. 2, as viewed from the lateral side of said stripe electrode array.

5 Fig. 4 is a schematic view showing a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region as formed on a stripe electrode array, as viewed from above said array.

10 Fig. 5 is a schematic view showing the lines of electric force formed in the region of potential difference shown in Fig. 4, as viewed from the lateral side of said stripe electrode array.

15 Fig. 6 is a schematic view showing the comb-shaped electrodes used in a microparticle spraying apparatus embodying the principles of the invention.

Fig. 7 is a schematic view showing a microparticle spraying apparatus embodying the principles of the invention.

Fig. 8 is a schematic view showing another microparticle spraying apparatus embodying the principles of the invention.

20 Fig. 9 is a schematic view showing still another microparticle spraying apparatus embodying the principles of the invention.

Fig. 10 is a sectional view showing the electrode pattern according to one embodiment of the invention.

25 Fig. 11 is a schematic view illustrating the mode of disposition of the spacer according to electric fields in the embodiment of the invention.

Fig. 12 is a schematic section view of the conventional liquid crystal display device.

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EXPLANATION OF THE NUMERIC SYMBOLS

- 1. substrate (insulating substrate)
- 2. board
- 3, 3a, 3b. transparent electrode (display electrode)
- 35 4. color filter

- 5. black matrix
- 6. over coat
- 7. liquid crystal
- 8. microparticle (spacer)
- 5 9. alignment film
- 10. spraying chamber
- 11. microparticle supply device
- 11a. microparticle delivery duct
- 11b. microparticle tank
- 10 12. voltage application means
- 13. humidity controller
- 14. vent hole
- 15. conductive stage
- 16. variable speed fan
- 15 17. piping
- 18. 18a, 18b. lead wire
- 19. charged element
- 20, 20a, 20b. conductor segments

20 DISCLOSURE OF INVENTION

The present invention is now described in detail.

The first aspect of the present invention is directed to a microparticle spraying apparatus for selective disposition of a charged microparticle on a substrate carrying a plurality
25 of electrodes which comprises a spraying chamber adapted to accommodate said substrate, a microparticle supply means for supplying said microparticle into said spraying chamber and spraying it on said substrate, and a voltage application means for applying voltages to the electrodes disposed on said
30 substrate, said voltage application means being capable of applying different levels of voltages to said electrodes respectively.

Generally speaking, when two different levels of voltage are applied to two electrodes formed on a flat surface, a
35 relatively high potential [+ (positive)] region and a

relatively low potential [- (negative)] region are formed and lines of electric force are formed by the potential difference. Thus, assuming that both of the voltages applied to the two electrodes are of the same polarity with respect to the earth potential (ground potential) as reference (0), insofar as a potential difference exists between the voltages applied to the two electrodes, one of the electrodes functions as an electrode of relatively + (positive) polarity to form a relatively high potential [+ (positive)] region, with the other electrode functioning as an electrode of relatively - (negative) polarity to form a relatively low potential [- (negative)] region. In this state, lines of electric force are formed from the electrode of relatively + (positive) polarity to the electrode of relatively negative [- (negative)] polarity. When charged microparticles are brought into the electric field in which such lines of electric force have been formed, the charged microparticles are subject to a force in the direction of the line of electric force if they are + (positively) charged or in the direction opposite to the direction of the line of electric force if they are - (negatively) charged.

The microparticle spraying apparatus according to the first aspect of the present invention achieves microparticle disposition control by applying different levels of voltages to each of said electrodes formed on a substrate to create said lines of electric force and spraying charged microparticles into the region.

The microparticle spraying apparatus according to the first aspect of the present invention comprises a spraying chamber, a microparticle supply means and a voltage application means.

The spraying chamber mentioned above is adapted to accommodate a substrate to be sprayed with microparticles and constitutes the body of the microparticle spraying apparatus of the present invention.

The spraying chamber mentioned above may comprise metal

or synthetic resin. It may be a double-walled structure comprising an inner wall and an outer wall. In setting the substrate in said spraying chamber, it is preferable to provide a distance of at least 15 cm between the periphery of said substrate and the inner wall of the spraying chamber.

The spraying chamber is preferably such that the vertical flow rate of air in said spraying chamber can be freely adjusted.

As mentioned above, the microparticle spraying apparatus of this invention achieves microparticle disposition control by forming lines of electric force over a substrate and spraying charged microparticles there. The disposition characteristic depends much on the falling speed of microparticles, for the inertia force of microparticles varies with the magnitude of falling velocity, with the result that the mode in which the locus of microparticles is curved by said lines of electric force is remarkably varied.

The falling speed of microparticles is defined by the flow rate of air within the spraying chamber and the relationship of electrostatic polarity and charging amount of the microparticles to the lines of electric force formed over the substrate, among other factors. In the present invention, it is preferable to seek accurate disposition control of microparticles by adjusting the vertical flow rate of air within said spraying chamber to thereby control the falling speed of microparticles.

The falling speed of microparticles at which the precise disposition of microparticles can be achieved is not limited to one point but there are a plurality of such points; there are the case in which the falling speed of microparticles is high and the case in which the speed is low. In the present invention, the falling speed of microparticles can be controlled to such a preferred point by adjusting the vertical flow rate of air in said spraying chamber.

The method for adjusting the vertical flow rate of air in the spraying chamber is not particularly restricted but

includes, among others; the method which comprises feeding compressed air or the like from the ceiling of the spraying chamber; the method in which a fan means is installed either above or below the substrate; and the method which comprises withdrawing air from a vent hole provided at the lower part of the spraying chamber. These kinds of methods can be used in a combination of two or more kinds. Particularly when compressed air is used, it is preferable to withdraw the air for creating a stream of air.

Fig. 8 shows an example of said spraying chamber in which a fan is disposed below the substrate. By means of the fan, the vertical flow rate of air in the spraying chamber can be adjusted. When a fan is installed in the spraying chamber, it is preferable to provide the ceiling of the spraying chamber with apertures or use a mesh-like ceiling material so that a more uniform air stream may be created (Because of such a stream of air, the microparticles are prevented from migrating out of the spraying chamber).

Furthermore, said spraying chamber is preferably provided with a discharge port which can be opened and closed. Since the superfluous microparticles in the spraying chamber can then be withdrawn from the discharge port, the microparticle disposition accuracy can be further improved and, moreover, when the substrate carrying the microparticles disposed is withdrawn from the spraying chamber, scattering of the microparticles can be prevented.

The microparticle spraying apparatus according to the first aspect of the present invention accomplishes microparticle disposition control by bending the falling path of microparticles under the influence of lines of electric force formed over the substrate but if said discharge port is opened during the spraying of microparticles, the falling speed of microparticles is increased to thereby increase inertia force, so that the microparticles reach the substrate before their path is altered, thus detracting from disposition accuracy.

Therefore, it is preferable to arrange so that the discharge port will be kept closed during the spraying of microparticles and opened after completion of spraying.

5 The opening and closing of said discharge port can be timer-controlled, for instance.

The discharge port mentioned above is preferably located at a level above the substrate set in the spraying chamber. If said discharge port is located at a level below the substrate in the spraying chamber, an excess of microparticles will be
10 deposited on the substrate to detract from the accuracy of microparticle disposition.

The spraying chamber preferably has a structure which allows control of internal humidity or permits dry air purging. The electrode pattern of the substrate for liquid crystal
15 display use is fine-detailed; for example, the electrode gap between transparent stripe electrodes on the substrate for an STN liquid crystal display device is as narrow as about 10 to 20 μm . When an electric potential is applied across electrodes with such a narrow gap, a short-circuit usually occurs. However,
20 the risk of short-circuit is dependent on the moisture content of the atmosphere in which the substrate is located; there is a high risk of short circuit under high humidity conditions, while the risk is low in a relatively dry environment. Therefore, by using a spraying chamber which permits control
25 of internal humidity or dry gas purging, a larger electric potential can be consistently applied between electrodes to thereby improve the accuracy of microparticle disposition as well as product yield. Moreover, since the humidity-dependent variation in the electrostatic polarity of microparticles is
30 a cause of poor reproducibility of disposition accuracy, insuring a constant humidity environment contributes to an improved reproducibility of electrostatic polarity and accuracy of microparticle disposition.

The preferred humidity within said spraying chamber is
35 70% RH or less at the ambient temperature of 20 to 30°C. The

dry gas which can be used for said dry gas purging may for example be air or N^2 .

The spraying chamber is preferably provided with a stage for setting the substrate thereon. The stage is preferably a grounded stage with a volume resistivity of not more than $10^{10}\Omega$ cm. When the stage is thus composed of a conductor and a high voltage repelling the linear transparent electrodes (of the kV order) is applied, a charge of opposite polarity appears on the stage due to electrostatic induction, with the result that the effect of relatively reversed polarity is developed across the electrodes owing to depolarization to favor the selective disposition of microparticles in the electrode gaps. (This does not mean that no disposition occurs at a higher volume resistivity but rather a better disposition is obtained under specified conditions.)

Moreover, when the glass substrate has been charged in a preceding step, the antistatic effect can also be obtained.

As said stage, a conductive stage comprising metal, etc. can be used with advantage but a conductive stage overlaid with an antistatic sheet may also be employed.

Furthermore, for the purpose of eliminating a fraction of microparticles charged to the opposite polarity to improve the selectivity of disposition in the electrode-free areas (electrodes gaps), the microparticle spraying apparatus according to the first aspect of the present invention is preferably provided with a charged element for eliminating such microparticles of opposite polarity within the spraying chamber.

Said charged element set in the spraying chamber is preferably provided in at least a domain of the surface extending from the nozzle orifice of a microparticle delivery nozzle duct to the periphery of the substrate.

Preferably, to said charged element, a potential of the same polarity as the microparticles is applied. Moreover, the potential to be applied is preferably larger than the potential

to be applied to each of said electrodes on the substrate.

The microparticle spraying apparatus according to the first aspect of the present invention has a microparticle supply means. This microparticle supply means is adapted to feed
5 microparticles into said spraying chamber and spraying them over the substrate.

The microparticle supply means is not particularly restricted but is preferably a device comprising a microparticle nozzle duct means and a microparticle tank and
10 adapted to feed microparticles to said spraying chamber from said microparticle tank through said microparticle nozzle duct means with a pressurized gas as the vehicle.

With this microparticle supply means comprising said microparticle nozzle duct and microparticle tank, the
15 microparticles can be charged + (positive) or - (negative) by letting the microparticles repeatedly contact the internal wall of said microparticle nozzle duct.

The pressurized gas to be used as said vehicle is not particularly restricted but includes compressed air and N^2 ,
20 among others. The pressurized gas is preferably a dry gas with a minimum of moisture content.

The charging polarity of particles is defined by the work function of the material constituting the surface of microparticles and the work function of the material forming
25 the internal wall of the microparticle delivery duct. Thus, generally when two kinds of materials differing from each other in work function are brought into contact, the electrons begin to shift from the material with a smaller work function to the material with a larger work function so that a potential
30 difference known as contact potential difference is produced between the two materials. As a result, the material with a smaller work function is positively charged while the material with a larger work function is negatively charged. Thus, when the work function of the material constituting the surface of
35 microparticles is smaller than the work function of the material

constituting the internal wall of the microparticle delivery duct, the microparticles are positively (+) charged.

Conversely, when the former is larger than the latter, the microparticles are negatively (-) charged. In this connection,

5 there is the tendency that the larger the difference in work function is, the more strongly charged are the microparticles, while the microparticles are weakly charged when said difference is smaller. Incidentally, the work function of a material can be calculated according to the contact potential
10 difference from a material with a known work function.

In the first aspect of the present invention, the microparticle supply means comprising said microparticle delivery duct and microparticle tank may be a device having only one microparticle delivery duct or a device having two or more
15 microparticle delivery ducts but is preferably a device having two or more microparticle delivery ducts varying in constituent material. With a microparticle supply means of such construction, the microparticles can be selectively charged + (positive) or - (negative) by routing the microparticles
20 through the proper one of said plural delivery nozzle ducts comprising dissimilar materials.

The constituent materials of said two or more microparticle delivery nozzle ducts can be judiciously selected according to the relationship to the material of the
25 microparticles used.

The above microparticle supply means having said two or more microparticle delivery ducts comprising dissimilar materials may have only one microparticle tank but may optionally have two or more microparticle tanks.

30 When, as said microparticle supply means having two or more microparticle delivery ducts comprising dissimilar materials, a device having two delivery ducts, for instance, is used, microparticles of one and the same composition can be selectively charged + (positive) or - (negative) by routing them
35 through one or the other of the two microparticle delivery ducts

of different materials. Therefore, by switching the microparticle delivery nozzle ducts from one to the other during spraying of microparticles, the + (positive)-charged microparticles and - (negative)-charged microparticles can be alternately or sequentially sprayed on the substrate.

Furthermore, in this first aspect of the present invention, a microparticle supply means having two or more microparticle tanks can also be used with advantage as said microparticle supply means comprising said microparticle delivery duct and microparticle tank. When it is so arranged that the two or more microparticle tanks contain microparticles comprising dissimilar kinds of materials or having dissimilar surface compositions, the microparticles from said microparticle tanks can be charged + (positive) or - (negative) by routing them through the delivery duct.

When, as said microparticle supply means having two or more microparticle tanks, one having two microparticle tanks is used, for instance, one of two kinds of microparticles varying in constituent material or surface composition may be charged + (positive) by routing them through the microparticle delivery duct while the other of said two kinds of microparticles varying in constituent material or surface composition can be charged - (negative) by routing them through the same microparticle delivery duct. Therefore, by performing the spraying operation with two kinds of microparticles varying in constituent material or surface composition alternately or in sequence, the + (positive)-charged microparticles and - (negative)-charged microparticles can be alternately or sequentially disposed on the substrate.

As the microparticle delivery duct of the above microparticle supply means, it is preferable to use two or more nozzle ducts dissimilar in constituent material as connected in series. As mentioned above, the first aspect of the present invention accomplishes the disposition control of

microparticles through the interaction of charged particles with the electric field formed by the potential difference between electrodes on the substrate. However, unless the relationship of said charging amount of microparticles to said potential difference is adequate, the microparticles may not be disposed selectively in the electrode gaps but deposited on the electrodes as well. Thus, when either said charging amount or said potential difference is too large, the falling microparticles are too greatly attracted to the electrodes or the stream of microparticles is biased too much, resulting in deposition thereof on the electrodes. When the charging amount or potential difference is too small, too, the microparticles may fall on the electrodes because the locus of falling microparticles is not sufficiently altered.

While the potential difference between electrodes can be adjusted by varying the voltage values to be applied to said electrodes respectively, it has heretofore been impossible to control the charging amount of microparticles, although microparticles can, of course, be charged. The above microparticle supply means according to the first aspect of the present invention has the above microparticle delivery duct means and, therefore, is capable of controlling the charging amount of microparticles which has not been achieved by the prior art.

Since the charging amount of microparticles is defined by the relationship of microparticles to the duct material as mentioned above, the charging amount of microparticles can be controlled to a suitable level by, for example, connecting a duct composed of a material capable of charging microparticles in a great degree in series with a duct composed of a material capable of charging microparticles only in a minor degree. As an alternative, the charging amount, inclusive of the charging polarity, of microparticles can be judiciously controlled by connecting a duct composed of a material capable of charging microparticles + (positive) in series with a duct composed of

a material capable of charging microparticles - (negative).

The constituent material of said duct means may be a metal or a resin and can be judiciously selected in consideration of charging polarity and charging amount.

5 The metallic duct is not particularly restricted but may be a duct composed of a simple metal such as Ni, Cu, Al or Ti or a duct comprising an alloy such as SUS. Moreover, it may be a duct internally covered with a metallic film comprising Au, Cr, etc. as formed by plating, for instance. Moreover, the
10 internal wall of a metallic duct may be covered with a thin film composed of a different metal or a synthetic resin.

 When a resin pipe is used as said delivery duct means, the outer wall of the pipe is preferably covered with a
15 conductive metal. The microparticles are electrostatically charged as they contact with the internal wall of the duct but the electric charge comes in and goes out between the resin duct and the microparticles. The apparatus itself is grounded and, therefore, when the outer wall of the resin duct is covered with
20 a metal, the electric charge comes in and goes out between the resin duct and the ground so that the charge on the
 microparticles can be stabilized.

 The microparticle delivery duct is preferably such that the ratio of the lengths of its component ducts connected in series can be freely altered. By changing the relative lengths
25 of component ducts comprising dissimilar materials, the charging amount of microparticles can be fine-controlled. Assuming, for example, that A is a component duct adapted to charge microparticles in a high degree and B is a component duct adapted to charge microparticles in a low degree, the charging
30 amount of microparticles can be fine-controlled by means of the microparticle delivery duct constituted by connecting component ducts A and/or B in series in the combination of AAA, ABA, or ABB, for instance.

 Furthermore, the microparticle delivery duct is
35 preferably such that its total length is freely adjustable. By

varying the total length, the charging amount of microparticles can be further fine-controlled.

The thus-controlled charging amount of microparticles can be assessed by means of E-SPART Analyzer (Hosokawa Micron Co.), for instance.

When, as said microparticle supply means, one having two or more microparticle delivery ducts comprising dissimilar materials is used, the combination of said two or more delivery ducts may comprise a metal component duct and a resin component duct covered with a metal, or two or more ducts comprising dissimilar materials.

The microparticle spraying apparatus according to the first aspect of the present invention is equipped with a voltage application means. This voltage application means is designed to apply voltage to a plurality of electrodes formed on a substrate and is capable of applying different levels of voltages to said electrodes respectively.

The voltage to be applied by said voltage application means is preferably DC voltage or pulse voltage.

The application of different levels of voltages to said electrodes respectively by said voltage application means can be carried out typically as follows. Thus, in the case where said plurality of electrodes formed on a substrate are stripes for instance, the pattern of applying a relatively high level of voltage to two adjacent electrodes and a relatively low level of voltage to one neighboring electrode is repeated as illustrated in Fig. 2. By applying the voltage in the above pattern, a region with a relatively high potential (+ (positive)) and a region with a relatively low potential (- (negative)) are alternately formed on the substrate, with the result that lines of electric force are produced as illustrated in Fig. 3. Therefore, when the microparticles fed and ejected from said microparticle supply means have been negatively charged (-), the microparticles are subjected to forces acting in the direction opposite to said lines of electric force so

that they are disposed in the gap between each two electrodes to which a relatively high voltage has been applied.

The voltage of dissimilar levels as applied for selective disposition of microparticles may be voltage of mutually
5 different polarities or voltage of the same polarity. Furthermore, when the polarity of charged microparticles is - (negative), both of said voltages of dissimilar levels may be either + (positive) or - (negative). In any event, it is necessary and sufficient that said voltage levels may form a
10 gradient such that a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region will be alternately formed. Thus, even when the microparticles are negatively (-) charged or when both the polarity of a relatively high voltage and that of a relatively low voltage are -
15 (negative), the microparticles are not strongly repelled because of the lines of electric force although the number of microparticles reaching the substrate will be somewhat decreased, so that the microparticles can be disposed in the intended positions. When the microparticles have been
20 positively (+) charged, too, provided that the voltage form a gradient, the polarity of voltage is immaterial.

When microparticles have been positively (+) charged, the pattern-wise application of dissimilar voltage may comprise applying a relatively low voltage to each two adjacent
25 electrodes and a relatively high voltage to one neighboring electrode, whereby the microparticles can be disposed in the electrode gaps as in the foregoing arrangement.

Moreover, the pattern-wise application of dissimilar voltage to said electrodes respectively by said voltage
30 application means may for example comprise applying a relatively high voltage and a relatively low voltage to two electrodes each in an alternate fashion and repeating this application pattern as illustrated in Fig. 4. By applying voltages in accordance with the above application pattern, a
35 relatively high potential (+ (positive)) region and a

relatively low potential (- (negative)) region are formed alternately on the substrate so that the lines of electric force illustrated in Fig. 5 are produced. Therefore, when the microparticles supplied and sprayed from said microparticle supply means have been negatively (-) charged, the microparticles are subject to forces acting in the direction opposite to the lines of electric force, with the result that the microparticles are disposed in the gap between the two electrodes to which a relatively high voltage has been applied. When the microparticles have been positively (+) charged, the microparticles are subject to forces corresponding to the lines of electric force so that they are disposed in the gap between two electrodes to which a relatively low voltage has been applied.

When such a voltage application pattern is adopted, both of positively (+) charged microparticles and negatively (-) charged microparticles can be sprayed and disposed in independent and different positions. In this case, if the positively (+) charged microparticles and negatively (-) charged microparticles are delivered concurrently, the (+) and (-) charged microparticles may form aggregates. Therefore, the differently charged microparticles are preferably delivered alternately or one after another.

Furthermore, when such an application pattern is used, the position of microparticle disposition may be switched by changing the polarity and level of voltage in the course of spraying of the microparticles. Thus, the voltage application means is preferably one capable of changing the polarity and level of voltage to be applied to each electrode on a substrate in the course of spraying.

The application of voltage at different levels to a plurality of electrodes by said voltage application means may also comprise applying a relatively high voltage to an even number of electrodes arranged side by side and a relatively low voltage to an even number of similarly arranged electrodes

adjacent to the first-mentioned even number of electrodes and repeating this application pattern. More particularly, expressing the relatively high voltage as + and the relatively low voltage as -, the above voltage application pattern may for example be

5 ····--++++--++++--····. As the voltage is applied in such a pattern, a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region are alternately formed on the substrate to produce lines of electric force. The relatively + (positive) valley of the lines of electric force and the relatively - (negative) valley of the lines of electric force are respectively formed in the central position of the relatively high potential (+ (positive)) region and the central position of the relatively low potential (- (negative)) region, that is to say in agreement with the positions of electrode gaps. Therefore, just as in the voltage pattern obtained by applying a relatively high voltage and a relatively low voltage to two electrodes each, positively (+) charged microparticles and negatively (-) charged microparticles can be disposed in different positions by delivering those microparticles alternately or in sequence.

The application of voltages to stripe electrodes according to the above-mentioned pattern by means of said voltage application means may for example be accomplished as illustrated in Fig. 6, that is to say by constituting a stripe electrode array by disposing two comb-shaped electrode members each having a given pattern in staggered relation and attaching the connecting terminals for two electrodes each to conductor segments 20 of the two comb-shaped electrode members. As an alternative, the voltage application may be achieved by forming connecting terminals each in a width corresponding to 2 electrodes forming the stripe electrode array and attaching the connecting terminals to each two electrodes alternately at both ends of the stripe electrode array. It is also possible to form each of said connecting terminals in a width corresponding to

one electrode and attaching the needle-shaped connecting terminal to the corresponding electrode. The voltage application may also be carried out by applying a voltage directly by means of a prover.

5 In applying voltages to each of said electrodes on the substrate by said voltage application means, for example by applying a voltage of 1000 V to one of the two terminals connected to the electrodes and a voltage of 1100 V to the other terminal to provide a potential difference of 100 V, it is preferable
10 to apply a voltage of 1000 V to both terminals and, then, increase the voltage of the other terminal to 1100 V. This is because, when a voltage of 1000 V is applied only to one of the two terminals in advance with both terminals having been connected to the electrodes, the potential difference between the two
15 terminals will become 1000 V and be liable to cause a short circuit. As an alternative, it is possible to connect the terminal, to which a voltage of 1000 V has been applied to the electrode and, then, connect the terminal to which a voltage of 1100 V has been applied, to the electrode.

20 The voltage application conditions for use in applying voltages to said electrodes respectively on the substrate by said voltage application means can be judiciously selected according to the magnitude of electrode gap and the charging amount of microparticles, among other factors. For example,
25 even when the polarity of charge on microparticles is - (negative), it is sometimes more conducive to an improved disposition of microparticles to provide a potential difference of 100 V by applying a potential difference between -1100 V and -1000 V, thus 100 V, than applying a potential difference
30 between 0 to 100 V, thus 100 V. The rationale is as follows. In the case of a potential difference formed by a polarity opposite to the polarity of charge on microparticles, the microparticles are first subjected to the influence of a gravitational force in a position far away from the substrate
35 to have their falling speed accelerated but in the case of a

potential difference formed by the same polarity as the polarity of charge on microparticles, the falling speed of the microparticles tends to be decelerated by the influence of a repulsive force and altered in their inertia force so that the degree of compliance of microparticles with the lines of electric force is changed, thus resulting in a change in the position of microparticles disposed on the substrate.

5 Depending on cases, it is preferable to form a large potential difference by using a polarity opposite to the polarity of charge on microparticles to cause the stream of microparticles to comply as much as practicable with the lines of electric force.

10 In spraying microparticles with the microparticle spraying apparatus according to the first aspect of the present invention, the microparticles may be sprayed on an intermittent basis, for example by carrying out 10 seconds of spraying and 1 second of cessation in 10 cycles. By such an intermittent spraying of microparticles, the mis-disposition of microparticles due to a turbulence of pressurized gas can be prevented.

20 The microparticles which can be disposed by means of the spraying apparatus according to the first aspect of the present invention is not particularly restricted but may be metallic microparticles, synthetic resin microparticles, inorganic microparticles, and light-opaque microparticles comprising a dispersion of pigment particles in a synthetic resin matrix, colored microparticles, microparticles responsive to heat or light to develop adhesion, and metal, synthetic resin or inorganic microparticles whose surfaces have been plated with a metal, among others. The method of spraying said microparticles may be whichever of dry and wet spraying methods. In the wet spraying system, the spacer is dispersed in a mixed solvent such as water-alcohol but since the spacer can be charged even under such conditions, the effects of the invention are not comprised. However, since microparticles with a larger

charging amount can be more accurately disposed, the dry spraying system is preferred.

As the substrate on which microparticles can be deposited by means of the microparticle spraying apparatus according to the first aspect of the present invention, there can be mentioned, for example, glass substrates, resin substrates and metal substrates each carrying a plurality of electrodes on the surface. However, when a metal substrate is used, an insulation layer should be formed on the substrate to prevent short-circuiting of the surface electrodes.

The electrodes on a substrate in the context of the first invention are not particularly restricted but may for example be transparent electrodes, such as linear transparent electrodes. A stripe electrode pattern constituted by such linear transparent electrodes arranged in parallel on a substrate can be adopted.

The stripe electrode pattern mentioned above is the pattern used for the display electrodes of a liquid crystal display device.

The second invention is directed to a microparticle spraying method comprising applying an electric potential to a plurality of electrodes on a substrate, charging a microparticle electrostatically, and spraying and disposing said microparticle selectively on said substrate, wherein a microparticle spraying apparatus includes a means for eliminating an oppositely charged microparticle.

In accordance with this invention, therefore, said fraction of microparticles charged to an opposite polarity can be eliminated to improve the selectivity of disposing microparticles in the electrode-free areas (electrode gaps).

The third aspect of the present invention is concerned with a microparticle spraying method comprising applying an electric potential to a plurality of electrodes on a substrate, charging a microparticle electrostatically, selectively spraying and disposing said microparticle on said substrate,

wherein a charged element with an electric potential of the same polarity as said microparticle being applied is disposed in at least a domain of the surface extending from the nozzle orifice of a microparticle delivery duct to the periphery of said
5 substrate.

Thus, the stream of oppositely charged microparticles ejected from the nozzle orifice is subjected to a force attracting them toward said charged element and thereby diverted so that the microparticles are sprayed away from the
10 substrate or outside of said plurality of electrodes.

Only provided that it is on said surface extending from the nozzle orifice of said microparticle delivery duct to the periphery of said substrate, comparative effect can be obtained.

15 However, when such a charged element is disposed on the wall of the spraying chamber as in the prior art, no comparable effect can be obtained because of the large distance between the charged element and the microparticles.

The potential applied to said charged element is
20 preferably higher than the potential to be applied to the electrodes on the substrate.

Thus, microparticles charged to a given polarity are disposed in selected positions on the substrate. If the potential applied to said charged element is low, the stream
25 of microparticles is diverted by the repulsive force from the electrodes on the substrate so that the microparticles are rather deposited on the charged element.

The fourth aspect of the present invention relates to a microparticle spraying method comprising spraying plural kinds
30 of microparticles constituted by dissimilar constituent material or surface composition from the corresponding microparticle tanks with a pressurized gas as the vehicle using a microparticle spraying apparatus, wherein said microparticle spraying apparatus comprises a spraying chamber for
35 accommodating a substrate, a microparticle supply means

comprising at least one microparticle delivery nozzle duct and at least one microparticle tank, both for supplying a microparticle into said spraying chamber and spraying it onto said substrate, and a voltage application means for applying
5 voltages to a plurality of electrodes formed on said substrate, said voltage application means being capable of applying dissimilar levels of voltages to each of said electrodes.

By this method, microparticles contained in said microparticle tanks, respectively, can be charged positively
10 (+) or negatively (-) and sprayed from said microparticle spraying apparatus.

Preferably, said microparticles are sprayed as positively (+) charged by passage through one of said microparticle delivery ducts and as negatively (-) charged by
15 passage through another microparticle delivery duct.

It is also preferable that one of two kinds of microparticles varying in constituent material or surface composition be positively (+) charged by routing them through a microparticle delivery duct while the other kind of
20 microparticles be negatively (-) charged by passage through the microparticle delivery duct.

Thus, by spraying two kinds of microparticles varying in constituent material or surface composition alternately or serially, the microparticles charged positively (+) and the
25 microparticles charged negatively (-) can be independently disposed on a substrate.

From the standpoint of preventing inaccurate disposition of microparticles due to a turbulence of pressurized gas within said spraying chamber, the spraying of microparticles is
30 preferably carried out on an intermittent basis.

The fifth aspect of the present invention is directed to a method of manufacturing a liquid crystal display device, which comprises using the microparticle spraying apparatus according to the first aspect of the present invention, disposing a spacer
35 selectively on a substrate carrying a stripe transparent

electrode pattern constituted by plural linear transparent electrodes arranged in parallel, and applying a relatively high level of voltage to an even number of linear transparent electrodes arranged in parallel and a relatively low level of voltage to an even number of similarly arranged linear transparent electrodes neighboring the first-mentioned even number of linear transparent electrodes to thereby produce a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region in an alternate pattern and, in this condition, spraying either a positively (+) charged spacer or a negatively (-) charged spacer onto said substrate, or a positively (+) charged spacer and a negatively (-) charged spacer alternately or in succession onto the substrate.

The method of manufacturing a liquid crystal display device according to the fifth aspect of the present invention comprises using the microparticle spraying apparatus according to the first aspect of the invention. Thus, by means of the microparticle spraying apparatus of the first aspect of the invention, the microparticle spacer is disposed selectively on a substrate carrying a stripe transparent electrode array constituted by a plurality of linear transparent electrodes arranged in parallel.

In this fifth aspect of the invention, a relatively high level of voltage is applied to each even number of linear transparent electrodes arranged in parallel and a relatively low level of voltage to each even number of linear transparent electrodes neighboring the first-mentioned even number of linear transparent electrodes as similarly arranged in parallel. By applying voltages according to the above application pattern, a relatively high potential (+ (positive)) region and a relatively low potential (- (negative)) region are formed alternately on the stripe transparent electrode pattern.

In the potential regions thus formed, the relatively + (positive) valley and the relatively - (negative) valley of

lines of electric force invariably coincide with the gaps between linear transparent electrodes.

Therefore, by spraying a positively (+) charged spacer or a negatively (-) charged spacer selectively by means of the microparticle spraying apparatus according to the first aspect
5 of the invention, the spacer microparticles can be exactly disposed in the gaps between linear transparent electrodes.

In the method of manufacturing a liquid crystal display device according to the fifth aspect of the present invention,
10 spacer spraying may be carried out on an intermittent basis, for example in 10 cycles each comprising 10 seconds of spraying followed by 1 second of cessation. By such an intermittent spraying of spacer microparticles, the disturbance of spacer disposition due to a turbulence of pressured gas can be
15 prevented.

The spraying apparatus according to the first aspect of the present invention is capable of disposing microparticles accurately on a substrate. Therefore, in the liquid crystal display device, particularly STN liquid crystal display device,
20 which has been manufactured by the liquid crystal display manufacturing method according to this fifth aspect of the invention, the spacer is exactly disposed under the black matrix pattern so that the device features a high contrast without light leaks attributable to the spacer.

25 An embodiment of the microparticle spraying apparatus of the present invention is now described, reference being had to the accompanying drawings.

Fig. 1 is a schematic view showing a microparticle spraying apparatus embodying the principles of the present
30 invention. A spraying chamber 10 is provided with a microparticle supply device 11 comprising a microparticle delivery duct 11a and a microparticle tank 11b, a voltage application means 12, and a humidity controller 13.

The spraying chamber 10 is further equipped with a vent
35 hole 14 and a conductive stage 15. The vent hole 14 is disposed

at a level above a substrate 1 and can be switched ON and OFF by timer-control. The substrate 1 is set on said stage 15.

The voltage application means 12 can be set to any output voltage value and polarity and is connected to a plurality of
5 transparent electrodes 3 formed on the substrate 1 through connecting terminals.

The humidity control means 13 maintains the relative humidity within the spraying chamber 10 at a constant level.

The microparticles (spacer) 8 fed from the microparticle
10 tank 11b through the microparticle delivery duct 11a to the spraying chamber 10 by means of compressed air are charged as they repeatedly contact (collide with) the inner wall of said microparticle delivery duct 11a. To the electrodes 3 formed on the substrate 1, different levels of voltage are applied by
15 the voltage application means 12, so that lines of electric force are formed in certain patterns on the substrate 1. Therefore, the charged microparticles (spacer) 8 are subjected to the influence of these lines of electric force, whereby the disposition thereof on the substrate 1 is controlled.

20 Fig. 7 is a schematic view showing another microparticle spraying apparatus embodying the principles of the present invention. In this embodiment, the microparticle supply means 11 has at least two microparticle delivery ducts 11a. Otherwise, the construction of the apparatus is identical to the
25 construction according to the embodiment described hereinbefore.

Fig. 9 is a schematic view showing still another spraying apparatus embodying the principles of the invention. In the microparticle spraying apparatus according to this embodiment,
30 a hermetically or substantially hermetically sealed, clean spraying chamber 10 is provided, at its top, with a microparticle delivery duct 11a used for ejecting charged spacer microparticles 8. This microparticle delivery duct 11a is connected to a supply device for feeding the spacer 8 and
35 nitrogen gas (not shown) through piping 17. In the lower region

of the spraying chamber 10, an insulating substrate 1 comprising glass or the like and carrying display electrodes 3 is disposed, with a lead wire 18 for applying potentials to the display electrodes 3 to form an electric field being further provided.

5 The wall surface of the microparticle spraying chamber comprises polyvinyl chloride so that, when spraying the charged spacer 8, the wall surface is charged to the same polarity as the spacer 8, with the result that the charged spacer will not be attracted onto the wall. Moreover, a charged element 19 to
10 which a potential of the same polarity as the spacer 8 is disposed within the microparticle spraying chamber.

The method of charging the spacer 8 includes the method of charging microparticles with the microparticle supply means described above, the method of applying a potential to the
15 spacer 8 with a static charger (not shown) installed within the microparticle spraying chamber, and the method of charging the spacer by friction using a microparticle delivery means comprising a stainless steel or other metal duct, among others, and any of those methods can be selectively used.

20 As shown in Fig. 10, the electrode pattern of said plurality of electrodes comprises, as formed on the insulating substrate 1, stripe display electrodes 3a, 3b, and conductors 20a, 20b for applying potentials to the display electrodes 3a, 3b. Connected to conductors 20a, 20b are lead wires 18a, 18b
25 for supplying a current to conductors 20a, 20b for forming an electric field. As an alternative, an electric potential may be directly applied to each of display electrodes 3a, 3b by means of probe pins or the like, i.e. without provision of conductors 20a, 20b.

30 The display electrodes 3a are paired. The display electrode 3b is a display electrode interposed between a pair of display electrodes 3a and another pair of display electrodes 3a. As explained below, the spacer 8 is selectively disposed exclusively between the display electrodes 3a forming a pair.

35 As shown in Fig. 11, dissimilar levels of voltage are

applied to the plurality of linear transparent electrodes arranged in parallel. Thus, negative voltage (-) are applied to the linear transparent electrodes 3a, 3b but a relatively high potential is applied to the linear transparent electrodes 3a than to the linear transparent electrodes 3b. Furthermore, the spacer 8 is charged negatively and, then, sprayed. In this arrangement, the spacer can be disposed exclusively between the display electrodes 3a forming a pair.

Although a simple matrix liquid crystal display cell is used in this embodiment, the invention is not restricted to the simple matrix liquid crystal display cell but can of course be applied to a ferroelectric liquid crystal display cell or a TFT liquid crystal display cell.

BEST MODE FOR CARRYING OUT THE INVENTION

The following examples illustrate the present invention in further detail and should by no means be construed as defining the scope of the invention.

Example 1

In the common electrode design for STN liquid crystal display devices (color filter-formed substrate, RGB pixel aperture size $80 \times 285 \mu\text{m}$, black matrix line width $20 \mu\text{m}$, ITO electrode width $290 \mu\text{m}$, electrode gap $15 \mu\text{m}$, sheet thickness 0.7 mm), a substrate with the stripe electrodes (ITO electrodes) wired through conductive segments out of the display unit to form a 2:2 comb electrode assembly was fabricated (Fig. 6).

On the substrate thus prepared, a $0.05 \mu\text{m}$ -thick polyimide alignment film was constructed and subjected to rubbing treatment.

Then, as illustrated in Fig. 1, said substrate was set in the spraying chamber of a spraying apparatus, and terminals for voltage application were connected to said conductive segments so that a direct current voltage could be applied independently to each of the conductive segments.

The microparticle tank was filled with the synthetic resin microparticle Micropearl BB (particle diameter 5.1 μm , Sekisui Fine Chemical Co.). The Micropearl BB had been negatively (-) charged.

5 A DC voltage of +150 V was applied to one of said voltage application terminals, while a DC voltage of -150 V was applied to the other terminal. In this condition, under timer control, the spacer was ejected with the aid of compressed air over the substrate for 20 seconds and, after a settling time of 60 seconds,
10 the vent hole was opened for 30 seconds. At the end of this vent time, the voltage application was turned OFF.

The internal temperature was set to 25°C and the humidity within the spraying chamber was controlled at 40% RH.

Microscopic examination of the substrate sprayed with the
15 spacer as above revealed that the spacer had been disposed exclusively between the electrodes to which a voltage of +150 V was applied, that is to say under the black matrix (disposed at intervals of every 4 stripe electrodes). The spacer microparticles on the substrate were counted and the number per
20 1 mm^2 was calculated. The number was 200/ mm^2 .

By cutting the conductive part of the substrate used, a common electrode panel similar to the conventional one was obtained.

25 Example 2

Except that the spraying time was set to 20 seconds and the voltage was applied under the same conditions as in Example 1 for an initial 10 seconds and thereafter in the reversed polarity for the remaining 10 seconds, the spacer was sprayed
30 in otherwise the same manner as in Example 1.

Microscopic examination of the substrate sprayed with the spacer as above revealed that, in addition to the same disposition lines as in Example 1, the spacer had been disposed between the other comb-shaped electrodes (at intervals of every
35 two stripe electrodes). The number of spacer microparticles

on the substrate was counted and converted to the count per mm^2 . The result was $200/\text{mm}^2$.

Example 3

5 Except that the humidity controller was switched OFF and, instead, the spraying chamber was purged with dry nitrogen gas, the spacer was sprayed in otherwise the same manner as Example 1.

10 Microscopic examination of the substrate sprayed with the spacer as above showed that the spacer had been disposed in the same pattern as in Example 1.

Example 4

15 Except that a prover-like terminal device capable of energizing every two stripe electrodes at two-electrode intervals was prepared and connected to both sides so that voltage could be applied to the individual electrodes in the stripe direction of the ordinary common substrate, the spacer was sprayed in otherwise the same manner as in Example 1.

20 Microscopic examination of the substrate sprayed with the spacer as above revealed that the spacer had been disposed in the same pattern as in Example 1.

Comparative Example 1

25 The common electrode for ordinary STN liquid crystal display devices (the conventional common electrode not in the comb-shape) was prepared to the same size as the electrode of Example 1.

30 The conventional spraying equipment was provided with electrodes and wiring so that a voltage could be applied to the entire ceiling. Then, a DC voltage of -1 kV was applied to the ceiling electrodes and the wires of the common electrode were grounded, whereby lines of electric force were established between the common electrode array and the ceiling. Therefore,
35 when a negatively charged spacer was sprayed, the spacer

microparticles could be disposed on the common electrodes (not disposed in electrode gaps).

When the spacer was sprayed in the above condition, the spacer microparticles were disposed without positional
5 selectivity on the whole substrate surface. The reason is probably that because the electrode gap was narrow, the lines of electric force formed were substantially equivalent to a homogeneous electric field over the substrate.

10 Example 5

A liquid crystal display device was constructed using the microparticle spraying apparatus shown in Fig. 7. This microparticle spraying apparatus is equipped with four microparticle delivery ducts 11a varying in constituent
15 material and has a structure such that the spacer can be routed selectively through these four microparticle delivery ducts 11a and sprayed with the aid of compressed air. More particularly, the following spraying modes are used.

On selecting SW 1, the spacer microparticles are sprayed
20 via the Ni duct.

On selecting SW 2, the microparticles are sprayed via the SUS duct.

On selecting SW 3, the microparticles are sprayed via the gold-plated SUS duct.

25 On selecting SW 4, the microparticles are sprayed via the Al film-clad PVC duct.

A microparticle tank 11b is capable of accommodating two kinds of spacers.

A spraying chamber 10 is provided with a vent hole 14 in
30 its side wall at a level above a stage 15 and this vent hole 14 is opened and closed under timer control after completion of spraying. A humidity controller 13 is also provided so that the interior of the microparticle spraying chamber can be maintained at a constant relative humidity (25°C, 40% RH).

35 The conductive stage 15 disposed in the lower part of the

spraying chamber is adapted to support a glass substrate.

In the common electrode design for STN liquid crystal display devices (color filter substrate, RGB pixel aperture size $80 \times 285 \mu\text{m}$, black matrix line width $20 \mu\text{m}$, ITO electrode width $290 \mu\text{m}$, electrode gap $15 \mu\text{m}$, sheet thickness 0.7 mm), a substrate with the stripe electrodes (ITO electrodes) being wired through conductive segments out of the display unit to form a 2:2 comb electrode assembly was fabricated (Fig. 6).

A voltage of $+150 \text{ V}$ was applied to one of said conductive segments and a voltage of -150 V to the other conductor. In this condition, the synthetic resin microparticle spacer Micropeal BB (particle diameter; $6 \mu\text{m}$, Sekisui Fine Chemical Co.) was sprayed. First, SW 1 was selected to perform spraying for 10 seconds. After a settling time of 60 seconds, ventilation was performed for 15 seconds. Then, SW 3 was selected to perform spraying for an additional 10 seconds, followed by 60 seconds of settling and 15 seconds of ventilation in the same manner as above. Finally, the power supply was switched off and the substrate was taken out.

It was found that the spacer was negatively (-) charged by the Ni duct and the spacer was positively (+) charged by the Au-plated SUS duct.

Microscopic examination of the substrate sprayed with the spacer as above revealed that the spacer had been disposed between the adjacent electrodes to which a voltage of $+150 \text{ V}$ was applied and between the adjacent electrodes to which a voltage of -150 V was applied. Thus, the spacer was disposed under the black matrix.

Example 6

Except that SW 1 and SW 4 were selected, spacer spraying was performed in the same manner as in Example 5.

It was found that, the spacer was negatively (-) charged by the Ni duct and the spacer was positively (+) charged by the Al film-lined PVC duct.

Microscopic examination of the substrate sprayed with the spacer as above revealed that the spacer had been disposed between the adjacent electrodes to which a voltage of +150 V was applied and between the adjacent electrodes to which a
5 voltage of -150 V was applied. Thus, the spacer was disposed under the black matrix.

Comparative Example 2

Except that a voltage of +150 V was applied to both
10 conductive segments, i.e. all the electrodes, and SW 1 was selected to perform spraying for 20 seconds, spacer spraying was otherwise performed in the same manner as in Example 5.

As a result, the spacer was uniformly sprayed on the substrate.

15 This is probably because the ceiling electrodes were distant and the electrode gap was narrow, the lines of electric force were substantially equivalent to a homogeneous electric field so that no positional selectivity was obtained in spraying.

20

Comparative Example 3

Except that a voltage of -150 V was applied to both conductive segments, i.e. all the electrodes, and SW 1 was selected to perform spraying for 20 seconds, spacer spraying
25 was performed in otherwise the same manner as in Example 5.

As a result, the spacer was distributed uniformly on the substrate, the only difference from Comparative Example 3 being a fewer number of microparticles deposited.

30 This is probably because the ceiling electrode were distant and the electrode gap was narrow, the lines of electric force were substantially equivalent to a homogeneous electric field so that no positional selectivity was expressed.

Example 7

35 As the spacer microparticles, A: the synthetic resin

Micropearl BBP (particle diameter 6 μm , Sekisui Fine Chemical Co.) and B: Micropearl BBP (particle diameter 6 μm) surface-treated with alkyl isocyanate were provided. These spacers were accommodated in independent microparticle tanks and SW 2 was selected to spray both spacers through the same duct in succession in otherwise the same manner as in Example 5.

As a result, A was negatively (-) charged and B positively (+) charged by the SUS duct.

Microscopic examination of the substrate sprayed with the spacer as above revealed that the spacer had been disposed between the adjacent electrodes to which a voltage of +150 V was applied and between the adjacent electrodes to which a voltage of -150 V was applied. Thus, the spacer could be disposed under the black matrix.

Example 8

Using the microparticle spraying apparatus illustrated in Fig. 8, a liquid crystal display device was constructed. The spraying chamber of this apparatus has two voltage application terminals connected to the voltage application means 12 so that varying DC voltage may be applied to transparent electrodes on a substrate. The voltage application means 12 is adjustable to the desired voltage value and polarity.

The spraying chamber has a microparticle delivery duct 11a in its upper position so that microparticles 8 can be sprayed by means of compressed air into the spraying chamber. Installed in a lower part of the spraying chamber is a grounded aluminum stage overlayed with an antistatic sheet (volume resistivity $\leq 10^{10} \Omega\text{cm}$) on which a substrate is to be placed.

Disposed below the stage is a variable speed fan 16, by which a stream of air can be created within the spraying chamber. In addition, the ceiling of the spraying chamber had a mesh-structure for improved uniformity of air flow.

The rotational speed of the fan 16 was set at 50 rpm (the

direction of rotation was to insure a flow of air from the ceiling to the substrate).

In the common electrode design for STN liquid crystal display devices (color filter substrate, RGB pixel aperture size $80 \times 285 \mu\text{m}$, black matrix line width $20 \mu\text{m}$, ITO electrode width $290 \mu\text{m}$, electrode gap $15 \mu\text{m}$, sheet thickness 0.7 mm), a substrate board with the stripe electrodes (ITO electrodes) being wired through conductive segments outside of the display unit to form a 2:1 comb electrode assembly was fabricated (Fig. 6). (After spacer spraying, the conductive segments were cut off to provide a common electrode panel of the usual size).

A polyimide alignment film was formed in a thickness of $0.05 \mu\text{m}$ on the substrate 1 prepared above and subjected to rubbing treatment.

The microparticle delivery duct 11a was a nickel (Ni) duct measuring 3 meters in total length (three 1 m-long ducts connected in series).

Then, the voltage application terminals were connected and a voltage of -2.0 kV was applied to the conductive segment on the 2-electrode side of the 2:1 comb-shaped electrode assembly and a voltage of -2.1 kV to the other conductive segments.

In the above condition, the synthetic resin microparticle Micropearl BBS- $6.8 \mu\text{-PH}$ (Sekisui Fine Chemical Co.), i.e. microparticle spacer 8, was sprayed (the spacer 8 had been negatively (-) charged).

Microscopic examination of the substrate 1 sprayed with spacer 8 as above revealed that the spacer had been disposed under the black matrix in the electrode gaps on the 2-electrode side of the 2:1 comb-shaped electrode assembly.

Example 9

Except that the rotational speed of the fan 16 was set to 500 rpm, the spacer 8 was sprayed under otherwise the same conditions as in Example 8.

Microscopic examination of the substrate 1 sprayed with spacer 8 as above revealed that the spacer had been disposed under the black matrix in the electrode gaps on the 2-electrode side of the 2:1 comb-shaped electrode.

5

Example 10

Except that a voltage of -2.0 kV was applied to the conductive segment on the 2-electrode side of the 2:1 comb-shaped electrode assembly and a voltage of -2.3 kV to the other
10 conductive segment and that a duct comprising a 2 m-long SUS duct and a 1 m-long Ni duct as connected in series was used as the microparticle delivery duct 11a, the spraying of spacer 8 was performed under otherwise the same conditions as in Example 8.

15 Microscopic examination of the substrate 1 sprayed with spacer 8 as above revealed that the spacer 8 had been disposed under the black matrix in the electrode gaps on the 2-electrode side of the 2:1 comb-shaped electrode.

20 Example 11

Except that a 2 m-long Ni duct was used as the microparticle delivery duct 11a and that a voltage of -2.0 kV was applied to the conductive segment on the 2-electrode side of the 2:1 comb-shaped electrode assembly and a voltage of -2.3
25 kV to the other conductive segment, the spacer 8 was sprayed under otherwise the same conditions as in Example 8.

Microscopic examination of the substrate 1 sprayed with spacer 8 as above revealed that the spacer 8 had been disposed in the black matrix area in the electrode gap of the 2-electrode
30 side of the 2:1 comb-shaped electrode.

Example 12

In the common electrode design for STN liquid crystal display devices, which utilizes a pair of insulating substrates
35 comprising soda glass and each measuring 370×480 mm and 0.7 mm

thick, an insulating substrate formed with a color filter layer and an overcoat layer and an insulating substrate having a stripe electrode array consisting of 300 nm-thick ITO electrodes with the electrodes connected outside of the display area to form a 2:1 comb-shaped electrode assembly were prepared (Fig. 10).

An alignment film was formed on each insulating substrate and rubbed. Then, the insulating substrate carrying the color filter layer and overcoat layer was coated with a sealant by screen printing. The sealant contained glass beads which served as the intraseal spacer.

Then, the insulating substrate 1 formed with the stripe electrode pattern 3 was set in the spraying chamber as shown in Fig. 9, and the voltage application terminals were connected so that DC voltage can be independently applied to said conductors.

As spacer 8, the synthetic resin microparticle BBS-60510-PH (Sekisui Fine Chemical Co.) was negatively charged and sprayed.

Thus, as shown in Fig. 11, a DC voltage of -2000 V was applied to display electrodes 3a and a DC voltage of -2080 V to display electrodes 3b to create a potential difference of 80 V between the two groups of display electrodes 3a and 3b. The charged element 19 was charged to the same polarity as spacer 8 to -5000 V.

As a result, the spacer 8 could be disposed exclusively between the display electrodes 3a. The spacer charged to the opposite polarity was diverted away by the force of attraction acting between the spacer and the charged element 19 so that an improved topographic selectivity of spacer disposition was obtained as compared with the absence of the charged element 19.

Then, the pair of insulating substrates 1 were laminated by hot pressing at 180°C and 0.8 kg/cm and the laminate was after-baked at 150°C. Then, the unwanted parts were cut off.

Thus, conductors 20a and 20b were cut off. Thereafter, a liquid crystal 7 was injected to complete a liquid crystal display device comprising said pair of insulating substrates.

5

INDUSTRIAL APPLICABILITY

The present invention, constituted as above, enables accurate control of microparticle disposition on a substrate. Therefore, the method of manufacturing a liquid crystal display device comprising the use of the microparticle spraying apparatus of the invention accomplishes high-precision disposition of a spacer in the electrode gaps of the transparent stripe electrode array, especially in the manufacture of an STN liquid crystal display device, unlike the conventional random spraying method. As a consequence, the spacer can be disposed selectively under the black matrix to provide a liquid crystal display device featuring a high contrast and free from the incidence of spacer-associated light leaks.

CLAIMS

1. (Amended) A microparticle spraying apparatus for selective disposition of a charged microparticle on a substrate
5 carrying a plurality of electrodes

comprising a spraying chamber adapted to accommodate said substrate, a microparticle supply means for supplying said microparticle into said spraying chamber and spraying it on said substrate, and a voltage application means for applying
10 voltages to the electrodes disposed on said substrate, wherein said microparticle is disposed in an electrode gap.

2. The microparticle spraying apparatus according to
15 Claim 1

wherein the spraying chamber is adjustable for the vertical flow rate of air therein.

3. The microparticle spraying apparatus according to
20 Claim 1 or 2

wherein the spraying chamber is adjustable for internal humidity or purgeable with dry air.

4. The microparticle spraying apparatus according to
25 Claim 1, 2. or 3

wherein the spraying chamber is provided with a stage for setting said substrate and

said stage has a volume resistivity of not more than 10^{10} Ωcm .

30

5. The microparticle spraying apparatus according to Claim 1, 2, 3 or 4

wherein the spraying chamber is internally provided with a charged element.

35

6. The microparticle spraying apparatus according to Claim 1, 2, 3, 4 or 5

wherein the charged element is disposed in at least one domain of the surface extending from a nozzle orifice of the microparticle delivery duct to the periphery of the substrate.

7. The microparticle spraying apparatus according to Claim 1, 2, 3, 4, 5 or 6

wherein the microparticle supply means comprises two or more microparticle delivery ducts and one or more microparticle tanks,

and supplies a microparticle, using a pressurized gas as the vehicle, from said microparticle tank into the spraying chamber via one of said two or more delivery ducts as selected, and

said two or more microparticle delivery ducts comprise dissimilar constituent materials.

8. The microparticle spraying apparatus according to Claim 1, 2, 3, 4, 5, 6 or 7

wherein the microparticle supply means has a microparticle delivery duct comprising two or more ducts of dissimilar materials as connected in series.

9. The microparticle spraying apparatus according to Claim 7 or 8

wherein the microparticle delivery duct is adjustable for the relative lengths of component ducts connected in series.

10. The microparticle spraying apparatus according to Claim 1, 2, 3, 4, 5, 6, 7, 8 or 9

wherein the microparticle supply means comprises two or more microparticle tanks.

11. The microparticle spraying apparatus according to

Claim 7, 8 or 9

wherein the microparticle delivery duct is a metal duct.

12. The microparticle spraying apparatus according to
5 Claim 11

wherein the metal duct is internally covered with either
a metal different from the metal constituting said metal duct,
or a resin thin film.

13. The microparticle spraying apparatus according to
10 Claim 7, 8, 9 or 11

wherein the microparticle delivery duct is a resin pipe
externally covered with a metal.

14. The microparticle spraying apparatus according to
15 Claim 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12 or 13

wherein the voltage application means is capable of
changing the polarity and level of voltages to be applied to
each of said electrodes on the substrate in the course of
20 spraying.

15. (Amended) A microparticle spraying method
comprising applying an electric potential to a plurality
of electrodes on a substrate, charging a microparticle
25 electrostatically, spraying and disposing said microparticle
selectively on said substrate,

wherein a microparticle spraying apparatus includes a
means for eliminating an oppositely charged microparticle, and
said microparticle is disposed in an electrode gap.

30 16. (Amended) A microparticle spraying method
comprising applying an electric potential to a plurality
of electrodes formed on a substrate and charging a microparticle
electrostatically, and selectively spraying and disposing said
35 microparticle on said substrate,

wherein a charged element with an electric potential of the same polarity as said microparticle being applied is disposed in at least a domain of the surface extending from the nozzle orifice of a microparticle delivery nozzle duct to the periphery of said substrate, and
5 said microparticle is disposed in an electrode gap.

17. The microparticle spraying method according Claim 16, wherein the potential to be applied to the charged element
10 is higher than the potential to be applied to the electrodes formed on the substrate.

18. A microparticle spraying method
comprising spraying plural kinds of microparticles
15 constituted by dissimilar constituent material or surface composition from the corresponding microparticle tanks with a pressurized gas as the vehicle using a microparticle spraying apparatus,

wherein said microparticle spraying apparatus comprises
20 a spraying chamber for accommodating a substrate, a microparticle supply means comprising at least one microparticle delivery nozzle duct and at least one microparticle tank, both for supplying a microparticle into said spraying chamber and spraying it onto said substrate, and
25 a voltage application means for applying voltages to a plurality of electrodes formed on said substrate,

said voltage application means being capable of applying dissimilar levels of voltages to each of said electrodes.

30 19. The microparticle spraying method according Claim 18 comprising spraying a microparticle positively charged (+) by routing them through one of the microparticle delivery ducts and negatively (-) charged by routing them through another microparticle delivery duct using a microparticle spraying
35 apparatus,

wherein said microparticle spraying apparatus comprises a spraying chamber for accommodating a substrate, a microparticle supply means comprising at least one microparticle delivery duct and at least one microparticle tank, both for supplying a microparticle into said spraying chamber and spraying it onto said substrate, and a voltage application means for applying voltages to a plurality of electrodes on the substrate,

said voltage application means being capable of applying different levels of voltages to each of said electrodes on the substrate.

20. The microparticle spraying method according Claim 18 or 19

wherein one microparticle of two kinds varying in constituent material or surface composition is positively (+) charged by routing them through a microparticle delivery duct and a microparticle of the other kind is negatively (-) charged by routing them through the microparticle delivery duct.

21. The microparticle spraying method according Claim 18, 19 or 20

wherein a microparticle is sprayed on an intermittent basis.

22. A method of manufacturing a liquid crystal display device

which comprises using the microparticle spraying apparatus according to Claim 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13 or 14,

disposing a spacer selectively on a substrate carrying a stripe transparent electrode array constituted by a plurality of linear transparent electrodes arranged in parallel, and

applying a relatively high level of voltage to an even number of linear transparent electrodes arranged in parallel

and a relatively low level of voltage to an even number of arranged linear transparent electrodes neighboring said even number of linear transparent electrodes to thereby produce a region with a relatively high potential (+ (positive)) and a
5 region with a relatively low potential (- (negative)) in an alternate pattern and, in this condition,

further spraying either a positively (+) charged spacer or a negatively (-) charged spacer onto said substrate or

further spraying a positive (+) charged spacer and a
10 negatively (-) charged spacer alternately or in succession onto the substrate.