

Production of at least 1-hexene and octene from ethene

The invention is concerned with the production of 1-hexene and octenes from ethene. 1-Butene is optionally also to be produced.

5

Hydrocarbons are chemical compounds which consist exclusively of carbon and hydrogen. Alkenes (synonym: olefins) are hydrocarbons which have a C=C double bond in the molecule. Alkanes (synonym: paraffins), on the other hand, are hydrocarbons which have only single bonds. They are therefore also referred to as saturated.

10

In organic chemistry, hydrocarbons are frequently designated according to the number of carbon atoms which they have per molecule, in that the respective class of substances is preceded by the prefix C_n. "n" is the respective number of carbon atoms in a molecule. Thus, C₄ olefins are substances from the class of alkenes having four carbon atoms. C₈ olefins correspondingly have eight carbon atoms per molecule. Where the prefix C_{n+} is used hereinafter, it refers to a class of substances which have more than n carbon atoms per molecule. A C₄₊ olefin accordingly has at least five carbon atoms.

15

The simplest olefin is ethene (ethylene). It has two carbon atoms. Ethene is an important commodity chemical and is therefore produced in large quantities. This is usually effected by cracking of naphtha. In addition, it can be obtained by dehydrogenation of ethane, which in turn is a constituent of natural gas. Owing to the increasing exploitation of unconventional sources of natural gas and decreasing recovery of petroleum, the proportion of ethene based on natural gas is steadily increasing. The physical properties of ethene and the production thereof are described in:

20

Zimmermann, Heinz and Walzl, Roland: Ethylene. Ullmann's Encyclopedia of Industrial Chemistry (2009).

25

Oligomerization is understood to mean the reaction of hydrocarbons with themselves to form correspondingly longer-chain hydrocarbons, the so-called oligomers. Olefins having from two to eight carbon atoms can be oligomerized quite efficiently.

30

Thus, for example, olefins having six carbon atoms (hexene) can be formed by oligomerization of two olefins having three carbon atoms. The oligomerization of two molecules with one another is also referred to as dimerization. If, in contrast, three olefins having three carbon atoms are joined to one another (trimerization), the result is an olefin having nine carbon atoms. The tetramerization of ethene results in octenes, i.e. olefins having eight carbon atoms

35

It should be noted that oligomerization always results in a mixture of different oligomers (oligomerizate). Thus the oligomerization of ethane forms not only ethene dimers but also, in parallel, trimers and tetramers. The oligomerizate thus comprises a range of C_{2+} olefins of different lengths.

5

The oligomers of one carbon atom count are moreover present in different isomeric structures: thus the dimerization of ethene forms the three isomeric C_4 olefins 1-butene, cis-2-butene and trans-2-butene, while the trimerization of ethene can form up to ten different C_6 olefin isomers, namely 1-hexene, (*E*)-2-hexene, (*Z*)-2-hexene, (*E*)-3-hexene, (*Z*)-3-hexene, (*R*)-3-methyl-1-pentene, (*S*)-3-methyl-1-pentene, (*E*)-3-methyl-2-pentene, (*Z*)-3-methyl-2-pentene and 2-ethyl-1-butene. The variety of C_8 olefins formed by C_2 tetramerization is even greater.

10

It can therefore be stated that oligomerization of ethene forms a highly complex mixture of different olefins.

15

However, only the substances 1-butene and 1-hexene, which are used as monomers or comonomers in the production of plastics, are of industrial interest. Olefins having eight carbon atoms may be converted by hydroformylation and hydrogenation into C_9 alcohols which in turn serve as starting materials for the production of a very wide variety of PVC plasticizers.

20

Those oligomerizing ethene are thus faced with the problem of removing the less sought-after substances from the oligomerizate.

Provided that olefins having different numbers of carbon atoms are to be separated this is readily possible by thermal separation methods (distillation) since the different chain lengths result in widely spaced boiling points. However, there is no such hard separation criterion for mixtures of isomers having identical carbon atom counts because the boiling points of the isomers are usually very close together. Distillative separation is then possible only with great apparatus complexity and high energy use, thus resulting in a separation that is far too costly.

25

30

Thus for example the boiling point of 1-hexene is 63°C and that of isohexene (correct name: 4-methyl-1-pentene) is 54°C . This small difference in the boiling point makes it uneconomic to obtain the two pure substances 1-hexene and isohexene from a mixture by distillation; even more so when it is not a binary mixture of these two substances that is concerned but rather an oligomerizate having a multiplicity of further C_6 olefin isomers whose respective boiling points are likewise within this narrow temperature window.

35

US2010/0099934A1 employs a trick to economically separate a mixture comprising isohexene and 1-hexene: the C₆ olefin mixture is subjected to an etherification step where the isohexene is reacted with methanol to afford ether.

- 5 The etherification converts markedly more isohexene than 1-hexene. This affords a reaction mixture which comprises not only 1-hexene but also the ether 3-methyl-3-methoxypentane in place of the isohexene. Since 3-methyl-3-methoxypentane - also known as methyl tert-hexyl ether (MTHxE) - has a higher boiling point than 1-hexene, the 1-hexene can be removed from the MTHxE by distillation at low cost and complexity. In this way, selective isohexene etherification
10 makes it possible to obtain pure 1-hexene from C₆ olefin mixtures such as are generated in ethene oligomerization.

- With regard to the process described in US2010/0099934A1, the question of what happens to the removed MTHxE remains. An obvious option is to feed the ether mixture into the fuel pool as an
15 anti-knock agent, similarly to the teaching in US5752992. The carbon atoms bound therein are thus ultimately burned and are no longer available as a starting material for high-value specialty chemicals.

- It should moreover be noted that ethene oligomerization does not provide any isohexene (4-methyl-
20 1-pentene) at all but rather only the ten C₆ olefins listed above. The technical problem of separating 1-hexene and isohexene solved in US2010/0099934A1 consequently does not arise at all in the workup of ethene oligomerizates; on the contrary it must be solved when C₆ olefin mixtures originating from metathesis of C₄ olefins are to be utilized.

- 25 In the light of this prior art the problem addressed by the present invention is that of developing the known process for producing 1-hexene from ethene to achieve better chemical utilization of the employed carbon atoms.

- This problem is solved by catalytic retrocleavage of MTHxE into the C₆ olefins and the alcohol,
30 reuse of the alcohol in the etherification and reaction of the obtained C₆ olefins with ethene to afford C₈ olefins. In this way the alcohol is not lost from the process but rather is internally recirculated as a derivatizing agent. The less attractive C₆ olefins from the cleavage product are upgraded to octene with further ethene in order to provide a further commercial product.

- 35 Specifically, the invention provides a process for producing at least 1-hexene and octene from ethene comprising the steps of:

- a) providing a feedstock mixture comprising ethene;

- 5
- b) subjecting the ethene to a first oligomerization to obtain a first oligomerizate which comprises olefins having less than six carbon atoms, at least the C₆ olefins 1-hexene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene and olefins having more than six carbon atoms,
- c) distillative workup of the first oligomerizate to obtain a C₆ fraction which comprises at least 1-hexene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene,
- 10 d) subjecting the C₆ fraction to an etherification by addition of an alcohol in the presence of a heterogeneous catalyst to obtain a first reaction mixture comprising at least 1-hexene and 3-methyl-3-methoxypentane;
- 15 e) distillative workup of the first reaction mixture to obtain a first target fraction comprising 1-hexene and an ether fraction at least comprising 3-methyl-3-methoxypentane;
- f) wherein the ether fraction is subjected to a cleavage reaction to obtain a cleavage product which comprises 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene and the alcohol;
- 20 g) wherein the alcohol is removed from the cleavage product by distillation and reused in the etherification;
- 25 h) wherein a first intermediate at least comprising 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene is removed from the cleavage product by distillation;
- i) wherein the first intermediate is reacted with ethene to obtain a second reaction mixture which comprises olefins having at least eight carbon atoms;
- 30 k) and wherein a second target fraction comprising octene is obtained from the second reaction mixture by distillation.

The improvement consists in the features f) to k).

The invention is based on the finding that the etherification is reversible and that octenes can be produced from reaction of C_6 olefins with ethene. Skilful integration of these process steps into the distillation setup allows the products of value to be obtained with little additional cost and complexity; more on this later.

In a particularly preferred development of the process described here the ethene is used to produce not only 1-hexene and octen but also 1-butene as a third target product. This is achieved as follows:

- a) the first oligomerization is performed such that the first oligomerizate comprises 1-butene, cis-2-butene and trans-2-butene;
- b) distillative workup of the first oligomerizate affords a C_4 fraction which comprises 1-butene, cis-2-butene and trans-2-butene;
- c) the C_4 fraction is separated by distillation into a third target fraction comprising 1-butene and into a second intermediate which comprises cis-2-butene and trans-2-butene;
- d) the second intermediate is subjected to a second oligomerization to obtain a second oligomerizate which comprises olefins having at least eight carbon atoms;
- e) the second oligomerizate is worked up by distillation together with the second reaction mixture to obtain the second target fraction.

Provided that the oligomerization of ethene generates the butenes listed in step a) (which will generally be the case) this extension makes it possible to obtain the sought-after 1-butene as a third target product. Less useful 2-butene is converted via the second oligomerization into the C_8 fraction and subjected to the workup that exists in any case.

The oligomerization of the ethene will also generate olefins having more than six carbon atoms. These may be worked up together with the corresponding olefins from the second reaction mixture in order to save apparatus costs. A development of the process accordingly provides that the distillative workup of the first oligomerizate affords a C_{6+} fraction which comprises olefins having more than six carbon atoms and that the C_{6+} fraction is worked up by distillation together with the second reaction mixture to obtain the second target fraction.

Provided that 1-butene is also produced from ethene the oligomerization of the 2-butene likewise forms olefins having a chain length of C_{6+} which may be cost-effectively worked up together. A corresponding development of the process accordingly provides that the distillative workup of the first oligomerizate affords a C_{6+} fraction which comprises olefins having more than six carbon

atoms and that the C₆+ fraction is worked up by distillation together with the second reaction mixture and with the second oligomerizate to obtain the second target fraction.

5 The oligomerization of the ethene may take place in the liquid phase or in the gas phase. Provided that gas phase oligomerization of the ethene is performed the feedstock mixture should comprise more than 95 wt% of ethene and the reaction conditions of the first oligomerization should be chosen such that the first oligomerization is effected in the gas phase. A solid-state catalyst is then required (heterogeneous catalyst).

10 It is better to perform the first oligomerization in the liquid phase in the presence of a solid-state catalyst because this results in a greater process intensity of the reaction. There are various options for oligomerizing ethene in the liquid state:

15 A first option consists of dissolving the ethene in a solvent. Accordingly a feedstock mixture which comprises less than 25 wt% of ethene and more than 75 wt% of the solvent is employed. The reaction conditions of the first oligomerization and the concentration of the ethene in the solvent should then be chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the liquid solvent. The ratio of ethene to solvent is then adjusted to a value between 0.1 and 0.5; the temperature is between 20°C and 150°C and the pressure is
20 between $1 \cdot 10^5$ Pa und $50 \cdot 10^5$ Pa. The catalyst may then either be homogeneously codissolved in the solvent or preferably be present as a heterogeneous catalyst in the form of a solid.

Suitable solvents are in principle substances which exhibit inert behaviour in the oligomerization, i.e. essentially do not take part in the reaction. Specifically, C₃- to C₇-alkanes and C₃- to C₇-
25 cycloalkanes are suitable solvents (pure or in admixture). Since the solvent exhibits inert behaviour it ends up in the first reaction mixture. It is removed from the first oligomerizate by distillation and recycled. In this way the solvent is always recirculated and is therefore not lost. The location of removal of the solvent from the first oligomerizate depends on the boiling point of the solvent. If for example propane or isobutene is employed as solvent these boil before the dimers of ethene and
30 are removed beforehand. If by contrast n-hexane oder n-heptane are used as solvent the removal of the solvent is effected downstream of the hexene removal.

If ethene is present as the only reactive component in the feedstock mixture, depending on the chosen reaction regime, incomplete conversion of ethene may result. Ethene present in excess,
35 and therefore unconverted in the first oligomerization, is removed by distillation from the first oligomerizate and recycled into the first oligomerization.

A particular embodiment of the process provides that the feedstock mixture comprises not only ethene but also olefins having four carbon atoms, wherein the reaction conditions of the first

oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having four carbon atoms. The idea behind this is to use a reactive material as solvent, namely olefins having four carbon atoms, more particularly 1-butene, cis-2-butene and trans-2-butene. This is because these olefins can be liquefied at comparatively low pressures and are therefore suitable as solvents for ethene. Since the C₄ olefins are themselves reactive they are reacted to afford C₈ and C₈⁺ in the first oligomerization. Since the octenes are in any case obtained as a target fraction and discharged a recirculation of the solvent becomes unnecessary. Admittedly, fresh C₄ alkene must always be supplied to the first oligomerization. Since butene-containing mixtures are traded as standard feedstocks in downstream petrochemistry this is in most cases not a problem.

However, if no C₄ source is available, C₆ olefin, which is in any case formed in the process by ethene trimerization, may be used as reactive solvent. A preferred variant of the process therefore provides that the feedstock mixture comprises not only ethene but also olefins having six carbon atoms, wherein the reaction conditions of the first oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having six carbon atoms. The olefins having six carbon atoms used as a reactive solvent are preferably diverted immediately before the etherification and recycled into the ethene oligomerization. This assumes that the process forms sufficient hexene; only a part of the C₆ fraction may be used as solvent since otherwise insufficient C₆ remains available for the etherification.

It will be appreciated that if a low C₆ formation rate does not allow the amount of hexene required as solvent to be recycled, C₄ olefin can also be used as a second solvent. This process variant is characterized in that the feedstock mixture comprises not only ethene but also olefins having four carbon atoms and olefins having six carbon atoms, wherein the reaction conditions of the first oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having four and six carbon atoms.

Finally it is also possible to use a solvent mixture which is partly inert and partly reactive. Thus for example a mixture of C₆ olefin and n-hexane and/or of n-butene and isobutene could be used as solvent. The above then applies correspondingly.

Preferably the first and/or the second oligomerization and preferably also the reaction of the second intermediate with the ethene are performed in the presence of the same heterogeneous catalyst. A solid body which is capable of catalysing all three reactions comprises at least two components, wherein the first component comprises at least one element selected from Ni, Cr, Fe, Ti which is present in metallic and/or oxidic and/or hydridic form and wherein the second

component comprises at least one metal oxide selected from Al_2O_3 , SiO_2 , TiO_2 , ZrO_2 . An example of a catalyst of this kind is known from US2581228.

Typical reaction conditions for the first and second oligomerization over this catalyst in the liquid phase are in the following range:

Temperature:	20°C to 150°C
Pressure:	$1 \cdot 10^5$ Pa to $50 \cdot 10^5$ Pa
Space/time loading:	3 h^{-1} to 50 h^{-1}

10

The reaction of the second intermediate with ethene in the presence of said catalyst is effected at a temperature between 20°C and 150°C and at a pressure between $1 \cdot 10^5$ Pa and $50 \cdot 10^5$ Pa, wherein the quantitative ratio of the ethene to the second intermediate is chosen such that the second intermediate is present in the liquid phase and the ethene is fully dissolved therein. This is achieved at a ratio of ethene to intermediate in the range from 0.1 to 0.5.

15

The etherification is effected in the liquid phase at a pressure of $1 \cdot 10^5$ Pa to $7 \cdot 10^5$ Pa and a temperature of 50°C to 130°C in the presence of a polystyrene-divinylbenzene copolymer bearing sulphonic acid groups or carboxylic acid groups. Said substance is for example an acidic ion exchange resin, for example Amberlyst® 15 from Rohm & Haas.

20

In the simplest case the alcohol used is methanol. The reaction of hexene with methanol to afford MTHxE is described in detail in:

25

Krause, A.O.I.; Hammarström, L.G.; Joutsimo, M.: Etherification of C6-Olefins with Methanol. In Proceedings of the 8th International Congress on Catalysis, Berlin, Germany, July 2-6, 1984; Vol. V, V553-V563.

30

In contrast with the other reactions the cleavage reaction is preferably performed in the gas phase at a pressure of $1 \cdot 10^5$ Pa to $25 \cdot 10^5$ Pa and a temperature of 130°C to 350°C. The ether cleavage can be heterogeneously catalysed with a solid body having the following composition which sums to 100 wt%:

35

•	silicon dioxide:	61 wt% to 74 wt%;
•	aluminum oxide:	19 wt% to 23 wt%;
•	magnesium oxide:	10 wt% to 12 wt%;
•	sum of other substances:	0 to 10 wt%.

The production of such a cleavage catalyst is described in EP1894621B1.

In the first oligomerization not only 1-hexene but in most cases also 2-hexene and 3-hexene are formed. Provided that it does not undergo further reaction it then ends up in the first reaction mixture. The yield of 1-hexene in the overall process can be enhanced when the 2-hexene and 3-hexene present in the first reaction mixture are separated by distillation from the 1-hexene and then subjected to an isomerization which isomerizes the 2-hexene and the 3-hexene to afford 1-hexene. The thus obtained isomerizate is recycled back into the removal of the 1-hexene from the 2-hexene and 3-hexene. The yield of 1-hexene is enhanced by separation of 2-hexene and 3-hexene and isomerization thereof.

The isomerization is effected in the gas phase at a temperature between 100°C and 300°C and at a pressure between $1 \cdot 10^5$ Pa and $10 \cdot 10^5$ Pa. The isomerization is heterogeneously catalysed over a solid catalyst which comprises as the catalytically active material at least one of the following oxides: MgO, CaO, BaO, Li₂O, SrO.

Specifically, basic catalysts may also be used in the isomerization. Such basic catalysts comprise as primary components aluminium oxide and/or zirconium oxide and/or abovementioned alkali metal oxides and/or alkaline earth metal oxides. Further components that may be present in the catalyst in amounts of 0.01 wt% to 3 wt%, preferably 0.5 wt% to 5 wt%, are titanium dioxide, silicon dioxide and/or thorium oxide. Such materials are disclosed in WO2004/052809A1.

Various process variants are now to be elucidated with reference to simplified flow diagrams. The figures show the following:

- Figure 1: basic implementation, only ethene feedstock;
- Figure 2: implementation with ethene and butene feedstock;
- Figure 3: as figure 2 but further including recycling of excess methanol;
- Figure 4: implementation with only ethene feedstock using hexene as solvent;
- Figure 5: implementation with only ethene feedstock using high-boiling solvent;
- Figure 6: implementation with only ethene feedstock using low-boiling solvent;

Figure 1 shows the simplest embodiment of the process. Ethene C₂ is provided as feedstock. Purity > 95%. In a first oligomerization 1 ethene is oligomerized in the gas phase over a heterogeneous catalyst.

The first oligomerization 1 is effected in the presence of a solid body which comprises at least two components, wherein the first component comprises at least one element selected from Ni, Cr, Fe, Ti which is present in metallic and/or oxidic and/or hydridic form and wherein the second component comprises at least one metal oxide selected from Al₂O₃, SiO₂, TiO₂, ZrO₂.

The first oligomerization 1 forms a first oligomerizate C_2, C_{2+} comprising the oligomers C_{2+} and unconverted ethene C_2 . In a first distillation column a fraction C_2, C_4 comprising the unconverted ethene and the ethene dimers are removed overhead while the olefins having more than four carbon atoms C_{4+} are withdrawn from the bottom of the first distillation column 2.

In a second distillation column 3 the unconverted ethene C_2 is withdrawn overhead, recycled and mixed with freshly provided feed mixture.

10 A C_4 fraction C_4 comprising 1-butene, cis-2-butene and trans-2-butene is withdrawn from the bottom of the second distillation column 3. Thermal separation thereof is readily possible and is effected in a third distillation column 4. Obtained at the top of the third distillation column 4 is a third target fraction 1B comprising the 1-butene.

15 The two 2-butenes remain in the bottom of the third distillation column 4 and are withdrawn there as second intermediate 2B. The second intermediate 2B is subjected to a second oligomerization 5 to generate a second oligomerizate C_8, C_{8+} . This comprises sought-after octenes C_8 , for example di-n-butene, and olefins having more than eight carbon atoms C_{8+} .

20 The second oligomerization 5 is effected in the presence of the solid body which comprises at least two components, wherein the first component comprises at least one element selected from Ni, Cr, Fe, Ti which is present in metallic and/or oxidic and/or hydridic form and wherein the second component comprises at least one metal oxide selected from Al_2O_3 , SiO_2 , TiO_2 , ZrO_2 .

25 The octenes are obtained from the second oligomerizate C_8, C_{8+} as a first target fraction C_8 using a fourth distillation column at the top thereof. In the bottom thereof are the olefins having more than eight carbon atoms C_{8+} which are discharged from the process as high boilers.

30 Back to the first distillation column 2, at the bottom of which are the olefins having more than four carbon atoms C_{4+} which were formed in the ethene oligomerization 1. This includes a C_6 fraction C_6 which comprises at least 1-hexene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene and also 2-hexene, 3-hexene and 2-ethyl-1-butene. The C_6 fraction C_6 is obtained at the top of a fifth distillation column 7 and then subjected to an etherification 8.

35 The etherification is effected with methanol MeOH over an acidic ion exchange resin. In the etherification 8, 2-ethyl-1-butene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene are selectively reacted with the methanol to afford 3-methyl-3-methoxypentane. This ether is also known as methyl tert-hexyl ether (MTHxE). The first reaction mixture 1H, 2H, 3H, MTHxE withdrawn from the etherification 8 comprises not only MTHxE but also unconverted 1-hexene 1H and also 2-hexene

2H and 3-hexene 3H. This is because these linear hexenes 1H, 2H, 3H are not etherified to afford MTHxE.

By contrast, the branched C₆ olefins 2-ethyl-1-butene 2EB and also 3-methyl-cis-2-pentene and 3-methyl-trans-2-pentene 3MP are bound in the ether and can be withdrawn from the bottom of a sixth distillation column 9 as high-boiling ether fraction MTHxE.

According to the invention the ether fraction MTHxE is then retrocleaved to afford a mixture comprising 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene, 2-ethyl-1-butene and methanol which is described here as cleavage product MeOH, 2EB, 3MP.

The cleavage reaction 10 of the MTHxE is the reverse reaction of the etherification 8 and is effected in the gas phase over a solid catalyst comprising silicon dioxide, aluminum oxide and magnesium oxide. Since the ether fraction MTHxE is withdrawn from the bottom of the sixth distillation column 9 in liquid form an evaporation (not shown here) is first required.

The cleavage product MeOH, 2EB, 3MP is then separated in a seventh distillation column 11 into the alcohol MeOH and into a first intermediate 2EB, 3MP comprising the branched C₆ olefins 2-ethyl-1-butene, 3-methyl-cis-2-pentene and 3-methyl-trans-2-pentene.

The alcohol MeOH is recycled into the etherification 8 and thus fully reused.

The first intermediate 2EB, 3MP is reacted with ethene C₂ in a separate reactor 12 according to the teaching of the invention. This forms a second reaction mixture C₈, C₈₊ comprising olefins having at least eight carbon atoms. In this way the undesired branched C₆ olefins 2EB and 3MP are converted into sought-after octenes C₈.

The reaction in the reactor 12 is effected in the presence of the same catalyst that is also employed in the first oligomerization 1 and the second oligomerization 5.

Since the second reaction mixture C₈, C₈₊ is similar in composition to the second oligomerizate C₈, C₈₊ obtained from the second oligomerization 5 and the bottoms product C₆₊ from the fifth distillation column 7 these three fractions are mixed and worked up together in the fourth distillation column 6.

To enhance the yield of 1-hexene the plant shown in figure 1 features an isomerization 13 capable of converting 2-hexene and 3-hexene into 1-hexene. This is achieved over a heterogeneous catalyst comprising at least one of the oxides MgO, CaO, BaO, Li₂O, SrO as catalytically active material.

The isomerization 13 is arranged in the bottoms circuit of an eighth distillation column 14, at the top of which the first target fraction 1H is withdrawn with the 1-hexene. The eighth distillation column 14 is fed with the tops fraction from the sixth distillation column 9 comprising the linear hexanes 1H, 2H, 3H and with the 1-hexene obtained from the isomerization 13. Since the isomerization 13 is effected in the gas phase the bottoms circuit of the eighth distillation column 14 requires an evaporator upstream of the isomerization 13 (not shown in the figure).

The embodiment of the process shown in figure 2 is characterized in that the feedstock mixture comprises not only ethene C_2 but also olefins having four carbon atoms C_4 , in particular 1-butene, cis-2-butene and trans-2-butene. Before the first oligomerization 1, these feedstocks are mixed such that the ethene is fully dissolved in the butene. The first oligomerization 1 then takes place in the liquid phase. The reaction is controlled such that the ethene is fully converted so that no separate removal of unconverted ethene is required. In case of traces of unconverted ethylene these may be discharged via the offgas stream from distillation column 2. The C_4 fraction C_4 is thus directly obtained at the top of the first distillation column 2. The remaining process steps are identical to that in figure 1.

The embodiment shown in figure 3 differs from the process shown in figure 2 by a ninth distillation column 15. Said column is used to remove methanol MeOH unconverted in the etherification 8 from the first reaction mixture and recycle it into the etherification 8. This is necessary in particular when methanol is fed into the etherification in superstoichiometric amounts.

Figure 4 shows an embodiment where a part of the C_6 fraction C_6 obtained at the top of the fifth distillation column 7 is diverted and together with the ethene C_2 is sent to the first oligomerization 1. The other part of the C_6 fraction is sent to the etherification 8. The recycled C_6 olefin mixture C_6 serves as solvent for the ethene C_2 so that the first oligomerization 1 may be performed in the liquid phase. The ethene is dissolved in the liquid C_6 olefin. Since the C_6 olefin is reactive in the oligomerization correspondingly more C_8 is formed. As a result the yield of hexene 1H is reduced. The advantage of this process variant is that it requires solely ethene as the feedstock since the reactive solvent C_6 is formed internally in the process. By contrast, in the process shown in figure 3 the reactive solvent C_4 needs to be supplied from outside as a feedstock.

Figures 5 and 6 each show a process variant employing an inert solvent SOLV which is recirculated and therefore likewise need not be supplied from outside.

In figure 5 an inert solvent SOLV that is high-boiling compared to butenes, such as n-heptane or n-hexane, is used. Ethene C_2 is fully dissolved therein and the first oligomerization 1 is therefore effected in the liquid phase. Since the solvent SOLV exhibits inert behaviour it is not converted and

ends up in the first oligomerizate C_4 , SOLV, C_{4+} . In the first distillation column 2 it ends up in the bottoms since it has a higher boiling point than the C_4 -olefins C_4 which go overhead in the first column 2. In order to separate the solvent SOLV from the olefins having more than four carbon atoms C_{4+} a tenth distillation column 16 is provided. Said column separates the solvent overhead so that it may be fully recovered and fresh ethene C_2 may be dissolved therein. The olefins having more than four carbon atoms C_{4+} are withdrawn from the bottom of the tenth distillation column 16 and as in the other embodiments sent to the fifth distillation column 7.

In figure 6 an inert solvent SOLV that is low-boiling compared to butenes, such as propane or isobutane, is used. Ethene C_2 is fully dissolved therein and the first oligomerization 1 is therefore effected in the liquid phase. Since the solvent SOLV exhibits inert behaviour it is not converted and ends up in the first oligomerizate C_4 , SOLV, C_4 , C_{4+} . Since it is lower-boiling than the C_4 olefins C_4 the tenth distillation column 16 is arranged directly downstream of the first oligomerization 1. Therein, the solvent SOLV is removed overhead and recycled. The bottoms from the tenth distillation column 16 are sent to the first distillation column 2 and worked up therein in the same way as in the other embodiments.

Finally, the arrangement of the first distillation column 1 and the tenth distillation column 16 is reversed in the embodiments in figures 5 and 6 since the solvent boils at a temperature higher in one case (figure 5) and lower in the other case (figure 6) than the butenes.

List of reference symbols

	1	first oligomerization
	2	first distillation column
5	3	second distillation column
	4	third distillation column
	5	second oligomerization
	6	fourth distillation column
	7	fifth distillation column
10	8	etherification
	9	sixth distillation column
	10	cleavage reaction
	11	seventh distillation column
	12	reactor
15	13	isomerization
	14	eighth distillation column
	15	ninth distillation column
	16	tenth distillation column
	C ₂	ethene (feedstock mixture)
20	C ₂₊	olefins having more than two carbon atoms
	C ₄	C ₄ fraction comprising olefins having four carbon atoms
	C ₄₊	olefins having more than four carbon atoms
	C ₂ , C ₂₊	first oligomerizate
	C ₆ :	C ₆ fraction comprising olefins having six carbon atoms
25	C ₆₊	C ₆₊ fraction comprising olefins having more than six carbon atoms
	C ₈ :	octene (second target fraction)
	C ₈₊	C ₈₊ fraction comprising olefins having more than six carbon atoms
	C ₈ , C ₈₊	second oligomerizate, second reaction mixture
	1B	1-butene (third target fraction)
30	2B	second intermediate comprising cis-2-butene and trans-2-butene
	1H	1-hexene (first target fraction)
	2H	2-hexene
	3H	3-hexene
	MeOH:	methanol
35	MTHxE:	ether fraction comprising 3-methyl-3-methoxypentane
	1H, 2H, 3H, MTHxE	first reaction mixture
	2EB	2-ethyl-1-butene
	3MP	3-methyl-cis-2-pentene and 3-methyl-trans-2-pentene
	MeOH, 2EB, 3MP	cleavage product

2EB, 3MP
SOLV

first intermediate
solvent

Claims

1. Process for producing at least 1-hexene and octene from ethene comprising the steps of:
 - 5 a) providing a feedstock mixture comprising ethene;
 - b) subjecting the ethene to a first oligomerization to obtain a first oligomerizate which comprises olefins having less than six carbon atoms, at least the C₆ olefins 1-hexene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene and olefins having

10 more than six carbon atoms,
 - c) distillative workup of the first oligomerizate to obtain a C₆ fraction which comprises at least 1-hexene, 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene,
 - 15 d) subjecting the C₆ fraction to an etherification by addition of an alcohol in the presence of a heterogeneous catalyst to obtain a first reaction mixture comprising at least 1-hexene and 3-methyl-3-methoxypentane;
 - e) distillative workup of the first reaction mixture to obtain a first target fraction

20 comprising 1-hexene and an ether fraction at least comprising 3-methyl-3-methoxypentane;
 - f) wherein the ether fraction is subjected to a cleavage reaction to obtain a cleavage product which comprises 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene and

25 the alcohol;
 - g) wherein the alcohol is removed from the cleavage product by distillation and reused in the etherification;
 - 30 h) wherein a first intermediate comprising at least 3-methyl-cis-2-pentene, 3-methyl-trans-2-pentene is removed from the cleavage product by distillation;
 - i) wherein the first intermediate is reacted with ethene to obtain a second reaction mixture which comprises olefins having at least eight carbon atoms;

35
 - k) and wherein a second target fraction comprising octene is obtained from the second reaction mixture by distillation.

2. Process according to Claim 1, wherein not only 1-hexene and octene but also 1-butene are produced as follows:
- a) the first oligomerization is performed such that the first oligomerizate further comprises 1-butene, cis-2-butene and trans-2-butene;
 - b) distillative workup of the first oligomerizate affords a C₄ fraction which comprises 1-butene, cis-2-butene and trans-2-butene;
 - c) the C₄ fraction is separated by distillation into a third target fraction comprising 1-butene and into a second intermediate which comprises cis-2-butene and trans-2-butene;
 - d) the second intermediate is subjected to a second oligomerization to obtain a second oligomerizate which comprises olefins having at least eight carbon atoms;
 - e) the second oligomerizate is worked up by distillation together with the second reaction mixture to obtain the second target fraction.
3. Process according to Claim 1, wherein the distillative workup of the first oligomerizate affords a C₆₊ fraction which comprises olefins having more than six carbon atoms and in that the C₆₊ fraction is worked up by distillation together with the second reaction mixture to obtain the second target fraction.
4. Process according to Claim 2, wherein the distillative workup of the first oligomerizate affords a C₆₊ fraction which comprises olefins having more than six carbon atoms and in that the C₆₊ fraction is worked up by distillation together with the second reaction mixture and with the second oligomerizate to obtain the second target fraction.
5. Process according to any of Claims 1 to 4, wherein the feedstock mixture comprises more than 95 wt% of ethene and that the reaction conditions of the first oligomerization are chosen such that the first oligomerization is effected in the gas phase in the presence of a heterogeneous catalyst.
6. Process according to any of Claims 1 to 4, wherein the feedstock mixture comprises less than 25 wt% of ethene, in that the feedstock mixture comprises more than 75 wt% of a solvent, wherein the reaction conditions of the first oligomerization and the concentration of the ethene in the solvent are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the liquid solvent.

- 7 Process according to Claim 5 or 6, wherein ethene unconverted in the first oligomerization is removed by distillation from the first oligomerizate and recycled into the first oligomerization.
- 5
8. Process according to any of Claims 1 to 4, wherein the feedstock mixture comprises not only ethene but also olefins having four carbon atoms, wherein the reaction conditions of the first oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having four carbon atoms.
- 10
9. Process according to any of Claims 1 to 4, wherein the feedstock mixture comprises not only ethene but also olefins having six carbon atoms, wherein the reaction conditions of the first oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having six carbon atoms.
- 15
10. Process according to any of Claims 1 to 4, wherein the feedstock mixture comprises not only ethene but also olefins having four carbon atoms and olefins having six carbon atoms, wherein the reaction conditions of the first oligomerization and the composition of the feedstock mixture are chosen such that the first oligomerization is effected in the liquid phase and the ethene is fully dissolved in the olefins having four and six carbon atoms.
- 20
11. Process according to any of Claims 1 to 10, wherein a solid body comprising at least two components is employed as a heterogeneous catalyst in one or more of the following reactions:
- 25
- in the first oligomerization;
 - in the second oligomerization;
 - in the reaction of the second intermediate with ethene;
- 30
- wherein the first component comprises at least one element selected from Ni, Cr, Fe, Ti which is present in metallic and/or oxidic and/or hydridic form and wherein the second component comprises at least one metal oxide selected from Al_2O_3 , SiO_2 , TiO_2 , ZrO_2 .
12. Process according to Claim 11, wherein the reaction of the second intermediate with ethene is effected in the presence of said catalyst, wherein this reaction is effected at a temperature between 20°C and 150°C and at a pressure between $1 \cdot 10^5$ Pa and $50 \cdot 10^5$ Pa, wherein the quantitative ratio of the ethene to the second intermediate is chosen such that the second intermediate is present in the liquid phase and the ethene is fully dissolved therein.
- 35

13. Process according to any of Claims 1 to 12, wherein the cleavage reaction is effected in the gas phase at a pressure of $1 \cdot 10^5$ Pa to $25 \cdot 10^5$ Pa and a temperature of 130°C to 350°C in the presence of a solid body having the following composition which sums to 100 wt%:
- 5
- silicon dioxide: 61 wt% to 74 wt%;
 - aluminum oxide: 19 wt% to 23 wt%;
 - magnesium oxide: 10 wt% to 12 wt%;
 - sum of other substances: 0 to 10 wt%.
- 10
- 14 Process according to any of Claims 1 to 13, wherein the etherification is effected in the liquid phase at a pressure of $1 \cdot 10^5$ Pa to $7 \cdot 10^5$ Pa and a temperature of 50°C to 130°C in the presence of a polystyrene-divinylbenzene copolymer bearing sulfonic acid groups or carboxylic acid groups.