

SPECIFICATION

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1. Title of the Invention

INK JET HEAD AND MANUFACTURING METHOD THEREOF

2. Background of the Invention

(a) Field of the Invention

The present invention relates to an ink jet head of an important portion of an ink jet recording apparatus, having its drive system of static electricity, for outletting ink drops when a recording is necessary and attaching the drops onto a recording paper face, and a manufacturing method of the ink jet head effectively attaining a purpose of the present invention.

(b) Description of the Prior Art

The ink jet recording apparatus has many merits or advantages, such as very small sound during a recording, high speed printing, high flexibility on ink, and use of low cost plain paper. According to the recent trend, an ink jet recording apparatus of an ink-on-demand system emitting ink drops only when recording is necessary mainly has been employed because it is not necessary to recover ink drops not used to the recording.

According to Patent Laid-Open Publication No. 1990-



51734, the ink jet head of an ink-on-demand has a drive means using a piezoelectric element. According to Patent Laid-Open Publication No. 1986-59911, the ink jet head heats ink and generates bubbles and pressure making ink drops emit.

The conventional ink jet head mentioned above has problems below.

According to the ink jet head using a piezoelectric element, it is necessary to carry out a complicated process of attaching a chip of piezoelectric element to the vibrating plates used to generate pressure in a pressure chamber in a manufacturing process the ink jet head. In particular, the recent ink jet recording apparatus necessitates a printing of a high speed and a high appearance quality. In order to attain the necessity or purpose, it has been necessary to make the ink jet nozzles of a multi-nozzle and a high density of the nozzle necessitating a fine manufacturing of piezoelectric elements and attachment of the fine elements to respective vibrating plates. These processes are very troublesome and time consuming.

In order to make the nozzles of a high density, it has been necessary to manufacture the piezoelectricity elements at the order of several tens micron meter to ten hundreds micron meter. It has been difficult to make dispersion or scattering of printing



quality small as soon as possible by means of the conventional machine processing.

According to the ink heating system above, the drive means is constructed by a thin membrane resistance heater element having no problem of the conventional piezoelectricity element apparatus above. However, the drive means is suffered or damaged by high-speed repetition of heating and cooling and shock of bursting bubbles shortening a lifetime of the ink jet head.

In order to solve such problems of the prior art, the applicant of the present invention filed an application U.S. Application No.757,691 filed Sept. 11, 1991 of an ink jet head recording apparatus using a drive means of the static electricity force. The apparatus has merits of printings of high density, high quality and of a small size and a long lifetime.

However, the ink jet head recording apparatus of the application has problems to be solved in order to still improve such merits above.

The first problem concerns a vibrating plate constituting an ink limiting or discharging chamber, and a gap between the vibrating plate and an electrode for driving the vibrating plate. According to the ink drop emitting system using static electricity, emitting pressure to be generated by the same pressure is very low comparing to that of the jet head of piezoelectric



element. In addition, because generated pressure is proportional to a square of an inverse number of the gap distance, it is necessary, in order to prevent printing quality from scattering, to hold the size of gap in the predetermined range with a very high precision.

The second problem concerns size precision of the vibrating plate. Emitting pressure is proportional to a cube of the thickness of the vibrating plate. When a square-shaped vibrating plate is used, emitting pressure is proportional to fifth power of an inverse number of the short side length of the square-shaped vibrating plate, thereby even small scattering or variations of the size of the vibrating plate affects an ink emitting characteristic very much.

The third problem concerns a head manufacturing method for realizing or attaining a size precision of the high precised gap and the vibrating plate mentioned above. An anode bonding method has been used to joint the substrates of such kind to each other. According to the anode connecting method, a boro-silicated gas substrate is connected to a cathode side, and a silicon substrate provided with nozzles and the vibrating plate is connected to an anode side and a 500V voltage is impressed to them at a temperature  $300^{\circ}\text{C}$ . At the temperature of  $300^{\circ}\text{C}$ , Na ions contained in the boro-silicated glass move to cathode side by an electric field, thereby a very strong static electricity



attractive force is generated between the boro-silicated glass and the silicon and they are contacted. However, through a space between the electrode and the vibrating plate, a large current instantly flows due to dielectric break of gas and electric field. Then there are possibility as that the electrode melts and the melt is attached to the vibrating plate generating a short circuit. In addition, when they are connected by an anode process, they are connected with a very high voltage comparing to that when the ink jet head is driven. Accordingly, the vibrating plate is fixed through its circumference after it is deformed due to the electric field generated while an anode connecting. As a result, remaining stress is generated changing natural frequency of respective vibrating plates and, consequently, an ink emitting characteristic, or the dielectric membrane material on the electrode is pulled along the direction of vibrating plate due to static electricity attractive force resulting in a peeling-off of the dielectric membrane from the electrode.

### 3. Summary of the Invention

Consequently, it is the purpose of the present invention to provide a manufacturing method of an ink jet head using static electricity power, which head having a high precision gap holding means for adjusting a gap size between the electrode and the vibrating plate



in order to obtain a stable and high quality of printing, and being driven with a low drive voltage.

It is another purpose of the present invention to provide an ink jet head and a manufacturing method thereof, wherein the gap portion and the vibrating plate of the head have very high size precision, thereby it is possible to attain a compact and high density mechanism.

It is still another purpose of the present invention to provide an ink jet head of a printer, wherein a prohibition or sealing means between the gap portion and the outside is provided in order to keep the size precision of the gap portion and prevent dust from entering the gap portion.

According to the ink jet head of the present invention, it has a single or plural nozzle holes for emitting ink drops, an emitting chamber led to respective nozzle holes, a vibrating plate constituting at least one wall of the emitting chamber, a drive means for generating a deformation in the vibrating plate, wherein the drive means consists of an electrode for deforming the vibrating plate by static electricity force.

Further an opposing obstacle between the vibrating plate and the electrode is made  $0.05\text{ }\mu\text{m}$  or more than  $0.05\text{ }\mu\text{m}$ , and  $2.0\text{ }\mu\text{m}$  or less than  $2.0\text{ }\mu\text{m}$ .

Additionally, the opposing distance holding means of the ink jet head of the present invention is a dent



for a vibrating chamber forced on the first substrate of the vibrating plate, or another dent for electrode mounting, which is formed in the second substrate of the electrode, or both dents.

According to another mode or embodiment of the present invention, the first substrate and the second substrate, respectively are mono-crystal silicon substrates, and a  $\text{SiO}_2$  membrane formed on at least one face of the connecting portion of both substrates constitutes a holding means for the opposing gap or distance.

It is possible to make the  $\text{SiO}_2$  membrane by thermal oxidized membrane of silicon, or the  $\text{SiO}_2$  membrane can be produced by sputtering process a sintering process of inorganic silicon compound, or a CVD process vaporizing process, Sol-Gel process, thermal oxidation process or others. The electrode is formed by p-type or n-type impurities.

According to still another embodiment of the present invention, the electrode is covered by a dielectric membrane with a gap formed between the electrode and the vibrating plate.

According to the preferable mode of the manufacturing method of the ink jet head of the present invention, the method comprises at least one of the steps of pattern-forming of  $\text{SiO}_2$  membrane of a predetermined thickness on the connecting face of the



first silicon substrate forming the vibrating plate excepting its part for the vibrating plate, and of pattern-forming of  $\text{SiO}_2$  membrane of a predetermined thickness on the connecting face of the second silicon substrate forming the electrode excepting its part for the electrode, and of anode connecting the first and the second silicon substrates through the  $\text{SiO}$  membrane by means of a Si direct connecting process.

According to another embodiment of the ink jet head manufacturing method of the present invention, the method has a vibrating plate forming step carried by an alkali anisotropy etching to be done on the first silicon substrate, and a step for manufacturing the electrode consisting of p-type or n-type impurities by carrying out a doping on the second silicon substrate.

According to still another embodiment of the ink jet head of the present invention, the ink jet head has the second electrode integrally formed in the vibrating plate so as to keep the gap between the opposing distance or parts. The second electrode is formed with p-type or n-type impurities.

According to another embodiment of the ink jet head of the present invention, the gap distance holding means of the head is a gap spacer formed by a boro-silicated glass membrane previously formed on at least one face of the connecting portion of the first and the second substrates. The boro-silicated glass membrane is



produced by a sputtering process.

According to still another embodiment of the ink jet head of the present invention, the vibrating plate is formed by a n-type impurities layer or a high density p-type impurities layer. A driving wiring layer containing the second electrode is formed by a high density p-type impurities layer.

According to still another embodiment of the ink jet head of the present invention, the first substrate is a silicon substrate of crystal face direction (110) and made by epitaxially growing a n-type impurities layer on a p-type silicon substrate.

Another embodiment of the ink jet manufacturing method has a step of forming a n-type impurity layer on a p-type silicon substrate, and a step of forming the vibrating plate by carrying out an electric chemical anisotropy etching process on the silicon substrate.

According to still another embodiment of the ink jet head manufacturing method of the present invention, the anode bonding method for bonding the first substrate having the vibrating plate formed thereon to the second substrate having the electrode formed thereon so as to drive the vibrating plate has a step for controlling in a manner that a voltage difference between the vibrating plate and the electrode when the anode bonding process is done. A potential of the electrode is made identical with that of the vibrating plate.



According to still another embodiment of the ink jet head manufacturing method of the present invention, the anode bonding process for anode bonding the first substrate having the vibrating plate formed thereon and the second substrate having the electrode driving the vibrating plate comprises a step for forming a common electrode adapted to be connected to respective electrode on the second substrate, a step for controlling or decreasing a potential between the vibrating plate and the common electrode when these first and second substrates are anode-connected, and a step for separating the common electrode from the electrode driving the vibrating plate after the anode-connecting process.

According to another embodiment of the ink jet head of the present invention, the gap between the vibrating plate and the electrode has a passage led to the outside before the first substrate provided with the vibrating plate formed thereon and the second substrate provided with the electrode are anode bonding and the outlet of the passage is sealed by the sealing member after the anode connection process is done.

According to still another embodiment of the ink jet head of the present invention, the opposed distance holding mean is a photo-sensitive resin layer or adhesive agent layer of a pattern around the electrode.

According to the ink jet head of the present



invention, impressing a pulse voltage to the electrode functions static electricity attractive force or repelling force between the electrode and the vibrating plate opposed to the electrode, deforming the vibrating plate and emitting ink drops through the nozzle holes. Because of a restriction of the opposed gap or distance between the vibrating plate and the electrode, it is possible to drive the ink jet head with a low voltage, and emitting speed and emitting volume of ink drops are stable attaining very high quality of printing.

It is of course that the gap length or distance of the opposed gap is confirmed by experiments. The reasons why the gap length is  $0.05\text{ }\mu\text{m}$  or more than  $0.05\text{ }\mu\text{m}$  are the volume of emitted ink drop is not enough to print a letter when the length is less than  $0.05\text{ }\mu\text{m}$ , and the vibrating plate contact with the electrode breaking the electrode.

The reason why the gap length is  $2.0\text{ }\mu\text{m}$  or less than that is caused by driving voltage. If the length is more than  $2.0\text{ }\mu\text{m}$ , it is impossible to attain substantive high capacity of the ink jet head.

As a means for holding the gap length restricted as described above, there are a dent for the vibrating chamber, a dent for mounting the electrode,  $\text{SiO}_2$  membrane formed on the connecting face of the substrate to be connected, boro-silicated glass membrane, or photo-sensitive resin layer or adhesive



agent layer. The necessary gap length is held by these dents or membranes.

In particular, SiO membrane or boro-silicated glass membrane is used, it is possible to control the thickness the membrane with a high precision and to equalize the vibration characteristic of the vibrating plate resulting accordingly in a uniformed quality of printing.

Also, because of the second electrode is integrally formed on the vibrating plate, electric resistance of the second electrode lowers improving driving frequency of the ink jet head of the present invention and resulting in a high speed printing.

Still also, when the first substrate forming the vibrating plate is formed by a silicon substrate of crystal face direction (110), it is possible to make a wall face of the cavity perpendicular to the face of the silicon substrate due to an etching the miniaturize the pitch distance of the nozzles, and to attain a small and high density of the ink jet head.

Due to the fact that the vibrating plate is made of a high density p-type impurity layer, it is possible to improve the driving frequency and crosstalk of the ink jet head.

Additionally, when the potential between the vibrating plate and the electrode is controlled to lower, for example to equalize both potentials of them



during an anode connection between the first substrate provided with the vibrating plate formed thereon and the second substrate provided with the electrode formed thereon being anode bonded, it is possible to prevent discharging between the vibrating plate and the electrode or dispersion of electric field when they are anode bonded and peeling-off of the dielectric membrane due to static electricity attractive force.

As a result, generation of electrode melting and remaining stress of the vibrating plate is fortunately prohibited from happening.

Due to a formation of the passage on the gap portion between the vibrating plate and the electrode so as to lead to the outside, it is possible to prevent pressure in the gap space owing to heating process of the anode-connection from rising, keep the gap length at the predetermined one, and prevent a generation of remaining stress in the vibrating plate and a contact between the vibrating plate and electrode. In addition, the outlet of the passage is sealed by the sealing member after the anode-connection process is done and the temperature of the whole construction of the ink jet head lowers to a room temperature preventing dust from invading into the gap space.

#### 4. Brief Description of the Drawings

Fig. 1 is an exploded perspective view of the first



embodiment of the ink jet head according to the present invention;

Fig. 2 is a sectional side elevation of the first embodiment;

Fig. 3 is a A-A view of Fig.1;

Fig. 4 is an exploded perspective view of the second embodiment of the ink jet head according to the present invention;

Fig. 5 is a sectional side elevation of the second embodiment;

Fig. 6 is a B-B view of Fig. 5;

Fig. 7 is an exploded perspective view of the third embodiment of the ink jet head according to the present invention;

Fig. 8 is an enlarged perspective view of a part of the third embodiment of the present invention;

Fig. 9 is a manufacturing step diagram of the first substrate of the third embodiment;

Fig. 10 is a view showing a measurement of a part of the vibrating plate of the third embodiment according to the present invention;

Fig. 11 is a manufacturing step diagram of the second substrate of the third embodiment;

Fig. 12 is a perspective view of the first substrate of the fourth embodiment of the ink jet head according to the present invention;

Fig. 13 is a manufacturing step diagram of the



first substrate of the fourth embodiment;

Fig. 14 is an exploded perspective view of the ink jet head according to the fifth embodiment of the present invention;

Fig. 15 is a manufacturing step diagram of the first substrate according to the fifth embodiment;

Fig. 16 is a perspective view of the first substrate of the ink jet head according to the sixth embodiment of the present invention; Fig. 17 is a manufacturing step diagram of the first substrate according to the sixth embodiment of the present invention; Fig. 18 is a view showing an electric-chemical anisotropic etching process to the sixth embodiment; Fig. 19 is a perspective view of the first substrate of the ink jet head according to the seventh embodiment of the present invention; Fig. 20 is a manufacturing step diagram of the first substrate of the seventh embodiment; Fig. 21 is a perspective view of the first substrate of the ink jet head according to the eighth embodiment of the present invention; Fig. 22 is a manufacturing step diagram of the first substrate according to the eighth embodiment; Fig. 23 is a relationship view of boron density and etching rate at an alkali anisotropic etching process; Fig. 24 is a sectional view of an embodiment of an anode connecting apparatus used in the anode connecting process of the present invention; Fig. 25 is a plan view of the anode



connecting apparatus above; Fig 26 is a sectional view of another embodiment of the anode connecting apparatus used in the anode connecting process according to the present invention; Fig. 27 is a plan view of the anode connecting apparatus shown in Fig. 26; Fig. 28 is a plan view of still another embodiment of the anode connecting apparatus used to the anode connecting process according to the present invention; Fig. 29 is a plan view of the second substrate shown in Fig. 28; Fig. 30 is a sectional view showing still another embodiment of the anode connecting apparatus used to the anode connecting process of the present invention; Fig. 31 is a sectional view of another embodiment of a dust prohibition method of the present invention; Fig. 32 is a plan view of the embodiment shown in Fig. 31; Fig. 33 is a sectional view of another embodiment of the dust prohibition of the present invention; Fig. 34 is a sectional view showing another embodiment of the distance holding means according to the present invention; and Fig. 35 is schematic diagram of the printer with the ink jet head of the first embodiment of the present invention.

#### 5. Detailed Explanation of the preferred Embodiments

Hereinafter, the preferred embodiments of the ink



jet head of the present invention will be explained with reference to the accompanying drawings.

(Embodiment 1)

Fig. 1 is an exploded perspective view showing the ink head according to the first embodiment of the present invention and a part of the head is shown in a section. The first embodiment is the ink jet head of an edge ink jet type wherein ink drops emit through a nozzle hole formed at an end portion of the substrate. Fig. 2 is a sectional elevation of the whole structure of the assembled ink jet head, and Fig. 3 is a section along the arrows A-A of Fig. 2. The ink jet head 10 of the embodiment has a laminated structure of three substrates 1, 2 and 3, respectively have a construction as described below.

The first middle substrate 1 is of a silicon one and has a plurality of nozzle grooves 11 placed at an end of the face of the substrate 1 and at a regular interval in parallel to each other ending with plurality of nozzle holes 4, a plurality of dents or concave portions 12 constituting emitting chambers 6 respectively led to each nozzle grooves 11 and having their bottom walls of the vibrating plates 5, a plurality of their grooves 13 of ink flowing inlets constituting orifices 7 at rear portions of the concave portions 12, and a dent or concave portion 14 of a



common ink cavity 8 for supplying ink to respective emitting chambers 6. Also, there are dents 15 on the lower portions of the vibrating plates 5, which dents constituting vibrating chambers 9. Electrodes are mounted in the vibrating chambers 9 as described below.

In the embodiment of the ink jet head of the present invention, a distance holding means is constituted by the dents 15 used as vibrating chambers formed on the bottom face of the first substrate 1 in order to make the opposed distance between the vibrating plate 5 and an electrode oppositely placed to the plate, or a length of the gap portion (see Fig 2, hereinafter referred to as gap length) identical with a difference between a depth of the dent 15 and a thickness of the electrode. According to the embodiment, the dent 15 is etched to have a depth of  $0.6\mu\text{m}$ . A pitch of the nozzle grooves 11 is  $0.72\text{mm}$  and a width of the nozzle groove 11 is  $70\mu\text{m}$ .

The second substrate 2 attached to the bottom face of the first substrate 1 is made of (boro-silicated glass) and these attached substrates 1 and 2 constitute a vibrating chamber 9. At respective positions of the second substrate 2 corresponding to respective vibrating plates 5, gold of a pattern similar to the shape of the vibrating plate is spatted with a thickness of  $0.1\mu\text{m}$  in order to obtain a golden pattern of a shape almost identical with that of the vibrating plate



5. It is an electrode 21 having a lead 22 and a terminal 23. A boro-silicated glass spattering film covers the second substrate 2 excepting the electrode terminals 23 with a thickness of  $0.2\mu\text{m}$ . It is a dielectric layer 24 preventing dielectric breaks and short circuits when the ink jet head is driven. The dielectric layer 24 may consist of silicone compound.

The third substrate 3 attached to an upper face of the first substrate 1 is made of boro-silicated glass identical with that of the second substrate 2. Combining the third substrate 3 forms the nozzle hole 4, the emitting chamber 6, the orifice 7, and the ink cavity 8. The substrate 3 has an ink supply opening 31 led to the ink cavity 8. The ink supply opening 31 is connected to an ink tank (not shown) through a connecting pipe 32 and a tube 33.

Next, the first substrate 1 and the second substrate 21 are anode bonding by impressing a voltage of 500V at a temperature  $300^{\circ}\text{C}$  to them. With the same condition above, the first substrate 1 and the third substrate 3 are connected and the ink jet head shown in Fig. 2 is assembled. After an anode bonding, a difference between the depth of the dent 15 and the thickness of the electrode 21 is the gap length between the vibrating plate 5 and an electrode 21 on the second substrate 2 is made  $0.5\mu\text{m}$ . A space distance G1 between the vibrating plate 5 and the dielectric layer 24 on the electrode 21 is made  $0.3\mu\text{m}$ .



After the ink jet head is assembled as described above, oscillation circuit 102 is connected between the substrate 1 and a terminal 23 of the electrode 21 through a wire 101 in order to form an ink jet recording apparatus. Ink 103 is supplied to an interior of the substrate 1 from an ink tank (not shown) through the ink supply port 31 and the ink cavity 8 and the emitting chamber 6, etc. are filled with ink.

In Fig. 2, an ink drop 104 is emitted from the nozzle hole 4 onto a recording paper 105.

An operation of the ink jet head constructed as described above according to the present invention will be explained. First, pulse voltage of 0V to 70V is impressed to the electrode 21 by the oscillation circuit 102 and a surface of the electrode 21 is charged plus or positive. Then, a lower face of the opposed vibrating plate 5 is charged negative. As a result, the vibrating plate 5 bends downward by sucking effect of static electricity. Next, the electrode 21 is made off, the vibrating plate 5 returns to its original position. Thus, pressure in the emitting chamber 6 abruptly rises and an ink drop 104 is emitted onto the recording paper 105 through the nozzle hole 4. Then, the vibrating plate 5 again bends downward and ink 103 is supplied to the emitting chamber 6 from the ink cavity 8 through the orifice 7.

According to experiments carried by the inventor,



the ink jet head 10 of the present invention is assembled to a printer as shown at Fig. 35, 5 KHz drive power flies ink drops with a speed 7m/sec onto the recording paper. Resulting printing efficiency was very good with such low voltage for driving or flying ink drops, in Fig. 35, numeral 300 is a platen, 301 is a ink tank, and 302 is a carriage of the ink head 10. When the gap length between the vibrating plate 5 and the electrode 21 is 2.5  $\mu\text{m}$ , drive voltage was unpractically more than 250V.

(Embodiment 2)

Fig. 4 is an exploded perspective view of the ink jet head according to the second embodiment of the present invention and a part of the ink jet head is shown by breaking in section. The ink jet head shown is of a face ink jet type having nozzle holes formed at a face portion of a substrate, through which holes ink drops emit. Fig. 5 shows a sectional side elevation of the whole construction of an assembled ink jet head according to the present invention and Fig. 6 shows a sectional view taken along a B-B line in Fig. 2. Hereinafter, the part or members of the ink jet head identical with or similar to that of the embodiment 1 will be explained with the identical reference numbers of the embodiment 1.

The ink jet head 10 of the second embodiment is



adapted to emit ink drops through the nozzle holes 4 formed in a face of the third substrate 3.

The first substrate 1 of this second embodiment is made of a silicon of crystal face direction (110) of a thickness 380  $\mu\text{m}$ . The bottom wall of the dent 12 constituting the emitting chamber 6 is a vibrating plate 5 of a thickness 3 $\mu\text{m}$ . There is no dent of the vibrating chamber of the first embodiment at the lower portion of the vibrating plate 5, instead the lower face of the vibrating chamber 5 of the second embodiment is a flat and smooth face polished or finished as a mirror.

The second substrate 2 attached to the bottom face of the first substrate 1 is made of Boro-Silicated glass as that of the first embodiment. The gap length G is formed on the second substrate by a dent 25 formed by an etching process of 0.5  $\mu\text{m}$  in order to mount the electrode 21. The dent 25 is made in a pattern larger a little than a shape of the electrode in order to mount the electrode 21, lead 22, terminal 23 in the dent 25. The electrode 21 is made by spattering ITO of 0.1 $\mu\text{m}$  thickness in the dent 25 to form ITO pattern, and gold used to bondings are spattered only on the terminal 23. Except for the electrode terminal 23, Boro-Silicated glass spatter film is covered on a whole surface with a thickness 0.1  $\mu\text{m}$  making a dielectric layer 24. In Fig. 4, the dielectric layer 24 is drawn as a flat



shape. In fact, the dielectric layer 24 has dents 25 formed in the flat surface.

Consequently, according to the second embodiment, the gap length is  $0.4\mu\text{m}$  and the space distance G1 is  $0.3\mu\text{m}$  after an anodic bonding.

The third substrate 3 attached to the top face of the first substrate 1 is made of SUS plate of a thickness  $100\mu\text{m}$ . On the face of the third substrate 3, there are nozzle holes 4 respectively led to the dent 12 of the emitting chambers. The ink supply port 31 is formed so as to be led to the dent or concave 14 of the ink cavity.

When the ink jet head 10 of the third embodiment is used and a plate voltage of 0V to 100V is impressed from the oscillation circuit 102 to the electrode 21, a good printing efficiency corresponding to that of the first embodiment is obtained. When the ink jet head provided with a gap length G of  $2.3\mu\text{m}$  is used, the driving voltage becomes more than 250V, thereby the ink jet head is not practical in the printer.

(Embodiment 3)

Fig. 7 shows an exploded perspective view of the ink jet head according to the third embodiment of the present invention and a part of the head is shown in section. Fig. 8 is an enlarged perspective view of a part of the ink jet head.



According to the third embodiment of the ink jet head, the gap length holding means is formed by  $\text{SiO}_2$  membranes 41 and 42, respectively and previously formed at the space between the first substrate 1 and the second substrate 2. These  $\text{SiO}_2$  membranes 41 and 42 function as gap spacers. The first substrate 1 is made of a single crystal silicon wafer of a crystal face direction (100). On the bottom face of the wafer except a part corresponding to the vibrating plate 5, the  $\text{SiO}_2$  membrane 41 of, for example, a thickness  $0.3 \mu\text{m}$  is formed. Similarly, the second substrate 2 is made of a single crystal silicon wafer of a crystal face direction (100).  $\text{SiO}_2$  membrane 42 of, for example,  $0.2 \mu\text{m}$  is formed on the upper face of the second substrate 2 except the electrode 21.

As a result, the gap length between these substrates 1 and 2 becomes  $0.5 \mu\text{m}$  (see Fig. 8).

Fig. 9 shows the manufacturing steps of the first substrate according to the third embodiment of the present invention.

First, both faces of the silicon wafer of a crystal face direction (100) are mirror-polished in order to make a silicon substrate 51 of a thickness  $200 \mu\text{m}$  (see Fig. 9(a)). The silicon substrate 51 is treated with thermal oxidization treatment in oxygen and steam atmosphere of a temperature  $1100^\circ\text{C}$  for 4 hours in order to form a  $\text{SiO}_2$  membranes 41a and 41b of a



thickness 1  $\mu\text{m}$  on both the faces of the silicon substrate 51 (see Fig. 9(b)).  $\text{SiO}_2$  membranes 41a and 41b function as an anti-etching material.

Next, on the upper face of the  $\text{SiO}_2$  membrane 41a, a photo-resist pattern (not shown) having a pattern of nozzle 4, emitting chamber 6, orifice 7 and ink cavity 8 is formed. The exposed portion of the  $\text{SiO}_2$  membrane 41a is etched by fluoric acid etching agent and the photo-resist pattern is removed (see Fig. 9(c)).

Next, the silicon substrate 51 is anisotropy-etched by alkali agent. When single crystal silicon is etched by alkali, such as potassium hydroxide solution and hydrazine, etc. as well known, difference between etching speeds on various crystal faces of the single crystal silicon is large, thereby it is possible to carry out anisotropy etching on them. In practical, because the etching speed of (111) crystal face is the least or the lowest, the crystal face (111) is remained after the etching process is finished.

According to the third embodiment, caustic potash solution containing isopropyl alcohol is used in the etching treatment. Because mechanical deformation characteristics of the vibrating plate is determined by each size or measurement of the vibrating plate, the design size of every part of the vibrating plate is determined with reference to ink emitting characteristics necessary to the ink jet head of the



present invention. According to the third embodiment, a width  $h$  of the vibrating plate 5 is  $500\text{ }\mu\text{m}$  and its thickness is  $30\text{ }\mu\text{m}$  (see Fig. 10).

In the silicon substrate 51 of (11) face direction, (111) face crosses structurally with (100) face of the substrate at an angle of about  $55^\circ$ , so that when the sizes of the vibrating plate to be formed in the silicon substrate of (100) face direction are determined, the mask pattern size of anti-etching material is primarily determined with reference to the thickness of the first substrate. As shown in Fig. 10, the width  $d$  of the top opening of the emitting chamber 6 is determined  $740\text{ }\mu\text{m}$  and an etching treatment of  $170\text{ }\mu\text{m}$  width is done, so that the vibrating plate 5 of a width  $h$  of  $500\text{ }\mu\text{m}$  and a thickness  $t$  of  $30\text{ }\mu\text{m}$  is obtained. In a practical etching process, (111) face is a little etched or undercut and the size  $d$  shown in Fig. 10 becomes a little larger than the mask pattern width  $d_1$ . Consequently, it is necessary to make the mask pattern width  $d_1$  small by a part corresponding to that of (111) face 12a undercut, so that it is  $730\text{ }\mu\text{m}$  in the third embodiment of the present invention and the predetermined length ( $170\text{ }\mu\text{m}$ ) is etched by alkali etching solution (see Fig. 9(d)).

Next,  $\text{SiO}_2$  membrane 41b on the bottom face of the silicon substrate 51 is patterned. The thickness of the  $\text{SiO}_2$  membrane 41b was  $1\text{ }\mu\text{m}$  at the stage Fig. 9(b).



In an alkali anisotropy etching process shown in Fig. 9(d), the  $\text{SiO}_2$  membrane 41b is etched by alkali solution and its thickness decreased to  $0.3 \mu\text{m}$ . According to the third embodiment, an etching rate of the  $\text{SiO}_2$  membrane is very small, so a reproductivity of decrease in a thickness of the  $\text{SiO}_2$  membrane 41b is good and uniform.

Next, a photo-resist pattern (not shown) of a shape corresponding to the vibrating plate 5 is formed on the  $\text{SiO}_2$  membrane 41b(41), the exposed portion of the  $\text{SiO}_2$  membrane 41b is etched by fluoric acid etching solution so as to remove the photo-resist pattern. Simultaneously, all material of the  $\text{SiO}_2$  membrane 41a remained on the upper face of the substrate 51 is removed (see Fig. 9(e)).

After such steps are finished, the first substrate 1 shown in Fig. 7 is completed.

Next, the manufacturing steps of the second substrate according to the third embodiment of the present invention will be explained with reference to Fig. 11.

First, both the faces of a n-type silicon substrate 52 of (100) face direction are mirror-polished and heat and oxidization treatment is done on the substrate 52 in oxygen and steam atmosphere at  $1100^\circ \text{C}$  for a predetermined time in order to form the  $\text{SiO}_2$  membranes 42a and 42b on both the faces of the silicon substrate



52 (see Fig. 11(a)).

Next, a photo-resist pattern (not shown) corresponding to the shape of the electrode 21 is formed on the upper  $\text{SiO}_2$  membrane 42a and the exposed portion of the  $\text{SiO}_2$  membrane 42a is etched by fluororic acid etching solution to remove the photo-resist pattern (see Fig. 11(b)).

In the next step, the exposed Si portion 43 of the silicon substrate 52 is boron-doped. A boron-doping process is shown below. The silicon substrate 52 is held in a quartz tube through a quartz holder, steam with bubbled  $\text{BBr}_3$  of  $\text{N}_2$  carriers is led together with  $\text{O}_2$  into the quartz tube. After the silicon substrate 52 is treated at  $1100^\circ\text{C}$  for a predetermined time, the substrate 52 is lightly etched by fluororic acid etching agent, then driven-in within  $\text{O}_2$ . The exposed part of Si 43 is a p-type layer 44 (see Fig. 11(c)). The p-type layer 44 functions as the electrode 21 as shown in Fig. 7.

In the step of Fig. 11(c), the thickness of the  $\text{SiO}_2$  membranes 42a and 42b on the upper face of the silicon substrate 52 increases, so in the third embodiment the thickness of the  $\text{SiO}_2$  membrane 42a is made to increase to  $0.2\mu\text{m}$ . Next, a photo-resist pattern (not shown) corresponding to the shape of the p-type layer 44 (electrode 21) is formed and the exposed ones of the  $\text{SiO}_2$  membrane 42a are etched by fluororic acid



etching agent removing them (see Fig. 11(d)). Thus, the second substrate 2 shown in Fig. 7 is obtained.

According to the ink jet head of the third embodiment of the present invention, the size of the gap length  $G$  between the vibrating plate 5 and the electrode 21 is determined to  $0.5 \mu\text{m}$  on the basis of an ink emitting characteristic of the ink jet head. Because the thickness of the  $\text{SiO}_2$  membrane 41b of the first substrate 1 is  $0.3 \mu\text{m}$  as mentioned above, the process is carried out so that the thickness of the  $\text{SiO}_2$  membrane 42a in the step of Fig. 11 (c) becomes  $0.2 \mu\text{m}$ .

The substrate 1 and 2 formed according to the steps above are joined by a Si-Si direct connecting method making the head construction as shown enlargely in Fig. 8. The joining steps will be described.

First, the silicon substrate 1 is washed with a mixture of sulfuric acid and hydrogen peroxide of  $100^\circ\text{C}$ , then positions of the corresponding patterns of both the substrates 1 and 2 are matched, and finally they are piled each other. After that, both the substrates 1 and 2 are thermally treated at a temperature of  $1100^\circ\text{C}$  for one hour obtaining firm combination of them.

The sizes of the gap length  $G$  of one hundred ink jet heads manufactured are scattered in  $0.50 \pm 0.05 \mu\text{m}$ . and the thicknesses of the vibrating plates are scattered or distributed in a range of  $30.0 \pm 0.8 \mu\text{m}$ .



When the ink jet heads are driven with 100V and 5 KHz, ink drop emitting speeds are scattered in a range of  $8 \pm 0.5 \text{ } \mu\text{m/sec.}$  and ink drop volumes are distributed in a range of  $(0.1 \pm 0.01) \times 10^{-6} \text{ cc.}$  In a practical printing test of the one hundred ink jet heads, good results of printing are obtained.

According to the third embodiment of the present invention, a gaseous process using  $\text{BBr}_3$  forms a p-type layer and the electrode 21. However, the p-type layer forming method includes ones, such as an ion injection method, a spin-coating method in which coating agent  $\text{B}_2\text{O}_3$  scattered in inorganic solvent is spinned, and other method using a distribution source of BN (Boron nitrogen) plate. It is possible to use other elements in group III, such as Al, Ga in order to form p-type layers.

It is also possible to make the electrode 21 a n-type layer supposing that the silicon substrate 2 is a p-type substrate. In this case, various doping methods are used, that is V group elements such as P, As, Sb and the like are doped making the electrode 21.

According to the third embodiment, the  $\text{SiO}_2$  membranes 41 and 42 form the gap portions. However, because it is possible if anyone of the  $\text{SiO}_2$  membranes is not used to connect both the substrates owing to the principle of Si-Si direct connecting process, one of the membranes 41 and 42 may have the necessary length



of the gap and another membrane may be removed by fluoric acid etching agent in a Si-Si direct connecting process obtaining the gap portion of the same material.

In the third embodiment, the  $\text{SiO}_2$  membrane of the gap spacer is used as an etching mask when an alkali anisotropy etching process is done and the size of the membrane decreases, so that the face condition a little deteriorates while an etching step. When the face deteriorates to a certain degree, once all the  $\text{SiO}_2$  membrane is removed by fluoric acid etching agent and then a thermal oxidization process is used to form  $\text{SiO}_2$  membrane of a necessary thickness obtaining a suitable gap spacer.

In addition, according to the third embodiment, considering the specification of the ink jet head, the gap length is determined temporarily to  $0.5 \mu\text{m}$ . However, because Si thermal oxidized membranes can be manufactured precisely and easily until their thicknesses reach  $1.5 \mu\text{m}$ , only controlling the thickness of the Si thermal oxidized membranes of the gap spacers according to the specification in case that the specified size of the gap length is  $0.05$  to  $2.0 \mu\text{m}$  enables to obtain an ink jet head provided with the gap portion having a precise measurement similar to that of the third embodiment.

(Embodiment 4)



Fig. 12 shows a partly-broken perspective view of the first substrate used to the ink jet head according to the fourth embodiment of the present invention. The second substrate and the third substrate on which electrodes are formed are identical with that of the third embodiment of the present invention and the explanations for them are omitted from the specification.

According to the fourth embodiment of the ink jet head, a second electrode 46 consisting of a p-type or n-type impurity layer is formed on the gap opposed face 45 of the vibrating plate 5 as shown in Fig. 12 in order to improve frequency characteristic of the oscillation circuit or crosstalk when the ink jet head is driven. The gap length G of the fourth embodiment is the space distance between the second electrode 46 and the electrode 21 on the second substrate (see Fig. 7). The distance holding means is constructed by the  $\text{SiO}_2$  membrane 41 formed on the bottom face of the first substrate 1 in a manner described below and the second substrate of the third embodiment. In this case too, it is possible to obtain the gap length G by only one of the  $\text{SiO}_2$  membranes.

The manufacturing steps of the first substrate of the fourth embodiment of the present invention is shown in Fig. 13.

First, both the sides of a silicon wafer of n-type



(100) face direction are mirror-polished to manufacture a silicon substrate 53 of a thickness 200  $\mu\text{m}$  (see Fig. 13(a)), the silicon substrate 53 is thermally oxidization-treated in an oxygen-steam atmosphere at 1100°C for 4 hours in order to form  $\text{SiO}_2$  membranes 41a and 41b of thickness 1  $\mu\text{m}$  on both the faces of the silicon substrate 53 (see Fig. 13b)).

Next, on the lower  $\text{SiO}_2$  membrane 41b, a photo-resist pattern (not shown) corresponding to the shape of the electrode 46 shown in Fig. 12 and a lead (not shown) is formed, and the exposed portion of the  $\text{SiO}_2$  membrane 41b is etched and removed by fluoric acid etching agent in order to remove the photo-resist pattern (see Fig. 13(c)).

At the next stage, the exposed Si portion 47 of the silicon substrate 53 is doped according to the treatment process identical with that of the third embodiment of the present invention in order to form a p-type layer 48. The p-type layer 48 functions as the second electrode 46 (see Fig. 13(d)).

A photo-resist pattern is (not shown) corresponding to the shape of the nozzle holes 4, emitting chambers 6 and the like are formed on the upper  $\text{SiO}_2$  membrane 41a. The exposed portion of the  $\text{SiO}_2$  membrane 41a is etched to remove the photo-resist pattern (see Fig. 13(e)).



The following steps of the manufacturing process are identical with that of the third embodiment of the ink jet head and the  $\text{SiO}_2$  membrane 41b is pattern-treated so as to form the vibrating plate 5, nozzles 4, emitting chambers 6, orifices 7, and ink cavity 8, and gap portion between the vibrating plate 5 and the second substrate (see Fig. 13(e) to (g)).

Similar to that of the third embodiment, various methods can be used to form the electrode 46 and various kinds of dopants can be used to the doping process.

According to the embodiment, respective vibrating plates 5 has respective driving electrodes 46 formed thereon, so it is possible to obtain a high speed driving of the oscillation circuit, or a high printing speed of the ink jet head of the present invention.

According to the third embodiment, the highest driving frequency for forming independently ink drops was 5 KHz, however in the fourth embodiment, the highest driving frequency is 7 KHz. Also, the lead wires for connecting respective electrodes 46 and the oscillation circuit are integrally and simultaneously formed with the electrodes 46 attaining a compact and high speed ink jet head.

(Embodiment 5)

Fig. 14 shows a partly-broken exploded perspective



view of the ink jet head of the fifth embodiment of the present invention. The ink jet head of the fifth embodiment has a structure basically identical with that of the third embodiment shown in Fig. 7 and has a characteristic of thin membrane or film for restricting the distance of the gap formed between the vibrating plate 5 and the electrode 21 when the first substrate 1 and the second substrate 2 are combined is made of borosilicated glass thin membrane 49 and formed on the bottom face of the first substrate 1.

Fig. 5 shows the manufacturing steps of the first substrate according to the fifth embodiment of the present invention.

First, both the faces of silicon wafer of (100) face direction is micro-polished to manufacture a silicon substrate 54 of a thickness 200  $\mu\text{m}$  (see Fig. 15(d)), and the silicon substrate 54 is thermally oxidation-treated in an oxygen and steam atmosphere at 1100°C, for 4 hours in order to form  $\text{SiO}_2$  membranes 41a and 41b of thickness 1  $\mu\text{m}$  on the silicon substrate 54 (see Fig. 15(b)).

Next, a photo-resist pattern (not shown) corresponding to the shapes of nozzle holes 4, emitting chambers 6, etc. is formed on the upper  $\text{SiO}_2$  membrane 41a, and the exposed portion of the  $\text{SiO}_2$  membrane 41a is etched by fluoric acid etching agent in order to remove the photo-resist pattern (see Fig. 15(c)).



An anisotropy etching is carried out on the silicon by using alkali agent. According to the anisotropy etching process described in regard to the third embodiment, the nozzle holes 4 and the emitting chamber 6, etc. are formed and then the  $\text{SiO}_2$  membranes 41a and 42b of anti-etching material are removed by fluoric acid etching magnet (see Fig. 15(d)).

Next, boro-silicated glass thin membrane 49 functioning as a gap spacer precisely restricting the distance between the vibrating plate 5 and the electrode 21 and as a combined layer attached by an anode bonding method is formed on the lower face of the silicon substrate 54.

First, a photo-resist pattern 50 corresponding to a shape of the vibrating plate 5 is formed on the bottom face of the silicon substrate 54 (see Fig. 15(e)). Next, a sputtering apparatus forms a boro-silicated glass thin membrane 49 on the bottom face of the silicon substrate 54 (see Fig. 15(f)), the silicon substrate 54 is sintered in organic solvent, is added with ultrasound vibration in order to remove the photo-resist pattern 50. Consequently, a boro-silicated glass thin membrane 49 of a gap spacer is formed on the portions or places other than that of the vibrating plate 5 as shown in Fig. 15 (g).

The sputtering conditions of the boro-silicated glass thin membrane 49 are shown below.



Corning corporation made #7740 glass is used as a sputtering target, a sputtering atmosphere is 80% Ar - 20% O<sub>2</sub> pressure 5m Torr, and RF power 6W/cm<sup>2</sup> is impressed. Thus, 0.5  $\mu$ m thickness glass thin membrane 49 is obtained.

The second substrate 2 and the third substrate 3 shown in Fig. 14 and used to assemble the ink jet head of the present invention are manufactured by the method of the third embodiment. The first substrate 1 and third substrate 3 are anode bonding or attached integrally by the method of the third embodiment. The vibrating plate 5 formed on the substrate 1 and the electrode 21 formed on the substrate 2 are matched in their positions and they are abutted. Combined substrates 1 and 2 are heated to 300°C on a hot plate, a DC voltage 50V is impressed to them for 10 minutes with the first substrate being plus charged and the second substrate being minus charged.

The ink jet head manufactured according to the fifth embodiment of the present invention is tested in real-printing function and a good result of printing similar to that of the third embodiment is obtained.

According to the fifth embodiment, in order to form the gap portion between the vibrating plate 5 and the electrode 21, a boro-silicated glass thin membrane 49 is formed on the bottom face of the first substrate 1. It is possible to form the boro-silicated glass thin



membrane 49 on the upper face of the second substrate 2 instead of the bottom face of the first substrate 1 obtaining the same effect.

The boro-silicated glass thin membrane is formed by the method of the fifth embodiment on the second substrate 2. In an anode bonding of the first substrate and second substrate, a DC voltage 50V is impressed to them with the first substrate being charged plus electricity and the second substrate being charged minus electricity at a temperature  $300^{\circ}\text{C}$  obtaining the ink jet head of a quality and a performance identical with that of the fifth embodiment.

According to the fifth embodiment, it is possible to bond the first substrate and the second substrate at  $300^{\circ}\text{C}$  obtaining the effects mentioned below.

It is possible to use not only p-type or n-type impurities of the third embodiment but also, for example, a metal membrane or film of Au or Al, etc. having a melting point of several hundreds or  $100^{\circ}\text{C}$  for the electrode formed on the second substrate. When such metal film is used, it is possible to decrease electric resistance value of the electrode improving driving frequency of the ink jet head.

(Embodiment 6)

Fig. 16 shows a partly-broken perspective view of the first substrate 1 used to the ink jet head



according to the sixth embodiment of the present invention. The second substrate and the third substrate having electrodes formed thereon of the ink jet head of the sixth embodiment have the structures identical with that of the third embodiment.

The first substrate 1 of the sixth embodiment is made of the silicon substrate 57 having a p-type silicon substrate 55 and a n-type Si layer 56 epitaxially grown on the bottom face of the p-type silicon substrate 55. In detail, a part of the p-type silicon substrate 55 is selectively etched through an electric-chemical alkali anisotropy etching process (be explained later) in order to remove the part obtaining a vibrating plate 5 of a precised thickness.

The manufacturing steps of the first substrate of the sixth embodiment is shown in Fig. 17.

First, both the faces of a silicon wafer of p-type (100) face direction are mirror-polished in order to manufacture a silicon substrate 55 of a thickness  $170\text{ }\mu\text{m}$ , and n-type Si layer 56 of a thickness  $30\text{ }\mu\text{m}$  is epitaxially grown on a bottom face of the silicon substrate 55 obtaining a silicon substrate 57 (see Fig. 17(a)). For example, boron is doped into the silicon substrate 55 and its density is  $4 \times 10^{15}\text{ cm}^{-3}$ . Al is doped into the n-type Si layer 56 and its density is  $5 \times 10^{15}\text{ cm}^{-3}$ . The epitaxial growth process above can form a Si layer 56 having a uniform thickness. It is



possible to control the thickness with allowance  $\pm 0.2$   $\mu\text{m}$  of its target of 30  $\mu\text{m}$ .

Next, the silicon substrate 57 is brought under heat-oxidization-treatment in an oxygen-steam atmosphere at  $1100^{\circ}\text{C}$ , for 4 hours and  $\text{SiO}_2$  membranes 41a and 41b of thickness 1  $\mu\text{m}$  are formed on both the faces of the silicon substrate 57 (see Fig. 17(b)).

A photo-resist pattern (not shown) corresponding to the shapes of nozzle holes 4, emitting chambers 6, and etc. is formed on the upper  $\text{SiO}_2$  membrane 41a, a photo-resist pattern (not shown) corresponding to an electrically-led opening portion 58 is formed on the lower  $\text{SiO}_2$  membrane 41b, then the exposed portions of the  $\text{SiO}_2$  membranes 41a and 41b are etched by fluoric acid etching agent in order to remove the photo-resist pattern (see Fig. 17(c)).

Using the apparatus shown in Fig. 18, the electric-chemical anisotropy etching steps are carried out. As shown in Fig. 18, a DC voltage of 0.6V is impressed when n-type Si layer 56 is charged plus and platinum plate 80 is charged minus, the silicon substrate 57 is sunk in KOH solution ( $70^{\circ}\text{C}$ ) containing isopropyl alcohol carrying out an etching step. When the exposed portions of p-type silicon substrate 55 (the portions a  $\text{SiO}_2$  membrane 41a fails to cover) are completely etched and removed, n-type Si layer 56 is non-activated by a plus DC voltage preventing the etching process from



proceeding. At this time, the etching is finished and the silicon substrate of a condition shown in Fig. 17(d) is obtained.

In the next stage, a photo-resist (not shown) of a shape corresponding to the vibrating plate 5 is formed on the lower  $\text{SiO}_2$  membrane 41b, an exposed portion of the  $\text{SiO}_2$  membrane 41b is etched by fluorine acid etching agent and the photo-resist is removed. Simultaneously, all material of the  $\text{SiO}_2$  membrane 41a remained on the surface of p-type silicon substrate 55 and the first substrate 1 shown in Fig. 16 is obtained (see Fig. 17(e)).

Other steps than that described above are identical that of the third embodiment. The thickness of the vibrating plates of one hundred (100) ink jet head manufacturing by the steps of the sixth embodiment are distributed in a range of  $30.0 \pm 0.2 \mu\text{m}$  and it is the thickness precision of n-type Si layer 56 formed by the epitaxial process. When the ink jet head of the sixth embodiment is driven with 100V, 5 KHz, the emitting speeds of ink drops are distributed in a range of  $8 \pm 0.2 \mu\text{m}/\text{sec}$ . and the ink drop volumes are in a range of  $(0.1 \pm 0.005) \times 10^{-6} \text{cc}$ , resulting in a good printing.

(Embodiment 7)

Fig. 19 shows a partly-broken perspective view of the first substrate used in the ink jet head according



to the seventh embodiment of the present invention. The second substrate and the third substrate on which electrodes are formed on the ink jet head of the seventh embodiment and the manufacturing method of these substrates are identical with that of the third embodiment, so that explanations for them are omitted from the specification.

The first substrate 1 of the seventh embodiment is obtained by treating a silicon substrate 63 formed by an epitaxially growing of n-type Si layer 62 on the bottom face of the p-type silicon substrate 61. A crystal face direction of p-type silicon substrate 61 is (110). According to the silicon substrate of (110) face direction, as well known the (111) face perpendicularly crosses to the substrate face of (110) face direction in a direction (211) and an alkali anisotropy etching process enables to form a wall structure perpendicularly to the substrate face.

The seventh embodiment uses the fact above, and pitch distances, when a number of ink jet structural units consisting of nozzles and emitting chambers, etc. are employed, are narrowed realizing a high density arrangement of the nozzles.

The manufacturing steps of the first substrate of the seventh embodiment is shown in Fig. 20.

The steps shown in Fig. 20(a) to (d) correspond to that of the C-C line sections of Fig. 19 and steps of



Fig. 20 (e) to (g) correspond to the D-D line sections of Fig. 19.

First, both the faces of the silicon wafer of p-type (110) face direction are mirror-polished to form a silicon substrate 61 of a thickness 170  $\mu\text{m}$ , n-type Si layer 62 of 3  $\mu\text{m}$  is formed on the bottom face of the silicon substrate 61 by an epitaxial grown step, and the silicon substrate 63 is obtained (see Fig. 20(a)). For example, the silicon substrate 61 is doped with B (boron) and its density is  $4 \times 10^{15} \text{ cm}^{-3}$ , and the n-type Si layer 62 is doped with A and its density is  $5 \times 10^{14} \text{ cm}^{-3}$ . In the epitaxial grown step, it is possible to control the target thickness 3  $\mu\text{m}$  within the allowance  $\pm 0.05 \mu\text{m}$ .

Next, the silicon substrate 63 is thermally oxidized-treated at  $1100^{\circ}\text{C}$  in an oxygen and steam atmosphere in order to form  $\text{SiO}_2$  membranes 41a and 41b of the thickness 1  $\mu\text{m}$  on both the faces of the silicon substrate 63 (see Fig. 20(b)).

A photo-resist pattern (not shown) corresponding to the shapes of cavities and ink cavity, etc. is formed on the upper  $\text{SiO}_2$  membrane 41a, a photo-resist pattern (not shown) corresponding to an electrically leading opening portion 64 is formed on the lower  $\text{SiO}_2$  membrane 41b, and the exposed portions of the  $\text{SiO}_2$  membranes 41a and 41b are etched by fluoric acid etching agent to remove the photo-resist pattern (see Fig. 20(c)).



As of the size of the photo-resist patterns corresponding to the shape of the emitting chamber 6, its width is 50  $\mu\text{m}$ , a distance from the neighboring pattern is 20.7  $\mu\text{m}$ , that is 70.7  $\mu\text{m}$  of a pitch distance, ink drop density per an inch is 360 dpi (dot per inch).

Next, the electric-chemical anisotropy etching mentioned above is applied to the silicon substrate 63 through the method identical with that of the sixth embodiment and the etching is done until the p-type silicon substrate 61 is broken through (see Fig. 20(d)). The dents formed in the step shown in Fig. 20(d) consist of perpendicular walls relative to the surfaces of the silicon substrate 63.

The electric-chemical anisotropy etching process forms a photo-resist pattern (not shown) corresponding to the nozzles 4 and the orifices 7 on the  $\text{SiO}_2$  membrane 41a which is a little thinned, a photo-resist membrane (not shown) covers all the lower  $\text{SiO}_2$  membrane 41b, fluoric acid etching agent etches the exposed portion of the  $\text{SiO}_2$  membrane 41a, and the photo-resist pattern is removed (see Fig. 20(e)).

Next, identical with the steps shown in Fig. 20(d), an electric-chemical etching process etches the substrate until the nozzles 4 and the orifices 7 of thickness 30  $\mu\text{m}$  are formed (see Fig. 20(f)).

Last, the whole silicon substrate is sunk in fluoric acid etching agent to remove  $\text{SiO}_2$  membranes 41a



and 41b in order to obtain the first substrate 1 (see Fig. 20(g)). The width of the emitting chamber formed on the resulting first substrate becomes 55  $\mu\text{m}$  which is a little enlarged by undercutting during the etching step. The pitch distance is 70.7  $\mu\text{m}$ , so it is said the first substrate obtained has the ideal measurements. The most suitable value of the width of the cavity is determined due to ink emitting characteristic. Considering the undercutting, the size of the photo-resist pattern is determined to obtain the ideally-shaped cavity.

(Embodiment 8)

Fig. 21 is a partly-broken perspective view of the first substrate of the ink jet head according to the eighth embodiment of the present invention. The vibrating plate 5 in the ink jet head of the eighth embodiment of the present invention is a boron doped layer 66 of a density and has a thickness identical with that of the necessary vibrating plate. It is known that the etching rate of alkali used Si etching step becomes very small in the range of a high density (about  $5 \times 10^{19} \text{ cm}^{-3}$  and more) when the dopant is boron.

According to the eighth embodiment using the facts above, the vibrating plate forming range is supposed that a high density boron doped layer. When an alkali



anisotropy etching forms the emitting chamber 6 and the ink cavity 8, so-called etching stop technique in which the etching rate greatly lessens at the time the boron doped layer 66 is exposed forms of the vibrating plate 5 and emitting chambers 6 of the necessary shapes.

The manufacturing steps of the first substrate according to the eighth embodiment of the present invention are shown in Fig. 22.

First, the faces of a silicon wafer of n-type (110) face direction are mirror-polished in order to form a silicon substrate 65 of a thickness 200  $\mu\text{m}$ . The silicon substrate 65 is brought under a thermal-oxidization treatment of 1100°C for 4 hours in an oxygen and steam atmosphere so as to form  $\text{SiO}_2$  membranes 41a and 41b of thickness 1  $\mu\text{m}$  on both the faces of the silicon substrate 65 (see Fig. 22(a)).

Next, a photo-resist pattern (not shown) corresponding to the shapes of the vibrating plate (boron doped layer) 66, ink cavity 8, electrode leads (not shown) is formed on the lower  $\text{SiO}_2$  membrane 41b, the exposed portion (part corresponding to the vibrating plate, ink cavity, leads) of the  $\text{SiO}_2$  membrane 41b is etched by fluoric acid etching agent, and the photo-resist pattern is removed (see Fig. 22(b)).

The exposed Si portion of the silicon substrate 65



is doped with boron. The treatment method of doping is identical with that of the third embodiment and the boron doping layer 66 of a boron density  $5 \times 10^{20} \text{ cm}^{-3}$  and of a doped layer thickness  $10 \text{ } \mu\text{m}$  is formed (see Fig. 22(c)). In order to attain such high density of boron and high thickness of doped layer, it is preferable to employ a spin-coating process of  $\text{B}_2\text{O}_3$  agent and a diffusion process using BN plate of various methods described in the third embodiment above. It is possible to employ anyone to attain such doped layer above.

Next, a photo-resist pattern (not shown) corresponding to the shapes of emitting chambers 6, ink cavity 8, and etching end detection pattern 71 is formed on the upper  $\text{SiO}_2$  membrane 41a, the exposed portions of the  $\text{SiO}_2$  membrane 41a are etched by fluoric acid etching agent, and the photo-resist pattern is removed (see Fig. 22 (d)). The photo-resist pattern corresponding to the emitting chamber 6 has a width  $50 \text{ } \mu\text{m}$ , and apart-distance from the neighboring pattern  $20.7 \text{ } \mu\text{m}$ , which are identical with that of the seventh embodiment.

The silicon substrate 65 is brought under an alkali anisotropy etching treatment. Etching agent of KOH solution (density: 20 weight %, temperature:  $80^\circ\text{C}$ ) was used. As described above, the etching rates of silicon alkali etching depend on as shown in Fig. 23 the boron



density. With regard to n-type silicon substrates, the etching process proceeds at an etching rate of about  $1.5 \mu\text{m}/\text{min}$ , however in the boron high density range the etching rate lowers to about  $0.01 \mu\text{m}/\text{min}$ .

Because the thickness (designed value) of the vibrating plate 5 is  $10 \mu\text{m}$ , it is sufficient to etch and remove only  $190 \mu\text{m}$  of the total thickness  $200 \mu\text{m}$  of the silicon substrate 65 in order to form the emitting chambers 6 and the ink cavity 8. In practice, it is difficult to make the thickness of the vibrating plates 5 uniform since the thickness values of the silicon substrates 65 distribute in some range ( $\pm 1$  to  $2 \mu\text{m}$ ).

According to the eighth embodiment, the process mentioned below can form the thickness to the vibrating plates correctly.

It is necessary to etch the silicon substrate for about 126 minutes 40 seconds calculated in order to etch and remove  $190 \mu\text{m}$  of a thickness of the silicon substrate. In order to etch a thickness  $10 \mu\text{m}$ , an etching step for about 6 min 40 sec. is necessary. Consequently, in order to etch and remove  $200 \mu\text{m}$  thickness, a total time of 133 min 20 sec. is needed.

On the silicon substrate of the condition shown in Fig. 22 (d), an etching step of total time of about 133 min 20 sec. using the etching agent is done. After a start of the etching process and about 126 min. 40 sec.



is elapsed, about 190  $\mu\text{m}$  of etching is done on the emitting chamber and the face on etching (not shown) reaches about almost a boundary of the boron doped layer 66 or the boundary itself. While, on the etching end detection pattern 71, similarly about 190  $\mu\text{m}$  has been etched. Continuously, an etching of about 6 min 40 sec. is carried out. If the etching face or front does not reach the boron doped layer 66, it proceeds at an etching rate of similarly 1.5  $\mu\text{m}/\text{min}$ . When the etching front reaches the boron doped layer 66, the etching rate suddenly drops to about 0.01  $\mu\text{m}/\text{min}$ , consequently only about 6 min at most of the etching time length cannot etch the boron doped layer 66 obtaining the vibrating plate having a boron doped layer of thickness 10  $\mu\text{m}$ . On the contrary, on the etching end detection pattern 71, similarly the etching step advances at an etching rate of about 1.5  $\mu\text{m}/\text{min}$ . At last after the etching for a total time of about 133 min 20 sec, a through hole 72 is formed.

As described above, the etching time necessary to make the through hole is distributed owing to various thicknesses of the silicon substrate 65, so it is necessary to detect when the through hole 72 is completed at the time of about 133 min being elapsed after the etching starts through various means (for example, seeing observation of the operator, applying a laser beam on the etching end detection pattern from a



side of the pattern and receiving the laser beam by a light receiving element placed on another side of the pattern when the through hole is completed) (see Fig. 22(e)).

Next, similar to that of the third embodiment, a pattern machining for restricting the distances between electrodes formed on the second substrates is carried out so as to obtain the first substrate 1.

Notwithstanding that the silicon substrate 65 has various thicknesses portion by portion of the substrate ( $\pm 1$  to  $2 \mu\text{m}$ ), the vibrating plate 5 formed by the process about has a precision of  $10 \pm 0.1 \mu\text{m}$ . Such error or allowance of  $\pm 0.1 \mu\text{m}$  seems that it depends on distribution of the boron doping depth, and does not depend on the distribution of the alkali etching results.

According to the eighth embodiment of the ink jet head, the precision of the thickness of boron doped layer determines the thickness precision of the vibrating plate. In order to obtain the correct thickness precision in the range of about  $10 \mu\text{m}$  thickness, it is the most preferable method to use  $\text{BBr}_3$  of the diffusion source. However, if the treatment condition is made to the most suitable one, other methods can be used to attain the doped thickness precision corresponding to that obtained by the method of BBr diffusion source.



According to the eighth embodiment, simultaneously with the boron doping step for the vibrating plate, the doping is done to the leads continuous to the vibrating plate. Because that the driving electrodes having the structure identical with the vibrating plate of the fourth embodiment and corresponding to each vibrating plate of high density boron doped portions are formed, it is possible also to attain an improvement of the driving frequency.

In addition, according to the eighth embodiment, n-type substrate is used for the silicon substrate, however if p-type substrate is used for the silicon one, it is possible to form the boron doped vibrating plates.

The substrates anode-junction methods of the present invention will be explained with reference to the following embodiments 9 to 12.

(Embodiment 9)

Fig. 24 shows an outline of the ninth embodiment of the anode bonding method according to the present invention. It shows a section of a bonding apparatus used to the method and of the substrates while they are bonding. Fig. 25 is a plan view of the bonding apparatus.

The ninth embodiment shown relates to an anode bonding method for bonding or the first



silicon substrate 1 and the second boro-silicated glass substrate 2.

The bonding apparatus of the ninth embodiment consists of an anode bonding electrode plate 111 to be connected to a plus side of a power source 113, an cathode bonding electrode plate 112, and a terminal plate 115 protruding from the anode bonding electrode plate 111 through a spring 114. Gold plating is applied on the surfaces of the anode bonding electrode plate 111 and the cathode bonding electrode plate 112 in order to decrease contact resistance of the surfaces. The terminal plate 115 is constructed by a single contact plate in order to equalize in potential a plurality of electrodes 21 on the boro-silicated glass substrate 2, and the silicon substrate 1. The terminal plate 115 is connected to the anode bonding electrode plate 111 by means of the spring 114 and the spring keeps the terminal plate 115 in its suitable contact pressure with the electrode 21. The terminal plate 115 comes to contact with the terminal portion 23 of the electrode 21.

The silicon substrate 1 and the boro-silicated glass substrate 2 are aligned and in detail the vibrating plate 5 and the electrode 21, respectively formed thereon are aligned by an aligner device (not shown) after they are washed and then they are set as shown in Fig. 24 and Fig. 25. The electrode 21, and



the electrode plates 111 and 112 are placed in nitrogen gas atmosphere in order to prevent the surfaces of them from being oxidized.

During the anode bonding method, first both the substrates 1 and 2 are heated. In order to prevent the boro-silicated glass substrate 2 from breaking due to sudden rise of temperature, it is necessary to heat it gradually to 300 °C for about 20 min. Next, the power source 113 impresses 500V voltage for about 20 min so as to bond both the substrates 1 and 2. During the anode bonding method, Na ions in the boro-silicated glass substrate 2 move and current flow through the substrate 2. It is possible to judge the joined condition of them when they are connected because a value of current decreases. In order to prevent strain-crack due to thermal conductivities of both the substrates 1 and 2 after they are connected, it is necessary to cool them gradually for about 20 min.

It is possible to prevent discharging and electric field dispersion when the terminal plate 115 and the spring 114 decreases the potential difference between the electrode 21 and vibrating plate 5 making electric field disappear. As a result, a large current does not flow between the electrode 21 and the vibrating plate 5 preventing the electrode 21 from melting. Also, because that static electricity attractive force due to electric field does not function in the vibrating plate 5, no



remaining stress is generated in the vibrating plate 5 after the plate 5 is secured through its circumference. The dielectric membrane 24 is charged when transformation of electric charge from the vibrating plate 5. In electric field, the dielectric membrane 24 receives static electricity attractive force along a direction of the vibrating plate 5 and peeled off. When the electrode 21 and the vibrating plate 5 are made equal in their potential, it is possible to prevent the dielectric membrane 24 from being peeled off.

(Embodiment 10)

Fig. 26 is an outline view of another embodiment of the anode bonding method according to the present invention and a section of both the substrates in their bonding procedure and a bonding apparatus used to the anode bonding apparatus. Fig.27 is a plan view of the bonding apparatus.

According to the tenth embodiment of the ink jet head of the present invention, terminal 116 respectively consisting of coil springs are used and the terminal plates contact with respective electrodes 21. Other structure of the embodiment than that above is identical with that shown in Fig. 24.

The terminals 116 are made of SUS which is durable to high temperature. Ordinarily, a material SUS is not preferable to be used as terminal material because it



has resistance on the surface having oxidized films. However, in the anode bonding, it is purpose of applying high voltage and making them equal potential, so that it is possible to obtain good results if a value of current is low. When respective terminals 16 are independent coil springs, it is possible to prevent the substrates from curving due to being heated when the anode bonding process and these terminals 16 from not being led to the electrode 21 due to worn terminal.

(Embodiment 11)

Fig. 28 shows a plan view of the anode bonding apparatus according to another embodiment of the present invention. Fig. 29 is a plan view showing an arrangement relation of the electrode on the second substrate and the common electrode. In Fig. 29, the dielectric membrane is omitted.

According to the eleventh embodiment, a photolithography uses a batch treatment system in order to form simultaneously a plurality of electrodes 21 for a plural sets (in the embodiment, it is two) of ink jet heads and respectively electrode 21 for the plural sets on a single boro-silicated glass substrate 2A. The common electrode 120 has lead portions 121a and 121b to be connected to the terminal portion 23 of all the electrodes 21 of respective sets. In addition, a single silicon substrate (not shown) to be connected to the



boro-silicated glass substrate 2A has a plurality of sets of elements (nozzle, emitting chamber, vibrating plate, orifice, ink cavity) having the structures shown in Fig. 24 and Fig. 26, respective sets being placed at the corresponding positions. Then, in the joining step, a single terminal 116 consisting of a coil spring shown in Fig. 26 comes to contact with the common electrode 120 in order to lead it to the anode-side joining electrode plate 111.

Consequently, it is possible to make all electrodes 21 and all vibrating plates of respective sets equal to each other in potential obtaining the same effect as that of the embodiments above.

After they are connected, they are cut by diesing (phonetic) per each ink jet head and the common electrodes 120 are cut off from the electrodes 21 of respective sets through the connecting ends of lead portions 121a and 121b.

(Embodiment 12)

Fig. 30 is a section of an anode bonding apparatus according to other embodiment of the present invention.

According to the twelfth embodiment, three substrates 1, 2 and 3 are simultaneously anode-bonding to each other. The first substrate 1 is a silicon one, and the second and third substrate 2 and 3 are boro-silicated ones. The third substrate 3 function merely



as a lid of nozzle holes 4, emitting chamber 6, orifice 7, ink cavity 8. It is enough to make the third substrate 3 of a material of less joining precision than that of boro-silicated glass substrate, so that soda glass joining is sufficient. When the third substrate, however, is made of boro-silicated glass, it is possible to improve its reliability.

And, in accordance with the twelfth embodiment of the ink jet head of the present invention, upper and lower joining electrode plates 111 and 112 to be contacted with the second and third boro-silicated glass substrates 2 and 3 are connected to a minus side of the power source 113, the first silicon substrate 1 and the electrode 21 on the boro-silicated glass substrate 2 are connected to a plus or positive of the power source 113, and they are simultaneously anode bonding. As a result, according to the simultaneous anode bonding process, it is possible to reduce the time used to heat and gradual cool the substrates 1, 2 and 3 shortening largely the bonding time of them. Additionally, as described in regard to the ninth embodiment and eleventh embodiment above, it is possible to protect the surface on the silicon substrate 1 from being polluted by direct contact with the upper bonding electrode plate 111.



In the thirteenth embodiment and fourteenth the embodiment below, structures preventing dust from invading into the gap portion formed as described above. Here, a static electricity actuator is exemplified, however it is possible to use the same structure when an ink jet head is employed.

(Embodiment 13)

Fig. 31 is a section of a static electricity actuator of the thirteenth embodiment of the present invention. Fig. 32 is its plan view.

As apparent from the previous embodiments, the first substrate 1 and the second substrate 2 are directly Si bonding or anode bonding with the predetermined gap length. Because a temperature when the anode bonding or bonding process is done is high, air in the gap portion 16 expands. When air temperature lowers to the room temperature after the connection, the pressure in the gap portion 16 lowers than the atmosphere, so the vibrating plate 5 bends toward the electrode 21 becoming into contact with the electrode 21 and being short-circuited, or more disadvantageously unnecessary stress being given to the vibrating plate 5. When the gap portion 16 is open to the atmosphere in order to prevent such disadvantageous effects and kept at such open condition, static electricity in the gap portion and the surrounding mechanism sucks dust. As a result, such dust is attached to the electrode 21 changing a vibration characteristic of the vibrating



plate 5.

In order to solve such problem above, the gap portion 16 of the ink jet head of the thirteenth embodiment of the present invention, the gap portion 16 is open to the atmosphere through the passage 18, as well as outlet ports 19a and 19b of the passage 18 are sealed by sealer agent 20 of epoxy and the like which has a high viscosity when the substrates 1 and 2 are cooled to the room temperature after they are anode-bonding.

The reference numerals 23 is a terminal portion of the electrode 23, 41 means  $\text{SiO}_2$  membrane of a dielectric membrane formed on the substrate 1, 102 is an oscillation circuit, and 106 is a metal membrane formed to connect one terminal of the oscillation circuit 102 to the substrate 1. The passage 18 extends surround the electrode 21.

Because that the silicon substrate constituting the substrate 1 has a high thermal conductivity, the sealer is made of thermal plastic resin and the pressure in the gap portion does not rise. Because that the sealing member 20 has a high viscosity, it fails to flow in the passage 18.

Consequently, according to the thirteenth embodiment of the present invention, the gap portion 16 is open or led to the atmosphere through the passage 18 while an anode bonding, so that any heating of the anode-



bonding operation fails to raise the pressure in the gap portion 16. After anode-bonding is finished and the temperature lowers to the room temperature, the sealing member 20 seals the outlet of the passage 18 preventing dust from invading the gap portion 16 and the problems above happening.

The aforesaid effect is available if a gaseous body such as nitrogen, argon, etc. is enclosed in said gap portion 16 when it is sealed.

(Embodiment 14)

Fig. 33 is a section of the static electricity actuator according to another embodiment of the present invention.

According to the fourteenth embodiment, the static electricity actuator has a second electrode 46 placed under the vibrating plate 5 so as to oppose to the electrode 21. The second electrode 46 is made of Cr or Au thin membrane.

The static electricity actuator functions as a capacitor. When a V volt is impressed to the opposed electrodes 21 and 46, Vc of the voltage between the opposed electrodes 21 and 46 raised when they are charged and discharged is shown below:

$$V_c = V (1 - \exp (-t/T)) \quad \text{charging time}$$

$$V_c = V \exp (-t/T) \quad \text{discharging time}$$

Wherein T: time constant.

It is apparent from the equations above that they



are exponential functions. When the time constant  $T$  is large, rising speed of  $V_c$  is made slow. The time constant  $T$  is given by an equation  $RC$  (wherein the resistance is  $R$  and static electricity capacitor is  $C$ ). Because a resistance of silicon is higher than metals, the electrode 46 of Cr or Au thin membrane having low resistance is used as a vibrating plate 5 so as to drive the ink jet head at a high speed. When the time constant is made low, responsibility of the actuator improves.

(Embodiment 15)

Fig. 34 shows a section of the ink jet head according to still another embodiment of the present invention.

In the fifteenth embodiment, the gap  $G$  to be formed under the vibrating plate 5 is kept by a thickness of photo-sensitive resin layer or adhesive agent layer 200. That is, patterns of the photo-sensitive resin layer or adhesive agent layer 200 are printed around the electrode 21 of the second substrate 2 and both the second substrate 2 and the first substrate 1 are adhered to each other making a lamination. In practice, soda glass is used as the second substrate 2 and it is constructed as described on the second embodiment.

A photo-sensitive polyimide is used as a photo-



sensitive resin and it is printed around the electrode 21 of the second substrate 2 with its thickness/ $\mu\text{m}$  forming the pattern 200 of photo-sensitive resin layer. While, similar to that of the second embodiment, the bottom face of the first silicon substrate 1 is planely polished and the first substrate 1 and second substrate 2 are laminated. As a result, when the photo-sensitive resin is used, the gap length G between the vibrating plate 5 and the electrode 21 is  $1.4 \mu\text{m}$ . When an adhesive agent of epoxy bond is used, the its thickness G is  $1.5 \mu\text{m}$ , and the substrates 1 and 2 are laminated at a temperature  $100^{\circ}\text{C}$ . In this case, the gap length G is a little less than  $1.9 \mu\text{m}$ . When adhesive agent is used, it is necessary to press the substrate 1 and other substrate 2, so the gap length G decreases differing from that of the photo-sensitive resin.

It is possible to use such gap holding means of photo-sensitive resin and adhesive agent keeping the predetermined length or thickness of the gap. It is noted that the ink jet head of the present invention using such gap holding mean scan be driven by a low voltage identical with that of the second embodiment attaining a good printing result.

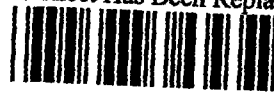
Not only polyimid but also other materials of photo-sensitive resin such as acryl, epoxy and the like can be used. Temperature of thermal treatment is



controlled according to the kind of various resins.  
With regard to adhesive agents, acryl, cyano, urethane,  
silicon of various materials can be used.

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C L A I M S

1. An ink jet head comprising one or more nozzles (4) for ejecting ink drops, a respective ejecting chamber (6) connected to the or each said nozzle (4), a vibrating plate (5) constituting at least one wall of the ejecting chamber (6), and a driving means for generating a deformation in said vibrating plate, characterised in that said driving means is an electrode (21) for static-electrically deforming the vibrating plate (5) and in that said vibrating plate (5) and said electrode (21) are spaced by a distance of at least 0.05  $\mu\text{m}$  and no more than 2.0  $\mu\text{m}$ .

2. An ink jet head according to claim 1, characterised in that said distance is defined by a dent (15) forming a vibrating chamber (9) in a first substrate (1).

3. An ink jet head according to claim 1, characterised in that said distance is defined by a dent (15) for mounting an electrode (21) formed in a second substrate (2).

4. An ink jet head according to any one of the preceding claims, characterised in that a first substrate (1) and a second substrate (2) each comprise single crystal silicon substrates and the distance defining means is constituted by a gap spacer of a  $\text{SiO}_2$  membrane previously formed on at least one face of facing portions of the substrates.

5. An ink jet head according to claim 4, characterised in that said  $\text{SiO}_2$  membrane is a thermally oxidized membrane of silicon.





6. An ink jet head according to claim 4, characterised in that said  $\text{SiO}_2$  membrane is formed by a spattering process, CVD process, vaporizing process, ion-plating process, sol-gel process, thermal oxidation process or organic silicon composition sintering process.
7. An ink jet head according to claim 4, characterised in that said electrode (21) comprises p-type or n-type impurities.
8. An ink jet head according to any one of the preceding claims, characterised in that said electrode (21) is covered by a dielectric membrane (24) leaving a space between the electrode (21) and the vibrating plate (5).
9. An ink jet head according to any one of the preceding claims, characterised in that said vibrating plate (5) has a second electrode integrally formed on the vibrating plate so as to fill said distance.
10. An ink jet head according to claim 9, characterised in that said second electrode comprises a p-type or n-type impurity.
11. An ink jet head according to claim 1, characterised in that a boro-silicate glass thin membrane previously formed on at least one face of an attaching portion of the first substrate or the second substrate is used as a gap spacer for maintaining said distance.
12. An ink jet head according to claim 11, characterised in that the boro-silicate glass thin membrane is formed by a spattering method.





13. An ink jet head according to claim 1, characterised in that said vibrating plate (5) comprises a n-type impurity layer.

14. An ink jet head according to claim 1, characterised in that said vibrating plate (5) comprises a p-type impurity layer of high density.

15. An ink jet head according to claim 9, characterised in that a driving wiring layer including the second electrode comprises a p-type impurity layer of high density.

16. An ink jet head according to any one of claims 4 to 15, characterised in that said first substrate (1) is a silicon substrate of crystal face direction (110).

17. An ink jet head according to any one of claims 4 to 16, characterised in that said first substrate (1) is a p-type silicon substrate of which n-type impurity layer is epitaxially grown.

18. An ink jet head according to claim 1, characterised in that a zone forming said distance between the vibrating plate (5) and an electrode (21) connects with a passage led to the outside before the first substrate (1) having the vibrating plate (5) formed thereon, and a second substrate (2) having an electrode (21) formed thereon is anode bonded thereto and the outlet of the passage is sealed by a sealing member after the anode-bonding process.

19. An ink jet head according to claim 1, characterised in that the distance maintenance means is a photo-sensitive resin layer or an adhesive agent layer formed patternly around the electrode.





20. An ink jet head according to claim 8, characterised in that said dielectric membrane is made of silicon oxide, boro-silicate glass or silicone compound.

21. An ink jet head according to claim 18,  
5 characterised in that said zone is filled with gas, preferably air, nitrogen or argon.

22. An ink jet printing machine including an ink jet head according to any one of the preceding claims.

23. A method of manufacturing an ink jet head,  
10 characterised in that it comprises the steps of patterning a  $\text{SiO}_2$  membrane of a predetermined thickness on a face of a first silicon substrate forming a vibrating plate except a part for the vibrating plate, or patterning a  $\text{SiO}_2$   
15 membrane of a predetermined thickness on an opposing face of a second silicon substrate forming an electrode except a part for the electrode, and anode-joining by a Si direct joining method for the first silicon substrate and the second silicon substrate through the  $\text{SiO}_2$  membrane.

24. A method according to claim 23, characterised in  
20 that it comprises the further step of forming the vibrating plate by carrying out an alkali anisotropy etching process on the first silicon substrate.

25. A method according to claim 23, characterised in  
25 that it comprises a further step of forming the electrode of p-type or n-type impurity by doping said second silicon substrate.

26. A method as claimed in either claim 23 or claim 24, characterised in that it includes the steps of forming n-type impurity on the p-type silicon substrate, and





forming a vibrating plate by applying an electric-chemical anistropy etching step on the silicon substrate.

27. A method for anode-bonding a first substrate having a vibrating plate formed thereon and a second substrate having an electrode for driving the vibrating plate, said electrode being formed on said second substrate, characterised in that it comprises a step of controlling a potential difference between the vibrating plate and the electrode to decrease the potential difference during the anode-bonding process.
28. A method according to claim 27, characterised in that the potential of the electrode is made equal to that of the vibrating plate.
29. A method for anode-bonding a first substrate on which a vibrating plate is formed and a second substrate on which is formed an electrode for driving the vibrating plate, characterised in that it comprises the steps of forming a common electrode to be connected to respective electrodes on the second substrate, controlling the potential difference between said vibrating plate and the common electrode to decrease the potential difference during the anode bonding process, and separating the common electrode from the electrode after the anode bonding process.

