

DEPLOYMENT SYSTEM

TECHNOLOGICAL FIELD

5 The presently disclosed subject matter relates to deployment systems for deploying pivotably connected panel elements, in particular solar panels.

BACKGROUND

10 Many types of spacecraft, including satellites, are equipped with one or more panel assemblies of solar panels, each panel assembly including a plurality of solar panels. Such spacecraft are typically launched with the panels in a compact state – commonly in a folded state or rolled state – and the panels are deployed once the spacecraft has reached the appropriate flight stage in space.

15 Many different mechanisms have been provided over the years for deploying such panels.

20 By way of non-limiting example, US 4,155,524 discloses synchronized angular displacement of articulated elements of an outwardly-extendable solar-cell panel, carried out by means of a device mounted between any two successive panel elements constituting a driving element and a driven element. Two independent and parallel traction members are pivotally mounted on support plates which are rigidly fixed to two successive driving elements. Two link-arms for traction members such as cables are pivotally attached to pins forming anchoring points for the cables. Each support plate has two stationary stops for limiting the angular displacements of the link-arms during the relative pivotal movement of the driven element with respect to the driving element.

25 Further by way of non-limiting example, US 6,031,178 discloses a panel assembly including a number of rectangular panels each carrying solar cells or a cooling radiator on one of the two main surfaces, where the panels are interconnected mutually by hinges such that the assembly from a first state, in which the panels are folded into a package,

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can be brought into a second state in which the package is unfolded and the panels are situated alongside each other. A torsion element substantially extends across the other main surface of each panel from a first position on the hinge axis between the panel and the adjoining panel at one side, to a second position on the hinge axis between the panel
5 and the adjoining panel at the other side, whereby the torsion element at or near the first and second positions is attached to the respective adjoining panel.

Further by way of non-limiting example, US 6,008,447 discloses a transmission for folding out the solar cell panels folded in an accordion-like manner on a spacecraft having cable pulleys at the hinges, around pairs of which pulleys endless cables are
10 wound. To adapt its change in length during temperature changes to the change in the length of the panels and to increase its rigidity to elongation, the cable is provided with a plastic sheathing firmly connected to same outside the area of the cable pulleys.

Further by way of non-limiting example, US 4,555,585 discloses a foldable solar cell panel apparatus having at least two panel portions which are connected together at a
15 foldable edge to form at least one foldable pair which, in the folded-together state, is preferably stored in a panel container. A stationary folding and unfolding system brings the solar cell panel into the folded or unfolded state. During the folding process, the lowermost deployed foldable pair is folded together while the foldable pairs above it remain unfolded. The deployed foldable pairs are folded together individually in
20 succession. During the unfolding process, the uppermost foldable pair stored in the panel container is unfolded while the fold pairs below it are held in the folded state. The stored foldable pairs are unfolded in succession during deployment.

Further by way of non-limiting example, EP 0955237 discloses solar energy panels used on satellite system are arranged as a series of folded units that can unfold to
25 provide a continuous projection. The panels are coupled together by tensioned wire loops that pass around pairs of rollers. The wire is produced of a material with a neutral thermal expansion coefficient.

Further by way of non-limiting example, KR 100540978 discloses an unfurling device for solar panels in a satellite.

GENERAL DESCRIPTION

According to a first aspect of the presently disclosed subject matter, there is provided a deployment system for pivotably deploying a first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective panel element pair pivot axis, the deployment system comprising a second plurality of actuators, an actuation cable and a drive unit, wherein:

at least one said actuator is associated with each respective pair of said panel elements, each said actuator comprising a first bracket, a second bracket and a linear motion to rotary motion converter, the first bracket being configured for being fixedly mounted to one panel element of the pair, the second bracket being configured for being fixedly mounted to another panel element of the pair, the respective first bracket and the respective second bracket being pivotably mounted with respect to one another about an actuator pivot axis co-axial with the respective panel element pair pivot axis, and wherein the linear motion to rotary motion converter is configured for pivoting the respective first bracket with respect to the respective second bracket responsive to a predetermined datum linear displacement being applied to the linear motion to rotary motion converter;

the actuation cable being serially coupled to each said actuator of said second plurality of actuators, the actuation cable configured for being displaced linearly with respect to the plurality of actuators at least between a first cable position, corresponding to the stowed configuration, and a second cable position, corresponding to the deployed configuration, responsive to operation of the drive unit, such as to apply a corresponding said datum linear displacement to the respective linear motion to rotary motion converter of each said actuator;

the drive unit being configured for selectively displacing the actuation cable at least between the first cable position and the second cable position.

For example, each respective said linear motion to rotary motion converter comprises a linearly movable shaft element, coupled to the actuation cable. For example, each respective said linear motion to rotary motion converter comprises a respective rotary element operatively coupled to the shaft element such that the rotary element pivots

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the respective first bracket with respect to the respective second bracket responsive to a respective said datum linear displacement being applied to the shaft element. For example, the rotary element comprises an outer cylinder co-axial with and overlying at least part of the shaft element, the outer cylinder fixedly mounted with respect to the first
5 bracket, the outer cylinder comprising a cam groove having at least one helical portion, and wherein the shaft element is movably mounted with respect to said second bracket, the shaft element being constrained for axial movement with respect to the second bracket and prevented from relative rotary movement with respect to the second bracket, wherein the shaft element comprises a cam follower coupled to the cam groove, and wherein
10 application of a first axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said at least one helical portion, causing the cylinder together with the first bracket to pivot about a corresponding pivot angle about the respective pivot axis, wherein said first displacement corresponds to said datum linear displacement. For example, the cam groove comprises at least one linear
15 portion, and wherein application of a second axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said linear portion, preventing the cylinder together with the first bracket from pivoting about the respective pivot axis. For example, the cam groove comprises at least one tapering portion smoothly connecting one said linear portion with one end of one said helical
20 portion.

In at least some examples, at least one said linear motion to rotary motion converter can be in the form of a rack and pinion arrangement.

In at least some examples, at least one said respective said linear motion to rotary motion converter is in the form of a slider crank arrangement.

25 Additionally or alternatively, for example, said pivot angle is between about 90° and about 270°.

Additionally or alternatively, for example, said pivot angle is about 180°.

Additionally or alternatively, for example, all said actuators of said second plurality of actuators are configured for pivoting simultaneously responsive to a

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predetermined said datum linear displacement being applied to all the respective linear motion to rotary motion converters.

Alternatively, for example, all said actuators of said second plurality of actuators are configured for pivoting at the same pivoting rate responsive to a predetermined said datum linear displacement rate being applied to all the respective linear motion to rotary motion converters.

Alternatively, for example, said actuators of said second plurality of actuators are configured for pivoting non-simultaneously with respect to one another, responsive to a predetermined said datum linear displacement being applied simultaneously to all the respective linear motion to rotary motion converters.

Alternatively, for example, at least some said actuators of said second plurality of actuators are configured for pivoting at respective pivoting rates that are different with respect to one another, responsive to a predetermined said datum linear displacement rate being applied simultaneously to all the respective linear motion to rotary motion converters. Alternatively, for example, said actuators of said second plurality of actuators are configured for pivoting in a synchronized manner with respect to one another responsive to operation of the drive unit and the actuation cable.

Alternatively, for example, the actuation cable is enclosed within an envelope comprising a second plurality of windows, the envelope configured for maintaining a predetermined tension in the actuation cable.

For example, said envelope is provided by a sheath.

For example, said envelope is in the form of an incompressible sheath having a lumen that allows relative axial movement between the actuation cable and the sheath.

For example, the envelope is in the form of a Bowden cable.

For example, the envelope is provided by channels provided in the panel elements.

Additionally or alternatively, for example, each said actuator is operatively coupled to the actuation cable at a respective said window.

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Additionally or alternatively, for example, the deployment system further comprises a locking arrangement, coupled to the actuation cable, wherein the locking arrangement is configured for maintaining the plurality of panels elements locked in the stowed configuration at least until the drive unit is activated.

5 According to the first aspect of the presently disclosed subject matter, there is also provided a deployment system pivotably deploys panel elements between a stowed configuration and a deployed configuration. Actuator(s) associated with each pair of panel elements include a first bracket mountable to one panel element, a second bracket mountable to the other panel element, and a linear motion to rotary motion converter
10 (LMRMC) for pivoting the first bracket with respect to the second bracket responsive to a predetermined datum linear displacement being applied to the LMRMC. An actuation cable, coupled to each actuator, can be displaced linearly with respect thereto between a first position, corresponding to the stowed configuration, and a second position, corresponding to the deployed configuration, responsive to operation of the drive unit,
15 such as to apply at least a corresponding datum linear displacement to the respective LMRMC of each actuator. The drive unit is configured for selectively displacing the actuation cable between the first position and the second position.

 According to a second aspect of the presently disclosed subject matter, there is provided a panel system comprising a first plurality of panel elements and a deployment
20 system for pivotably deploying the first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective pivot axis, the deployment system being as defined herein with respect to the first aspect of the presently disclosed subject matter.

25 For example, said panel elements are in the form of solar panels.

 Additionally or alternatively, for example, at least one said panel element is configured for being pivotably mounted to a structure. For example, said structure is a space vehicle.

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According to a third aspect of the presently disclosed subject matter, there is provided a space vehicle comprising a panel system as defined herein with respect to the second aspect of the presently disclosed subject matter.

According to a fourth aspect of the presently disclosed subject matter, there is
5 provided an actuator for a deployment system, said actuator comprising a first bracket, a second bracket and a linear motion to rotary motion converter, the first bracket being configured for being fixedly mounted to a panel element, the second bracket being configured for being fixedly mounted to another panel element, the respective first bracket and the respective second bracket being pivotably mounted with respect to one
10 another about an actuator pivot axis co-axial with the respective panel element pair pivot axis, and wherein the linear motion to rotary motion converter is configured for pivoting the respective first bracket with respect to the respective second bracket responsive to a predetermined datum linear displacement being applied to the linear motion to rotary motion converter, and wherein the linear motion to rotary motion converter is configured
15 for being coupled to an actuation cable.

For example, each respective said linear motion to rotary motion converter comprises a linearly movable shaft element, configured for being coupled to the actuation cable.

For example, each respective said linear motion to rotary motion converter
20 comprises a respective rotary element operatively coupled to the shaft element such that the rotary element pivots the respective first bracket with respect to the respective second bracket responsive to a respective said datum linear displacement being applied to the shaft element.

For example, the rotary element comprises an outer cylinder co-axial with and
25 overlying at least part of the shaft element, the outer cylinder fixedly mounted with respect to the first bracket, the outer cylinder comprising a cam groove having at least one helical portion, and wherein the shaft element is movably mounted with respect to said second bracket, the shaft element being constrained for axial movement with respect to the second bracket and prevented from relative rotary movement with respect to the
30 second bracket, wherein the shaft element comprises a cam follower coupled to the cam groove, and wherein application of a first axial displacement of the shaft element relative

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to the second bracket causes the cam follower to follow at least a portion of said at least one helical portion, causing the cylinder together with the first bracket to pivot about a corresponding pivot angle about the respective pivot axis, wherein said first displacement corresponds to said datum linear displacement.

5 For example, the cam groove comprises at least one linear portion, and wherein application of a second axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said linear portion, preventing the cylinder together with the first bracket from pivoting about the respective pivot axis.

10 For example, the cam groove comprises at least one tapering portion smoothly connecting one said linear portion with one end of one said helical portion.

According to a fifth aspect of the presently disclosed subject matter, there is provided a method for deploying a panel system comprising

15 providing a first plurality of panel elements and a deployment system for pivotably deploying the first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective pivot axis, the deployment system being as defined herein regarding the first aspect of the presently disclosed subject matter;

20 operating the deployment system to cause the panel system to transition the first plurality of panel elements between the stowed configuration and the deployed configuration.

In at least some examples, said panel elements are in the form of solar panels.

25 Additionally or alternatively, for example, at least one said panel element is pivotably mounted to a structure. For example, said structure is a space vehicle.

BRIEF DESCRIPTION OF THE DRAWINGS

In order to better understand the subject matter that is disclosed herein and to exemplify how it may be carried out in practice, embodiments will now be described, by way of non-limiting example only, with reference to the accompanying drawings, in
5 which:

Fig. 1 is an isometric view of a panel system according to an example of the presently disclosed subject matter, and in which the panel system is in a stowed configuration.

Fig. 2 is an isometric view of the panel system example of Fig. 1, in the deployed
10 configuration.

Fig. 3 is a first example of an actuator comprised in the panel system example of Fig. 1.

Fig. 4 illustrates in unfolded partial view an example of an outer cylinder and an actuation portion of the actuator example of Fig. 3.

Fig. 5 illustrates in unfolded partial view another example of an outer cylinder of
15 the actuator example of Fig. 3.

Fig. 6 illustrates in unfolded partial view another example of an outer cylinder of the actuator example of Fig. 3.

Fig. 7 schematically illustrates in unfolded partial view respective examples of an
20 outer cylinder and an actuation portion of a plurality of actuators of the example of Fig. 3 comprised in the panel system example of Fig. 1.

Fig. 8 is an isometric view of a panel system according to a second example of an actuator comprised in the panel system example of Fig. 1.

Fig. 9 is an isometric view of a panel system according to a third example of an
25 actuator comprised in the panel system example of Fig. 1.

Fig. 10(a) schematically illustrates an alternative variation of the panel system example of Fig. 1; **Fig. 10(b)** schematically illustrates another alternative variation of the panel system example of Fig. 1.

Fig. 11(a) schematically illustrates an alternative variation of the panel system
30 example of Fig. 1 in stowed configuration; **Fig. 11(b)** schematically the example of Fig. 1 in deployed configuration.

DETAILED DESCRIPTION

Referring to Figs. 1 and 2, a panel system according to a first example of the presently disclosed subject matter, generally designated **100**, comprises a first plurality of panel elements **200**, and a deployment system **500**.

5 In at least this example, the panel system **100** is configured to be mounted to a structure **800**, which in at least this example is in the form of a space vehicle, and the panel elements **200** are solar panels configured for generating electrical power. For example, the space vehicle can be a satellite, space station, ground vehicle, manned or unmanned space vehicle, or indeed a static space structure such as for example a base on the moon, and
10 asteroid or other space body. However, in alternative variations of this example, the panel system **100** can instead be mounted to any other suitable structure, for example in environments in which effects of gravity are not significant, for example underwater, and/or, the panel elements can instead be antenna elements, mechanical grappling elements, and so on.

15 The deployment system **500** is configured for deploying the plurality of panel elements **200** between a stowed configuration **SC** and a deployed configuration **DC**. In at least this example, the deployment system **500** is configured for deploying the plurality of panel elements **200** from the stowed configuration **SC** to the deployed configuration **DC**, and optionally to an intermediate partially deployed configuration, and also for deploying
20 the plurality of panel elements **200** from the deployed configuration **DC** to the stowed configuration **SC**, or to an intermediate partially deployed configuration. However, in at least some alternative variations of this example, the deployment system **500** is configured for non-reversibly deploying the plurality of panel elements **200** from the stowed configuration **SC** to the deployed configuration **DC**.

25 In at least this example, the panel elements **200** are essentially identical to one another, in size and shape, and each panel element **200** is generally planar, having a general rectangular plan form, with opposite facing faces **210**, **220**. However, in at least some alternative variations of this example, the panel elements can have any suitable shape and/or size, and may be identical to one another or different from one another.

30 In yet other alternative variations of this example, the panel elements can have a non-flat form, and/or can be hollow. For example, such "panel elements" can refer to any suitable

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structural components that are pivotably mounted to one another serially, and can be pivoted with respect to one another from a respective stowed configuration and a respective deployed configuration. In some examples, such panel elements can be in the form of strut modules that are stowed together in a compact manner in the respective stowed configuration, and
5 the strut modules pivot outwardly with respect to one another to form a mast or the like when fully pivoted to the deployed configuration.

While in the illustrated example in Figs. 1 and 2 the panel system **100** is shown as having five panel elements **200** serially disposed with respect to one another, this is for the purpose of illustration only. According to an aspect of the presently disclosed subject matter
10 the aforesaid first plurality of panel elements **200** can include 2, 3, 4, 6 or more than 6 panel elements **200**, and furthermore, the panel elements **200** can be pivotably mounted to one another in a variety of ways, not limited to the serially disposed example of Figs. 1 and 2.

For example, in the example illustrated in Fig. 10(a) there are a plurality of more than five panel elements **200** serially arranged in single file along a single deployment axis
15 **DA1**.

For example, in the example illustrated in Fig. 10(b) the plurality of panel elements **200** are divided into four sets: in the first set **200A**, the respective panel elements **200** are serially arranged in single file along a first deployment axis **DA1**, while in the other three sets **200B**, **200C**, **200D** the respective panel elements **200** are serially arranged in single file
20 along respective second deployment axis **DA2**, third deployment axis **DA3** and fourth deployment axis **DA4**. In the example of Fig. 10(b) the second deployment axis **DA2**, third deployment axis **DA3** and fourth deployment axis **DA4** are parallel to one another and orthogonal to the first deployment axis **DA1**, and furthermore all four deployment axes are generally co-planar. However, in alternative variations of this example, the plurality of panel
25 elements can include any number of sets of panel elements, and each set can have a respective deployment axis having any desired suitable orientation with respect to the other sets or their respective deployment axes.

In the examples illustrated in Figs. 1, 2, 10(a) and 10(b) the actuators of each adjacent pairs of actuators (along the deployment axis **DA**) are configured for pivoting in mutually
30 opposite directions, such that during deployment between the stowed configuration **SC** and

deployed configuration **DC** the panel system adopts an accordion-like intermediate configuration.

However, in at least some other examples, and referring for example to Fig. 11(a) and Fig. 11(b), adjacent pairs of actuators **550'** (along the deployment axis **DA**) are
5 configured for pivoting in the same direction, such that during deployment between the respective stowed configuration **SC** and the respective deployed configuration **DC** the panel system essentially unrolls about an unrolling axis **UA** from a generally spiral configuration, for example as illustrated in Fig. 11(a), to a nominally linear configuration, for example as illustrated in Fig. 11(b). In such examples, for example, the width of the respective panel
10 elements **200'** can diminish along the deployment axis **DA** in a direction away from the respective structure **800'** on the which the respective panel system **500'** is mounted.

Referring again in particular to Fig. 1, in at least this example, in the stowed configuration **SC**, the panel elements **200** have a compact configuration, for example in which the panel elements **200** are essentially serially superposed over one another, as
15 illustrated in Fig. 1 for example in a zig-zag manner. Thus, in the stowed configuration **SC** the faces **210**, **220** of one panel element are facing and in close proximity to the faces **210**, **220** of a respective adjacent panel element.

Referring in particular to Fig. 2, in the deployed configuration **DC**, the panel elements **200** are deployed along a respective deployment axis **DA**, as will become clearer
20 herein, to adopt a general planar configuration, in which the panel elements **200** are nominally planar with respect to one another, or at least in a relatively flat open accordion configuration, for example.

In at least this example, the first plurality of panel elements **200** comprises serially adjacent pairs of panel elements **200**, and for each such adjacent pair, the respective panel
25 elements **200** are pivotably mounted to one another about a respective pivot axis **PA**. Accordingly, each such adjacent pair of panel elements **200** comprises a suitable respective hinge arrangement **230**, comprising one or more hinges **232** having their pivot axes co-axial with the respective pivot axis **PA**.

It is to be noted that the innermost panel element **200** of the first plurality of panel elements is also pivotably mounted about a respective pivot axis **PA** with respect to the structure **800**.

The deployment system **500** comprises a second plurality of actuators **550**, an
5 actuation cable **590** and a drive unit **599**.

In at least this example, one such actuator **550** is associated with each respective pair of said panel elements, and is configured for transitioning the panel elements **200** of the respective adjacent pair between the respective stowed configuration **SC** and the respective deployed configuration **DC**, responsive to operation of drive unit **599** via the actuation cable
10 **590**.

However, in alternative variations of this example, each respective adjacent pair of panel elements **200** can instead have two or more than two such actuators **550**. In such a case, the two or more such actuators **550** are together configured for transitioning the panel elements **200** of the respective adjacent pair of panel elements **200**, between the stowed
15 configuration **SC** and the deployed configuration **DC**, responsive to operation of drive unit **599** via the actuation cable **590**.

Referring to Fig. 3, a first example of an actuator **550** comprises a first bracket **552**, a second bracket **554**, and a linear motion to rotary motion converter **600**.

The first bracket **552** is configured for being fixedly mounted to one panel element
20 **200** of the respective adjacent pair of panel elements, while the second bracket **554** is configured for being fixedly mounted to the other panel element of the respective adjacent pair of panel elements **200**. The first bracket **552** and the second bracket **554** can thus be mounted to the respective panel elements **200** in any suitable manner, for example by bolting, riveting, welding, bonding, and so on. Alternatively, the first bracket **552** and the
25 second bracket **554** can each be integrally formed with the respective panel element **200**.

The first bracket **552** and the second bracket **554** are also pivotably mounted with respect to one another about a respective actuator pivot axis **APA**, which is co-axial with the respective panel element pair pivot axis **PA**.

As will become clearer herein, the linear motion to rotary motion converter **600** is configured for pivoting the respective first bracket **552** with respect to the respective second bracket **554** responsive to a predetermined datum linear displacement being applied to the linear motion to rotary motion converter **600**.

- 5 The actuation cable **590** is serially coupled to each one of the actuators **550**, in a manner such as to enable applying at least the aforesaid datum linear displacement to the respective linear motion to rotary motion converter **600** of each actuator **550**.

 The actuation cable **590** is configured for being displaced linearly with respect to the plurality of actuators **550** at least between a first cable position **P1** and a second cable
10 position **P2**, responsive to operation of the drive unit **599**. The first position **P1** corresponds to the stowed configuration **SC**, while the second position **P2** corresponds to the deployed configuration **DC**.

 The drive unit **599** is configured for selectively displacing the actuation cable **590** at least between the first cable position **P1** and the second cable position **P2**. For example, the
15 drive unit **599** can be in the form of a rotary motor or linear motor, driven by electrical power or by pneumatic pressure or by hydraulic pressure, or can be in the form of a mechanical stored energy device, for example suitable spring arrangement, or can be in the form of a pyrotechnic device coupled to a piston arrangement, and so on.

 In at least this example, the linear motion to rotary motion converter **600**
20 comprises a linearly movable shaft element **610** and a rotary element **650**.

 The linearly movable shaft element **610** is slidably mounted between two ends **555A**, **555B** of the second bracket **554**, allowing relative axial movement between the shaft element **610** and the second bracket along the actuator pivot axis **APA**.

 The linearly movable shaft element **610** is fixedly coupled to the actuation cable
25 **590**.

 In at least the illustrated example, the second bracket **554** comprises an actuation portion **560**, comprising a pair of mechanical tabs **561**, **562**, fixedly mounted to the second bracket **554**, and spaced by an axial spacing **SP** from one another along an axis **AX** parallel to the actuator pivot axis **APA**. The mechanical tabs **561**, **562** each have a

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respective opening **563**, and the actuation cable **590** passes through the two openings **563**, exposing a length of actuation cable **590** between the two mechanical tabs **561**, **562** corresponding to the axial spacing **SP**. One end **610B** of the shaft element **610** projects out of the second end **555B** of the second bracket **554**, and is fixedly mounted via arm **592** to the actuation cable **590** at a location **591** within the exposed length of actuation cable **590** between the two mechanical tabs **561**, **562**. The arm **592** can thus be axially displaced between the two mechanical tabs **561**, **562** as the actuation cable **590** is concurrently displaced between the two mechanical tabs **561**, **562**. The two mechanical tabs **561**, **562** thus provide axial displacement limits for the actuation cable **590** via the arm **592**.

The rotary element **650** is fixedly mounted to the first bracket **552**.

Furthermore, the rotary element **650** is operatively coupled to the shaft element **610** such that the rotary element **650** pivots together with the first bracket **552** with respect to the second bracket **554** responsive to the aforesaid datum linear displacement being applied to the shaft element **610**.

In at least this example, the rotary element **650** comprises a jacket in the form of an outer cylinder **652** co-axial with and overlying at least part of the shaft element **610**. The outer cylinder **652** is fixedly mounted with respect to the first bracket **552**. The outer cylinder **652** comprises a cam groove **660** having at least one helical portion **660H**. The outer cylinder **652** is also co-axial with the respective actuator pivot axis **APA**.

As disclosed above, the shaft element **610** is movably mounted with respect to second bracket **554** in an axial direction parallel to, and in at least this example co-axial with, the actuator pivot axis **APA**. The shaft element **610** is mechanically constrained for enabling axial movement with respect to the second bracket **554**, and concurrently prevented from relative rotary movement with respect to the second bracket **554**. In at least this example, a first shaft element end portion **612** including end **610B** of the shaft element **610** has a non-circular cross-section, for example polygonal. The corresponding second end **555B** of the second bracket **554** with respect to which the first shaft element end portion **612** is mounted has an internal cross-section that is complementary to that of the first shaft element end portion **612**, thereby enabling relative axial movement of the shaft element **610** with respect to the second end **555B**, and thus with respect to the second

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bracket **554**, while concurrently preventing relative rotation of the shaft element **610** with respect to the second end **555B** about the actuator pivot axis **APA**, and thus with respect to the second bracket **554**.

In alternative variations of this example, other mechanical arrangements can be provided for constraining relative movement between the shaft element **610** and the second bracket **554** to axial movement while preventing relative rotary movement. For example, one of the shaft element **610** and the second bracket **554** can comprise a radial pin projecting towards the other, and the other one of the shaft element **610** and the second bracket **554** can comprise a complementary channel running along a direction parallel to the actuator pivot axis **APA**, in which the pin is received in and is able to slide along the channel.

The shaft element **610** comprises a cam follower **620**. In at least this example, the cam follower **620** is in the form of a pin radially projecting from a mid-section **655** of the shaft element **610**. The cam follower **620** is coupled to the cam groove **660**, such that relative movement between the shaft element **610** and the outer cylinder **652** is determined by the relative movement between the cam follower **620** and the cam groove **660**.

Thus, the shape of the cam groove **660** can be designed to provide the desired relative movement between the shaft element **610** and the outer cylinder **652** responsive to an axial displacement of the shaft element **610** with respect to the outer cylinder **652**.

Fig. 4 illustrates the outer cylinder **652** unfolded into a flat sheet, and compares (a) the movement of the cam follower **620** with respect to the cam groove **660**, with (b) the concurrent axial movement of the arm **592** with respect to the spacing **SP**.

In the example illustrated in Fig. 4, the cam groove **660** comprises:

- the aforesaid helical portion **660H**, located generally centrally;
- a first linear portion **660A1** located at a top end of the cam groove **660**;
- a first tapering portion **660T1** smoothly connecting the first linear portion **660A1** with one end of the helical portion **660H**;
- a second linear portion **660A2** located at a bottom end of the cam groove **660**;

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- a second tapering portion **660T2** smoothly connecting the second linear portion **660A2** with the other end of the helical portion **660H**.

Each one of the first linear portion **660A1**, the first tapering portion **660T1**, the
5 helical portion **660H**, the second tapering portion **660T2**, and the second linear portion
660A2 has a respective axial dimension **CY1**, **CY2**, **CY3**, **CY4**, **CY5**, respectively,
corresponding to respective axial displacement zones within the spacing **SP**: **SP1**, **SP2**,
SP3, **SP4**, **SP5**, respectively.

Since the arm **592**, shaft element **610** and cam follower **620** move as a rigid body,
10 any axial displacement of the arm **592** within the spacing **SP** results in the same axial
displacement of the cam follower **620** with respect to the cam groove **660**.

Thus, when the arm **592** is in axial displacement zone **SP1** or in axial displacement
zone **SP5**, the cam follower **620** is in first linear portion **660A1** or second linear portion
A2, respectively. Thus, axial displacement of the arm **592** within the first axial
15 displacement zone **SP1** causes the cam follower **620** to correspondingly move with
respect to the first linear portion **660A1**, while axial displacement of the arm **592** within
the fifth axial displacement zone **SP5** causes the cam follower **620** to correspondingly
move with respect to the second linear portion **660A2**. However, since the first linear
portion **660A1** and the second linear portion **A2** are each parallel to the actuator pivot
20 axis **APA**, such axial displacements do not result in any relative rotation between the
cylinder **650** and the shaft element **610**, and thus there is no pivoting between the first
bracket **552** and the second bracket **554**.

The first linear portion **660A1** and the second linear portion **660A2** provide
position tolerance for the cam follower **620**.

25 It is further to be noted that the first linear portion **660A1** and the second linear
portion **660A2** each provide a locking effect when the respective cam follower **620** is
located therein, since any external rotational force applied to the cylinder **650** is resisted
by the cam follower **620**, preventing pivoting.

Furthermore, the respective axial dimension **CY1**, **CY5** of the first linear portion
30 **660A1** and the second linear portion **660A2**, respectively, can be chosen such as to
provide a desired delay of the onset of pivoting (corresponding to the cam follower **620**
being in the helical portion **660H**) with respect to the axial displacement of the arm **592**.

When the arm **592** is in the central, third axial displacement zone **SP3**, the cam follower **620** is in the helical portion **660H**, and thus, axial displacement of the arm **592** within the third axial displacement zone **SP3** causes the cam follower **620** to correspondingly move with respect to the helical portion **660H**. The helical geometry of the helical portion **660H** ensures that any relative axial movement between the cam follower **620** and the cam groove **660** results in a corresponding and concurrent rotational movement between the cylinder **650** and the shaft element **610**, which in turn causes corresponding pivoting between the first bracket **552** and the second bracket **554** about the actuator pivot axis **APA**. It is to be noted that at least in this example, the third axial displacement zone **SP3** corresponds to the aforesaid datum linear displacement.

In at least this example, the helical portion **660H** corresponds to a half helix turn, and thus the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 180° , thereby enabling the respective adjacent pair of panel elements **200** mounted to the first bracket **552** and the second bracket **554** to pivot 180° about the actuator pivot axis **APA** from the stowed configuration **SC** to a flat and open (coplanar) deployed configuration **DC**.

In the unfolded view provided in Fig. 4, the contour of the helical portion **660H** appears as a sinusoidal groove, of half period corresponding to the half helix turn.

However, the helical portion **660H** can have any desired proportion of a full helix turn, and this will result in a corresponding pivoting angle between the first bracket **552** and the second bracket **554**. For example, if the helical portion **660H** corresponds to any one of $1/4$, $1/3$, $1/6$ helix turn, the corresponding pivoting angle will be 90° , 120° , 60° , respectively.

It is also to be noted that the helical portion **660H** also has a corresponding helix pitch, which in this example (in which the helical portion **660H** corresponds to a half helix turn) is $2 \cdot \text{CY3}$. The magnitude of the helix pitch determines the pivoting rate of the pivoting between the first bracket **552** and the second bracket **554**, with respect to linear displacement rate of the arm **592**. The smaller the helix pitch, the larger the corresponding pivot angle between the first bracket **552** and the second bracket **554** for a given axial displacement of the arm **592** within the third axial displacement zone **SP3**. Conversely, the higher the helix pitch, the smaller the corresponding pivot angle between the first bracket **552** and the second bracket **554** for a given axial displacement of the arm **592** within the third axial displacement zone **SP3**.

The first tapering portion **660T1** provides a smooth geometric transition between the first linear portion **660A1** and the helical portion **660H**, and similarly the second tapering portion **660T2** provides a smooth geometric transition between the second linear portion **660A2** and the helical portion **660H**. This enables the cam follower **620** to travel
5 the full extent of the cam groove **660**, in either direction, with a minimum or absence of jerking.

Thus, in the example of Fig. 4, as the arm **592** is displaced from a first arm position **AP1** at or close to first mechanical tab **561** to a second arm position **AP2** at or close to second mechanical tab **562** (responsive to the actuator cable **590** being corresponding
10 displaced), serially passing through the respective axial displacement zones within the spacing **SP**, i.e. spacings **SP1**, **SP2**, **SP3**, **SP4**, **SP5**, the cam follower **620** concurrently passes through the first linear portion **660A1**, the first tapering portion **660T1**, the helical portion **660H**, the second tapering portion **660T2**, and the second linear portion **660A2**, and causing relative pivoting between the first bracket **552** and the second bracket **554**
15 (in at least this example, to provide total pivoting of 180°) while the cam follower **620** is passing through the helical portion **660H**.

It is to be noted that the profile of the cam groove **660** can be chosen to provide the desired deployment profile for the respective actuator **550**, and thus for the respective adjacent pair of panel elements **200**.

It is to be further noted that in at least some examples, each one of the first linear portion **660A1**, the first tapering portion **660T1**, the second linear portion **660A2** and the second tapering portion **660T2** are optional, and the profile of the cam groove **660** can be chosen to include only the helical portion **660H**, or the helical portion **660H** plus any combination of the first linear portion **660A1**, the first tapering portion **660T1**, the second
25 linear portion **660A2** and the second tapering portion **660T2**.

For example, in at least some examples, the profile of the cam groove **660** can be chosen to include only the helical portion **660H**, and thus omits the first linear portion **660A1**, the first tapering portion **660T1**, the second linear portion **660A2** and the second tapering portion **660T2**.

For example, in at least some other examples, the profile of the cam groove **660** can be chosen to include the helical portion **660H** plus one or both of the first linear portion **660A1** and the second linear portion **660A2**, and thus omits the first tapering portion **660T1** and the second tapering portion **660T2**.

For example, in at least some other examples, the profile of the cam groove **660** can be chosen to include the helical portion **660H** plus one or both of first tapering portion **660T1** and the second tapering portion **660T2**, and thus omits the first linear portion **660A1** and the second linear portion **660A2**.

5 For example, Fig. 5 illustrates the outer cylinder **652** unfolded into a flat sheet, and provides an alternative example for the profile for the respective cam groove **660**. In this example, the respective cam groove **660** comprises:

- a first linear portion **660A1** located at a top end of the cam groove **660**;
- a first helical portion **660H1**, smoothly connected to the first linear portion **660A1** via a first tapering portion **660T1**;
- 10 - a second linear portion **660A2** located at a bottom end of the cam groove **660**;
- a second helical portion **660H2**, smoothly connected to the second linear portion **660A2** via a second tapering portion **660T2**;
- a centrally disposed third linear portion **660A3**, smoothly connected to the first helical portion **660H1** via a third tapering portion **660T3**, and smoothly connected to the second helical portion **660H2** via a fourth tapering portion **660T4**.
- 15

The first helical portion **660H1** and the second helical portion **660H2** are in the same rotational direction, for example both are right-handed or both are left-handed.

20 Thus, as the corresponding arm **592** is displaced from a first arm position **AP1** at or close to first mechanical tab **561** to a second arm position **AP2** at or close to second mechanical tab **562** (responsive to the actuator cable **590** being correspondingly displaced), serially passing through the respective axial displacement zones within the spacing **SP**, the cam follower **620** concurrently passes through the first linear portion **660A1**, the first tapering portion **660T1**, the first helical portion **660H1**, the third tapering portion **660T3**, the third axial portion **660A3**, the fourth tapering portion **660T4**, the second helical portion **660H2**, the second tapering portion **660T2**, and the second linear portion **660A2**. This motion causes pivoting between the first bracket **552** and the second bracket **554** while the cam follower **620** is passing through the first helical portion **660H1** and while passing through the second helical portion **660H2**, while stopping pivoting while the cam follower **620** is passing through the third axial portion **660A3**.

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In other words, full pivoting between the first bracket **552** and the second bracket **554** is carried out in two stages, with a break in-between, and this can be useful in situations for example in which, once the actuator **550** has finished pivoting re the first helical portion **660H1**, it is necessary to prevent interfering with another panel element
5 or other equipment that is also deploying, and once cleared the panel elements **200** can continue to deploy to its final position via the second helical portion **660H2** of the actuator **550**.

For example, the combination of the first helical portion **660H1** and the second helical portion **660H2** corresponds to a half helix turn, and thus the first bracket **552** and
10 the second bracket **554** pivot with respect to one another by a total pivot angle of 180° , thereby enabling the respective adjacent pair of panel elements **200** mounted to the first bracket **552** and the second bracket **554** to pivot 180° from the stowed configuration **SC** to a flat and open (coplanar) deployed configuration **DC**, though in two stages.

For example, the first helical portion **660H1** and the second helical portion **660H2**
15 are equal in magnitude and direction. For example, the first helical portion **660H1** and the second helical portion **660H2** each correspond to $1/4$ helix turn. Thus, the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 90° corresponding to the first helical portion **660H1**, and subsequently the first bracket **552** and the second bracket **554** pivot with respect to one another by another pivot angle of
20 90° corresponding to the second helical portion **660H2**.

In another variation of this example, the first helical portion **660H1** and the second helical portion **660H2** are not equal in magnitude. For example, the first helical portion **660H1** corresponds to $1/6$ helix turn, while the second helical portion **660H2** corresponds to $2/6$ helix turn. Thus, the first bracket **552** and the second bracket **554** pivot with respect
25 to one another by a pivot angle of 60° corresponding to the first helical portion **660H1**, and subsequently the first bracket **552** and the second bracket **554** pivot with respect to one another by another pivot angle of 120° corresponding to the second helical portion **660H2**.

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It is to be noted that the full pivot angle of any one of the examples herein is not required to be 180°, and can be any desired angle, for example 90°, 120°, 270°, or any other pivot angle up to just under 360°.

For example, Fig. 6 illustrates the outer cylinder **652** unfolded into a flat sheet,
5 and provides another alternative example for the profile for the respective cam groove **660**. In this example, the respective cam groove **660** comprises:

- a first linear portion **660A1** located at a top end of the cam groove **660**;
- a first helical portion **660H1**, smoothly connected to the first linear portion **660A1** via a first tapering portion **660T1**;
- 10 - a second linear portion **660A2** located at a bottom end of the cam groove **660**;
- a second helical portion **660H2**, smoothly connected to the second linear portion **660A2** via a second tapering portion **660T2**;
- a centrally disposed third linear portion **660A3**, smoothly connected to the first helical portion **660H1** via a third tapering portion **660T3**, and smoothly
15 connected to the second helical portion **660H2** via a fourth tapering portion **660T3**.

The first helical portion **660H1** and the second helical portion **660H2** are in opposite rotational directions, for example one is right-handed and the other is left-handed.

20 Thus, as the corresponding arm **592** is displaced from a first arm position **AP1** at or close to first mechanical tab **561** to a second arm position **AP2** at or close to second mechanical tab **562** (responsive to the actuator cable **590** being correspondingly displaced), serially passing through the respective axial displacement zones within the spacing **SP**, the cam follower **620** concurrently passes through the first linear portion **660A1**, the first
25 tapering portion **660T1**, the first helical portion **660H1**, the third tapering portion **660T3**, the third axial portion **660A3**, the fourth tapering portion **660T4**, the second helical portion **660H2**, the second tapering portion **660T2**, and the second linear portion **660A2**. This motion causes pivoting between the first bracket **552** and the second bracket **554** while the cam follower **620** is passing through the first helical portion **660H1** and while
30 passing through the second helical portion **660H2**, while stopping pivoting while the cam follower **620** is passing through the third axial portion **660A3**.

In other words, the first bracket **552** and the second bracket **554** first pivot in one direction (for example to open, from the stowed configuration **SC** to the deployed configuration **DC**), and then the first bracket **552** and the second bracket **554** can pivot back in the opposite direction (for example to close, from the deployed configuration **DC** to the stowed configuration **SC**), with a break in-between. This configuration can be useful in situations for example in which it is desired to both deploy and subsequently stow the panel elements **200**, and in which the drive unit **599** and actuator cable **590** can only operate in one direction (for example in tension but not in compression).

For example, each one of the first helical portion **660H1** and the second helical portion **660H2** corresponds to a half helix turn, and thus the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 180° , and then by a pivot angle of -180° . This enables the respective adjacent pair of panel elements **200** mounted to the first bracket **552** and the second bracket **554** to pivot 180° from the stowed configuration **SC** to a flat and open (coplanar) deployed configuration **DC**, and then back from the deployed configuration **DC** to the stowed configuration **SC**.

However, in at least one alternative variation of this example, the first helical portion **660H1** and the second helical portion **660H2** are not equal in magnitude. For example, the first helical portion **660H1** corresponds to $1/2$ helix turn in one direction, while the second helical portion **660H2** corresponds to $1/4$ helix turn in the opposite direction. Thus, the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 180° in one direction, corresponding to the first helical portion **660H1**, and subsequently the first bracket **552** and the second bracket **554** pivot with respect to one another by another pivot angle of 90° in the opposite direction corresponding to the second helical portion **660H2**.

In another example, the first helical portion **660H1** corresponds to $4/6$ helix turn in one direction, while the second helical portion **660H2** corresponds to $1/6$ helix turn in the opposite direction. Thus, the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 240° in one direction, corresponding to the first helical portion **660H1**, and subsequently the first bracket **552** and the second bracket **554** pivot with respect to one another by another pivot angle of 60° in the opposite direction

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corresponding to the second helical portion **660H2**, thereby leaving the first bracket **552** and the second bracket **554** at a final pivot angle with respect to one another of 180° .

In another example, the first helical portion **660H1** corresponds to $3/4$ helix turn in one direction, while the second helical portion **660H2** corresponds to $1/4$ helix turn in the opposite direction. Thus, the first bracket **552** and the second bracket **554** pivot with respect to one another by a pivot angle of 270° in one direction, corresponding to the first helical portion **660H1**, and subsequently the first bracket **552** and the second bracket **554** pivot with respect to one another by another pivot angle of -90° , i.e., in the opposite direction, corresponding to the second helical portion **660H2**, thereby leaving the first bracket **552** and the second bracket **554** at a final pivot angle with respect to one another of 180° .

Thus, such examples of the configuration as exemplified by Fig. 6 can be useful in examples in which it may be necessary for one panel element **200** to overshoot the respective position corresponding to the final deployed configuration, perhaps to prevent interfering with another panel element or other equipment that is also deploying, and once cleared the panel element **200** can return to its final position.

Referring again to Fig. 2, Fig. 3 and Fig. 7, for example, the actuation cable **590** is coupled to all the actuators **550** comprised in the panel system **500**. The drive unit **599** is configured for selectively displacing the actuation cable **590** at least between the first cable position **P1** and the second cable position **P2**, corresponding to a cable displacement of **CD**.

The cable displacement **CD** is less than or equal to the axial spacing **SP** of the actuators **550**. It is to be noted that while in this example all the actuators **550** are similar or identical to one another, and have the same axial spacing **SP** with respect to one another, in alternative variations of this example, it is possible for the actuators **550** of the panel system **500** to be different from one another, or to at least have corresponding axial spacing **SP** that can be different from one another. In cases in which the actuators of the panel system **500** have axial spacing **SP** different from one another, the cable displacement **CD** is less than or equal to the axial spacing **SP** of the actuator **550** having the smallest axial spacing **SP**.

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In any case, the cable displacement **CD** is at least equal to the spacing between the first arm position and the second arm position of the actuators **550** of the actuator **550** having the smallest axial spacing **SP**.

As the actuation cable **590** is displaced between the first cable position **P1** and the
5 second cable position **P2**, the arms **592** corresponding to all the actuators **550** are concurrently displaced from the respective first arm positions **AP1** to the respective second arm positions **AP2**, concurrently driving the respective cam followers **620** with respect to the respective cam grooves **660** of the actuators.

In at least the above examples, the actuation cable **590** is enclosed within an
10 envelope **700** comprising a second plurality of windows **780**, the envelope **700** being configured for maintaining a predetermined tension in the actuation cable **590**. One such window **780** is provided for each actuator **550**, and is co-extensive with the actuation portion **560**, in particular between the first tab **561** and the second tab **562**, thereby exposing the actuation cable **590** between the first tab **561** and the second tab **562**.

15 Referring again to Fig. 2, each actuator **550** is operatively coupled to the actuation cable **590** at a respective window **780**, wherein the respective arm **592** is affixed to the cable **590** and is free to move with the actuation cable **590** between the respective first tab **561** and the respective second tab **562**.

Such a predetermined tension ensures that any displacement of the actuation cable
20 **590** at the end thereof coupled to the drive unit **599** is concurrently transmitted and reproduced at each actuation portion **560**.

It can be readily appreciated that the actuators **550** of the second plurality of actuators **550** are configured for operating in a synchronized manner with respect to one another, and in particular for pivoting in a synchronized manner with respect to one
25 another, responsive to operation of the drive unit and the actuation cable, since displacement of the actuation cable **590** is transmitted simultaneously to all the actuators **550**.

In at least this example, the envelope is in the form of a sheath, in particular in the form of an incompressible sheath having a lumen that allows relative axial movement
30 between the cable and the sheath, but essentially preventing the cable from buckling. For

example, the sheath is longitudinally incompressible, and in at least some examples can be in the form of a Bowden cable. Such a sheath is fixedly attached at the outer facing ends of each respective pair of first tab **561** and second tab **562**.

In alternative variations of this example, such an envelope can be integrated within the panel elements **200**, and for example can be in the form of suitable incompressible channels or lumens provided in the panel elements **200**.

As disclosed above, in at least the illustrated examples, the deployment system **500** is configured for reversibly deploying the plurality of panel elements **200** between the stowed configuration **SC** and the deployed configuration **DC**. For example, the deployment system **500** is configured for deploying the plurality of panel elements **200** from the stowed configuration **SC** to the deployed configuration **DC**, and also for deploying the plurality of panel elements **200** from the deployed configuration **DC** to the stowed configuration **SC**, or to an intermediate partially deployed configuration. In such cases, and referring again to Fig. 2, the deployment system **500** can further comprise a tensioning arrangement **580** coupled to the actuation cable **590**. The tensioning arrangement **580** provides a tensile force to the actuation cable **590** regardless of which direction the actuation cable **590** is being displaced. For example, when the actuation cable **590** is being pulled in one direction towards the drive unit **599**, this of itself provides a tension in the actuation cable **590** and the tensioning arrangement **580** may not be required. However, when the actuation cable **590** is being pushed in the opposite direction away from the drive unit **599**, the tensioning arrangement **580** provides the required tension in the actuation cable **590** to enable displacement of the actuation cable **590** at the drive unit end to be reproduced at each actuator **550**. For example, the tensioning arrangement **580** can be in the form of a pre-stressed spring, anchored at one end to one of the panels, and coupled at another end of the spring to the actuation cable **590**.

At least in the example of Fig. 2, all the actuators **550** of the second plurality of actuators **550** are configured for pivoting simultaneously responsive to a predetermined linear displacement being applied to each one of the respective linear motion to rotary motion converters **600**. Also in at least this example, all the actuators **550** of the second plurality of actuators **550** are configured for pivoting at the same pivoting rate responsive

to a predetermined linear displacement rate being applied to all the respective linear motion to rotary motion converters **600**.

As such, all the actuators **550** have the same cam groove configuration for the respective cam grooves **660**. In other words, the shape and size of the respective cam
5 grooves **660** are the same for all the actuators **550**.

Thus, as the actuation cable **590** is displaced from the first cable position **P1** through to the second cable position **P2**, the respective arms **592** of all the actuators are concurrently displaced from the respective first arm positions **AP1** to the respective second arm positions **AP2**, simultaneously pivoting each adjacent pair of panel elements
10 from the respective stowed configuration **SC** to the deployed configuration **DC**. Similarly, actuation of the drive unit **599** in the opposite direction such as to displace the actuation cable from the second cable position **P2** to the first cable position **P1** causes all the actuators **550** to unfold the panel elements **200** simultaneously from the deployed configuration **DC** to the stowed configuration **SC**.

15 However, in alternative variations of this example, the actuators **550** of the second plurality of actuators **550** can instead be configured for pivoting non-simultaneously with respect to one another, responsive to a predetermined linear displacement being applied simultaneously to all the respective linear motion to rotary motion converters **600**, and/or, at least some of the actuators **550** of the second plurality of actuators **550** are configured
20 for pivoting at respective pivoting rates that are different with respect to one another, responsive to a predetermined linear displacement rate being applied simultaneously to all the respective linear motion to rotary motion converters **600**. Thus, for example, the drive unit **599** can be operated to displace the actuation cable **590** at a constant displacement rate, and this can cause the actuators **550** to pivot at respective pivoting
25 rates that are different with respect to one another, thereby causing the respective panels **200** to transit between the respective stowed configurations **SC** and the respective deployed configurations **DC** at relatively different rates with respect to one another.

For example, it may be desired that one set of the panel elements **200** are to concurrently fully deploy from the respective stowed configuration **SC** to the deployed
30 configuration **DC**, while another set of the panel elements **200** are to delay their respective deployment.

By way of example, and referring to Fig. 7, only four actuators **550** of the second plurality of actuators **550** are illustrated, for the sake of simplification, in which the actuation cable **590** is operatively connected to the respective linear motion to rotary motion converters **600**. The four actuators **550** – individually referred to as actuators **550A**, **550B**, **550C**, **550D** – have respective cylinders **650A**, **650B**, **650C**, **650D**, each having its respective cam groove **660A**, **660B**, **660C**, **660D**, coupled to the respective cam followers **620A**, **620B**, **620C**, **620D**.

Also for the sake of simplification, each respective cam groove **660A**, **660B**, **660C**, **660D** is shown having a first linear portion **A1**, a helical portion **H**, and a second linear portion **A2**. However, each respective cam groove **660A**, **660B**, **660C**, **660D** can optionally also have transition portions between each respective first linear portion **A1** and helical portion **H**, and between respective helical portion and the second linear portion **A2**.

The respective first linear portions **A1** of the first cam groove **660A** and the second cam groove **660B** are of the same axial length, and are significantly shorter than the lengths of the respective first linear portions **A1** of the third cam groove **660C** and the fourth cam groove **660D**.

The respective helical portion **H** of the second cam groove **660B** is axially longer than the respective helical portion **H** of the first cam groove **660A**; the respective second linear portion **A2** of the second cam groove **660B** is correspondingly axially shorter than the respective first linear portion **A1** of the first cam groove **660A**.

In at least this example, the third cam groove **660C** and the fourth cam groove **660D** are identical. The respective first linear portions **A1** of the third cam groove **660C** and the fourth cam groove **660D** are longer than the respective first linear portions **A1** of the first cam groove **660A** and the second cam groove **660B**. In at least this example, the respective first linear portions **A1** of the third cam groove **660C** and the fourth cam groove **660D** are longer than the combination of the respective first linear portion **A1** and helical portion **H** of the first cam groove **660A** or of the second cam groove **660B**.

The respective second linear portions **A2** of the third cam groove **660C** and the fourth cam groove **660D** are shorter than the respective second linear portions **A2** of the

first cam groove **660A** and the second cam groove **660B**. In at least this example, the respective first linear portions **A1** of the first cam groove **660A** and the second cam groove **660B** are each longer than the combination of the respective second linear portion **A2** and helical portion **H** of the third cam groove **660C** or of the fourth cam groove **660D**.

5 The respective arms (not shown in this figure) of the respective actuators **550A**, **550B**, **550C**, **550D** are fixedly connected to the actuation cable **590** such that when the actuation cable is at the first cable position **P1**, the respective cam followers **620A**, **620B**, **620C**, **620D** are each located at the uppermost end of the respective cam groove **660A**, **660B**, **660C**, **660D** (as seen in Fig. 7).

10 As the actuation cable **590** is displaced from the first cable position **P1** towards the second cable position **P2**, under the action of the drive unit **599**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced by the same displacement.

 As the actuation cable **590** is displaced from the first cable position **P1** towards the second cable position **P2** by a first cable displacement **CD1**, all four cam followers
15 **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD1**, and are located, at the end of the displacement, still in the respective first linear portion **A1** of the respective cam groove **660A**, **660B**, **660C**, **660D**. Accordingly, during this displacement, there is no relative rotation between the respective first bracket and second bracket of any of the four actuators **550A**, **550B**, **550C**, **550D**, and the respective
20 panel elements **200** remain effectively in the stowed configuration **SC**.

 As the actuation cable **590** is displaced further towards the second cable position **P2** by a second cable displacement **CD2**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD2**. During the course of the second cable displacement **CD2**, the first cam follower **620A** completes passage with
25 respect to the respective helical portion **H** of the first cam groove **660A**, and thus the two respective panel elements **200** mounted to the first actuator **550A** are fully deployed from the respective stowed configuration **SC** to the respective deployed configuration **DC**. Concurrently, the second cam follower **620B** travels along a first part of the respective helical portion **H** of the second cam groove **660B**, and thus the two respective panel
30 elements **200** mounted to the second actuator **550B** are only partially deployed from the respective stowed configuration **SC** to the respective deployed configuration **DC**.

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Concurrently, the third cam follower **620C** and the fourth cam follower **620D** are still within the respective first linear portions **A1** of the respective third cam groove **660C** and fourth cam groove **660D**, and thus the two respective panel elements **200** mounted to the third and fourth actuators **550C**, **550D** remain in the respective stowed configuration **SC**.

5 As the actuation cable **590** continues to be displaced further towards the second cable position **P2** by a third cable displacement **CD3**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD3**. During the course of the third cable displacement **CD3**, the first cam follower **620A** is now in the respective second linear portion **A2** of the first cam groove **660A**, and thus the two
10 respective panel elements **200** mounted to the first actuator **550A** are effectively locked in the respective deployed configuration **DC**. Concurrently, the second cam follower **620B** completes its passage with respect to the respective helical portion **H** of the second cam groove **660B**, and thus the two respective panel elements **200** mounted to the second actuator **550B** are now fully deployed from the previous partially deployed configuration
15 to the respective deployed configuration **DC**. Concurrently, the third cam follower **620C** and the fourth cam follower **620D** are still within the respective first linear portions **A1** of the respective third cam groove **660C** and fourth cam groove **660D**, and thus the two respective panel elements **200** mounted to the third actuator **550C**, and the two respective panel elements **200** mounted to the fourth actuator **550D** remain in the respective stowed
20 configuration **SC**.

 As the actuation cable **590** continues to be displaced further towards the second cable position **P2** by a fourth cable displacement **CD4**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD4**. The first cam follower **620A** and the second cam follower **620B** are located, at the end of
25 this displacement, within the respective second linear portions **A2** of the first cam groove **660A** and second cam groove **660B**, respectively. Concurrently, the third cam follower **620C** and the fourth cam follower **620D** are still located, at the end of this displacement, within the respective first linear portions **A1** of the third cam groove **660C** and fourth cam groove **660D**, respectively. Accordingly, during this fourth cable displacement **CD4**,
30 there is no relative rotation between the respective first bracket and second bracket of any of the four actuators **550A**, **550B**, **550C**, **550D**, and the panel elements **200** remain

effectively in the same relative positions as at the end of the third cable displacement **CD3**.

As the actuation cable **590** continues to be displaced further towards the second cable position **P2** by a fifth cable displacement **CD5**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD5**. The first cam follower **620A** and the second cam follower **620B** continue to travel in, and thus are still located, within the respective second linear portions **A2** of the first cam groove **660A** and second cam groove **660B**, respectively. Thus, there is no relative rotation between the respective first bracket and second bracket of first actuator **550A**, or between the respective first bracket and second bracket of second actuator **550B**. Concurrently, the third cam follower **620C** completes passage with respect to the helical portion **H** of the third cam groove **660C**, and thus the two respective panel elements **200** mounted to the third actuator **550C** are fully deployed from the respective stowed configuration **SC** to the respective deployed configuration **DC**. Also concurrently, the fourth cam follower **620D** completes passage with respect to the helical portion **H** of the fourth cam groove **660D**, and thus the two respective panel elements **200** mounted to the fourth actuator **550D** are fully deployed from the respective stowed configuration **SC** to the respective deployed configuration **DC**.

As the actuation cable **590** continues to be displaced further by a sixth cable displacement **CD6** to now reach the second cable position **P2**, all four cam followers **620A**, **620B**, **620C**, **620D** are concurrently displaced axially by the same displacement **CD6**. The four cam followers **620A**, **620B**, **620C**, **620D** are located during this displacement and at the end of the displacement, in the respective second linear portion **A2** of the respective cam groove **660A**, **660B**, **660C**, **660D**. Accordingly, during this displacement, there is no relative rotation between the respective first bracket and second bracket of any of the four actuators **550A**, **550B**, **550C**, **550D**, and the panel elements **200** remain effectively in the deployed configuration **DC**.

Thus, in summary, as the actuation cable **590** is displaced from the first cable position **P1** to the second cable position **P2**, the first actuator **550A** and the second actuator **550B** simultaneously begin deployment from the respective stowed configurations **SC**, with the second actuator **550B** reaching the respective deployed

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configuration **DC** some time after the first actuator **550A** has been fully deployed to the respective deployed configuration **DC**. Up to this point, the third actuator **550C** and the fourth actuator **550D** remain in the respective stowed configurations **SC**. Subsequently, as the actuation cable **590** continues to be displaced towards the second cable position

5 **P2**, the third actuator **550C** and the fourth actuator **550D** concurrently deploy from the respective stowed configurations **SC** to the respective deployed configurations **DC**. After this point, all four actuators **550A**, **550B**, **550C**, **550D** are essentially locked in the respective deployed configurations **DC**, and remain in this condition until the actuation cable **590** reaches the second cable position **P2**.

10 While in the above examples each adjacent pair of panel elements has respective hinges **232**, independent from the respective actuator(s) **550**, in at least some alternative variations of these examples, one, or more than one, or all such hinges **232** can each be replaced with a respective actuator **550**, such that each such actuator **550** operates both as a hinge as well as an actuator.

15 While in the above examples the linear motion to rotary motion converter **600** has been exemplified with respect to a can follower/cam groove arrangement, in at least other examples, the respective linear motion to rotary motion converter can be any suitable mechanical arrangement in which an input in the form of an axial displacement results in a rotary motion output, the input being coupled to the actuation cable while the output is

20 coupled to the adjacent pair of panel elements.

For example, and referring to Fig. 8, a second example of an actuator, designated with reference numeral **550A** is similar to actuator **550** as disclosed herein with some differences *mutatis mutandis*, as will become clearer herein. The actuator **550A** comprises a first bracket **552A**, a second bracket **554A**, and a linear motion to rotary motion converter

25 **600A**. The first bracket **552A** and the second bracket **554A** can be similar to the first bracket **552** and the second bracket **554** as disclosed here, *mutatis mutandis*. Thus, the first bracket **552A** is configured for being fixedly mounted in any suitable manner to one panel element **200** of the respective adjacent pair of panel elements, while the second bracket **554A** is configured for being fixedly mounted in any suitable manner to the other panel element of

30 the respective adjacent pair of panel elements **200**.

In this example, the linear motion to rotary motion converter **600A** is in the form of a rack and pinion arrangement, comprising an axially movable element in the form of a rack element **620A**, coupled to a rotary element in the form of a pinion element **670A**, such that linear motion of the rack element **620A** along an actuation axis **AA** causes the pinion element **670A** to rotate about the rotational axis **RAA** of the pinion element **670A**. In at least this example, the rotational axis **RAA** of the pinion element **670A** is parallel to, and co-axial with, the respective actuator pivot axis **APAA**. Furthermore, in at least this example, the actuation axis **AA** is parallel to the rotational axis **RAA** and to, the respective actuator pivot axis **APAA**. For example, the rack element **620A** is reciprocally linearly movably mounted between two end brackets **661A**, **662A**, which are fixedly mounted to the second bracket **554A**, and spaced by an axial spacing from one another along the actuation axis **AA**. Thus, the rack element **620A** is reciprocally slidable between two end brackets **661A**, **662A**. Two mechanical tabs **561A**, **562A**, are fixedly mounted to the second bracket **554A**, and spaced by an axial spacing **SP** from one another along an axis **AX** parallel to the actuator pivot axis **APAA**, in a similar manner to the example of Fig. 3, *mutatis mutandis*.

In a similar manner to the first example, *mutatis mutandis*, the mechanical tabs **561A**, **562A** each have a respective opening, and the respective actuation cable **590A** passes through the two openings exposing a length of actuation cable **590A** between the two mechanical tabs **561A**, **562A** corresponding to the axial spacing **SP**.

The rack element **620A** is fixedly mounted via arm **592A** to the actuation cable **590A** at a location **591A** within the exposed length of actuation cable **590A** between the two mechanical tabs **561A**, **562A**. The arm **592A** can thus be axially displaced between the two mechanical tabs **561A**, **562A** as the actuation cable **590A** is concurrently displaced between the two mechanical tabs **561A**, **562A**, thereby concurrently displacing the rack element **620A** between two end brackets **661A**, **662A**. The two mechanical tabs **561A**, **562A** thus provide axial displacement limits for the actuation cable **590A**.

The rotary element in the form of pinion element **670A** is fixedly mounted to the first bracket **552A**. In at least this the pinion element **670A** is in the form of a worm gear,

Thus, in operation of the deployment system, as the actuation cable **590A** is linearly displaced between mechanical tabs **561A**, **562A** via the respective drive unit, the rack element **620A** is concurrently displaced linearly via the arm **592A**, which in turn causes the

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pinion element **670A** to rotate, thereby causing the respective two panel elements **200** to pivot about the respective pivot axis **PA**.

The magnitude of the displacement of the actuation cable **590A**, and thus of the arm **592A**, determines the pivoting angle between the first bracket **522A** and the second bracket **554A**, and thus between the two panel elements **200**.

In at least this example, the actuator **550A** is configured for reversibly pivoting, such that when the actuation cable **590A** is displaced in one direction the first bracket **522A** pivots with respect to the second bracket **554A** in one direction, while when the actuation cable **590A** is displaced in the opposite direction the first bracket **522A** pivots with respect to the second bracket **554A** in the opposite direction.

In a similar manner to that disclosed herein for the first example illustrated in Fig. 2, *mutatis mutandis*, in the example of Fig. 8 the actuation cable **590A** is enclosed within an envelope **700A** comprising a second plurality of windows **780A**.

Referring to Fig. 9, a third example of an actuator designated with reference numeral **550B** is similar to actuator **550** as disclosed herein with some differences *mutatis mutandis*, as will become clearer herein. The actuator **550B** comprises a first bracket **552B**, a second bracket **554B**, and a linear motion to rotary motion converter **600B**. The first bracket **552B** and the second bracket **554B** can be similar to the first bracket **552** and the second bracket **554** as disclosed here, *mutatis mutandis*. Thus, the first bracket **552B** is configured for being fixedly mounted in any suitable manner to one panel element **200** of the respective adjacent pair of panel elements, while the second bracket **554B** is configured for being fixedly mounted in any suitable manner to the other panel element of the respective adjacent pair of panel elements **200**.

In this example, the linear motion to rotary motion converter **600B** is in the form of a slider crank arrangement, comprising an axially movable element in the form of a slider element **620B**, coupled to a rotary element in the form of a crankshaft element **670B** via connecting rod **675B**, such that linear motion of the slider element **620B** along an actuation axis **BB** causes the crankshaft element **670B** to rotate about the rotational axis **RAB** of the crankshaft element **670B**. In at least this example, the rotational axis **RAB** of the crankshaft element **670B** is parallel to, and co-axial with, the respective actuator pivot axis **APAB**.

Furthermore, in at least this example, the actuation axis **BB** is orthogonal to the rotational axis **RAB** and to, the respective actuator pivot axis **APAB**. For example, the slider element **620B** is reciprocally linearly movably mounted between two end brackets **661B**, **662B**, which are fixedly mounted to the second bracket **554B**, and spaced by an axial spacing from one another along the actuation axis **BB**. Thus, the slider element **620B** is reciprocally slidable between two end brackets **661B**, **662B**. Two mechanical tabs **561B**, **562B**, are fixedly mounted to the second bracket **554B**, and spaced by an axial spacing **SP** from one another along an axis **BX** parallel to the actuation axis **BB**, in a similar manner to the example of Fig. 3, *mutatis mutandis*.

10 In a similar manner to the first example, *mutatis mutandis*, the mechanical tabs **561B**, **562B** each have a respective opening, and the respective actuation cable **590B** passes through the two openings exposing a length of actuation cable **590B** between the two mechanical tabs **561B**, **562B** corresponding to the axial spacing **SP**.

The slider element **620B** is fixedly mounted via arm **592B** to the actuation cable **590B** at a location **591B** within the exposed length of actuation cable **590B** between the two mechanical tabs **561B**, **562B**. The arm **592B** can thus be axially displaced between the two mechanical tabs **561B**, **562B** as the actuation cable **590B** is concurrently displaced between the two mechanical tabs **561B**, **562B**, thereby concurrently displacing the slider element **620B** between two end brackets **661B**, **662B**. The two mechanical tabs **561B**, **562B** thus provide axial displacement limits for the actuation cable **590B**.

The rotary element in the form of crankshaft element **670B** is fixedly mounted to the first bracket **552B**. In at least this the crankshaft element **670B** is in the form of a strut. The connecting rod **675B** is pivotably connected to the crankshaft element **670B** via a first pin **671B** about a first pivot axis **PA1**. The connecting rod **675B** is pivotably connected to the slider element **620B** via a second pin **672B** about a second pivot axis **PA2**.

Thus, in operation of the deployment system, as the actuation cable **590B** is linearly displaced between mechanical tabs **561B**, **562B** via the respective drive unit, the slider element **620B** is concurrently displaced linearly via the arm **592B**, which in turn causes the crankshaft element **670B**, via the connecting rod **675B**, to pivot about the actuator pivot axis

APAB, thereby causing the respective two panel elements **200** to pivot about the respective pivot axis **PA**.

The magnitude of the displacement of the actuation cable **590B**, and thus of the arm **592B**, determines the pivoting angle between the first bracket **552B** and the second bracket **554B**, and thus between the two panel elements **200**.

In at least this example, the actuator **550B** is configured for reversibly pivoting, such that when the actuation cable **590B** is displaced in one direction the first bracket **552B** pivots with respect to the second bracket **554B** in one direction, while when the actuation cable **590B** is displaced in the opposite direction the first bracket **552B** pivots with respect to the second bracket **554B** in the opposite direction.

In a similar manner to that disclosed herein for the first example illustrated in Fig. 2, *mutatis mutandis*, in the example of Fig. 9 the actuation cable **590B** is enclosed within an envelope **700B** comprising a second plurality of windows **780B**.

Referring again to Fig. 1, the panel system **100**, in particular the deployment system **500**, can further comprise a locking arrangement **585**, coupled to the actuation cable **590**. The locking arrangement **585** is configured for maintaining the plurality of panels **200** locked in the stowed configuration **SC** at least until the drive unit **599** is activated. For example, the locking arrangement **585** can be configured for transitioning to a respective unlocked mode, in which the locking arrangement **585** is no longer locking the panels **200**, responsive to a linear displacement of the actuation cable **590**. Thus, at the beginning of displacement of the actuation cable via the drive unit **590**, the locking arrangement **585** is first unlocked, and subsequent displacement of the locking arrangement **585** results in pivoting of the panels **200**, as disclosed herein for example. For example, such a locking arrangement **585** can be in the form of for example a bolt lock, barrel bolt, latch, and so on.

In the method claims that follow, alphanumeric characters and Roman numerals used to designate claim steps are provided for convenience only and do not imply any particular order of performing the steps.

Finally, it should be noted that the word “comprising” as used throughout the appended claims is to be interpreted to mean “including but not limited to”.

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While there has been shown and disclosed examples in accordance with the presently disclosed subject matter, it will be appreciated that many changes may be made therein without departing from the scope of the presently disclosed subject matter as set out in the claims.

CLAIMS:

1. A deployment system for pivotably deploying a first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective panel element pair pivot axis, the deployment system comprising a second plurality of actuators, an actuation cable and a drive unit, wherein:

at least one said actuator is associated with each respective pair of said panel elements, each said actuator comprising a first bracket, a second bracket and a linear motion to rotary motion converter, the first bracket being configured for being fixedly mounted to one panel element of the pair, the second bracket being configured for being fixedly mounted to another panel element of the pair, the respective first bracket and the respective second bracket being pivotably mounted with respect to one another about an actuator pivot axis co-axial with the respective panel element pair pivot axis, and wherein the linear motion to rotary motion converter is configured for pivoting the respective first bracket with respect to the respective second bracket responsive to a predetermined datum linear displacement being applied to the linear motion to rotary motion converter;

the actuation cable being serially coupled to each said actuator of said second plurality of actuators, the actuation cable configured for being displaced linearly with respect to the plurality of actuators at least between a first cable position, corresponding to the stowed configuration, and a second cable position, corresponding to the deployed configuration, responsive to operation of the drive unit, such as to apply at least a corresponding said datum linear displacement to the respective linear motion to rotary motion converter of each said actuator;

the drive unit being configured for selectively displacing the actuation cable at least between the first cable position and the second cable position.

2. The deployment system according to claim 1, wherein each respective said linear motion to rotary motion converter comprises a linearly movable shaft element, coupled to the actuation cable.

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3. The deployment system according to claim 2, wherein each respective said linear motion to rotary motion converter comprises a respective rotary element operatively coupled to the shaft element such that the rotary element pivots the respective first bracket with respect to the respective second bracket responsive to a respective said datum linear displacement being applied to the shaft element.

4. The deployment system according to claim 3, wherein the rotary element comprises an outer cylinder co-axial with and overlying at least part of the shaft element, the outer cylinder fixedly mounted with respect to the first bracket, the outer cylinder comprising a cam groove having at least one helical portion, and wherein the shaft element is movably mounted with respect to said second bracket, the shaft element being constrained for axial movement with respect to the second bracket and prevented from relative rotary movement with respect to the second bracket, wherein the shaft element comprises a cam follower coupled to the cam groove, and wherein application of a first axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said at least one helical portion, causing the cylinder together with the first bracket to pivot about a corresponding pivot angle about the respective pivot axis, wherein said first displacement corresponds to said datum linear displacement.

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5. The deployment system according to claim 4, wherein the cam groove comprises at least one linear portion, and wherein application of a second axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said linear portion, preventing the cylinder together with the first bracket from pivoting about the respective pivot axis.

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6. The deployment system according to claim 5, wherein the cam groove comprises at least one tapering portion smoothly connecting one said linear portion with one end of one said helical portion.

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7. The deployment system according to claim 3, wherein each respective said linear motion to rotary motion converter is in the form of a rack and pinion arrangement.

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8. The deployment system according to claim 3, wherein each respective said linear motion to rotary motion converter is in the form of a slider crank arrangement.
9. The deployment system according to any one of claims 4 to 8, wherein said pivot
5 angle is between about 90° and about 270°.
10. The deployment system according to any one of claims 4 to 9, wherein said pivot angle is about 180°.
- 10 11. The deployment system according to any one of claims 1 to 10, wherein all said actuators of said second plurality of actuators are configured for pivoting simultaneously responsive to a predetermined said datum linear displacement being applied to all the respective linear motion to rotary motion converters.
- 15 12. The deployment system according to any one of claims 1 to 10, wherein all said actuators of said second plurality of actuators are configured for pivoting at the same pivoting rate responsive to a predetermined said datum linear displacement rate being applied to all the respective linear motion to rotary motion converters.
- 20 13. The deployment system according to any one of claims 1 to 8, wherein said actuators of said second plurality of actuators are configured for pivoting non-simultaneously with respect to one another, responsive to a predetermined said datum linear displacement being applied simultaneously to all the respective linear motion to rotary motion converters.
- 25 14. The deployment system according to any one of claims 1 to 8, wherein at least some said actuators of said second plurality of actuators are configured for pivoting at respective pivoting rates that are different with respect to one another, responsive to a predetermined said datum linear displacement rate being applied simultaneously to all the
30 respective linear motion to rotary motion converters.
15. The deployment system according to any one of claims 1 to 15, wherein said actuators of said second plurality of actuators are configured for pivoting in a

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synchronized manner with respect to one another responsive to operation of the drive unit and the actuation cable.

16. The deployment system according to any one of claims 1 to 15, wherein the
5 actuation cable is enclosed within an envelope comprising a second plurality of windows, the envelope configured for maintaining a predetermined tension in the actuation cable.

17. The deployment system according to claim 16, wherein said envelope is provided
10 by a sheath.

18. The deployment system according to claim 16, wherein said envelope is in the
form of an incompressible sheath having a lumen that allows relative axial movement
between the actuation cable and the sheath.

19. The deployment system according to any one of claims 16 to 18, wherein the
15 envelope is in the form of a Bowden cable.

20. The deployment system according to claim 16, wherein said envelope is provided
by channels provided in the panel elements.

21. The deployment system according to any one of claims 16 to 20, wherein each
20 said actuator is operatively coupled to the actuation cable at a respective said window.

22. The deployment system according to any one of claims 1 to 21, further comprising
25 a locking arrangement, coupled to the actuation cable, wherein the locking arrangement is configured for maintaining the plurality of panels elements locked in the stowed configuration at least until the drive unit is activated.

23. A panel system comprising a first plurality of panel elements and a deployment
30 system for pivotably deploying the first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective pivot axis, the deployment system being as defined in any one of claims 1 to 22.

24. The panel system according to claim 23, wherein said panel elements are in the form of solar panels.
- 5 25. The panel system according to any one of claims 23 to 24, wherein at least one said panel element is configured for being pivotably mounted to a structure.
26. The panel system according to claim 25, wherein said structure is a space vehicle.
- 10 27. A space vehicle comprising a panel system as defined in any one of claims 23 to 26.
28. An actuator for a deployment system, said actuator comprising a first bracket, a second bracket and a linear motion to rotary motion converter, the first bracket being
15 configured for being fixedly mounted to a panel element, the second bracket being configured for being fixedly mounted to another panel element, the respective first bracket and the respective second bracket being pivotably mounted with respect to one another about an actuator pivot axis co-axial with the respective panel element pair pivot axis, and wherein the linear motion to rotary motion converter is configured for pivoting
20 the respective first bracket with respect to the respective second bracket responsive to a predetermined datum linear displacement being applied to the linear motion to rotary motion converter, and wherein the linear motion to rotary motion converter is configured for being coupled to an actuation cable.
29. The actuator according to claim 28, wherein each respective said linear motion to
25 rotary motion converter comprises a linearly movable shaft element, configured for being coupled to the actuation cable.
30. The actuator according to claim 29, wherein each respective said linear motion to rotary motion converter comprises a respective rotary element operatively coupled to the
30 shaft element such that the rotary element pivots the respective first bracket with respect to the respective second bracket responsive to a respective said datum linear displacement being applied to the shaft element.

31. The actuator according to claim 30, wherein the rotary element comprises an outer cylinder co-axial with and overlying at least part of the shaft element, the outer cylinder fixedly mounted with respect to the first bracket, the outer cylinder comprising a cam groove having at least one helical portion, and wherein the shaft element is movably mounted with respect to said second bracket, the shaft element being constrained for axial movement with respect to the second bracket and prevented from relative rotary movement with respect to the second bracket, wherein the shaft element comprises a cam follower coupled to the cam groove, and wherein application of a first axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said at least one helical portion, causing the cylinder together with the first bracket to pivot about a corresponding pivot angle about the respective pivot axis, wherein said first displacement corresponds to said datum linear displacement.
32. The actuator according to claim 31, wherein the cam groove comprises at least one linear portion, and wherein application of a second axial displacement of the shaft element relative to the second bracket causes the cam follower to follow at least a portion of said linear portion, preventing the cylinder together with the first bracket from pivoting about the respective pivot axis.
33. The actuator according to claim 32, wherein the cam groove comprises at least one tapering portion smoothly connecting one said linear portion with one end of one said helical portion.
34. A method for deploying a panel system comprising:
- providing a first plurality of panel elements and a deployment system for pivotably deploying the first plurality of panel elements between a stowed configuration and a deployed configuration, wherein adjacent pairs of the panel elements are pivotably mounted to one another about a respective pivot axis, the deployment system being as defined in any one of claims 1 to 22;
 - operating the deployment system to cause the panel system to transition the first plurality of panel elements between the stowed configuration and the deployed configuration.

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- 35.** The method according to claim 34, wherein said panel elements are in the form of solar panels.
- 5 **36.** The method according to any one of claims 34 or 35, wherein at least one said panel element is pivotably mounted to a structure.
- 37.** The method according to claim 36, wherein said structure is a space vehicle.