METHOD OF REDUCING THE EFFECT OF DIRECT INTERFERENCE CURRENT IN AN ELECTROCHEMICAL TEST STRIP

FIELD OF THE INVENTION

[0001] The present invention is related, in general to methods of reducing the effect of interfering compounds on measurements taken by analyte measurement systems and, more particularly, to a method of reducing the effects of direct interference currents in a glucose monitoring system using an electrochemical strip having electrodes with uncoated regions.

BACKGROUND OF INVENTION

[0002] In many cases, an electrochemical glucose measuring system may have an elevated oxidation current due to the oxidation of interfering compounds commonly found in physiological fluids such as, for example, acetaminophen, ascorbic acid, bilirubin, dopamine, gentisic acid, glutathione, levodopa, methyldopa, tolazimide, tolbutamide, and uric acid. The accuracy of glucose meters may, therefore, be improved by reducing or eliminating the portion of the oxidation current generated by interfering compounds. Ideally, there should be no oxidation current generated from any of the interfering compounds so that the entire oxidation current would depend only on the glucose concentration.

[0003] It is, therefore, desirable to improve the accuracy of electrochemical sensors in the presence of potentially interfering compounds such as, for example, ascorbate, urate, and, acetaminophen, commonly found in physiological fluids. Examples of analytes for such electrochemical sensors may include glucose, lactate, and fructosamine. Although glucose will be the main analyte discussed, it will be obvious to one skilled in the art that the invention set forth herein may also be used with other analytes.

[0004] Oxidation current may be generated in several ways. In particular, desirable oxidation current results from the interaction of the redox mediator with the analyte of interest (e.g., glucose) while undesirable oxidation current is generally comprised of interfering compounds being oxidized at the electrode surface and by interaction with the redox mediator. For example,

some interfering compounds (e.g., acetominophen) are oxidized at the electrode surface. Other interfering compounds (e.g., ascorbic acid), are oxidized by chemical reaction with the redox mediator. This oxidation of the interfering compound in a glucose measuring system causes the measured oxidation current to be dependent on the concentration of both the glucose and any interfering compound. Therefore, in the situation where the concentration of interfering compound oxidizes as efficiently as glucose and the interferent concentration is high relative to the glucose concentration, the measurement of the glucose concentration would be improved by reducing or eliminating the contribution of the interfering compounds to the total oxidation current.

[0005] One known strategy that can be used to decrease the effects of interfering compounds is to use a negatively charged membrane to cover the working electrode. As an example, a sulfonated fluoropolymer such as NAFION™ may be used to repel all negatively charged chemicals. In general, most interfering compounds such as ascorbate and urate have a negative charge, thus, the negatively charged membrane prevents the negatively charged interfering compounds from reaching the electrode surface and being oxidized at that surface. However, this technique is not always successful since some interfering compounds such as acetaminophen do not have a net negative charge, and thus, can pass through a negatively charged membrane. Nor would this technique reduce the oxidation current resulting from the interaction of interfering compounds with some redox mediators. The use of a negatively charged membrane on the working electrode could also prevent some commonly used redox mediators, such as ferricyanide, from passing through the negatively charged membrane to exchange electrons with the electrode.

[0006] Another known strategy that can be used to decrease the effects of interfering compounds is to use a size selective membrane on top of the working electrode. As an example, a 100 Dalton exclusion membrane such as cellulose acetate may be used to cover the working electrode to exclude all chemicals with a molecular weight greater than 100 Daltons. In general, most interfering compounds have a molecular weight greater than 100 Daltons, and thus, are excluded from being oxidized at the electrode surface. However,

such selective membranes typically make the test strip more complicated to manufacture and increase the test time because the oxidized glucose must diffuse through the selective membrane to get to the electrode.

[0007] Another strategy that can be used to decrease the effects of interfering compounds is to use a redox mediator with a low redox potential, for example, between about –300mV and +100 mV (when measured with respect to a saturated calomel electrode). Because the redox mediator has a low redox potential, the voltage applied to the working electrode may also be relatively low which, in turn, decreases the rate at which interfering compounds are oxidized by the working electrode. Examples of redox mediators having a relatively low redox potential include osmium bipyridyl complexes, ferrocene derivatives, and quinone derivatives. A disadvantage of this strategy is that redox mediators having a relatively low potential are often difficult to synthesize, unstable and have a low water solubility.

[0008] Another known strategy that can be used to decrease the effects of interfering compounds is to use a dummy electrode which is coated with a redox mediator. In some instances the dummy electrode may also be coated with an inert protein or deactivated redox enzyme. The purpose of the dummy electrode is to oxidize the interfering compound at the electrode surface and/or to oxidize the redox mediator reduced by the interfering compound. In this strategy, the current measured at the dummy electrode is subtracted from the total oxidizing current measured at the working electrode to remove the interference effect. A disadvantage of this strategy is that it requires that the test strip include an additional electrode and electrical connection (i.e., the dummy electrode) which cannot be used to measure glucose. The inclusion of dummy electrode is an inefficient use of an electrode in a glucose measuring system.

SUMMARY OF INVENTION

[0009] The invention described herein is directed to a method of reducing the effects of interferences when using an electrochemical sensor to detect analytes. An electrochemical sensor which would be useable in a method according to the present invention includes a substrate, at least first and second working electrodes and a reference electrode. A reagent layer is disposed on the electrodes such that the reagent layer completely covers all of the first working electrode and only partially covers the second working electrode. In a method according to the present invention, the oxidation current generated at the portion of the second working electrode not covered by the reagent layer is used to correct for the effect of interfering substances on the glucose measurement.

[00010] The invention described herein further includes a method of reducing interferences in an electrochemical sensor, including the steps of measuring a first oxidation current at a first working electrode, where the first working electrode is covered by a reagent layer; measuring a second oxidation current at a second working electrode, where the reagent layer only partially covers the second working electrode; and calculating a corrected oxidation current value representative of a concentration of a pre-selected analyte (e.g., glucose). In this calculation, a ratio of the covered area to the uncovered area of the second working electrode is used to remove the effects of interferences on the oxidation current. More particularly, the corrected current value may be calculated using the following equation,

$$G = WE_1 - \left\{ \left(\frac{A_{\text{cov}}}{A_{unc}} \right) X \left(WE_2 - WE_1 \right) \right\}$$

where G is the corrected current density, WE_1 is the uncorrected current density at the first working electrode, WE_2 is the uncorrected current density at the second working electrode, A_{cov} is the coated area of the second working electrode, and A_{unc} is the uncoated area of the second working electrode 2.

[00011] In one embodiment of an electrochemical strip useable in the present invention, the electrochemical glucose test strip includes a first and second working

electrodes, where the first working electrode is completely covered with a reagent layer and the second working electrode is only partially covered with the reagent laye Thus, the second working electrode has a reagent coated area and an uncoated area. The reagent layer may include, for example, a redox enzyme such as glucose oxidase and a redox mediator such as, for example, ferricyanide. The first working electrode will have a superposition of two oxidation current sources, one from glucose and a second from interferents. Similarly, the second working electrode will have a superposition of three oxidation current sources from glucose, interferents at the reagent coated portion, and interferents at the uncoated portion. The uncoated portio of the second working electrode will only oxidize interferents and not oxidize glucos because there is no reagent is in this area. The oxidation current measured at the uncoated portion of the second working electrode may then be used to estimate the total interferent oxidation current and calculate a corrected oxidation current which removes the effects of interferences.

[00012] In an alternative strip embodiment useable in the method according to the present invention, the electrochemical glucose test strip includes a first and second working electrodes, where the first and second working electrode are only partially covered with the reagent layer. Thus, in this embodiment both the first and second working electrode have a reagent coated portion and an uncoated portion. The first uncovered area of the first working electrode and the second uncovered area of the second working electrode are different. The oxidation current measured at the uncoated portion of the first and second working electrodes are used to estimate the interferent oxidation current for the uncoated portion and to calculate a corrected glucose current.

[00013] The invention described herein further includes a method of reducing interferences in an electrochemical sensor, including the steps of measuring a first oxidation current at a first working electrode, where the first working electrode is partially covered by a reagent layer; measuring a second oxidation current at a second working electrode, where the reagent layer only partially covers the second working electrode; and calculating a corrected oxidation current value representative of a concentration of a pre-selected analyte (e.g., glucose). In this calculation, a ratio of the covered area to the uncovered area of the first and second working electrodes is used to remove the effects of interferences on the oxidation current. More

particularly, the corrected current value may be calculated using the following equation

$$G = WE_1 - \left\{ \left(\frac{f_1 + f_2}{f_2 - 1} \right) \times (WE_2 - WE_1) \right\}$$

where f1 is equal to $\frac{A_{cov1}}{A_{unc1}}$; f2 is equal to $\frac{A_{cov1}}{A_{unc2}}$; A_{unc1} is the uncoated area of the first working electrode; A_{unc2} is the uncoated area of the second working electrode; A_{cov1} is a the coated area of said first working electrode; A_{cov2} is the coated area of the second working electrode; G is the corrected current value; WE_1 is the uncorrected current density at the first working electrode; and WE_2 is the uncorrected current density at the second working electrode.

BRIEF DESCRIPTION OF DRAWINGS

[00014] A better understanding of the features and advantages of the present invention will be obtained by reference to the following detailed description that sets forth illustrative embodiments, in which the principles of the invention are utilized, and the accompanying drawings, of which:

[00015] Figure 1 is an exploded perspective view of a test strip according to an embodiment of the present invention;

[00016] Figure 2 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 1 including a conductive layer and an insulation layer;

[00017] Figure 3 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 1 wherein the positio of a reagent layer is illustrated with the conductive layer and the insulation layer;

[00018] Figure. 4 is an exploded perspective view of a test strip according to a further embodiment of the present invention;

[00019] Figure 5 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 4 including of a conductive layer and an insulation layer; and

[00020] Figure 6 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 4 wherein a reagent layer is illustrated with the conductive layer and the insulation layer.

[00021] Figure 7 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 4 wherein a reagent layer is illustrated with the conductive layer.

[00022] Figure 8 is a simplified plane view of a distal portion of a test strip according to another embodiment of the present invention wherein a reagent layer is illustrated with the conductive layer that helps reduce an IR drop effect.

[00023] Figure 9 is a simplified plane view of a distal portion of a test strip according to yet another embodiment of the present invention wherein a reagent layer is illustrated with the conductive layer and the insulation layer such there are two working electrodes that have an uncoated portion.

[00024] Figure 10 is a simplified plane view of a distal portion of a test strip accordin to still yet another embodiment of the present invention wherein a reagent layer is illustrated with the conductive layer and the insulation layer such there are two working electrodes that have an uncoated portion.

[00025] Figure 11 is a graph showing the current at a first working electrode of a strip designed in accordance with the present invention tested with 70 mg/dL glucose samples in blood spiked with varying levels of uric acid.

[00026] Figure 12 is a graph showing the current at a first working electrode at a strip designed in accordance with the present invention tested with 240 mg/dL glucose samples in blood spiked with varying levels of uric acid.

[00027] Figure 13 is an exploded perspective view of a test strip that has an integrated lance.

[00028] Figure 14 is a simplified schematic showing a meter interfacing with a test strip that has a first contact, second contact, and reference contact disposed on a substrate.

DETAILED DESCRIPTION OF THE INVENTION

[00029] This invention described herein includes a test strip and method for improvin the selectivity of an electrochemical glucose measuring system.

[00030] Figure 1 is an exploded perspective view of a test strip according to a first embodiment of the present invention. In the embodiment of the present invention illustrated in Figure 1, an electrochemical test strip 62, which may be used for measuring glucose concentration in bodily fluids such as blood or interstitial fluid, includes a first working electrode 10 and a second working electrode 12, where first working electrode 10 is completely covered with a reagent layer 22 and second working electrode 12 is only partially covered with reagent layer 22. Thus, the secon working electrode has a reagent coated portion and an uncoated portion. Reagent layer 22 may include, for example, a redox enzyme such as, for example, glucose oxidase and a redox mediator such as, for example, ferricyanide. Because ferricyanid has a redox potential of approximately 400 mV (when measured with respect to a saturated calomel electrode) at a carbon electrode, the introduction of a bodily fluid e.g., blood may generate a significant oxidation of interferents by the redox mediator and /or the working electrode generating a significant undesirable oxidation current. Therefore, the oxidation current measured at first working electrode 10 will be a superposition of oxidation current sources: a first, desirable, oxidation current generated by the oxidation of glucose and a second, undesirable, oxidation current generated by the interferents. The oxidation current measured at second working electrode 12 will also be a superposition of oxidation current sources: a first, desirabl oxidation current generated by the oxidation of glucose, a second, undesirable oxidation current generated by interferents at the covered portion of working electrod 12 and a third oxidation current generated by interferents at the uncovered portion of working electrode 12. The uncoated portion of second working electrode 12 will onl oxidize interferents and not oxidize glucose because there is no reagent on the uncoated portion of second working electrode 12. Because the oxidation current measured at the uncoated portion of second working electrode 12 does not depend on glucose and the uncoated area of second working electrode 12 is known, it is possible to calculate the interferent oxidation current for the uncoated portion of the second working electrode 12. In turn, using the interferent oxidation current calculated for the uncoated portion of second working electrode 12 and knowing the area of first working electrode 10 and the area of the coated portion of second working electrode 12, it is possible to calculate a corrected glucose current which accounts for the effec of interfering compounds oxidized at the electrode.

[00031] Figure 1 is an exploded perspective view of a test strip 62 according to a first embodiment of the present invention. Test strip 62, as illustrated in Figure 1, may be manufactured by a series of 6 consecutive printing steps which lay down six layers of material on substrate 50. The six layers may be deposited by, for example, screen printing on substrate 50. In an embodiment of this invention, the 6 layers may includ a conductive layer 64, an insulation layer 16, a reagent layer 22, an adhesive layer 66, a hydrophilic layer 68, and a top layer 40. Conductive layer 64 may further includes first working electrode 10, second working electrode 12, reference electrode 14, first contact 11, second contact 13, reference contact 15, and strip detection bar 17. Insulation layer 16 may further include cutout 18. Adhesive layer 66 may further include first adhesive pad 24, second adhesive pad 26, and third adhesive pads 28. Hydrophilic layer 68 may further include first hydrophilic film 32, and second hydrophilic film 34. Top layer 40 may further includes a clear portion 36 and opaque portion 38. Test strip 62 has a first side 54 and second side 56, a distal electrode side 58, and a proximal electrode side 60 as illustrated in Figure 1. The following section will describe the respective layers of test strip 62 in more detail.

[00032] In one embodiment of the present invention, substrate 50 is an electrically insulating material such as plastic, glass, ceramic, and the like. In a preferred embodiment of this invention, substrate 50 may be a plastic such as, for example, nylon, polycarbonate, polyimide, polyvinylchloride, polyethylene, polypropylene, PETG, or polyester. More particularly the polyester may be, for example Melinex ® ST328 which is manufactured by DuPont Teijin Films. Substrate 50 may also includ an acrylic coating which is applied to one or both sides to improve ink adhesion.

[00033] The first layer deposited on substrate 50 is conductive layer 64 which include first working electrode 10, second working electrode 12, reference electrode 14, and strip detection bar 17. In accordance with the present invention, a screen mesh with an emulsion pattern may be used to deposit a material such as, for example, a conductive carbon ink in a defined geometry as illustrated in Figure 1. Reference electrode 14 may also be a counter electrode, a reference/counter electrode, or a quas reference electrode. Conductive layer 64 may be disposed on substrate 50 by using screen printing, rotogravure printing, sputtering, evaporation, electroless plating, ink jetting, sublimation, chemical vapor deposition, and the like. Suitable materials whi may be used for conductive layer 64 are Au, Pd, Ir, Pt, Rh, stainless steel, doped tin

oxide, carbon, and the like. In an embodiment of this invention, the carbon ink layer may have a height between 1 and 100 microns, more particularly between 5 and 25 microns, and yet even more particularly at approximately 13 microns. The height of the conductive layer can vary depending on the desired resistance of the conductive layer and the conductivity of the material used for printing the conductive layer.

[00034] First contact 11, second contact 13, and reference contact 15 may be used to electrically interface with a meter. This allows the meter to electrically communicate to first working electrode 10, second working electrode 12, and reference electrode 1⁴ via, respective, first contact 11, second contact 13, and reference contact 15.

[00035] The second layer deposited on substrate 50 is insulation layer 16. Insulation layer 16 is disposed on at least a portion of conductive layer 64 as shown in Figure 1. Figure 2 is a simplified plane view of a distal portion of test strip 62 which highlights the position of first working electrode 10, second working electrode 12, and reference electrode 14 with respect to insulation layer 16. Insulation layer 16 further includes a cutout 18 which may have a T-shaped structure as shown in Figure 1 and 2. Cutout 18 exposes a portion of first working electrode 10, second working electrode 12, and reference electrode 14 which can be wetted with liquid. Cutout 18 further includes a distal cutout width W1, proximal cutout width W2, a distal cutout length L4 and a proximal cutout length L5. Distal cutout width W1 corresponds to the width of first working electrode 10 and reference electrode 14 as illustrated in Figure 2. Distal cutout length L4 corresponds to a length which is greater than both first working electrode 10 and reference electrode 14 together. Proximal cutout width W2 and proximal cutout length L5 form a rectangular section which exposes the width and length of second working electrode 12. In accordance with the present invention, distal cutout width W1, proximal cutout width W2, distal cutout length L4 and proximal cutout length L5 may have a respective dimension of approximately 0.7, 1.⁹ 3.2, and 0.43 mm. In one embodiment of the present invention, first working electrode 10, reference electrode 14, and second working electrode 12 have a respective length of L1, L2, and L3 which may be about 0.8, 1.6, and 0.4 mm. In accordance with the present invention, electrode spacing S1 is a distance between fir working electrode 10 and reference electrode 14; and between reference electrode 14 and second working electrode 12 which may be about 0.4 mm.

[00036] The third layer deposited on substrate 50 is a reagent layer 22. Reagent layer 22 is disposed on at least a portion of conductive layer 64 and insulation layer 16 as shown in Figures 1. Figure 3 is a simplified plane view of a distal portion of test strip 62 according to the first embodiment of the present invention which highlights the position of reagent layer 22 with respect to first working electrode 10, second working electrode 12, reference electrode 14, and insulation layer 16. Reagent layer 22 may be in the shape of a rectangle having a reagent width W3 and a reagent length L6 as illustrated in Figure 1 and 3. In one embodiment of the invention, reagent width W3 may be about 1.3 mm and reagent length L6 may be about 4.7 mm. In a further embodiment of the present invention, reagent layer 22 has a sufficiently large width W3 and length L6 such that reagent layer 22 completely covers first working electrode 10 and reference electrode 14. However, reagent layer 22 has an appropriately sized width W3 and length L6 such that second working electrode is not completely covered with reagent layer 22. In such a scenario, second working electrode 12 has a coated portion 12c and an uncoated portions 12u as illustrated in Figure 3. Uncoated portions 12u may be in the shape of two rectangles where uncoated portions 12u has a wing width W4 and a length that corresponds to second working electrode length L3. As a non-limiting example, wing width W4 may be about 0.3 mm. In one embodiment of the present invention, reagent layer 22 may include a redox enzyme such as, for example, glucose oxidase or PQQ-glucose dehydrogenase (where PQQ is an acronym for pyrrolo-quinoline-quinone) and a redox mediator such as, for example, ferricyanide.

[00037] The fourth layer deposited on substrate 50 is an adhesive layer 66 which includes a first adhesive pad 24, a second adhesive pad 26, and a third adhesive pad 28. First adhesive pad 24 and second adhesive pad 26 form the walls of a sample receiving chamber. In one embodiment of the present invention, first adhesive pad 24 and second adhesive pad 26 may be disposed on substrate 50 such that neither of the adhesive pads touches reagent layer 22. In another embodiments of the present invention where the strip volume needs to be reduced, first adhesive pad 24 and/or second adhesive pad 26 may be disposed on substrate 50 such there is overlap with reagent layer 22. In an embodiment of the present invention, adhesive layer 66 has a height of about 70 to 110 microns. Adhesive layer 66 may include a double sided pressure sensitive adhesive, a UV cured adhesive, heat activated adhesive,

thermosetting plastic, or other adhesive known to those skilled in the art. As a non-limiting example, adhesive layer 66 may be formed by screen printing a pressure sensitive adhesive such as, for example, a water based acrylic copolymer pressure sensitive adhesive which is commercially available from Tape Specialties LTD in Tring, Herts, United Kingdom (part#A6435).

[00038] The fifth layer deposited on substrate 50 is a hydrophilic layer 68 which includes a first hydrophilic film 32 and second hydrophilic film 34 as illustrated in Figure 1. Hydrophilic layer 68 forms the "roof" of the sample receiving chamber. The "side walls" and "floor" of the sample receiving chamber are formed by a portion of adhesive layer 66 and substrate 50, respectively. As a non-limiting example, hydrophilic layer 68 may be an optically transparent polyester with a hydrophilic anti-fog coating such as those commercially obtained from 3M. The hydrophilic nature of the coating is used in the design of strip 62 because it facilitates filling of liquid into the sample receiving chamber.

[00039] The sixth and final layer deposited on substrate 50 is a top layer 40 which includes a clear portion 36 and opaque portion 38 as illustrated in Figure 1. In accordance with the present invention, top layer 40 includes a polyester which is coated on one side with a pressure sensitive adhesive. Top layer 40 has an opaque portion 38 which helps the user observe a high degree of contrast when blood is underneath clear portion 36. This allows a user to visually confirm that the sample receiving chamber is sufficiently filled. After strip 62 is fully laminated, it is cut along incision line A-A' and in the process creates sample inlet 52 as illustrated in Figure 3.

[00040] The first test strip embodiment as illustrated in Figures 1-3 may have a possible drawback in that reagent layer 22 may dissolve in a liquid sample and move portion of the dissolved reagent layer over the uncoated portions 12u of second working electrode 12. If such a scenario were to occur, uncoated portions 12u would also measure an oxidation current that is also proportional to the glucose concentration. This would degrade the ability to use mathematical algorithms for removing the effect of interferent oxidation. In an alternative embodiment of the present invention, reagent layer 22 should be designed to dissolve in such a way that does not migrate to uncoated portions 12u. For example, reagent layer 22 may be chemically bound to the first working electrode 10, second working electrode 12, and

reference electrode 14 or may have a thickening agent that minimizes the migration o dissolved reagent layer 22.

[00041] A further embodiment of the present invention as illustrated in Figure 4, the embodiment illustrated in Figure 4 reduces, and in certain circumstances minimizes, the immigration of dissolved reagent to an uncoated portion of the second working electrode. In this embodiment, second working electrode 102 has a C-shaped geometry where 2 discrete portions of second working electrode 102 are exposed by cutout 108 as illustrated in Figure 4. In accordance with the present invention, reage layer 110 is disposed on only a portion of second working electrode 102 to form an uncoated portion 102u and coated portion 102c as illustrated in Figure 6. Uncoated portion 102u is adjacent to sample inlet 52. Coated portion 102c is adjacent to first working electrode 100. When applying liquid to sample inlet 52 of an assembled test strip 162, the liquid will flow from sample inlet 52 to coated portion 102c until all electrodes are covered with liquid. By positioning uncoated portion 102u upstream o the liquid flow, this almost entirely prevents reagent layer 110 from dissolving and migrating to uncoated portion 102u. This enables the mathematical algorithm to accurately remove the effects of interferents from the measured oxidation current.

[00042] Figure 4 is an exploded perspective view of a test strip 162. Test strip 162 is manufactured in a manner similar to test strip 62 except that there are geometric or positional changes to a conductive layer 164, an insulation layer 106, and a reagent layer 110. For the second embodiment of this invention, substrate 50, adhesive layer 66, hydrophilic layer 68, and top layer 40 are the same as the first strip embodiment. Test strip 162 has a first side 54 and second side 56, a distal electrode side 58, and a proximal electrode side 60. It should also be noted that the first and second test strip embodiment of the present invention may have elements with similar structure which are denoted with the same element number and name. If analogous elements betwee the respective test strip embodiments are different in structure, the elements may hav the same name, but be denoted with a different element number. The following sections will describe the respective layers of test strip 162 in more detail.

[00043] For the strip embodiment illustrated in Figure 4, the first layer deposited on substrate 50 is conductive layer 164 which includes first working electrode 100, second working electrode 102, reference electrode 104, first contact 101, second contact 103, and reference contact 105, and strip detection bar 17. In accordance wit

the present invention, a screen mesh with an emulsion pattern may be used to deposit a material such as, for example, a conductive carbon ink in a defined geometry as illustrated in Figure 4. First contact 101, second contact 103, and reference contact 105 may be used to electrically interface with a meter. This allows the meter to electrically communicate to first working electrode 100, second working electrode 102, and reference electrode 104 via, respective, first contact 101, second contact 10: and reference contact 105.

[00044] The second layer deposited on substrate 50 in Figure 4 is insulation layer 106. Insulation layer 106 is disposed on at least a portion of conductive layer 164 as show in Figures 4. Figure 5 is a simplified plane view of a distal portion of test strip 162 which highlights the position of first working electrode 100, second working electrod 102, and reference electrode 104 with respect to insulation layer 106.

[00045] The third layer deposited on substrate 50 in Figure 4 is a reagent layer 110 such that reagent layer 110 is disposed on at least a portion of conductive layer 164 and insulation layer 106 as shown in Figure 6. Figure 6 is a simplified plane view of distal portion of test strip 162 according to the second embodiment of the present invention which highlights the position of reagent layer 110 with respect to first working electrode 100, second working electrode 102, reference electrode 104, and insulation layer 106. Reagent layer 110 may be in the shape of a rectangle having a reagent width W13 and a reagent length L16. In one embodiment of this invention, reagent width W13 may be about 1.3 mm and reagent length L16 may be about 3.2 mm. In a preferred embodiment of the present invention, reagent layer 110 has a sufficient width W13 and length L16 such that reagent layer 110 completely covers first working electrode 100, coated portion 102c, and reference electrode 104, but does not cover uncoated portion 102u.

[00046] Figure 7 is a simplified plane view of a distal portion of a test strip according to the embodiment of the present invention illustrated in Figure 4 wherein a reagent layer is illustrated with the conductive layer. In contrast to Figure 6, Figure 7 does n show insulation layer 106. This helps demonstrate the conductive relationship between uncoated portion 102u and coated portion 102c which was hidden underneat the opaque character of insulation layer 106.

[00047] For the strip embodiment illustrated in Figure 4, insulation layer 106 is used tc define the width of the first working electrode 100, second working electrode 102, an reference electrode 104. Insulation layer 106 further includes a cutout 108 which ma have a T-shaped structure as shown in Figure 4 to 6. Cutout 108 exposes a portion of first working electrode 100, second working electrode 102, and reference electrode 104 which can be wetted with liquid. Cutout 108 further includes a distal cutout width W11, proximal cutout width W12, a distal cutout length L14 and a proximal cutout length L15 as illustrated in Figure 5 and 6. Distal cutout width W11 corresponds to the width of uncoated portion 102u. Distal cutout length L14 is greate than the length uncoated portion 102u. Proximal cutout width W12 and proximal cutout length L15 forms a rectangular section which approximately exposes the width and length of first working electrode 100, reference electrode 104, and coated portion 102c.

[00048] In accordance with the present invention, distal cutout width W11, proximal cutout width W12, distal cutout length L14 and proximal cutout length L15 may have a respective dimension of approximately 1.1, 0.7, 2.5, and 2.6 mm.

[00049] In the embodiment of Figure 4, uncoated portion 102u, reference electrode 104, first working electrode 100, and coated portion 102c have a respective length of L10, L12, L11, and L13 which may be about 0.7, 0.7, 0.4, and 0.4 mm. Electrode spacing S11 is a distance between uncoated portion 102u and reference electrode 104 which may be between about 0.2 to 0.75 mm, and more preferably between 0.6 to 0.7 mm. Electrode spacing S10 is a distance between reference electrode 104 and first working electrode 100; and between coated portion 102c and first working electrode 100 which may be about 0.2 mm. It should be noted that electrode spacing S11 is greater than S10 to decrease the possibility of reagent dissolving and migrating to uncoated portion 102u. Additionally, electrode spacing S11 is greater than S10 to decrease the possibility of reagent layer 110 being disposed on uncoated portion 102u because of variations in the printing process. The fourth through sixth layer which is successively disposed on strip 162 in the same manner as the first strip embodiment. The relative position and shape of the adhesive layer 66, hydrophilic layer 68, and top layer 40 are illustrated in Figure 4.

[00050] In the embodiment of the invention illustrated in Figure 8, the C-shape of second working electrode 102 may be partially altered so that the order in which

liquid would wet the electrodes would be uncoated portion 102u, first working electrode 100, reference electrode 104, and then coated portion 102c. In the alternative format, first working electrode 100 and coated portion 102c would be equidistant from reference electrode 104 which is desirable from an IR drop perspective. In the second strip embodiment (i.e. test strip 162) illustrated in Figure 7 the electrodes are arranged so that the order in which liquid would wet the electrodes would be uncoated portion 102u, reference electrode 104, first working electrode 100 and then coated portion 102c. For test strip 162, coated portion 102c is farther away from reference electrode 104 than the distance between first working electrode 100 and reference electrode 104.

[00051] An algorithm may, therefore be used to calculate a corrected glucose current that is independent of interferences. After dosing a sample onto a test strip, a constan potential is applied to the first and second working electrodes and a current is measured for both electrodes. At the first working electrode where reagent covers the entire electrode area, the following equation can be used to describe the components contributing to the oxidation current,

$$WE_1 = G + I_{cov} \qquad \text{(Eq 1)}$$

where WE_1 is the current density at the first working electrode, G is the current densit due to glucose which is independent of interferences, and I_{cov} is the current density due to interferences at the portion of a working electrode covered with reagent.

[00052] At the second working electrode which is partially covered with reagent, the following equation can be used to describe the components contributing to the oxidation current,

$$WE_2 = G + I_{cov} + I_{unc} \qquad \text{(Eq 2)}$$

where WE_2 is the current density at the second working electrode and I_{unc} is the current density due to interferences at the portion of a working electrode not covered with reagent. Alternative embodiments of the present invention can be made using different areas of reagent coating for the first and second working electrode, but then the equations must account for the different uncoated areas.

[00053] To reduce the effects of interferences, an equation is formulated which describes the relationship between the interferent current at the coated portion of the second working electrode and the uncoated portion of the second working electrode. It is approximated that the interferent oxidation current density measured at the coate portion is the same as the current density measured at the uncoated portion. This relationship is further described by the following equation,

$$I_{\text{cov}} = \frac{A_{\text{cov}}}{A_{unc}} \times I_{unc} \qquad \text{(Eq 3a)}$$

where A_{cov} is the area of second working electrode covered with reagent and A_{unc} is th area of second working electrode not covered with reagent.

[00054] It should be noted that uncoated portions 12u and coated portions 12c may have a respective area denoted as A_{unc} and A_{cov}. Uncoated portions 12u can oxidize interferents, but not glucose because it is not coated with reagent layer 22. In contras coated portion 12c can oxidize glucose and interferents. Because it was experimentally found that uncoated portions 12u oxidizes interferents in a manner proportional to the area of coated portion 12c, it is possible to predict the proportion of interferent current measured overall at second working electrode 12. This allows the overall current measured at second working electrode 12 to be corrected by subtracting the contribution of the interferent current. In an embodiment of the present invention the ratio of A_{unc}:A_{cov} may be between about 0.5:1 to 5:1, and is preferably about 3:1. More details describing this mathematical algorithm for curren correction will be described in a later section.

[00055] In an alternative embodiment of the present invention, the interferent oxidatio current density measured at the coated portion may be different than the current density measured at the uncoated portion. This may be ascribed to a more efficient o less efficient oxidation of interferents at the coated portion. In one scenario, the presence of a redox mediators may enhance the oxidation of interferences relative to the uncoated portion. In another scenario, the presence of viscosity increasing substances such as hydroxyethyl cellulose may decrease the oxidation of interference relative to the uncoated portion. Depending on the components included in the reagent layer which partially coats the second working electrode, it is possible that th

interferent oxidation current density measured at the coated portion may be more or less than the uncoated portion. This behavior may be phenomenologically modeled b re-writing Equation 3a to the following form,

$$I_{\text{cov}} = f \times I_{unc} \qquad \text{(Eq 3b)}$$

where f is a correction factor which incorporates the effects of the interferent oxidation efficiency of the coated to uncoated portion.

[00056] In an embodiment of the present invention, Equation 1, 2, and 3a may be manipulated to derive an equation that outputs a corrected glucose current density independent of interferences. It should be noted that the three equations (Equation 1, 2, and 3a) collectively have 3 unknowns which are G, I_{cov}, and I_{unc}. Equation 1 can b rearranged to the following form.

$$G = WE_1 - I_{cov} \qquad \text{(Eq 4)}$$

Next, I_{cov} from Equation 3a can be substituted into Equation 4 to yield Equation 5.

$$G = WE_1 - \left[\frac{A_{\text{cov}}}{A_{unc}} \times I_{unc}\right] \qquad \text{(Eq 5)}$$

Next, Equation 1 and Equation 2 can be combined to yield Equation 6.

$$I_{unc} = WE_2 - WE_1 \qquad \text{(Eq 6)}$$

Next, I_{unc} from Equation 6 can be substituted into Equation 5 to yield Equation 7a.

$$G = WE_1 - \left\{\left(\frac{A_{\text{cov}}}{A_{unc}}\right) X (WE_2 - WE_1)\right\} \qquad \text{(Eq 7a)}$$

[00057] Equation 7a outputs a corrected glucose current density G which removes the effects of interferences requiring only the current density output of the first and secor

working electrode, and a proportion of the coated to uncoated area of the second working electrode. In one embodiment of the present invention the proportion $\frac{A_{cov}}{A_{unc}}$ may be programmed into a glucose meter, in, for example, a read only memory. In another embodiment of the present invention, the proportion $\frac{A_{cov}}{A_{unc}}$ may be transferre to the meter via a calibration code chip which would may account for manufacturing variations in A_{cov} or A_{unc}.

[00058] In an alternative embodiment to the present invention Equation 1, 2, and 3b may be used when the interferent oxidation current density for the coated portion is different from the interferent oxidation current density of the uncoated portion. In such a case, an alternative correction Equation 7b is derived as shown below.

$$G = WE_1 - \{f \times (WE_2 - WE_1)\} \qquad \text{(Eq 7b)}$$

[00059] In another embodiment of the present invention, the corrected glucose current Equation 7a or 7b may be used by the meter only when a certain threshold is exceeded. For example, if WE_2 is about 10% or greater than WE_1, then the meter would use Equation 7a or 7b to correct for the current output. However, if WE_2 is about 10% or less than WE_1, the meter would simple take an average current value between WE_1 and WE_2 to improve the accuracy and precision of the measurement. The strategy of using Equation 7a or 7b only under certain situations where it is likely that a significant level of interferences are in the sample mitigates the risk of overcorrecting the measured glucose current. It should be noted that when WE_2 is sufficiently greater than WE_1 (e.g. about 20% or more), this is an indicator of having a sufficiently high concentration of interferents. In such a case, it may be desirable to output an error message instead of a glucose value because a very high level of interferents may cause a breakdown in the accuracy of Equation 7a or 7b.

[00060] In the embodiment of the present invention illustrated in Figure 9 and 10, the first and second working electrodes are partially covered with the reagent layer in such a way that that the uncoated portions of the first and second working electrodes are different. This contrasts the previously described first and second test strip

embodiments where the first working electrode is completely covered with the reagen layer.

[00061] Figure 9 is a simplified plane view of a distal portion of a test strip 2000 according to yet another embodiment of the present invention wherein a reagent layer 22 is illustrated with the conductive layer and insulation layer 2002 such there are twc working electrodes which have an uncoated portion. Test strip 2002 is manufactured in a manner similar to test strip 62 except that there is a geometric change to cutout 1{ as shown in Figure 1. Test strip 2002 has the same substrate 50, conductive layer 64, reagent layer 22, adhesive layer 66, hydrophilic layer 68, and top layer 40 as test strip 62. Test strip 2002 was modified to have a cutout 2004 which has a dumbbell like shape as illustrated in Figure 9. The modified shape for cutout 2004 allows first working electrode 2008 to include a first coated portion 2008c and an first uncoated portion 2008u; and second working electrode 2006 to include a second coated portion 2006c and second uncoated portion 2006u. In order for test strip 2000 to effectively reduce the effects of interferents, first uncoated portion 2008u must have a different total area than second uncoated portion 2006u.

[00062] Figure 10 is a simplified plane view of a distal portion of a test strip 5000 according to still yet another embodiment of the present invention wherein a reagent layer 820 is illustrated with the conductive layer such there are two working electrode which have an uncoated portion. Test strip 5000 is manufactured in a manner similai to test strip 162 except that there is a geometric change to conductive layer 164 such that both a first working electrode 4002 and a second working electrode 4004 have a c-shape. Test strip 5000 has the same substrate 50, insulation layer 106, reagent layer 110, adhesive layer 66, hydrophilic layer 68, and top layer 40 as test strip 162. The modified geometry allows first working electrode 4002 to include a first coated portion 4002c and a first uncoated portion 4002u; and second working electrode 4004 to include a second coated portion 4004c and second uncoated portion 4004u. In order for test strip 2000 to effectively reduce the effects of interferents, first uncoated portion 4002u must have a different area than second uncoated portion 4004u.

[00063] Test strips 2000 and 5000 have an advantage in that they may be easier to manufacture in regards to depositing the reagent layer with the required registration and also any subsequently deposited layers. Furthermore, both the first and second working electrodes will have to some extent the same chemical and electrochemical

interactions with any interfering substances thus ensuring greater accuracy in the correction process. With both working electrodes having some level of uncoated area the same reactions will occur on both electrodes but to a different extent. Using a simple modification to Equation 7a, the following Equation 7c can be used as the correction equation for glucose,

$$G = WE_1 - \left\{ \left(\frac{f_1 + f_2}{f_2 - 1} \right) \times (WE_2 - WE_1) \right\} \qquad \text{(Eq 7c)}$$

where $f_1 = \frac{A_{cov1}}{A_{unc1}}$, $f_2 = \frac{A_{cov1}}{A_{unc2}}$, A_{unc1} = is an uncoated area of the first working electrode, A_{unc2} = is an uncoated area of the second working electrode, A_{cov1} = is a coated area of the first working electrode, and A_{cov2} = is a coated area of the second working electrode.

[00064] One advantage of the present invention is the ability to use the first and second working electrode to determine that the sample receiving chamber has been sufficiently filled with liquid. It is an advantage of this invention in that the second working electrode not only corrects the interferent effect, but can also measure glucose. This allows for a more accurate result because 2 glucose measurements can be averaged together while using only one test strip.

[00065]

Example 1

[00066] Test strips were prepared according to the first embodiment of the present invention as illustrated in Figure 1 to 3. These test strips were tested in blood having various concentrations of interferents. To test these strips, they were electrically connected to a potentiostat which has the means to apply a constant potential of 0.4 volts between the first working electrode and the reference electrode; and the second working electrode and the reference electrode. A sample of blood is applied to the sample inlet allowing the blood to wick into the sample receiving chamber and to we first working electrode, second working electrode, and reference electrode. The reagent layer becomes hydrated with blood and then generates ferrocyanide which

may be proportional to the amount of glucose and/or interferent concentration present in the sample. After about 5 seconds from the sample application to the test strip, an oxidation of ferrocyanide is measured as a current for both the first and second working electrode.

[00067] Figure 11 shows the current responses of the first working electrode tested with 70 mg/dL glucose samples in blood spiked with varying levels of uric acid. The uncorrected current at the first working electrode (depicted by squares) shows an increase in current that is proportional to the uric acid concentration. However, the corrected current (depicted by triangles) which is processed by Equation 7a shows no effect from the increasing uric acid concentration.

[00068] Figure 12 shows the current responses of the first working electrode tested with 240 mg/dL glucose samples in blood spiked with varying levels of uric acid. Th purpose of testing strips at 240 mg/dL glucose is to show that the correction algorithn of Equation 7a is also valid over a range of glucose concentrations. Similar to Figure 11, the uncorrected current at the first working electrode (depicted by squares) shows an increase in current that is proportional to the uric acid concentration. However, th corrected current (depicted by triangles) shows no effect from the increasing uric acic concentration.

Example 2

[00069] To show that the method of correcting the current for interferents applies to a wide variety of interferents, strips built according to the embodiment of Figure 1 wer also tested with acetaminophen and gentisic acid at various concentration levels, in addition to uric acid. For purposes of quantitating the magnitude of this effect, a change in glucose output of greater than 10% (for glucose level > 70 mg/dL) or 7 mg/dL (for glucose level <= 70 mg/dL) was defined as a significant interference. Table 1 shows that the uncorrected current at the first working electrode shows a significant interferent effect at a lower interferent concentration than strips tested wit a corrected current response using Equation 7a. This shows that the method of correcting the current output of the first working electrode using Equation 7a is effective in correcting for interferences. Table 1 shows that the current correction in Equation 7a is effective for interferences with respect to acetaminophen, gentisic acic and uric acid. Table 1 also shows the concentration range of the interferent which is

normally found in blood. In addition, Table 1 also shows that the current correction i Equation 7a is effective at 240 mg/dL glucose concentration level.

[00070] Figure 13 shows an exploded perspective view of a test strip 800 that is designed to lance a user's skin layer so as cause physiological fluid to be expressed and collected into test strip 800 in a seamless manner. Test strip 800 includes a substrate 50, a conductive layer 802, an insulation layer 804, a reagent layer 820, an adhesive layer 830, and a top layer 824. Test strip 800 further includes a distal end 5 and a proximal end 60.

[00071] In test strip 800, conductive layer 802 is the first layer disposed on substrate 50. Conductive layer 802 includes a second working electrode 806, a first working electrode 808, a reference electrode 810, a second contact 812, a first contact 814, a reference contact 816, a strip detection bar 17, as shown in Figure 13. The material used for conductive layer 802 and the process for printing conductive layer 802 is the same for both test strip 62 and test strip 800.

[00072] Insulation layer 804 is the second layer disposed on substrate 50. Insulation layer 16 includes a cutout 18 which may have a rectangular shaped structure. Cutout 18 exposes a portion of second working electrode 806, first working electrode 808, and reference electrode 810 which can be wetted with a liquid. The material used for insulation layer 804 and the process for printing insulation layer 804 is the same for both test strip 62 and test strip 800.

[00073] Reagent layer 820 is the third layer disposed on substrate 50, first working electrode 808 and reference electrode 810. The material used for reagent layer 820 and the process for printing reagent layer 820 is the same for both test strip 62 and te strip 800.

[00074] Adhesive layer 830 is the fourth layer disposed on substrate 50. The material used for adhesive layer 830 and the process for printing adhesive layer 830 is the sam for both test strip 62 and test strip 800. The purpose of adhesive layer 830 is to secu top layer 824 to test strip 800. In an embodiment of this invention, top layer 824 ma be in the form of an integrated lance as shown in Figure 13. In such an embodiment, top layer 824 may include a lance 826 which is located at distal end 58.

[00075] Lance 826, which may also be referred to as a penetration member, may be adapted to pierce a user's skin and draw blood into test strip 800 such that second

working electrode 806, first working electrode 808, and reference electrode 810 are wetted. Lance 826 includes a lancet base 832 that terminates at distal end 58 of the assembled test strip. Lance 826 may be made with either an insulating material such as plastic, glass, and silicon, or a conducting material such as stainless steel and gold. Further descriptions of integrated medical devices that use an integrated lance can be found in International Application No. PCT/GB01/05634 and U.S. Patent Applicatio No. 10/143,399. In addition, lance 826 can be fabricated, for example, by a progressive die-stamping technique, as disclosed in the aforementioned International Application No. PCT/GB01/05634 and U.S. Patent Application No. 10/143,399.

[00076] Figure 14 is a simplified schematic showing a meter 900 interfacing with a test strip. In an embodiment of this invention the following test strips may be suitable for use with meter 900 which are test strip 62, test strip 162, test strip 800, test strip 2000, test strip 3000, or test strip 5000. Meter 900 has at least three electrical contacts that form an electrical connection to the second working electrode, the first working electrode, and the reference electrode. In particular second contact (13, 103, or 812) and reference contact (15, 105, or 816)connect to a first voltage source 910; first contact (11, 101, or 814)and the reference contact (15, 105, or 816)connect to a second voltage source 920.

[00077] When performing a test, first voltage source 910 applies a first potential E1 between the second working electrode and the reference electrode; and second voltage source 920 applies a second potential E2 between the first working electrode and the reference electrode. In one embodiment of this invention, first potential E1 and second potential E2 may be the same such as for example about +0.4 V. In another embodiment of this invention, first potential E1 and second potential E2 may be different. A sample of blood is applied such that the second working electrode, the first working electrode, and the reference electrode are covered with blood. This allows the second working electrode and the first working electrode to measure a current which is proportional to glucose and/or non-enzyme specific sources. After about 5 seconds from the sample application, meter 900 measures an oxidation current for both the second working electrode and the first working electrode.

Table 1. Summary of Interference Performance Using Uncorrected and Corrected Current Output

Mode	Interferent	Glucose Concentration (mg/dL)	Inteferent Concentration where effect is signficant	Normal Concentration range of interferent
Uncorrected	Acetaminophen	70	11	1 - 2
Uncorrected	Gentisic Acid	70	10	0.05 - 0.5
Uncorrected	Uric Acid	70	5	2.6 - 7.2
Uncorrected	Acetaminophen	240	16	1 - 2
Uncorrected	Gentisic Acid	240	12	0.05 - 0.5
Uncorrected	Uric Acid	240	8	2.6 - 7.2
Corrected	Acetaminophen	70	120	1 - 2
Corrected	Gentisic Acid	70	47	0.05 - 0.5
Corrected	Uric Acid	70	33	2.6 - 7.2
Corrected	Acetaminophen	240	59	1 - 2
Corrected	Gentisic Acid	240	178	0.05 - 0.5
Corrected	Uric Acid	240	29	2.6 - 7.2

WHAT IS CLAIMED IS:

1. A method of reducing interferences in an electrochemical sensor comprising:

measuring a first current at a first working electrode, said first working electrode being covered by a reagent layer;

measuring a second current at a second working electrode, wherein said reagent layer partially covers said second working electrode, said second working electrode having a covered area and an uncovered area; and

calculating a corrected current value representative of a glucose concentration using a ratio of said covered area to said uncovered area of said second working electrode.

2. The method of claim 1, wherein said corrected current value is calculated using the equation:

$$G = WE_1 - \left\{\left(\frac{A_{\text{cov}}}{A_{unc}}\right) X\left(WE_2 - WE_1\right)\right\}$$

where G is the corrected current value, WE_1 is the uncorrected current density at said first working electrode, WE_2 is the uncorrected current density at said second working electrode, A_{cov} is the coated area of said second working electrode and A_{unc} is the uncoated area of said second working electrode.

3. A method of reducing interferences in an electrochemical sensor comprising:

measuring a second current at a first working electrode, wherein said reagent layer partially covers said first working electrode, said first working electrode having a first covered area and a first uncovered area;

measuring a second current at a second working electrode, wherein said reagent layer partially covers said second working electrode, said second working electrode having a second covered area and a second uncovered area; and

calculating a corrected current value representative of a glucose concentration using a ratio of said covered area to said uncovered area of said first and said second working electrodes.

4. The method of Claim 3, wherein said corrected current value is calculated using the equation:

$$G = WE_1 - \left\{ \left(\frac{f_1 + f_2}{f_2 - 1} \right) \times (WE_2 - WE_1) \right\} \quad \text{(Eq 7c)}$$

where

$f1 = \frac{A_{cov1}}{A_{unc1}}$;

$f2 = \frac{A_{cov1}}{A_{unc2}}$;

A_{unc1} is an uncoated area of said first working electrode;

A_{unc2} is an uncoated area of said second working electrode;

A_{cov1} is a coated area of said first working electrode;

A_{cov2} is a coated area of said second working electrode;

G is the corrected current value;

WE_1 is the uncorrected current density at said first working electrode; and

WE_2 is the uncorrected current density at said second working electrode.