

SITE SPECIFICATION FOR DIRECTIONAL GUIDED SURFACE WAVE TRANSMISSION IN A LOSSY MEDIA

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims priority to, and the benefit of, co-pending U.S. provisional application entitled "Site Specification for Directional Guided Surface Wave Transmission in a Lossy Media" having serial no. 62/305,910, filed March 9, 2016, which is hereby incorporated by reference in its entirety.

[0002] This application is related to co-pending U.S. Non-provisional Patent Application entitled "Excitation and Use of Guided Surface Wave Modes on Lossy Media," which was filed on March 7, 2013 and assigned Application Number 13/789,538, and was published on September 11, 2014 as Publication Number US2014/0252886 A1, and which is incorporated herein by reference in its entirety. This application is also related to co-pending U.S. Non-provisional Patent Application entitled "Excitation and Use of Guided Surface Wave Modes on Lossy Media," which was filed on March 7, 2013 and assigned Application Number 13/789,525, and was published on September 11, 2014 as Publication Number US2014/0252865 A1, and which is incorporated herein by reference in its entirety. This application is also related to co-pending U.S. Non-provisional Patent Application entitled "Excitation and Use of Guided Surface Wave Modes on Lossy Media," which was filed on September 10, 2014 and assigned Application Number 14/483,089, and which is incorporated herein by reference in its entirety. This application is also related to co-pending U.S. Non-provisional Patent Application entitled "Excitation and Use of Guided Surface Waves," which was filed on June 2, 2015 and assigned Application Number 14/728,507, and which is incorporated herein by reference in its entirety. This application is also related to co-pending U.S. Non-provisional Patent Application entitled "Excitation and Use of Guided Surface Waves," which was filed on June 2, 2015 and assigned Application Number 14/728,492, and which is incorporated herein by reference in its entirety. This application is also related to co-pending U.S. Non-provisional Patent Application entitled "Site Preparation

for Guided Surface Wave Transmission in a Lossy Media,” which was filed on September 9, 2015 and assigned Application Number 14/848,413, and which is incorporated herein by reference in its entirety.

BACKGROUND

[0003] For over a century, signals transmitted by radio waves involved radiation fields launched using conventional antenna structures. In contrast to radio science, electrical power distribution systems in the last century involved the transmission of energy guided along electrical conductors. This understanding of the distinction between radio frequency (RF) and power transmission has existed since the early 1900's.

SUMMARY

[0001] Aspects of the present disclosure are related to site specification for directional guided surface wave transmission in a lossy media.

[0002] In one aspect, among others, a probe site comprises a propagation interface in a surface of a lossy conducting medium, the propagation interface including a first region and a second region adjacent to the first region, the first region comprising a first lossy conducting medium and the second region comprising a second lossy conducting medium; and a guided surface waveguide probe positioned over the propagation interface, and adjacent to the first region and the second region, the guided surface waveguide probe configured to generate at least one electrical field that synthesizes a wave front having a complex Brewster angle of incidence corresponding to the first lossy conducting medium when excited by an excitation source, where the wave front launches a guided surface wave along the propagation interface and the surface of the lossy conducting medium in a radial direction that is defined by the first region and restricted by the second region. In one or more aspects of the present disclosure, the wave front can intersect with the propagation interface at the complex Brewster angle of incidence at a crossover distance from the guided surface waveguide probe. The first region and the second region can extend along the propagation interface from adjacent to the guided surface waveguide probe to beyond the crossover distance. The first lossy conducting medium can be a terrestrial medium (e.g., Earth). The second region can extend into the terrestrial medium at least to a depth of a complex image of the guided surface waveguide

probe or at least to a depth of a complex image plane of the guided surface waveguide probe.

[0003] In one or more aspects of the present disclosure, the second lossy conducting medium can be water. The second region can be a naturally occurring body of water. In one or more aspects of the present disclosure, the second lossy conducting medium can be a terrestrial medium. The first region can be a prepared region having a conductivity and permittivity that is different from the terrestrial medium. The prepared region can comprise an excavation containing water. The water can be seawater. The prepared region can comprise an excavation containing an aggregate composition of the terrestrial medium and an added material. In one or more aspects of the present disclosure, the second region can extend around the guided surface waveguide probe from a first side of the first region to a second side of the first region. The propagation interface can include a third region adjacent to the first region opposite the second region. The third region can comprise the second lossy conducting medium or can comprise a third lossy conducting medium.

[0004] Other systems, methods, features, and advantages of the present disclosure will be or become apparent to one with skill in the art upon examination of the following drawings and detailed description. It is intended that all such additional systems, methods, features, and advantages be included within this description, be within the scope of the present disclosure, and be protected by the accompanying claims. In addition, all optional and preferred features and modifications of the described embodiments are usable in all aspects of the disclosure taught herein. Furthermore, the individual features of the dependent claims, as well as all optional and preferred features and modifications of the described embodiments are combinable and interchangeable with one another.

BRIEF DESCRIPTION OF THE DRAWINGS

[0004] Many aspects of the present disclosure can be better understood with reference to the following drawings. The components in the drawings are not necessarily to scale, emphasis instead being placed upon clearly illustrating the principles of the disclosure.

Moreover, in the drawings, like reference numerals designate corresponding parts throughout the several views.

[0005] FIG. 1 is a chart that depicts field strength as a function of distance for a guided electromagnetic field and a radiated electromagnetic field.

[0006] FIG. 2 is a drawing that illustrates a propagation interface with two regions employed for transmission of a guided surface wave according to various embodiments of the present disclosure.

[0007] FIG. 3 is a drawing that illustrates a guided surface waveguide probe disposed with respect to a propagation interface of FIG. 2 according to various embodiments of the present disclosure.

[0008] FIG. 4 is a plot of an example of the magnitudes of close-in and far-out asymptotes of first order Hankel functions according to various embodiments of the present disclosure.

[0009] FIGS. 5A and 5B are drawings that illustrate a complex angle of incidence of an electric field synthesized by a guided surface waveguide probe according to various embodiments of the present disclosure.

[0010] FIG. 6 is a graphical representation illustrating the effect of elevation of a charge terminal on the location where the electric field of FIG. 5A intersects with the lossy conducting medium at a Brewster angle according to various embodiments of the present disclosure.

[0011] FIGS. 7A through 7C are graphical representations of examples of guided surface waveguide probes according to various embodiments of the present disclosure.

[0012] FIGS. 8A through 8C are graphical representations illustrating examples of equivalent image plane models of the guided surface waveguide probe of FIGS. 3 and 7A-7C according to various embodiments of the present disclosure.

[0013] FIGS. 9A through 9C are graphical representations illustrating examples of single-wire transmission line and classic transmission line models of the equivalent image

plane models of FIGS. 8B and 8C according to various embodiments of the present disclosure.

[0014] FIG. 9D is a plot illustrating an example of the reactance variation of a lumped element tank circuit with respect to operating frequency according to various embodiments of the present disclosure.

[0015] FIG. 10 is a flow chart illustrating an example of adjusting a guided surface waveguide probe of FIGS. 3 and 7A-7C to launch a guided surface wave along the surface of a lossy conducting medium according to various embodiments of the present disclosure.

[0016] FIG. 11 is a plot illustrating an example of the relationship between a wave tilt angle and the phase delay of a guided surface waveguide probe of FIGS. 3 and 7A-7C according to various embodiments of the present disclosure.

[0017] FIG. 12 is a drawing that illustrates an example of a guided surface waveguide probe according to various embodiments of the present disclosure.

[0018] FIG. 13 is a graphical representation illustrating the incidence of a synthesized electric field at a complex Brewster angle to match the guided surface waveguide mode at the Hankel crossover distance according to various embodiments of the present disclosure.

[0019] FIG. 14 is a graphical representation of an example of a guided surface waveguide probe of FIG. 12 according to various embodiments of the present disclosure.

[0020] FIG. 15A includes plots of an example of the imaginary and real parts of a phase delay (Φ_U) of a charge terminal T_1 of a guided surface waveguide probe according to various embodiments of the present disclosure.

[0021] FIG. 15B is a schematic diagram of the guided surface waveguide probe of FIG. 14 according to various embodiments of the present disclosure.

[0022] FIG. 16 is a drawing that illustrates an example of a guided surface waveguide probe according to various embodiments of the present disclosure.

[0023] FIG. 17 is a graphical representation of an example of a guided surface waveguide probe of FIG. 16 according to various embodiments of the present disclosure.

[0024] FIGS. 18A through 18C depict examples of receiving structures that can be employed to receive energy transmitted in the form of a guided surface wave launched by a guided surface waveguide probe according to the various embodiments of the present disclosure.

[0025] FIG. 18D is a flow chart illustrating an example of adjusting a receiving structure according to various embodiments of the present disclosure.

[0026] FIG. 19 depicts an example of an additional receiving structure that can be employed to receive energy transmitted in the form of a guided surface wave launched by a guided surface waveguide probe according to the various embodiments of the present disclosure.

[0027] FIG. 20 illustrates a cross sectional view of an example guided surface waveguide probe site including a propagation interface according to various embodiments of the present disclosure.

[0028] FIG. 21A illustrates a cross sectional view of another example guided surface waveguide probe site in which a portion of a region of the propagation interface in FIG. 20 is prepared to more efficiently launch a guided surface wave according to various embodiments of the present disclosure.

[0029] FIG. 21B illustrates a top down view of the guided surface waveguide probe site in FIG. 21A according to various embodiments of the present disclosure.

[0030] FIG. 22 illustrates a stage in the preparation of the portion of the region of the propagation interface in FIG. 21A according to various embodiments of the present disclosure.

[0031] FIGS. 23A-23D illustrate top down views of examples of guided surface waveguide probe sites prepared for directional guided surface wave transmission according to various embodiments of the present disclosure.

[0032] FIGS. 24A and 24B illustrate top down views of examples of guided surface waveguide probe sites prepared for directional guided surface wave transmission according to various embodiments of the present disclosure.

[0033] FIGS. 25A and 25B illustrate top down views of examples of guided surface waveguide probe sites utilizing geographic features of the landscape for directional guided surface wave transmission according to various embodiments of the present disclosure.

DETAILED DESCRIPTION

[0034] To begin, some terminology shall be established to provide clarity in the discussion of concepts to follow. First, as contemplated herein, a formal distinction is drawn between **radiated** electromagnetic fields and **guided** electromagnetic fields.

[0035] As contemplated herein, a radiated electromagnetic field comprises electromagnetic energy that is emitted from a source structure in the form of waves that are not bound to a waveguide. For example, a radiated electromagnetic field is generally a field that leaves an electric structure such as an antenna and propagates through the atmosphere or other medium and is not bound to any waveguide structure. Once radiated electromagnetic waves leave an electric structure such as an antenna, they continue to propagate in the medium of propagation (such as air) independent of their source until they dissipate regardless of whether the source continues to operate. Once electromagnetic waves are radiated, they are not recoverable unless intercepted, and, if not intercepted, the energy inherent in the radiated electromagnetic waves is lost forever. Electrical structures such as antennas are designed to radiate electromagnetic fields by maximizing the ratio of the radiation resistance to the structure loss resistance. Radiated energy spreads out in space and is lost regardless of whether a receiver is present. The energy density of the radiated fields is a function of distance due to geometric spreading. Accordingly, the term “radiate” in all its forms as used herein refers to this form of electromagnetic propagation.

[0036] A guided electromagnetic field is a propagating electromagnetic wave whose energy is concentrated within or near boundaries between media having different

electromagnetic properties. In this sense, a guided electromagnetic field is one that is bound to a waveguide and may be characterized as being conveyed by the current flowing in the waveguide. If there is no load to receive and/or dissipate the energy conveyed in a guided electromagnetic wave, then no energy is lost except for that which is dissipated in the conductivity of the guiding medium. Stated another way, if there is no load for a guided electromagnetic wave, then no energy is consumed. Thus, a generator or other source generating a guided electromagnetic field does not deliver real power unless a resistive load is present. To this end, such a generator or other source essentially runs idle until a load is presented. This is akin to running a generator to generate a 60 Hertz electromagnetic wave that is transmitted over power lines where there is no electrical load. It should be noted that a guided electromagnetic field or wave is the equivalent to what is termed a “transmission line mode.” This contrasts with radiated electromagnetic waves in which real power is supplied at all times in order to generate radiated waves. Unlike radiated electromagnetic waves, guided electromagnetic energy does not continue to propagate along a finite length waveguide after the energy source is turned off. Accordingly, the term “guide” in all its forms as used herein refers to this transmission mode of electromagnetic propagation.

[0037] Referring now to FIG. 1, shown is a graph 100 of field strength in decibels (dB) above an arbitrary reference in volts per meter as a function of distance in kilometers on a log-dB plot to further illustrate the distinction between radiated and guided electromagnetic fields. The graph 100 of FIG. 1 depicts a guided field strength curve 103 that shows the field strength of a guided electromagnetic field as a function of distance. This guided field strength curve 103 is essentially the same as a transmission line mode. Also, the graph 100 of FIG. 1 depicts a radiated field strength curve 106 that shows the field strength of a radiated electromagnetic field as a function of distance.

[0038] Of interest are the shapes of the curves 103 and 106 for *guided wave* and for *radiation* propagation, respectively. The radiated field strength curve 106 falls off geometrically ($1/d$, where d is distance), which is depicted as a straight line on the log-log

scale. The guided field strength curve 103, on the other hand, has a characteristic exponential decay of $e^{-\alpha d}/\sqrt{d}$ and exhibits a distinctive knee 109 on the log-log scale. The guided field strength curve 103 and the radiated field strength curve 106 intersect at point 112, which occurs at a crossing distance. At distances less than the crossing distance at intersection point 112, the field strength of a guided electromagnetic field is significantly greater at most locations than the field strength of a radiated electromagnetic field. At distances greater than the crossing distance, the opposite is true. Thus, the guided and radiated field strength curves 103 and 106 further illustrate the fundamental propagation difference between guided and radiated electromagnetic fields. For an informal discussion of the difference between guided and radiated electromagnetic fields, reference is made to Milligan, T., Modern Antenna Design, McGraw-Hill, 1st Edition, 1985, pp.8-9, which is incorporated herein by reference in its entirety.

[0039] The distinction between radiated and guided electromagnetic waves, made above, is readily expressed formally and placed on a rigorous basis. That two such diverse solutions could emerge from one and the same linear partial differential equation, the wave equation, analytically follows from the boundary conditions imposed on the problem. The Green function for the wave equation, itself, contains the distinction between the nature of radiation and guided waves.

[0040] In empty space, the wave equation is a differential operator whose eigenfunctions possess a *continuous* spectrum of eigenvalues on the complex wave-number plane. This transverse electro-magnetic (TEM) field is called the radiation field, and those propagating fields are called “Hertzian waves.” However, in the presence of a conducting boundary, the wave equation plus boundary conditions mathematically lead to a spectral representation of wave-numbers composed of a continuous spectrum *plus* a sum of *discrete* spectra. To this end, reference is made to Sommerfeld, A., “Über die Ausbreitung der Wellen in der Drahtlosen Telegraphie,” *Annalen der Physik*, Vol. 28, 1909, pp. 665-736. Also see Sommerfeld, A., “Problems of Radio,” published as Chapter 6 in Partial Differential

Equations in Physics – Lectures on Theoretical Physics: Volume VI, Academic Press, 1949, pp. 236-289, 295-296; Collin, R. E., “Hertzian Dipole Radiating Over a Lossy Earth or Sea: Some Early and Late 20th Century Controversies,” IEEE Antennas and Propagation Magazine, Vol. 46, No. 2, April 2004, pp. 64-79; and Reich, H. J., Ordnung, P.F, Krauss, H.L., and Skalnik, J.G., Microwave Theory and Techniques, Van Nostrand, 1953, pp. 291-293, each of these references being incorporated herein by reference in its entirety.

[0041] The terms “*ground wave*” and “*surface wave*” identify two distinctly different physical propagation phenomena. A surface wave arises analytically from a distinct *pole* yielding a *discrete* component in the plane wave spectrum. See, e.g., “The Excitation of Plane Surface Waves” by Cullen, A.L., (Proceedings of the IEE (British), Vol. 101, Part IV, August 1954, pp. 225-235). In this context, a *surface wave* is considered to be a guided *surface wave*. The *surface wave* (in the Zenneck-Sommerfeld guided wave sense) is, physically and mathematically, not the same as the *ground wave* (in the Weyl-Norton-FCC sense) that is now so familiar from radio broadcasting. These two propagation mechanisms arise from the excitation of different types of eigenvalue spectra (continuum or discrete) on the complex plane. The field strength of the *guided surface wave* decays exponentially with distance as illustrated by guided field strength curve 103 of FIG. 1 (much like propagation in a lossy waveguide) and resembles propagation in a radial transmission line, as opposed to the classical Hertzian radiation of the *ground wave*, which propagates spherically, possesses a *continuum* of eigenvalues, falls off geometrically as illustrated by radiated field strength curve 106 of FIG. 1, and results from branch-cut integrals. As experimentally demonstrated by C.R. Burrows in “The Surface Wave in Radio Propagation over Plane Earth” (Proceedings of the IRE, Vol. 25, No. 2, February, 1937, pp. 219-229) and “The Surface Wave in Radio Transmission” (Bell Laboratories Record, Vol. 15, June 1937, pp. 321-324), vertical antennas radiate *ground waves* but do not launch guided *surface waves*.

[0042] To summarize the above, first, the *continuous* part of the wave-number eigenvalue spectrum, corresponding to *branch-cut integrals*, produces the radiation field, and second, the *discrete* spectra, and corresponding *residue sum* arising from the poles

enclosed by the contour of integration, result in non-TEM traveling surface waves that are exponentially damped in the direction transverse to the propagation. Such surface waves are guided transmission line modes. For further explanation, reference is made to Friedman, B., Principles and Techniques of Applied Mathematics, Wiley, 1956, pp. pp. 214, 283-286, 290, 298-300.

[0043] In free space, antennas excite the *continuum* eigenvalues of the wave equation, which is a radiation field, where the outwardly propagating RF energy with E_z and H_ϕ in-phase is lost forever. On the other hand, waveguide probes excite *discrete* eigenvalues, which results in transmission line propagation. See Collin, R. E., Field Theory of Guided Waves, McGraw-Hill, 1960, pp. 453, 474-477. While such theoretical analyses have held out the hypothetical possibility of launching open surface guided waves over planar or spherical surfaces of lossy, homogeneous media, for more than a century no known structures in the engineering arts have existed for accomplishing this with any practical efficiency. Unfortunately, since it emerged in the early 1900's, the theoretical analysis set forth above has essentially remained a theory and there have been no known structures for practically accomplishing the launching of open surface guided waves over planar or spherical surfaces of lossy, homogeneous media.

[0044] According to the various embodiments of the present disclosure, various guided surface waveguide probes are described that are configured to excite electric fields that couple into a guided surface waveguide mode along the surface of a lossy conducting medium. Such guided electromagnetic fields are substantially mode-matched in magnitude and phase to a guided surface wave mode on the surface of the lossy conducting medium. Such a guided surface wave mode can also be termed a Zenneck waveguide mode. By virtue of the fact that the resultant fields excited by the guided surface waveguide probes described herein are substantially mode-matched to a guided surface waveguide mode on the surface of the lossy conducting medium, a guided electromagnetic field in the form of a guided surface wave is launched along the surface of the lossy conducting medium.

According to one embodiment, the lossy conducting medium comprises a terrestrial medium such as the Earth.

[0045] Referring to FIG. 2, shown is a propagation interface that provides for an examination of the boundary value solutions to Maxwell's equations derived in 1907 by Jonathan Zenneck as set forth in his paper Zenneck, J., "On the Propagation of Plane Electromagnetic Waves Along a Flat Conducting Surface and their Relation to Wireless Telegraphy," *Annalen der Physik*, Serial 4, Vol. 23, September 20, 1907, pp. 846-866. FIG. 2 depicts cylindrical coordinates for radially propagating waves along the interface between a lossy conducting medium specified as Region 1 and an insulator specified as Region 2. Region 1 can comprise, for example, any lossy conducting medium. In one example, such a lossy conducting medium can comprise a terrestrial medium such as the Earth or other medium. Region 2 is a second medium that shares a boundary interface with Region 1 and has different constitutive parameters relative to Region 1. Region 2 can comprise, for example, any insulator such as the atmosphere or other medium. The reflection coefficient for such a boundary interface goes to zero only for incidence at a *complex* Brewster angle. See Stratton, J.A., Electromagnetic Theory, McGraw-Hill, 1941, p. 516.

[0046] According to various embodiments, the present disclosure sets forth various guided surface waveguide probes that generate electromagnetic fields that are substantially mode-matched to a guided surface waveguide mode on the surface of the lossy conducting medium comprising Region 1. According to various embodiments, such electromagnetic fields substantially synthesize a wave front incident at a complex Brewster angle of the lossy conducting medium that can result in zero reflection.

[0047] To explain further, in Region 2, where an $e^{j\omega t}$ field variation is assumed and where $\rho \neq 0$ and $z \geq 0$ (with z being the vertical coordinate normal to the surface of Region 1, and ρ being the radial dimension in cylindrical coordinates), Zenneck's closed-form exact solution of Maxwell's equations satisfying the boundary conditions along the interface are expressed by the following electric field and magnetic field components:

$$H_{2\phi} = A e^{-u_2 z} H_1^{(2)}(-j\gamma\rho), \quad (1)$$

$$E_{2\rho} = A \left(\frac{u_2}{j\omega\epsilon_0} \right) e^{-u_2 z} H_1^{(2)}(-j\gamma\rho), \text{ and} \quad (2)$$

$$E_{2z} = A \left(\frac{-\gamma}{\omega\epsilon_0} \right) e^{-u_2 z} H_0^{(2)}(-j\gamma\rho). \quad (3)$$

[0048] In Region 1, where the $e^{j\omega t}$ field variation is assumed and where $\rho \neq 0$ and $z \leq 0$, Zenneck's closed-form exact solution of Maxwell's equations satisfying the boundary conditions along the interface is expressed by the following electric field and magnetic field components:

$$H_{1\phi} = A e^{u_1 z} H_1^{(2)}(-j\gamma\rho), \quad (4)$$

$$E_{1\rho} = A \left(\frac{-u_1}{\sigma_1 + j\omega\epsilon_1} \right) e^{u_1 z} H_1^{(2)}(-j\gamma\rho), \text{ and} \quad (5)$$

$$E_{1z} = A \left(\frac{-j\gamma}{\sigma_1 + j\omega\epsilon_1} \right) e^{u_1 z} H_0^{(2)}(-j\gamma\rho). \quad (6)$$

[0049] In these expressions, z is the vertical coordinate normal to the surface of Region 1 and ρ is the radial coordinate, $H_n^{(2)}(-j\gamma\rho)$ is a complex argument Hankel function of the second kind and order n , u_1 is the propagation constant in the positive vertical (z) direction in Region 1, u_2 is the propagation constant in the vertical (z) direction in Region 2, σ_1 is the conductivity of Region 1, ω is equal to $2\pi f$, where f is a frequency of excitation, ϵ_0 is the permittivity of free space, ϵ_1 is the permittivity of Region 1, A is a source constant imposed by the source, and γ is a surface wave radial propagation constant.

[0050] The propagation constants in the $\pm z$ directions are determined by separating the wave equation above and below the interface between Regions 1 and 2, and imposing the boundary conditions. This exercise gives, in Region 2,

$$u_2 = \frac{-jk_o}{\sqrt{1+(\epsilon_r - jx)}} \quad (7)$$

and gives, in Region 1,

$$u_1 = -u_2(\epsilon_r - jx). \quad (8)$$

The radial propagation constant γ is given by

$$\gamma = j\sqrt{k_o^2 + u_2^2} = j\frac{k_o n}{\sqrt{1+n^2}}, \quad (9)$$

which is a complex expression where n is the complex index of refraction given by

$$n = \sqrt{\varepsilon_r - jx}. \quad (10)$$

In all of the above Equations,

$$x = \frac{\sigma_1}{\omega\varepsilon_o}, \text{ and} \quad (11)$$

$$k_o = \omega\sqrt{\mu_o\varepsilon_o} = \frac{\lambda_o}{2\pi}, \quad (12)$$

where ε_r comprises the relative permittivity of Region 1, σ_1 is the conductivity of Region 1, ε_o is the permittivity of free space, and μ_o comprises the permeability of free space. Thus, the generated surface wave propagates parallel to the interface and exponentially decays vertical to it. This is known as evanescence.

[0051] Thus, Equations (1)-(3) can be considered to be a cylindrically-symmetric, radially-propagating waveguide mode. See Barlow, H. M., and Brown, J., Radio Surface Waves, Oxford University Press, 1962, pp. 10-12, 29-33. The present disclosure details structures that excite this “open boundary” waveguide mode. Specifically, according to various embodiments, a guided surface waveguide probe is provided with a charge terminal of appropriate size that is fed with voltage and/or current and is positioned relative to the boundary interface between Region 2 and Region 1. This may be better understood with reference to FIG. 3, which shows an example of a guided surface waveguide probe 200a that includes a charge terminal T_1 elevated above a lossy conducting medium 203 (e.g., the Earth) along a vertical axis z that is normal to a plane presented by the lossy conducting medium 203. The lossy conducting medium 203 makes up Region 1, and a second medium 206 makes up Region 2 and shares a boundary interface with the lossy conducting medium 203.

[0052] According to one embodiment, the lossy conducting medium 203 can comprise a terrestrial medium such as the planet Earth. To this end, such a terrestrial medium comprises all structures or formations included thereon whether natural or man-made. For

example, such a terrestrial medium can comprise natural elements such as rock, soil, sand, fresh water, sea water, trees, vegetation, and all other natural elements that make up our planet. In addition, such a terrestrial medium can comprise man-made elements such as concrete, asphalt, building materials, and other man-made materials. In other embodiments, the lossy conducting medium 203 can comprise some medium other than the Earth, whether naturally occurring or man-made. In other embodiments, the lossy conducting medium 203 can comprise other media such as man-made surfaces and structures such as automobiles, aircraft, man-made materials (such as plywood, plastic sheeting, or other materials) or other media.

[0053] In the case where the lossy conducting medium 203 comprises a terrestrial medium or Earth, the second medium 206 can comprise the atmosphere above the ground. As such, the atmosphere can be termed an “atmospheric medium” that comprises air and other elements that make up the atmosphere of the Earth. In addition, it is possible that the second medium 206 can comprise other media relative to the lossy conducting medium 203.

[0054] The guided surface waveguide probe 200a includes a feed network 209 that couples an excitation source 212 to the charge terminal T_1 via, e.g., a vertical feed line conductor. The excitation source 212 may comprise, for example, an Alternating Current (AC) source or some other source. As contemplated herein, an excitation source can comprise an AC source or other type of source. According to various embodiments, a charge Q_1 is imposed on the charge terminal T_1 to synthesize an electric field based upon the voltage applied to terminal T_1 at any given instant. Depending on the angle of incidence (θ_i) of the electric field (E), it is possible to substantially mode-match the electric field to a guided surface waveguide mode on the surface of the lossy conducting medium 203 comprising Region 1.

[0055] By considering the Zenneck closed-form solutions of Equations (1)-(6), the Leontovich impedance boundary condition between Region 1 and Region 2 can be stated as

$$\hat{z} \times \vec{H}_2(\rho, \varphi, 0) = \vec{J}_S, \quad (13)$$

where $\hat{z}$ is a unit normal in the positive vertical (+z) direction and $\vec{H}_2$ is the magnetic field strength in Region 2 expressed by Equation (1) above. Equation (13) implies that the electric and magnetic fields specified in Equations (1)-(3) may result in a radial surface current density along the boundary interface, where the radial surface current density can be specified by

$$J_\rho(\rho') = -A H_1^{(2)}(-j\gamma\rho') \quad (14)$$

where A is a constant. Further, it should be noted that close-in to the guided surface waveguide probe 200 (for $\rho \ll \lambda$), Equation (14) above has the behavior

$$J_{close}(\rho') = \frac{-A(j2)}{\pi(-j\gamma\rho')} = -H_\phi = -\frac{I_o}{2\pi\rho'}. \quad (15)$$

The negative sign means that when source current (I_o) flows vertically upward as illustrated in FIG. 3, the “close-in” ground current flows radially *inward*. By field matching on H_ϕ “close-in,” it can be determined that

$$A = -\frac{I_o\gamma}{4} = -\frac{\omega q_1\gamma}{4} \quad (16)$$

where $q_1 = C_1 V_1$, in Equations (1)-(6) and (14). Therefore, the radial surface current density of Equation (14) can be restated as

$$J_\rho(\rho') = \frac{I_o\gamma}{4} H_1^{(2)}(-j\gamma\rho'). \quad (17)$$

The fields expressed by Equations (1)-(6) and (17) have the nature of a *transmission line mode* bound to a lossy interface, *not radiation fields* that are associated with groundwave propagation. See Barlow, H. M. and Brown, J., Radio Surface Waves, Oxford University Press, 1962, pp. 1-5.

[0056] At this point, a review of the nature of the Hankel functions used in Equations (1)-(6) and (17) is provided for these solutions of the wave equation. One might observe that the Hankel functions of the first and second kind and order n are defined as complex combinations of the standard Bessel functions of the first and second kinds

$$H_n^{(1)}(x) = J_n(x) + jN_n(x), \text{ and} \quad (18)$$

$$H_n^{(2)}(x) = J_n(x) - jN_n(x). \quad (19)$$

These functions represent cylindrical waves propagating radially inward ($H_n^{(1)}$) and outward ($H_n^{(2)}$), respectively. The definition is analogous to the relationship $e^{\pm jx} = \cos x \pm j \sin x$. See, for example, Harrington, R.F., Time-Harmonic Fields, McGraw-Hill, 1961, pp. 460-463.

[0057] That $H_n^{(2)}(k_\rho \rho)$ is an outgoing wave can be recognized from its large argument asymptotic behavior that is obtained directly from the series definitions of $J_n(x)$ and $N_n(x)$. Far-out from the guided surface waveguide probe:

$$H_n^{(2)}(x) \xrightarrow{x \rightarrow \infty} \sqrt{\frac{2j}{\pi x}} j^n e^{-jx} = \sqrt{\frac{2}{\pi x}} j^n e^{-j\left(x - \frac{\pi}{4}\right)}, \quad (20a)$$

which, when multiplied by $e^{j\omega t}$, is an outward propagating cylindrical wave of the form $e^{j(\omega t - k\rho)}$ with a $1/\sqrt{\rho}$ spatial variation. The first order ($n = 1$) solution can be determined from Equation (20a) to be

$$H_1^{(2)}(x) \xrightarrow{x \rightarrow \infty} j \sqrt{\frac{2j}{\pi x}} e^{-jx} = \sqrt{\frac{2}{\pi x}} e^{-j\left(x - \frac{\pi}{2} - \frac{\pi}{4}\right)}. \quad (20b)$$

Close-in to the guided surface waveguide probe (for $\rho \ll \lambda$), the Hankel function of first order and the second kind behaves as

$$H_1^{(2)}(x) \xrightarrow{x \rightarrow 0} \frac{2j}{\pi x}. \quad (21)$$

Note that these asymptotic expressions are complex quantities. When x is a real quantity, Equations (20b) and (21) differ in phase by $\sqrt{j}$, which corresponds to an extra phase advance or “phase boost” of 45° or, equivalently, $\lambda/8$. The close-in and far-out asymptotes of the first order Hankel function of the second kind have a Hankel “crossover” or transition point where they are of equal magnitude at a distance of $\rho = R_x$.

[0058] Thus, beyond the Hankel crossover point the “far out” representation predominates over the “close-in” representation of the Hankel function. The distance to the Hankel crossover point (or Hankel crossover distance) can be found by equating Equations (20b) and (21) for $-j\gamma\rho$, and solving for R_x . With $x = \sigma/\omega\epsilon_0$, it can be seen that the far-out and close-in Hankel function asymptotes are frequency dependent, with the Hankel crossover

point moving out as the frequency is lowered. It should also be noted that the Hankel function asymptotes may also vary as the conductivity (σ) of the lossy conducting medium changes. For example, the conductivity of the soil can vary with changes in weather conditions.

[0059] Referring to FIG. 4, shown is an example of a plot of the magnitudes of the first order Hankel functions of Equations (20b) and (21) for a Region 1 conductivity of $\sigma = 0.010$ mhos/m and relative permittivity $\epsilon_r = 15$, at an operating frequency of 1850 kHz. Curve 115 is the magnitude of the far-out asymptote of Equation (20b) and curve 118 is the magnitude of the close-in asymptote of Equation (21), with the Hankel crossover point 121 occurring at a distance of $R_x = 54$ feet. While the magnitudes are equal, a phase offset exists between the two asymptotes at the Hankel crossover point 121. It can also be seen that the Hankel crossover distance is much less than a wavelength of the operation frequency.

[0060] Considering the electric field components given by Equations (2) and (3) of the Zenneck closed-form solution in Region 2, it can be seen that the ratio of E_z and E_ρ asymptotically passes to

$$\frac{E_z}{E_\rho} = \left(\frac{-j\gamma}{u_2} \right) \frac{H_0^{(2)}(-j\gamma\rho)}{H_1^{(2)}(-j\gamma\rho)} \xrightarrow{\rho \rightarrow \infty} \sqrt{\epsilon_r - j \frac{\sigma}{\omega\epsilon_0}} = n = \tan \theta_i, \quad (22)$$

where n is the complex index of refraction of Equation (10) and θ_i is the angle of incidence of the electric field. In addition, the vertical component of the mode-matched electric field of Equation (3) asymptotically passes to

$$E_{2z} \xrightarrow{\rho \rightarrow \infty} \left(\frac{q_{free}}{\epsilon_0} \right) \sqrt{\frac{\gamma^3}{8\pi}} e^{-u_2 z} \frac{e^{-j(\gamma\rho - \pi/4)}}{\sqrt{\rho}}, \quad (23)$$

which is linearly proportional to free charge on the isolated component of the elevated charge terminal's capacitance at the terminal voltage, $q_{free} = C_{free} \times V_T$.

[0061] For example, the height H_1 of the elevated charge terminal T_1 in FIG. 3 affects the amount of free charge on the charge terminal T_1 . When the charge terminal T_1 is near the ground plane of Region 1, most of the charge Q_1 on the terminal is "bound." As the charge terminal T_1 is elevated, the bound charge is lessened until the charge terminal T_1 reaches a height at which substantially all of the isolated charge is free.

[0062] The advantage of an increased capacitive elevation for the charge terminal T_1 is that the charge on the elevated charge terminal T_1 is further removed from the ground plane, resulting in an increased amount of free charge q_{free} to couple energy into the guided surface waveguide mode. As the charge terminal T_1 is moved away from the ground plane, the charge distribution becomes more uniformly distributed about the surface of the terminal. The amount of free charge is related to the self-capacitance of the charge terminal T_1 .

[0063] For example, the capacitance of a spherical terminal can be expressed as a function of physical height above the ground plane. The capacitance of a sphere at a physical height of h above a perfect ground is given by

$$C_{\text{elevated sphere}} = 4\pi\epsilon_0 a(1 + M + M^2 + M^3 + 2M^4 + 3M^5 + \dots), \quad (24)$$

where the diameter of the sphere is $2a$, and where $M = a/2h$ with h being the height of the spherical terminal. As can be seen, an increase in the terminal height h reduces the capacitance C of the charge terminal. It can be shown that for elevations of the charge terminal T_1 that are at a height of about four times the diameter ($4D = 8a$) or greater, the charge distribution is approximately uniform about the spherical terminal, which can improve the coupling into the guided surface waveguide mode.

[0064] In the case of a sufficiently isolated terminal, the self-capacitance of a conductive sphere can be approximated by $C = 4\pi\epsilon_0 a$, where a is the radius of the sphere in meters, and the self-capacitance of a disk can be approximated by $C = 8\epsilon_0 a$, where a is the radius of the disk in meters. The charge terminal T_1 can include any shape such as a sphere, a disk, a cylinder, a cone, a torus, a hood, one or more rings, or any other randomized shape or combination of shapes. An equivalent spherical diameter can be determined and used for positioning of the charge terminal T_1 .

[0065] This may be further understood with reference to the example of FIG. 3, where the charge terminal T_1 is elevated at a physical height of $h_p = H_1$ above the lossy conducting medium 203. To reduce the effects of the “bound” charge, the charge terminal T_1 can be

positioned at a physical height that is at least four times the spherical diameter (or equivalent spherical diameter) of the charge terminal T_1 to reduce the bounded charge effects.

[0066] Referring next to FIG. 5A, shown is a ray optics interpretation of the electric field produced by the elevated charge Q_1 on charge terminal T_1 of FIG. 3. As in optics, minimizing the reflection of the incident electric field can improve and/or maximize the energy coupled into the guided surface waveguide mode of the lossy conducting medium 203. For an electric field ($E_{\parallel}$) that is polarized parallel to the plane of incidence (not the boundary interface), the amount of reflection of the incident electric field may be determined using the Fresnel reflection coefficient, which can be expressed as

$$\Gamma_{\parallel}(\theta_i) = \frac{E_{\parallel,R}}{E_{\parallel,i}} = \frac{\sqrt{(\epsilon_r - jx) - \sin^2 \theta_i} - (\epsilon_r - jx) \cos \theta_i}{\sqrt{(\epsilon_r - jx) - \sin^2 \theta_i} + (\epsilon_r - jx) \cos \theta_i}, \quad (25)$$

where θ_i is the conventional angle of incidence measured with respect to the surface normal.

[0067] In the example of FIG. 5A, the ray optic interpretation shows the incident field polarized parallel to the plane of incidence having an angle of incidence of θ_i , which is measured with respect to the surface normal ($\hat{z}$). There will be no reflection of the incident electric field when $\Gamma_{\parallel}(\theta_i) = 0$ and thus the incident electric field will be completely coupled into a guided surface waveguide mode along the surface of the lossy conducting medium 203. It can be seen that the numerator of Equation (25) goes to zero when the angle of incidence is

$$\theta_i = \arctan(\sqrt{\epsilon_r - jx}) = \theta_{i,B}, \quad (26)$$

where $x = \sigma/\omega\epsilon_0$. This complex angle of incidence ($\theta_{i,B}$) is referred to as the Brewster angle. Referring back to Equation (22), it can be seen that the same complex Brewster angle ($\theta_{i,B}$) relationship is present in both Equations (22) and (26).

[0068] As illustrated in FIG. 5A, the electric field vector E can be depicted as an incoming non-uniform plane wave, polarized parallel to the plane of incidence. The electric field vector E can be created from independent horizontal and vertical components as

$$\vec{E}(\theta_i) = E_\rho \hat{\rho} + E_z \hat{z}. \quad (27)$$

Geometrically, the illustration in FIG. 5A suggests that the electric field vector E can be given by

$$E_\rho(\rho, z) = E(\rho, z) \cos \theta_i, \text{ and} \quad (28a)$$

$$E_z(\rho, z) = E(\rho, z) \cos\left(\frac{\pi}{2} - \theta_i\right) = E(\rho, z) \sin \theta_i, \quad (28b)$$

which means that the field ratio is

$$\frac{E_\rho}{E_z} = \frac{1}{\tan \theta_i} = \tan \psi_i. \quad (29)$$

[0069] A generalized parameter W , called “wave tilt,” is noted herein as the ratio of the horizontal electric field component to the vertical electric field component given by

$$W = \frac{E_\rho}{E_z} = |W|e^{j\Psi}, \text{ or} \quad (30a)$$

$$\frac{1}{W} = \frac{E_z}{E_\rho} = \tan \theta_i = \frac{1}{|W|}e^{-j\Psi}, \quad (30b)$$

which is complex and has both magnitude and phase. For an electromagnetic wave in Region 2 (FIG. 2), the wave tilt angle (Ψ) is equal to the angle between the normal of the wave-front at the boundary interface with Region 1 (FIG. 2) and the tangent to the boundary interface. This may be easier to see in FIG. 5B, which illustrates equi-phase surfaces of an electromagnetic wave and their normals for a radial cylindrical guided surface wave. At the boundary interface ($z = 0$) with a perfect conductor, the wave-front normal is parallel to the tangent of the boundary interface, resulting in $W = 0$. However, in the case of a lossy dielectric, a wave tilt W exists because the wave-front normal is not parallel with the tangent of the boundary interface at $z = 0$.

[0070] Applying Equation (30b) to a guided surface wave gives

$$\tan \theta_{i,B} = \frac{E_z}{E_\rho} = \frac{u_2}{\gamma} = \sqrt{\epsilon_r - j\chi} = n = \frac{1}{W} = \frac{1}{|W|}e^{-j\Psi}. \quad (31)$$

With the angle of incidence equal to the complex Brewster angle ($\theta_{i,B}$), the Fresnel reflection coefficient of Equation (25) vanishes, as shown by

$$\Gamma_{\parallel}(\theta_{i,B}) = \frac{\sqrt{(\varepsilon_r - jx) - \sin^2 \theta_i} - (\varepsilon_r - jx) \cos \theta_i}{\sqrt{(\varepsilon_r - jx) - \sin^2 \theta_i} + (\varepsilon_r - jx) \cos \theta_i} \Big|_{\theta_i = \theta_{i,B}} = 0. \quad (32)$$

By adjusting the complex field ratio of Equation (22), an incident field can be synthesized to be incident at a complex angle at which the reflection is reduced or eliminated. Establishing this ratio as $n = \sqrt{\varepsilon_r - jx}$ results in the synthesized electric field being incident at the complex Brewster angle, making the reflections vanish.

[0071] The concept of an electrical effective height can provide further insight into synthesizing an electric field with a complex angle of incidence with a guided surface waveguide probe 200. The electrical effective height (h_{eff}) has been defined as

$$h_{eff} = \frac{1}{I_0} \int_0^{h_p} I(z) dz \quad (33)$$

for a monopole with a physical height (or length) of h_p . Since the expression depends upon the magnitude and phase of the source distribution along the structure, the effective height (or length) is complex in general. The integration of the distributed current $I(z)$ of the structure is performed over the physical height of the structure (h_p), and normalized to the ground current (I_0) flowing upward through the base (or input) of the structure. The distributed current along the structure can be expressed by

$$I(z) = I_C \cos(\beta_0 z), \quad (34)$$

where β_0 is the propagation factor for current propagating on the structure. In the example of FIG. 3, I_C is the current that is distributed along the vertical structure of the guided surface waveguide probe 200a.

[0072] For example, consider a feed network 209 that includes a low loss coil (e.g., a helical coil) at the bottom of the structure and a vertical feed line conductor connected between the coil and the charge terminal T_1 . The phase delay due to the coil (or helical delay line) is $\theta_c = \beta_p l_C$, with a physical length of l_C and a propagation factor of

$$\beta_p = \frac{2\pi}{\lambda_p} = \frac{2\pi}{v_f \lambda_0}, \quad (35)$$

where V_f is the velocity factor on the structure, λ_0 is the wavelength at the supplied frequency, and λ_p is the propagation wavelength resulting from the velocity factor V_f . The phase delay is measured relative to the ground (stake or system) current I_0 .

[0073] In addition, the spatial phase delay along the length l_w of the vertical feed line conductor can be given by $\theta_y = \beta_w l_w$ where β_w is the propagation phase constant for the vertical feed line conductor. In some implementations, the spatial phase delay may be approximated by $\theta_y = \beta_w h_p$, since the difference between the physical height h_p of the guided surface waveguide probe 200a and the vertical feed line conductor length l_w is much less than a wavelength at the supplied frequency (λ_0). As a result, the total phase delay through the coil and vertical feed line conductor is $\Phi = \theta_c + \theta_y$, and the current fed to the top of the coil from the bottom of the physical structure is

$$I_c(\theta_c + \theta_y) = I_0 e^{j\Phi}, \quad (36)$$

with the total phase delay Φ measured relative to the ground (stake or system) current I_0 . Consequently, the electrical effective height of a guided surface waveguide probe 200 can be approximated by

$$h_{eff} = \frac{1}{I_0} \int_0^{h_p} I_0 e^{j\Phi} \cos(\beta_0 z) dz \cong h_p e^{j\Phi}, \quad (37)$$

for the case where the physical height $h_p \ll \lambda_0$. The complex effective height of a monopole, $h_{eff} = h_p$ at an angle (or phase delay) of Φ , may be adjusted to cause the source fields to match a guided surface waveguide mode and cause a guided surface wave to be launched on the lossy conducting medium 203.

[0074] In the example of FIG. 5A, ray optics are used to illustrate the complex angle trigonometry of the incident electric field (E) having a complex Brewster angle of incidence ($\theta_{i,B}$) at the Hankel crossover distance (R_x) 121. Recall from Equation (26) that, for a lossy conducting medium, the Brewster angle is complex and specified by

$$\tan \theta_{i,B} = \sqrt{\epsilon_r - j \frac{\sigma}{\omega \epsilon_0}} = n. \quad (38)$$

Electrically, the geometric parameters are related by the electrical effective height (h_{eff}) of the charge terminal T_1 by

$$R_x \tan \psi_{i,B} = R_x \times W = h_{eff} = h_p e^{j\Phi}, \quad (39)$$

where $\psi_{i,B} = (\pi/2) - \theta_{i,B}$ is the Brewster angle measured from the surface of the lossy conducting medium. To couple into the guided surface waveguide mode, the wave tilt of the electric field at the Hankel crossover distance can be expressed as the ratio of the electrical effective height and the Hankel crossover distance

$$\frac{h_{eff}}{R_x} = \tan \psi_{i,B} = W_{Rx}. \quad (40)$$

Since both the physical height (h_p) and the Hankel crossover distance (R_x) are real quantities, the angle (Ψ) of the desired guided surface wave tilt at the Hankel crossover distance (R_x) is equal to the phase (Φ) of the complex effective height (h_{eff}). This implies that by varying the phase at the supply point of the coil, and thus the phase delay in Equation (37), the phase, Φ , of the complex effective height can be manipulated to match the angle of the wave tilt, Ψ , of the guided surface waveguide mode at the Hankel crossover point 121: $\Phi = \Psi$.

[0075] In FIG. 5A, a right triangle is depicted having an adjacent side of length R_x along the lossy conducting medium surface and a complex Brewster angle $\psi_{i,B}$ measured between a ray 124 extending between the Hankel crossover point 121 at R_x and the center of the charge terminal T_1 , and the lossy conducting medium surface 127 between the Hankel crossover point 121 and the charge terminal T_1 . With the charge terminal T_1 positioned at physical height h_p and excited with a charge having the appropriate phase delay Φ , the resulting electric field is incident with the lossy conducting medium boundary interface at the Hankel crossover distance R_x , and at the Brewster angle. Under these conditions, the guided surface waveguide mode can be excited without reflection or substantially negligible reflection.

[0076] If the physical height of the charge terminal T_1 is decreased without changing the phase delay Φ of the effective height (h_{eff}), the resulting electric field intersects the lossy conducting medium 203 at the Brewster angle at a reduced distance from the guided surface waveguide probe 200. FIG. 6 graphically illustrates the effect of decreasing the physical height of the charge terminal T_1 on the distance where the electric field is incident at the Brewster angle. As the height is decreased from h_3 through h_2 to h_1 , the point where the electric field intersects with the lossy conducting medium (e.g., the Earth) at the Brewster angle moves closer to the charge terminal position. However, as Equation (39) indicates, the height H_1 (FIG. 3) of the charge terminal T_1 should be at or higher than the physical height (h_p) in order to excite the far-out component of the Hankel function. With the charge terminal T_1 positioned at or above the effective height (h_{eff}), the lossy conducting medium 203 can be illuminated at the Brewster angle of incidence ($\psi_{i,B} = (\pi/2) - \theta_{i,B}$) at or beyond the Hankel crossover distance (R_x) 121 as illustrated in FIG. 5A. To reduce or minimize the bound charge on the charge terminal T_1 , the height should be at least four times the spherical diameter (or equivalent spherical diameter) of the charge terminal T_1 as mentioned above.

[0077] A guided surface waveguide probe 200 can be configured to establish an electric field having a wave tilt that corresponds to a wave illuminating the surface of the lossy conducting medium 203 at a complex Brewster angle, thereby exciting radial surface currents by substantially mode-matching to a guided surface wave mode at (or beyond) the Hankel crossover point 121 at R_x .

[0078] Referring to FIG. 7A, shown is a graphical representation of an example of a guided surface waveguide probe 200b that includes a charge terminal T_1 . As shown in FIG. 7A, an excitation source 212 such as an AC source acts as the excitation source for the charge terminal T_1 , which is coupled to the guided surface waveguide probe 200b through a feed network 209 (FIG. 3) comprising a coil 215 such as, e.g., a helical coil. In other implementations, the excitation source 212 can be inductively coupled to the coil 215

through a primary coil. In some embodiments, an impedance matching network may be included to improve and/or maximize coupling of the excitation source 212 to the coil 215.

[0079] As shown in FIG. 7A, the guided surface waveguide probe 200b can include the upper charge terminal T_1 (e.g., a sphere at height h_p) that is positioned along a vertical axis z that is substantially normal to the plane presented by the lossy conducting medium 203. A second medium 206 is located above the lossy conducting medium 203. The charge terminal T_1 has a self-capacitance C_T . During operation, charge Q_1 is imposed on the terminal T_1 depending on the voltage applied to the terminal T_1 at any given instant.

[0080] In the example of FIG. 7A, the coil 215 is coupled to a ground stake (or grounding system) 218 at a first end and to the charge terminal T_1 via a vertical feed line conductor 221. In some implementations, the coil connection to the charge terminal T_1 can be adjusted using a tap 224 of the coil 215 as shown in FIG. 7A. The coil 215 can be energized at an operating frequency by the excitation source 212 comprising, for example, an excitation source through a tap 227 at a lower portion of the coil 215. In other implementations, the excitation source 212 can be inductively coupled to the coil 215 through a primary coil. The charge terminal T_1 can be configured to adjust its load impedance seen by the vertical feed line conductor 221, which can be used to adjust the probe impedance.

[0081] FIG. 7B shows a graphical representation of another example of a guided surface waveguide probe 200c that includes a charge terminal T_1 . As in FIG. 7A, the guided surface waveguide probe 200c can include the upper charge terminal T_1 positioned over the lossy conducting medium 203 (e.g., at height h_p). In the example of FIG. 7B, the phasing coil 215 is coupled at a first end to a ground stake (or grounding system) 218 via a lumped element tank circuit 260 and to the charge terminal T_1 at a second end via a vertical feed line conductor 221. The phasing coil 215 can be energized at an operating frequency by the excitation source 212 through, e.g., a tap 227 at a lower portion of the coil 215, as shown in FIG. 7A. In other implementations, the excitation source 212 can be inductively coupled to

the phasing coil 215 or an inductive coil 263 of a tank circuit 260 through a primary coil 269. The inductive coil 263 may also be called a “lumped element” coil as it behaves as a lumped element or inductor. In the example of FIG. 7B, the phasing coil 215 is energized by the excitation source 212 through inductive coupling with the inductive coil 263 of the lumped element tank circuit 260. The lumped element tank circuit 260 comprises the inductive coil 263 and a capacitor 266. The inductive coil 263 and/or the capacitor 266 can be fixed or variable to allow for adjustment of the tank circuit resonance, and thus the probe impedance.

[0082] FIG. 7C shows a graphical representation of another example of a guided surface waveguide probe 200d that includes a charge terminal T_1 . As in FIG. 7A, the guided surface waveguide probe 200d can include the upper charge terminal T_1 positioned over the lossy conducting medium 203 (e.g., at height h_p). The feed network 209 can comprise a plurality of phasing coils (e.g., helical coils) instead of a single phasing coil 215 as illustrated in FIGS. 7A and 7B. The plurality of phasing coils can include a combination of helical coils to provide the appropriate phase delay (e.g., $\theta_c = \theta_{ca} + \theta_{cb}$, where θ_{ca} and θ_{cb} correspond to the phase delays of coils 215a and 215b, respectively) to launch a guided surface wave. In the example of FIG. 7C, the feed network includes two phasing coils 215a and 215b connected in series with the lower coil 215b coupled to a ground stake (or grounding system) 218 via a lumped element tank circuit 260 and the upper coil 215a coupled to the charge terminal T_1 via a vertical feed line conductor 221. The phasing coils 215a and 215b can be energized at an operating frequency by the excitation source 212 through, e.g., inductive coupling via a primary coil 269 with, e.g., the upper phasing coil 215a, the lower phasing coil 215b, and/or an inductive coil 263 of the tank circuit 260. For example, as shown in FIG. 7C, the coil 215 can be energized by the excitation source 212 through inductive coupling from the primary coil 269 to the lower phasing coil 215b. Alternatively, as in the example shown in FIG. 7B, the coil 215 can be energized by the excitation source 212 through inductive coupling from the primary coil 269 to the inductive coil 263 of the lumped element tank circuit 260. The inductive coil 263 and/or the capacitor 266 of the lumped

element tank circuit 260 can be fixed or variable to allow for adjustment of the tank circuit resonance, and thus the probe impedance.

[0083] At this point, it should be pointed out that there is a distinction between phase delays for traveling waves and phase shifts for standing waves. Phase delays for traveling waves, $\theta = \beta l$, are due to propagation time delays on distributed element wave guiding structures such as, e.g., the coil(s) 215 and vertical feed line conductor 221. A phase delay is not experienced as the traveling wave passes through the lumped element tank circuit 260. As a result, the total traveling wave phase delay through, e.g., the guided surface waveguide probes 200c and 200d is still $\Phi = \theta_c + \theta_y$.

[0084] However, the position dependent phase shifts of standing waves, which comprise forward and backward propagating waves, and load dependent phase shifts depend on both the line-length propagation delay and at transitions between line sections of different characteristic impedances. It should be noted that phase shifts do occur in lumped element circuits. Phase shifts also occur at the impedance discontinuities between transmission line segments and between line segments and loads. This comes from the complex reflection coefficient, $\Gamma = |\Gamma|e^{j\phi}$, arising from the impedance discontinuities, and results in standing waves (wave interference patterns of forward and backward propagating waves) on the distributed element structures. As a result, the total standing wave phase shift of the guided surface waveguide probes 200c and 200d includes the phase shift produced by the lumped element tank circuit 260.

[0085] Accordingly, it should be noted that coils that produce both a phase delay for a traveling wave and a phase shift for standing waves can be referred to herein as “phasing coils.” The coils 215 are examples of phasing coils. It should be further noted that coils in a tank circuit, such as the lumped element tank circuit 260 as described above, act as a lumped element and an inductor, where the tank circuit produces a phase shift for standing waves without a corresponding phase delay for traveling waves. Such coils acting as lumped elements or inductors can be referred to herein as “inductor coils” or “lumped

element" coils. Inductive coil 263 is an example of such an inductor coil or lumped element coil. Such inductor coils or lumped element coils are assumed to have a uniform current distribution throughout the coil, and are electrically small relative to the wavelength of operation of the guided surface waveguide probe 200 such that they produce a negligible delay of a traveling wave.

[0086] The construction and adjustment of the guided surface waveguide probe 200 is based upon various operating conditions, such as the transmission frequency, conditions of the lossy conducting medium (e.g., soil conductivity σ and relative permittivity ϵ_r), and size of the charge terminal T₁. The index of refraction can be calculated from Equations (10) and (11) as

$$n = \sqrt{\epsilon_r - jx}, \quad (41)$$

where $x = \sigma / \omega \epsilon_0$ with $\omega = 2\pi f$. The conductivity σ and relative permittivity ϵ_r can be determined through test measurements of the lossy conducting medium 203. The complex Brewster angle ($\theta_{i,B}$) measured from the surface normal can also be determined from Equation (26) as

$$\theta_{i,B} = \arctan(\sqrt{\epsilon_r - jx}), \quad (42)$$

or measured from the surface as shown in FIG. 5A as

$$\psi_{i,B} = \frac{\pi}{2} - \theta_{i,B}. \quad (43)$$

The wave tilt at the Hankel crossover distance (W_{Rx}) can also be found using Equation (40).

[0087] The Hankel crossover distance can also be found by equating the magnitudes of Equations (20b) and (21) for $-j\gamma\rho$, and solving for R_x as illustrated by FIG. 4. The electrical effective height can then be determined from Equation (39) using the Hankel crossover distance and the complex Brewster angle as

$$h_{eff} = h_p e^{j\Phi} = R_x \tan \psi_{i,B}. \quad (44)$$

As can be seen from Equation (44), the complex effective height (h_{eff}) includes a magnitude that is associated with the physical height (h_p) of the charge terminal T₁ and a phase delay

(Φ) that is to be associated with the angle (Ψ) of the wave tilt at the Hankel crossover distance (R_x). With these variables and the selected charge terminal T_1 configuration, it is possible to determine the configuration of a guided surface waveguide probe 200.

[0088] With the charge terminal T_1 positioned at or above the physical height (h_p), the feed network 209 (FIG. 3) and/or the vertical feed line connecting the feed network to the charge terminal T_1 can be adjusted to match the phase delay (Φ) of the charge Q_1 on the charge terminal T_1 to the angle (Ψ) of the wave tilt (W). The size of the charge terminal T_1 can be chosen to provide a sufficiently large surface for the charge Q_1 imposed on the terminals. In general, it is desirable to make the charge terminal T_1 as large as practical. The size of the charge terminal T_1 should be large enough to avoid ionization of the surrounding air, which can result in electrical discharge or sparking around the charge terminal.

[0089] The phase delay θ_c of a helically-wound coil can be determined from Maxwell's equations as has been discussed by Corum, K.L. and J.F. Corum, "RF Coils, Helical Resonators and Voltage Magnification by Coherent Spatial Modes," Microwave Review, Vol. 7, No. 2, September 2001, pp. 36-45., which is incorporated herein by reference in its entirety. For a helical coil with $H/D > 1$, the ratio of the velocity of propagation (v) of a wave along the coil's longitudinal axis to the speed of light (c), or the "velocity factor," is given by

$$V_f = \frac{v}{c} = \frac{1}{\sqrt{1 + 20 \left(\frac{D}{s}\right)^{2.5} \left(\frac{D}{\lambda_o}\right)^{0.5}}}, \quad (45)$$

where H is the axial length of the solenoidal helix, D is the coil diameter, N is the number of turns of the coil, $s = H/N$ is the turn-to-turn spacing (or helix pitch) of the coil, and λ_o is the free-space wavelength. Based upon this relationship, the electrical length, or phase delay, of the helical coil is given by

$$\theta_c = \beta_p H = \frac{2\pi}{\lambda_p} H = \frac{2\pi}{V_f \lambda_o} H. \quad (46)$$

The principle is the same if the helix is wound spirally or is short and fat, but V_f and θ_c are easier to obtain by experimental measurement. The expression for the characteristic (wave) impedance of a helical transmission line has also been derived as

$$Z_c = \frac{60}{V_f} \left[\ell n \left(\frac{V_f \lambda_0}{D} \right) - 1.027 \right]. \quad (47)$$

[0090] The spatial phase delay θ_y of the structure can be determined using the traveling wave phase delay of the vertical feed line conductor 221 (FIGS. 7A-7C). The capacitance of a cylindrical vertical conductor above a prefect ground plane can be expressed as

$$C_A = \frac{2\pi\epsilon_0 h_w}{\ell n \left(\frac{h}{a} \right) - 1} \text{ Farads}, \quad (48)$$

where h_w is the vertical length (or height) of the conductor and a is the radius (in mks units). As with the helical coil, the traveling wave phase delay of the vertical feed line conductor can be given by

$$\theta_y = \beta_w h_w = \frac{2\pi}{\lambda_w} h_w = \frac{2\pi}{V_w \lambda_0} h_w, \quad (49)$$

where β_w is the propagation phase constant for the vertical feed line conductor, h_w is the vertical length (or height) of the vertical feed line conductor, V_w is the velocity factor on the wire, λ_0 is the wavelength at the supplied frequency, and λ_w is the propagation wavelength resulting from the velocity factor V_w . For a uniform cylindrical conductor, the velocity factor is a constant with $V_w \approx 0.94$, or in a range from about 0.93 to about 0.98. If the mast is considered to be a uniform transmission line, its average characteristic impedance can be approximated by

$$Z_w = \frac{60}{V_w} \left[\ell n \left(\frac{h_w}{a} \right) - 1 \right], \quad (50)$$

where $V_w \approx 0.94$ for a uniform cylindrical conductor and a is the radius of the conductor. An alternative expression that has been employed in amateur radio literature for the characteristic impedance of a single-wire feed line can be given by

$$Z_w = 138 \log \left(\frac{1.123 V_w \lambda_0}{2\pi a} \right). \quad (51)$$

Equation (51) implies that Z_w for a single-wire feeder varies with frequency. The phase delay can be determined based upon the capacitance and characteristic impedance.

[0091] With a charge terminal T_1 positioned over the lossy conducting medium 203 as shown in FIG. 3, the feed network 209 can be adjusted to excite the charge terminal T_1 with the phase delay (Φ) of the complex effective height (h_{eff}) equal to the angle (Ψ) of the wave tilt at the Hankel crossover distance, or $\Phi = \Psi$. When this condition is met, the electric field produced by the charge oscillating Q_1 on the charge terminal T_1 is coupled into a guided surface waveguide mode traveling along the surface of a lossy conducting medium 203. For example, if the Brewster angle ($\theta_{i,B}$), the phase delay (θ_y) associated with the vertical feed line conductor 221 (FIGS. 7A-7C), and the configuration of the coil(s) 215 (FIGS. 7A-7C) are known, then the position of the tap 224 (FIGS. 7A-7C) can be determined and adjusted to impose an oscillating charge Q_1 on the charge terminal T_1 with phase $\Phi = \Psi$. The position of the tap 224 may be adjusted to maximize coupling the traveling surface waves into the guided surface waveguide mode. Excess coil length beyond the position of the tap 224 can be removed to reduce the capacitive effects. The vertical wire height and/or the geometrical parameters of the helical coil may also be varied.

[0092] The coupling to the guided surface waveguide mode on the surface of the lossy conducting medium 203 can be improved and/or optimized by tuning the guided surface waveguide probe 200 for standing wave resonance with respect to a complex image plane associated with the charge Q_1 on the charge terminal T_1 . By doing this, the performance of the guided surface waveguide probe 200 can be adjusted for increased and/or maximum voltage (and thus charge Q_1) on the charge terminal T_1 . Referring back to FIG. 3, the effect of the lossy conducting medium 203 in Region 1 can be examined using image theory analysis.

[0093] Physically, an elevated charge Q_1 placed over a perfectly conducting plane attracts the free charge on the perfectly conducting plane, which then “piles up” in the region under the elevated charge Q_1 . The resulting distribution of “bound” electricity on the

perfectly conducting plane is similar to a bell-shaped curve. The superposition of the potential of the elevated charge Q_1 , plus the potential of the induced “piled up” charge beneath it, forces a zero equipotential surface for the perfectly conducting plane. The boundary value problem solution that describes the fields in the region above the perfectly conducting plane may be obtained using the classical notion of image charges, where the field from the elevated charge is superimposed with the field from a corresponding “image” charge below the perfectly conducting plane.

[0094] This analysis may also be used with respect to a lossy conducting medium 203 by assuming the presence of an effective image charge Q_1' beneath the guided surface waveguide probe 200. The effective image charge Q_1' coincides with the charge Q_1 on the charge terminal T_1 about a conducting image ground plane 130, as illustrated in FIG. 3. However, the image charge Q_1' is not merely located at some real depth and 180° out of phase with the primary source charge Q_1 on the charge terminal T_1 , as they would be in the case of a perfect conductor. Rather, the lossy conducting medium 203 (e.g., a terrestrial medium) presents a *phase shifted* image. That is to say, the image charge Q_1' is at a complex depth below the surface (or physical boundary) of the lossy conducting medium 203. For a discussion of complex image depth, reference is made to Wait, J. R., “Complex Image Theory—Revisited,” IEEE Antennas and Propagation Magazine, Vol. 33, No. 4, August 1991, pp. 27-29, which is incorporated herein by reference in its entirety.

[0095] Instead of the image charge Q_1' being at a depth that is equal to the physical height (H_1) of the charge Q_1 , the conducting image ground plane 130 (representing a perfect conductor) is located at a complex depth of $z = -d/2$ and the image charge Q_1' appears at a complex depth (*i.e.*, the “depth” has both magnitude and phase), given by $-D_1 = -(d/2 + d/2 + H_1) \neq H_1$. For vertically polarized sources over the Earth,

$$d = \frac{2\sqrt{\gamma_e^2 + k_0^2}}{\gamma_e^2} \approx \frac{2}{\gamma_e} = d_r + jd_i = |d|\angle\zeta, \quad (52)$$

where

$$\gamma_e^2 = j\omega\mu_1\sigma_1 - \omega^2\mu_1\varepsilon_1, \text{ and} \quad (53)$$

$$k_o = \omega\sqrt{\mu_o\varepsilon_o}, \quad (54)$$

as indicated in Equation (12). The complex spacing of the image charge, in turn, implies that the external field will experience *extra phase shifts* not encountered when the interface is either a dielectric or a perfect conductor. In the lossy conducting medium, the wave front normal is parallel to the tangent of the conducting image ground plane 130 at $z = -d/2$, and not at the boundary interface between Regions 1 and 2.

[0096] Consider the case illustrated in FIG. 8A where the lossy conducting medium 203 is a finitely conducting Earth 133 with a physical boundary 136. The *finitely* conducting Earth 133 may be replaced by a *perfectly* conducting image ground plane 139 as shown in FIG. 8B, which is located at a complex depth z_1 below the physical boundary 136. This equivalent representation exhibits the *same* impedance when looking down into the interface at the physical boundary 136. The equivalent representation of FIG. 8B can be modeled as an equivalent transmission line, as shown in FIG. 8C. The cross-section of the equivalent structure is represented as a (z-directed) end-loaded transmission line, with the impedance of the perfectly conducting image plane being a short circuit ($z_s = 0$). The depth z_1 can be determined by equating the TEM wave impedance looking down at the Earth to an image ground plane impedance z_{in} seen looking into the transmission line of FIG. 8C.

[0097] In the case of FIG. 8A, the propagation constant and wave intrinsic impedance in the upper region (air) 142 are

$$\gamma_o = j\omega\sqrt{\mu_o\varepsilon_o} = 0 + j\beta_o, \text{ and} \quad (55)$$

$$Z_o = \frac{j\omega\mu_o}{\gamma_o} = \sqrt{\frac{\mu_o}{\varepsilon_o}}. \quad (56)$$

In the lossy Earth 133, the propagation constant and wave intrinsic impedance are

$$\gamma_e = \sqrt{j\omega\mu_1(\sigma_1 + j\omega\varepsilon_1)}, \text{ and} \quad (57)$$

$$Z_e = \frac{j\omega\mu_1}{\gamma_e}. \quad (58)$$

For normal incidence, the equivalent representation of FIG. 8B is equivalent to a TEM transmission line whose characteristic impedance is that of air (z_o), with propagation constant of γ_o , and whose length is z_1 . As such, the image ground plane impedance Z_{in} seen at the interface for the shorted transmission line of FIG. 8C is given by

$$Z_{in} = Z_o \tanh(\gamma_o z_1). \quad (59)$$

Equating the image ground plane impedance Z_{in} associated with the equivalent model of FIG. 8C to the normal incidence wave impedance of FIG. 8A and solving for z_1 gives the distance to a short circuit (the *perfectly conducting* image ground plane 139) as

$$z_1 = \frac{1}{\gamma_o} \tanh^{-1} \left(\frac{Z_e}{Z_o} \right) = \frac{1}{\gamma_o} \tanh^{-1} \left(\frac{\gamma_o}{\gamma_e} \right) \approx \frac{1}{\gamma_e}, \quad (60)$$

where only the first term of the series expansion for the inverse hyperbolic tangent is considered for this approximation. Note that in the air region 142, the propagation constant is $\gamma_o = j\beta_o$, so $Z_{in} = jZ_o \tan \beta_o z_1$ (which is a purely imaginary quantity for a real z_1), but z_e is a complex value if $\sigma \neq 0$. Therefore, $Z_{in} = Z_e$ only when z_1 is a *complex distance*.

[0098] Since the equivalent representation of FIG. 8B includes a *perfectly conducting* image ground plane 139, the image depth for a charge or current *lying at the surface of the Earth* (physical boundary 136) is equal to distance z_1 on the other side of the image ground plane 139, or $d = 2 \times z_1$ beneath the Earth's surface (which is located at $z = 0$). Thus, the distance to the perfectly conducting image ground plane 139 can be approximated by

$$d = 2z_1 \approx \frac{2}{\gamma_e}. \quad (61)$$

Additionally, the "image charge" will be "*equal and opposite*" to the real charge, so the potential of the perfectly conducting image ground plane 139 at depth $z_1 = -d/2$ will be zero.

[0099] If a charge Q_1 is elevated a distance H_1 above the surface of the Earth as illustrated in FIG. 3, then the image charge Q_1' resides at a complex distance of $D_1 = d + H_1$ below the surface, or a complex distance of $d/2 + H_1$ below the image ground plane 130. The guided surface waveguide probes 200 of FIGS. 7A-7C can be modeled as an equivalent

single-wire transmission line image plane model that can be based upon the perfectly conducting image ground plane 139 of FIG. 8B.

[0100] FIG. 9A shows an example of the equivalent single-wire transmission line image plane model, and FIG. 9B illustrates an example of the equivalent classic transmission line model, including the shorted transmission line of FIG. 8C. FIG. 9C illustrates an example of the equivalent classic transmission line model including the lumped element tank circuit 260.

[0101] In the equivalent image plane models of FIGS. 9A-9C, $\Phi = \theta_y + \theta_c$ is the traveling wave phase delay of the guided surface waveguide probe 200 referenced to Earth 133 (or the lossy conducting medium 203), $\theta_c = \beta_p H$ is the electrical length of the coil or coils 215 (FIGS. 7A-7C), of physical length H , expressed in degrees, $\theta_y = \beta_w h_w$ is the electrical length of the vertical feed line conductor 221 (FIGS. 7A-7C), of physical length h_w , expressed in degrees. In addition, $\theta_d = \beta_o d/2$ is the phase shift between the image ground plane 139 and the physical boundary 136 of the Earth 133 (or lossy conducting medium 203). In the example of FIGS. 9A-9C, Z_w is the characteristic impedance of the elevated vertical feed line conductor 221 in ohms, Z_c is the characteristic impedance of the coil(s) 215 in ohms, and Z_o is the characteristic impedance of free space. In the example of FIG. 9C, Z_t is the characteristic impedance of the lumped element tank circuit 260 in ohms and θ_t is the corresponding phase shift at the operating frequency.

[0102] At the base of the guided surface waveguide probe 200, the impedance seen “looking up” into the structure is $Z_{\uparrow} = Z_{base}$. With a load impedance of:

$$Z_L = \frac{1}{j\omega C_T}, \quad (62)$$

where C_T is the self-capacitance of the charge terminal T_1 , the impedance seen “looking up” into the vertical feed line conductor 221 (FIGS. 7A-7C) is given by:

$$Z_2 = Z_w \frac{Z_L + Z_w \tanh(j\beta_w h_w)}{Z_w + Z_L \tanh(j\beta_w h_w)} = Z_w \frac{Z_L + Z_w \tanh(j\theta_y)}{Z_w + Z_L \tanh(j\theta_y)}, \quad (63)$$

and the impedance seen “looking up” into the coil 215 (FIGS. 7A and 7B) is given by:

$$Z_{base} = Z_c \frac{Z_2 + Z_c \tanh(j\beta_p H)}{Z_c + Z_2 \tanh(j\beta_p H)} = Z_c \frac{Z_2 + Z_c \tanh(j\theta_c)}{Z_c + Z_2 \tanh(j\theta_c)}. \quad (64)$$

Where the feed network 209 includes a plurality of coils 215 (e.g., FIG. 7C), the impedance seen at the base of each coil 215 can be sequentially determined using Equation (64). For example, the impedance seen “looking up” into the upper coil 215a of FIG. 7C is given by:

$$Z_{coil} = Z_{ca} \frac{Z_2 + Z_{ca} \tanh(j\beta_p H)}{Z_{ca} + Z_2 \tanh(j\beta_p H)} = Z_{ca} \frac{Z_2 + Z_{ca} \tanh(j\theta_{ca})}{Z_{ca} + Z_2 \tanh(j\theta_{ca})}, \quad (64.1)$$

and the impedance seen “looking up” into the lower coil 215b of FIG. 7C can be given by:

$$Z_{base} = Z_{cb} \frac{Z_{coil} + Z_{cb} \tanh(j\beta_p H)}{Z_{cb} + Z_{coil} \tanh(j\beta_p H)} = Z_{cb} \frac{Z_{coil} + Z_{cb} \tanh(j\theta_{cb})}{Z_{cb} + Z_{coil} \tanh(j\theta_{cb})}, \quad (64.2)$$

where Z_{ca} and Z_{cb} are the characteristic impedances of the upper and lower coils. This can be extended to account for additional coils 215 as needed. At the base of the guided surface waveguide probe 200, the impedance seen “looking down” into the lossy conducting medium 203 is $Z_{\downarrow} = Z_{in}$, which is given by:

$$Z_{in} = Z_o \frac{Z_s + Z_o \tanh[j\beta_o(d/2)]}{Z_o + Z_s \tanh[j\beta_o(d/2)]} = Z_o \tanh(j\theta_d), \quad (65)$$

where $Z_s = 0$.

[0103] Neglecting losses, the equivalent image plane model can be tuned to resonance when $Z_{\downarrow} + Z_{\uparrow} = 0$ at the physical boundary 136. Or, in the low loss case, $X_{\downarrow} + X_{\uparrow} = 0$ at the physical boundary 136, where X is the corresponding reactive component. Thus, the impedance at the physical boundary 136 “looking up” into the guided surface waveguide probe 200 is the conjugate of the impedance at the physical boundary 136 “looking down” into the lossy conducting medium 203. By adjusting the probe impedance via the load impedance Z_L of the charge terminal T_1 while maintaining the traveling wave phase delay Φ equal to the angle of the media’s wave tilt Ψ , so that $\Phi = \Psi$, which improves and/or maximizes coupling of the probe’s electric field to a guided surface waveguide mode along the surface of the lossy conducting medium 203 (e.g., Earth), the equivalent image plane models of FIGS. 9A and 9B can be tuned to resonance with respect to the image ground plane 139. In this way, the impedance of the equivalent complex image plane model is purely resistive, which maintains a superposed standing wave on the probe structure that

maximizes the voltage and elevated charge on terminal T_1 , and by Equations (1)-(3) and (16) maximizes the propagating surface wave.

[0104] While the load impedance Z_L of the charge terminal T_1 can be adjusted to tune the probe 200 for standing wave resonance with respect to the image ground plane 139, in some embodiments a lumped element tank circuit 260 located between the coil(s) 215 (FIGS. 7B and 7C) and the ground stake (or grounding system) 218 can be adjusted to tune the probe 200 for standing wave resonance with respect to the image ground plane 139 as illustrated in FIG. 9C. A phase delay is not experienced as the traveling wave passes through the lumped element tank circuit 260. As a result, the total traveling wave phase delay through, e.g., the guided surface waveguide probes 200c and 200d is still $\Phi = \theta_c + \theta_y$. However, it should be noted that phase shifts do occur in lumped element circuits. Phase shifts also occur at impedance discontinuities between transmission line segments and between line segments and loads. Thus, the tank circuit 260 may also be referred to as a “phase shift circuit.”

[0105] With the lumped element tank circuit 260 coupled to the base of the guided surface waveguide probe 200, the impedance seen “looking up” into the tank circuit 260 is $Z_{\uparrow} = Z_{tuning}$, which can be given by:

$$Z_{tuning} = Z_{base} - Z_t,$$

where Z_t is the characteristic impedance of the tank circuit 260 and Z_{base} is the impedance seen “looking up” into the coil(s) as given in, e.g., Equations (64) or (64.2). FIG. 9D illustrates the variation of the impedance of the lumped element tank circuit 260 with respect to operating frequency (f_o) based upon the resonant frequency (f_p) of the tank circuit 260. As shown in FIG. 9D, the impedance of the lumped element tank 260 can be inductive or capacitive depending on the tuned self-resonant frequency of the tank circuit. When operating the tank circuit 260 at a frequency below its self-resonant frequency (f_p), its terminal point impedance is inductive, and for operation above f_p the terminal point impedance is capacitive. Adjusting either the inductance 263 or the capacitance 266 of the

tank circuit 260 changes f_p and shifts the impedance curve in FIG. 9D, which affects the terminal point impedance seen at a given operating frequency f_o .

[0106] Neglecting losses, the equivalent image plane model with the tank circuit 260 can be tuned to resonance when $Z_{\downarrow} + Z_{\uparrow} = 0$ at the physical boundary 136. Or, in the low loss case, $X_{\downarrow} + X_{\uparrow} = 0$ at the physical boundary 136, where X is the corresponding reactive component. Thus, the impedance at the physical boundary 136 “looking up” into the lumped element tank circuit 260 is the conjugate of the impedance at the physical boundary 136 “looking down” into the lossy conducting medium 203. By adjusting the lumped element tank circuit 260 while maintaining the traveling wave phase delay Φ equal to the angle of the media’s wave tilt Ψ , so that $\Phi = \Psi$, the equivalent image plane models can be tuned to resonance with respect to the image ground plane 139. In this way, the impedance of the equivalent complex image plane model is purely resistive, which maintains a superposed standing wave on the probe structure that maximizes the voltage and elevated charge on terminal T_1 , and improves and/or maximizes coupling of the probe’s electric field to a guided surface waveguide mode along the surface of the lossy conducting medium 203 (e.g., earth).

[0107] It follows from the Hankel solutions, that the guided surface wave excited by the guided surface waveguide probe 200 is an outward propagating traveling wave. The source distribution along the feed network 209 between the charge terminal T_1 and the ground stake (or grounding system) 218 of the guided surface waveguide probe 200 (FIGS. 3 and 7A-7C) is actually composed of a superposition of a traveling wave plus a standing wave on the structure. With the charge terminal T_1 positioned at or above the physical height h_p , the phase delay of the traveling wave moving through the feed network 209 is matched to the angle of the wave tilt associated with the lossy conducting medium 203. This mode-matching allows the traveling wave to be launched along the lossy conducting medium 203. Once the phase delay has been established for the traveling wave, the load impedance Z_L of the charge terminal T_1 and/or the lumped element tank circuit 260 can be adjusted to bring the probe structure into standing wave resonance with respect to the image ground plane

(130 of FIG. 3 or 139 of FIG. 8), which is at a complex depth of $-d/2$. In that case, the impedance seen from the image ground plane has zero reactance and the charge on the charge terminal T_1 is maximized.

[0108] The distinction between the traveling wave phenomenon and standing wave phenomena is that (1) the phase delay of traveling waves ($\theta = \beta d$) on a section of transmission line of length d (sometimes called a “delay line”) is due to propagation time delays; whereas (2) the position-dependent phase of standing waves (which are composed of forward and backward propagating waves) depends on both the line length propagation time delay and impedance transitions at interfaces between line sections of different characteristic impedances. In addition to the phase delay that arises due to the physical length of a section of transmission line operating in sinusoidal steady-state, there is an extra reflection coefficient phase at impedance discontinuities that is due to the ratio of Z_{oa}/Z_{ob} , where Z_{oa} and Z_{ob} are the characteristic impedances of two sections of a transmission line such as, e.g., a helical coil section of characteristic impedance $Z_{oa} = Z_c$ (FIG. 9B) and a straight section of vertical feed line conductor of characteristic impedance $Z_{ob} = Z_w$ (FIG. 9B).

[0109] As a result of this phenomenon, two *relatively short* transmission line sections of widely differing characteristic impedance may be used to provide a *very large* phase shift. For example, a probe structure composed of two sections of transmission line, one of low impedance and one of high impedance, together totaling a physical length of, say, 0.05λ , may be fabricated to provide a phase shift of 90° , which is equivalent to a 0.25λ resonance. This is due to the large jump in characteristic impedances. In this way, a physically short probe structure can be electrically longer than the two physical lengths combined. This is illustrated in FIGS. 9A and 9B, where the discontinuities in the impedance ratios provide large jumps in phase. The impedance discontinuity provides a substantial phase shift where the sections are joined together.

[0110] Referring to FIG. 10, shown is a flow chart 150 illustrating an example of adjusting a guided surface waveguide probe 200 (FIGS. 3 and 7A-7C) to substantially mode-match to a guided surface waveguide mode on the surface of the lossy conducting medium, which launches a guided surface traveling wave along the surface of a lossy conducting medium 203 (FIGS. 3 and 7A-7C). Beginning with 153, the charge terminal T_1 of the guided surface waveguide probe 200 is positioned at a defined height above a lossy conducting medium 203. Utilizing the characteristics of the lossy conducting medium 203 and the operating frequency of the guided surface waveguide probe 200, the Hankel crossover distance can also be found by equating the magnitudes of Equations (20b) and (21) for $-j\gamma\rho$, and solving for R_x as illustrated by FIG. 4. The complex index of refraction (n) can be determined using Equation (41), and the complex Brewster angle ($\theta_{i,B}$) can then be determined from Equation (42). The physical height (h_p) of the charge terminal T_1 can then be determined from Equation (44). The charge terminal T_1 should be at or higher than the physical height (h_p) in order to excite the far-out component of the Hankel function. This height relationship is initially considered when launching surface waves. To reduce or minimize the bound charge on the charge terminal T_1 , the height should be at least four times the spherical diameter (or equivalent spherical diameter) of the charge terminal T_1 .

[0111] At 156, the electrical phase delay Φ of the elevated charge Q_1 on the charge terminal T_1 is matched to the complex wave tilt angle Ψ . The phase delay (θ_c) of the helical coil(s) and/or the phase delay (θ_y) of the vertical feed line conductor can be adjusted to make Φ equal to the angle (Ψ) of the wave tilt (W). Based on Equation (31), the angle (Ψ) of the wave tilt can be determined from:

$$W = \frac{E_\rho}{E_z} = \frac{1}{\tan \theta_{i,B}} = \frac{1}{n} = |W|e^{j\Psi}. \quad (66)$$

The electrical phase delay Φ can then be matched to the angle of the wave tilt. This angular (or phase) relationship is next considered when launching surface waves. For example, the electrical phase delay $\Phi = \theta_c + \theta_y$ can be adjusted by varying the geometrical parameters of the coil(s) 215 (FIGS. 7A-7C) and/or the length (or height) of the vertical feed line conductor

221 (FIGS. 7A-7C). By matching $\Phi = \Psi$, an electric field can be established at or beyond the Hankel crossover distance (R_x) with a complex Brewster angle at the boundary interface to excite the surface waveguide mode and launch a traveling wave along the lossy conducting medium 203.

[0112] Next at 159, the impedance of the charge terminal T_1 and/or the lumped element tank circuit 260 can be tuned to resonate the equivalent image plane model of the guided surface waveguide probe 200. The depth ($d/2$) of the conducting image ground plane 139 of FIG. 9A and 9B (or 130 of FIG. 3) can be determined using Equations (52), (53) and (54) and the values of the lossy conducting medium 203 (e.g., the Earth), which can be measured. Using that depth, the phase shift (θ_d) between the image ground plane 139 and the physical boundary 136 of the lossy conducting medium 203 can be determined using $\theta_d = \beta_o d/2$. The impedance (Z_{in}) as seen “looking down” into the lossy conducting medium 203 can then be determined using Equation (65). This resonance relationship can be considered to maximize the launched surface waves.

[0113] Based upon the adjusted parameters of the coil(s) 215 and the length of the vertical feed line conductor 221, the velocity factor, phase delay, and impedance of the coil(s) 215 and vertical feed line conductor 221 can be determined using Equations (45) through (51). In addition, the self-capacitance (C_T) of the charge terminal T_1 can be determined using, e.g., Equation (24). The propagation factor (β_p) of the coil(s) 215 can be determined using Equation (35) and the propagation phase constant (β_w) for the vertical feed line conductor 221 can be determined using Equation (49). Using the self-capacitance and the determined values of the coil(s) 215 and vertical feed line conductor 221, the impedance (Z_{base}) of the guided surface waveguide probe 200 as seen “looking up” into the coil(s) 215 can be determined using Equations (62), (63), (64), (64.1) and/or (64.2).

[0114] The equivalent image plane model of the guided surface waveguide probe 200 can be tuned to resonance by, e.g., adjusting the load impedance Z_L such that the reactance component X_{base} of Z_{base} cancels out the reactance component X_{in} of Z_{in} , or $X_{base} + X_{in} =$

0. Thus, the impedance at the physical boundary 136 “looking up” into the guided surface waveguide probe 200 is the conjugate of the impedance at the physical boundary 136 “looking down” into the lossy conducting medium 203. The load impedance Z_L can be adjusted by varying the capacitance (C_T) of the charge terminal T_1 without changing the electrical phase delay $\Phi = \theta_c + \theta_y$ of the charge terminal T_1 . An iterative approach may be taken to tune the load impedance Z_L for resonance of the equivalent image plane model with respect to the conducting image ground plane 139 (or 130). In this way, the coupling of the electric field to a guided surface waveguide mode along the surface of the lossy conducting medium 203 (e.g., Earth) can be improved and/or maximized.

[0115] The equivalent image plane model of the guided surface waveguide probe 200 can also be tuned to resonance by, e.g., adjusting the lumped element tank circuit 260 such that the reactance component X_{tuning} of Z_{tuning} , cancels out the reactance component X_{in} of Z_{in} , or $X_{tuning} + X_{in} = 0$. Consider the parallel resonance curve in FIG. 9D, whose terminal point impedance at some operating frequency (f_o) is given by

$$jX_T(f) = \frac{(j2\pi f L_p)(j2\pi f C_p)^{-1}}{(j2\pi f L_p) + (j2\pi f C_p)^{-1}} = j \frac{2\pi f L_p}{1 - (2\pi f L_p)^2 L_p C_p}.$$

As C_p (or L_p) is varied, the self-resonant frequency (f_p) of the parallel tank circuit 260 changes and the terminal point reactance $X_T(f_o)$ at the frequency of operation varies from inductive (+) to capacitive (−) depending on whether $f_o < f_p$ or $f_p < f_o$. By adjusting f_p , a wide range of reactance at f_o (e.g., a large inductance $L_{eq}(f_o) = X_T(f_o)/\omega$ or a small capacitance $C_{eq}(f_o) = -1/\omega X_T(f_o)$) can be seen at the terminals of the tank circuit 260.

[0116] To obtain the electrical phase delay (Φ) for coupling into the guided surface waveguide mode, the coil(s) 215 and vertical feed line conductor 221 are usually less than a quarter wavelength. For this, an inductive reactance can be added by the lumped element tank circuit 260 so that the impedance at the physical boundary 136 “looking up” into the lumped element tank circuit 260 is the conjugate of the impedance at the physical boundary 136 “looking down” into the lossy conducting medium 203.

[0117] As seen in FIG. 9D, adjusting f_p of the tank circuit 260 (FIG. 7C) above the operating frequency (f_o) can provide the needed impedance, without changing the electrical phase delay $\Phi = \theta_c + \theta_y$ of the charge terminal T_1 , to tune for resonance of the equivalent image plane model with respect to the conducting image ground plane 139 (or 130). In some cases, a capacitive reactance may be needed and can be provided by adjusting f_p of the tank circuit 260 below the operating frequency. In this way, the coupling of the electric field to a guided surface waveguide mode along the surface of the lossy conducting medium 203 (e.g., earth) can be improved and/or maximized.

[0118] This may be better understood by illustrating the situation with a numerical example. Consider a guided surface waveguide probe 200b (FIG. 7A) comprising a top-loaded vertical stub of physical height h_p with a charge terminal T_1 at the top, where the charge terminal T_1 is excited through a helical coil and vertical feed line conductor at an operational frequency (f_o) of 1.85 MHz. With a height (H_1) of 16 feet and the lossy conducting medium 203 (e.g., Earth) having a relative permittivity of $\epsilon_r = 15$ and a conductivity of $\sigma_1 = 0.010$ mhos/m, several surface wave propagation parameters can be calculated for $f_o = 1.850$ MHz. Under these conditions, the Hankel crossover distance can be found to be $R_x = 54.5$ feet with a physical height of $h_p = 5.5$ feet, which is well below the actual height of the charge terminal T_1 . While a charge terminal height of $H_1 = 5.5$ feet could have been used, the taller probe structure reduced the bound capacitance, permitting a greater percentage of free charge on the charge terminal T_1 providing greater field strength and excitation of the traveling wave.

[0119] The wave length can be determined as:

$$\lambda_o = \frac{c}{f_o} = 162.162 \text{ meters}, \quad (67)$$

where c is the speed of light. The complex index of refraction is:

$$n = \sqrt{\epsilon_r - jx} = 7.529 - j 6.546, \quad (68)$$

from Equation (41), where $x = \sigma_1/\omega\epsilon_o$ with $\omega = 2\pi f_o$, and the complex Brewster angle is:

$$\theta_{i,B} = \arctan(\sqrt{\varepsilon_r - jx}) = 85.6 - j 3.744^\circ. \quad (69)$$

from Equation (42). Using Equation (66), the wave tilt values can be determined to be:

$$W = \frac{1}{\tan \theta_{i,B}} = \frac{1}{n} = |W|e^{j\Psi} = 0.101e^{j40.614^\circ}. \quad (70)$$

Thus, the helical coil can be adjusted to match $\Phi = \Psi = 40.614^\circ$

[0120] The velocity factor of the vertical feed line conductor (approximated as a uniform cylindrical conductor with a diameter of 0.27 inches) can be given as $V_w \approx 0.93$. Since $h_p \ll \lambda_o$, the propagation phase constant for the vertical feed line conductor can be approximated as:

$$\beta_w = \frac{2\pi}{\lambda_w} = \frac{2\pi}{V_w \lambda_o} = 0.042 \text{ m}^{-1}. \quad (71)$$

From Equation (49) the phase delay of the vertical feed line conductor is:

$$\theta_y = \beta_w h_w \approx \beta_w h_p = 11.640^\circ. \quad (72)$$

By adjusting the phase delay of the helical coil so that $\theta_c = 28.974^\circ = 40.614^\circ - 11.640^\circ$, Φ will equal Ψ to match the guided surface waveguide mode. To illustrate the relationship between Φ and Ψ , FIG. 11 shows a plot of both over a range of frequencies. As both Φ and Ψ are frequency dependent, it can be seen that their respective curves cross over each other at approximately 1.85 MHz.

[0121] For a helical coil having a conductor diameter of 0.0881 inches, a coil diameter (D) of 30 inches and a turn-to-turn spacing (s) of 4 inches, the velocity factor for the coil can be determined using Equation (45) as:

$$V_f = \frac{1}{\sqrt{1 + 20\left(\frac{D}{s}\right)^{2.5} \left(\frac{D}{\lambda_o}\right)^{0.5}}} = 0.069, \quad (73)$$

and the propagation factor from Equation (35) is:

$$\beta_p = \frac{2\pi}{V_f \lambda_o} = 0.564 \text{ m}^{-1}. \quad (74)$$

With $\theta_c = 28.974^\circ$, the axial length of the solenoidal helix (H) can be determined using Equation (46) such that:

$$H = \frac{\theta_c}{\beta_p} = 35.2732 \text{ inches} . \quad (75)$$

This height determines the location on the helical coil where the vertical feed line conductor is connected, resulting in a coil with 8.818 turns ($N = H/s$).

[0122] With the traveling wave phase delay of the coil and vertical feed line conductor adjusted to match the wave tilt angle ($\Phi = \theta_c + \theta_y = \Psi$), the load impedance (Z_L) of the charge terminal T_1 can be adjusted for standing wave resonance of the equivalent image plane model of the guided surface waveguide probe 200. From the measured permittivity, conductivity and permeability of the Earth, the radial propagation constant can be determined using Equation (57)

$$\gamma_e = \sqrt{j\omega u_1(\sigma_1 + j\omega\epsilon_1)} = 0.25 + j 0.292 \text{ m}^{-1}, \quad (76)$$

and the complex depth of the conducting image ground plane can be approximated from Equation (52) as:

$$d \approx \frac{2}{\gamma_e} = 3.364 + j 3.963 \text{ meters} , \quad (77)$$

with a corresponding phase shift between the conducting image ground plane and the physical boundary of the Earth given by:

$$\theta_d = \beta_o(d/2) = 4.015 - j 4.73^\circ. \quad (78)$$

Using Equation (65), the impedance seen “looking down” into the lossy conducting medium 203 (i.e., Earth) can be determined as:

$$Z_{in} = Z_o \tanh(j\theta_d) = R_{in} + jX_{in} = 31.191 + j 26.27 \text{ ohms}. \quad (79)$$

[0123] By matching the reactive component (X_{in}) seen “looking down” into the lossy conducting medium 203 with the reactive component (X_{base}) seen “looking up” into the guided surface waveguide probe 200, the coupling into the guided surface waveguide mode may be maximized. This can be accomplished by adjusting the capacitance of the charge terminal T_1 without changing the traveling wave phase delays of the coil and vertical feed line conductor. For example, by adjusting the charge terminal capacitance (C_T) to 61.8126 pF, the load impedance from Equation (62) is:

$$Z_L = \frac{1}{j\omega C_T} = -j 1392 \text{ ohms}, \quad (80)$$

and the reactive components at the boundary are matched.

[0124] Using Equation (51), the impedance of the vertical feed line conductor (having a diameter ($2a$) of 0.27 inches) is given as

$$Z_w = 138 \log \left(\frac{1.123 V_w \lambda_0}{2\pi a} \right) = 537.534 \text{ ohms}, \quad (81)$$

and the impedance seen “looking up” into the vertical feed line conductor is given by Equation (63) as:

$$Z_2 = Z_w \frac{Z_L + Z_w \tanh(j\theta_y)}{Z_w + Z_L \tanh(j\theta_y)} = -j 835.438 \text{ ohms}. \quad (82)$$

Using Equation (47), the characteristic impedance of the helical coil is given as

$$Z_c = \frac{60}{V_f} \left[\ell n \left(\frac{V_f \lambda_0}{D} \right) - 1.027 \right] = 1446 \text{ ohms}, \quad (83)$$

and the impedance seen “looking up” into the coil at the base is given by Equation (64) as:

$$Z_{base} = Z_c \frac{Z_2 + Z_c \tanh(j\theta_c)}{Z_c + Z_2 \tanh(j\theta_c)} = -j 26.271 \text{ ohms}. \quad (84)$$

When compared to the solution of Equation (79), it can be seen that the reactive components are opposite and approximately equal, and thus are conjugates of each other. Thus, the impedance (Z_{ip}) seen “looking up” into the equivalent image plane model of FIGS. 9A and 9B from the perfectly conducting image ground plane is only resistive or $Z_{ip} = R + j0$.

[0125] When the electric fields produced by a guided surface waveguide probe 200 (FIG. 3) are established by matching the traveling wave phase delay of the feed network to the wave tilt angle and the probe structure is resonated with respect to the perfectly conducting image ground plane at complex depth $z = -d/2$, the fields are substantially mode-matched to a guided surface waveguide mode on the surface of the lossy conducting medium, a guided surface traveling wave is launched along the surface of the lossy conducting medium. As illustrated in FIG. 1, the guided field strength curve 103 of the

guided electromagnetic field has a characteristic exponential decay of $e^{-\alpha d}/\sqrt{d}$ and exhibits a distinctive knee 109 on the log-log scale.

[0126] If the reactive components of the impedance seen “looking up” into the coil and “looking down” into the lossy conducting medium are not opposite and approximately equal, then a lumped element tank circuit 260 (FIG. 7C) can be included between the coil 215 (FIG. 7A) and ground stake 218 (FIGS. 7A) (or grounding system). The self-resonant frequency of the lumped element tank circuit can then be adjusted so that the reactive components “looking up” into the tank circuit of the guided surface waveguide probe and “looking down” into the lossy conducting medium are opposite and approximately equal. Under that condition, by adjusting the impedance (Z_{ip}) seen “looking up” into the equivalent image plane model of FIG. 9C from the perfectly conducting image ground plane is only resistive or $Z_{ip} = R + j0$.

[0127] In summary, both analytically and experimentally, the *traveling wave* component on the structure of the guided surface waveguide probe 200 has a phase delay (Φ) at its upper terminal that matches the angle (Ψ) of the wave tilt of the surface traveling wave ($\Phi = \Psi$). Under this condition, the surface waveguide may be considered to be “mode-matched”. Furthermore, the resonant *standing wave* component on the structure of the guided surface waveguide probe 200 has a V_{MAX} at the charge terminal T_1 and a V_{MIN} down at the image plane 139 (FIG. 8B) where $Z_{ip} = R_{ip} + j0$ at a complex depth of $z = -d/2$, not at the connection at the physical boundary 136 of the lossy conducting medium 203 (FIG. 8B). Lastly, the charge terminal T_1 is of sufficient height H_1 of FIG. 3 ($h \geq R_x \tan \psi_{i,B}$) so that electromagnetic waves incident onto the lossy conducting medium 203 at the complex Brewster angle do so out at a distance ($\geq R_x$) where the $1/\sqrt{r}$ term is predominant. Receive circuits can be utilized with one or more guided surface waveguide probes to facilitate wireless transmission and/or power delivery systems.

[0128] Referring back to FIG. 3, operation of a guided surface waveguide probe 200 may be controlled to adjust for variations in operational conditions associated with the

guided surface waveguide probe 200. For example, an adaptive probe control system 230 can be used to control the feed network 209 and/or the charge terminal T_1 to control the operation of the guided surface waveguide probe 200. Operational conditions can include, but are not limited to, variations in the characteristics of the lossy conducting medium 203 (e.g., conductivity σ and relative permittivity ϵ_r), variations in field strength and/or variations in loading of the guided surface waveguide probe 200. As can be seen from Equations (31), (41) and (42), the index of refraction (n), the complex Brewster angle ($\theta_{i,B}$), and the wave tilt ($|W|e^{j\Psi}$) can be affected by changes in soil conductivity and permittivity resulting from, e.g., weather conditions.

[0129] Equipment such as, e.g., conductivity measurement probes, permittivity sensors, ground parameter meters, field meters, current monitors and/or load receivers can be used to monitor for changes in the operational conditions and provide information about current operational conditions to the adaptive probe control system 230. The probe control system 230 can then make one or more adjustments to the guided surface waveguide probe 200 to maintain specified operational conditions for the guided surface waveguide probe 200. For instance, as the moisture and temperature vary, the conductivity of the soil will also vary. Conductivity measurement probes and/or permittivity sensors may be located at multiple locations around the guided surface waveguide probe 200. Generally, it would be desirable to monitor the conductivity and/or permittivity at or about the Hankel crossover distance R_x for the operational frequency. Conductivity measurement probes and/or permittivity sensors may be located at multiple locations (e.g., in each quadrant) around the guided surface waveguide probe 200.

[0130] The conductivity measurement probes and/or permittivity sensors can be configured to evaluate the conductivity and/or permittivity on a periodic basis and communicate the information to the probe control system 230. The information may be communicated to the probe control system 230 through a network such as, but not limited to, a LAN, WLAN, cellular network, or other appropriate wired or wireless communication

network. Based upon the monitored conductivity and/or permittivity, the probe control system 230 may evaluate the variation in the index of refraction (n), the complex Brewster angle ($\theta_{i,B}$), and/or the wave tilt ($|W|e^{j\Psi}$) and adjust the guided surface waveguide probe 200 to maintain the phase delay (Φ) of the feed network 209 equal to the wave tilt angle (Ψ) and/or maintain resonance of the equivalent image plane model of the guided surface waveguide probe 200. This can be accomplished by adjusting, e.g., θ_y , θ_c and/or C_T . For instance, the probe control system 230 can adjust the self-capacitance of the charge terminal T_1 and/or the phase delay (θ_y , θ_c) applied to the charge terminal T_1 to maintain the electrical launching efficiency of the guided surface wave at or near its maximum. For example, the self-capacitance of the charge terminal T_1 can be varied by changing the size of the terminal. The charge distribution can also be improved by increasing the size of the charge terminal T_1 , which can reduce the chance of an electrical discharge from the charge terminal T_1 . In other embodiments, the charge terminal T_1 can include a variable inductance that can be adjusted to change the load impedance Z_L . The phase applied to the charge terminal T_1 can be adjusted by varying the tap position on the coil 215 (FIGS. 7A-7C), and/or by including a plurality of predefined taps along the coil 215 and switching between the different predefined tap locations to maximize the launching efficiency.

[0131] Field or field strength (FS) meters may also be distributed about the guided surface waveguide probe 200 to measure field strength of fields associated with the guided surface wave. The field or FS meters can be configured to detect the field strength and/or changes in the field strength (e.g., electric field strength) and communicate that information to the probe control system 230. The information may be communicated to the probe control system 230 through a network such as, but not limited to, a LAN, WLAN, cellular network, or other appropriate communication network. As the load and/or environmental conditions change or vary during operation, the guided surface waveguide probe 200 may be adjusted to maintain specified field strength(s) at the FS meter locations to ensure appropriate power transmission to the receivers and the loads they supply.

[0132] For example, the phase delay ($\Phi = \theta_y + \theta_c$) applied to the charge terminal T_1 can be adjusted to match the wave tilt angle (Ψ). By adjusting one or both phase delays, the guided surface waveguide probe 200 can be adjusted to ensure the wave tilt corresponds to the complex Brewster angle. This can be accomplished by adjusting a tap position on the coil(s) 215 (FIGS. 7A-7C) to change the phase delay supplied to the charge terminal T_1 . The voltage level supplied to the charge terminal T_1 can also be increased or decreased to adjust the electric field strength. This may be accomplished by adjusting the output voltage of the excitation source 212 or by adjusting or reconfiguring the feed network 209. For instance, the position of the tap 227 (FIG. 7A) for the excitation source 212 can be adjusted to increase the voltage seen by the charge terminal T_1 , where the excitation source 212 comprises, for example, an AC source as mentioned above. Maintaining field strength levels within predefined ranges can improve coupling by the receivers, reduce ground current losses, and avoid interference with transmissions from other guided surface waveguide probes 200.

[0133] The probe control system 230 can be implemented with hardware, firmware, software executed by hardware, or a combination thereof. For example, the probe control system 230 can include processing circuitry including a processor and a memory, both of which can be coupled to a local interface such as, for example, a data bus with an accompanying control/address bus as can be appreciated by those with ordinary skill in the art. A probe control application may be executed by the processor to adjust the operation of the guided surface waveguide probe 200 based upon monitored conditions. The probe control system 230 can also include one or more network interfaces for communicating with the various monitoring devices. Communications can be through a network such as, but not limited to, a LAN, WLAN, cellular network, or other appropriate communication network. The probe control system 230 may comprise, for example, a computer system such as a server, desktop computer, laptop, or other system with like capability.

[0134] Referring back to the example of FIG. 5A, the complex angle trigonometry is shown for the ray optic interpretation of the incident electric field (E) of the charge terminal T_1 with a complex Brewster angle ($\theta_{i,B}$) at the Hankel crossover distance (R_x). Recall that, for a lossy conducting medium, the Brewster angle is complex and specified by Equation (38). Electrically, the geometric parameters are related by the electrical effective height (h_{eff}) of the charge terminal T_1 by Equation (39). Since both the physical height (h_p) and the Hankel crossover distance (R_x) are real quantities, the angle of the desired guided surface wave tilt at the Hankel crossover distance (W_{Rx}) is equal to the phase (Φ) of the complex effective height (h_{eff}). With the charge terminal T_1 positioned at the physical height h_p and excited with a charge having the appropriate phase delay Φ , the resulting electric field is incident with the lossy conducting medium boundary interface at the Hankel crossover distance R_x , and at the Brewster angle. Under these conditions, the guided surface waveguide mode can be excited without reflection or substantially negligible reflection.

[0135] However, Equation (39) means that the physical height of the guided surface waveguide probe 200 can be relatively small. While this will excite the guided surface waveguide mode, this can result in an unduly large bound charge with little free charge. To compensate, the charge terminal T_1 can be raised to an appropriate elevation to increase the amount of free charge. As one example rule of thumb, the charge terminal T_1 can be positioned at an elevation of about 4-5 times (or more) the effective diameter of the charge terminal T_1 . FIG. 6 illustrates the effect of raising the charge terminal T_1 above the physical height (h_p) shown in FIG. 5A. The increased elevation causes the distance at which the wave tilt is incident with the lossy conductive medium to move beyond the Hankel crossover point 121 (FIG. 5A). To improve coupling in the guided surface waveguide mode, and thus provide for a greater launching efficiency of the guided surface wave, a lower compensation terminal T_2 can be used to adjust the total effective height (h_{TE}) of the charge terminal T_1 such that the wave tilt at the Hankel crossover distance is at the Brewster angle.

[0136] Referring to FIG. 12, shown is an example of a guided surface waveguide probe 200e that includes an elevated charge terminal T_1 and a lower compensation terminal T_2 that are arranged along a vertical axis z that is normal to a plane presented by the lossy conducting medium 203. In this respect, the charge terminal T_1 is placed directly above the compensation terminal T_2 although it is possible that some other arrangement of two or more charge and/or compensation terminals T_N can be used. The guided surface waveguide probe 200e is disposed above a lossy conducting medium 203 according to an embodiment of the present disclosure. The lossy conducting medium 203 makes up Region 1 with a second medium 206 that makes up Region 2 sharing a boundary interface with the lossy conducting medium 203.

[0137] The guided surface waveguide probe 200e includes a feed network 209 that couples an excitation source 212 to the charge terminal T_1 and the compensation terminal T_2 . According to various embodiments, charges Q_1 and Q_2 can be imposed on the respective charge and compensation terminals T_1 and T_2 , depending on the voltages applied to terminals T_1 and T_2 at any given instant. I_1 is the conduction current feeding the charge Q_1 on the charge terminal T_1 via the terminal lead, and I_2 is the conduction current feeding the charge Q_2 on the compensation terminal T_2 via the terminal lead.

[0138] According to the embodiment of FIG. 12, the charge terminal T_1 is positioned over the lossy conducting medium 203 at a physical height H_1 , and the compensation terminal T_2 is positioned directly below T_1 along the vertical axis z at a physical height H_2 , where H_2 is less than H_1 . The height h of the transmission structure may be calculated as $h = H_1 - H_2$. The charge terminal T_1 has an isolated (or self) capacitance C_1 , and the compensation terminal T_2 has an isolated (or self) capacitance C_2 . A mutual capacitance C_M can also exist between the terminals T_1 and T_2 depending on the distance therebetween. During operation, charges Q_1 and Q_2 are imposed on the charge terminal T_1 and the compensation terminal T_2 , respectively, depending on the voltages applied to the charge terminal T_1 and the compensation terminal T_2 at any given instant.

[0139] Referring next to FIG. 13, shown is a ray optics interpretation of the effects produced by the elevated charge Q_1 on charge terminal T_1 and compensation terminal T_2 of FIG. 12. With the charge terminal T_1 elevated to a height where the ray intersects with the lossy conductive medium at the Brewster angle at a distance greater than the Hankel crossover point 121 as illustrated by line 163, the compensation terminal T_2 can be used to adjust h_{TE} by compensating for the increased height. The effect of the compensation terminal T_2 is to reduce the electrical effective height of the guided surface waveguide probe (or effectively raise the lossy medium interface) such that the wave tilt at the Hankel crossover distance is at the Brewster angle as illustrated by line 166.

[0140] The total effective height can be written as the superposition of an upper effective height (h_{UE}) associated with the charge terminal T_1 and a lower effective height (h_{LE}) associated with the compensation terminal T_2 such that

$$h_{TE} = h_{UE} + h_{LE} = h_p e^{j(\beta h_p + \Phi_U)} + h_d e^{j(\beta h_d + \Phi_L)} = R_x \times W, \quad (85)$$

where Φ_U is the phase delay applied to the upper charge terminal T_1 , Φ_L is the phase delay applied to the lower compensation terminal T_2 , $\beta = 2\pi/\lambda_p$ is the propagation factor from Equation (35), h_p is the physical height of the charge terminal T_1 and h_d is the physical height of the compensation terminal T_2 . If extra lead lengths are taken into consideration, they can be accounted for by adding the charge terminal lead length z to the physical height h_p of the charge terminal T_1 and the compensation terminal lead length y to the physical height h_d of the compensation terminal T_2 as shown in

$$h_{TE} = (h_p + z) e^{j(\beta(h_p + z) + \Phi_U)} + (h_d + y) e^{j(\beta(h_d + y) + \Phi_L)} = R_x \times W. \quad (86)$$

The lower effective height can be used to adjust the total effective height (h_{TE}) to equal the complex effective height (h_{eff}) of FIG. 5A.

[0141] Equations (85) or (86) can be used to determine the physical height of the lower disk of the compensation terminal T_2 and the phase angles to feed the terminals in order to obtain the desired wave tilt at the Hankel crossover distance. For example, Equation (86)

can be rewritten as the phase delay applied to the charge terminal T_1 as a function of the compensation terminal height (h_d) to give

$$\Phi_U(h_d) = -\beta(h_p + z) - j \ln \left(\frac{R_x \times W - (h_d + y) e^{j(\beta h_d + \beta y + \Phi_L)}}{(h_p + z)} \right). \quad (87)$$

[0142] To determine the positioning of the compensation terminal T_2 , the relationships discussed above can be utilized. First, the total effective height (h_{TE}) is the superposition of the complex effective height (h_{UE}) of the upper charge terminal T_1 and the complex effective height (h_{LE}) of the lower compensation terminal T_2 as expressed in Equation (86). Next, the tangent of the angle of incidence can be expressed geometrically as

$$\tan \psi_E = \frac{h_{TE}}{R_x}, \quad (88)$$

which is equal to the definition of the wave tilt, W . Finally, given the desired Hankel crossover distance R_x , the h_{TE} can be adjusted to make the wave tilt of the incident ray match the complex Brewster angle at the Hankel crossover point 121. This can be accomplished by adjusting h_p , Φ_U , and/or h_d .

[0143] These concepts may be better understood when discussed in the context of an example of a guided surface waveguide probe. Referring to FIG. 14, shown is a graphical representation of an example of a guided surface waveguide probe 200f including an upper charge terminal T_1 (e.g., a sphere at height h_T) and a lower compensation terminal T_2 (e.g., a disk at height h_d) that are positioned along a vertical axis z that is substantially normal to the plane presented by the lossy conducting medium 203. During operation, charges Q_1 and Q_2 are imposed on the charge and compensation terminals T_1 and T_2 , respectively, depending on the voltages applied to the terminals T_1 and T_2 at any given instant.

[0144] An AC source can act as the excitation source 212 for the charge terminal T_1 , which is coupled to the guided surface waveguide probe 200f through a feed network 209 comprising a phasing coil 215 such as, e.g., a helical coil. The excitation source 212 can be connected across a lower portion of the coil 215 through a tap 227, as shown in FIG. 14, or can be inductively coupled to the coil 215 by way of a primary coil. The coil 215 can be

coupled to a ground stake (or grounding system) 218 at a first end and the charge terminal T_1 at a second end. In some implementations, the connection to the charge terminal T_1 can be adjusted using a tap 224 at the second end of the coil 215. The compensation terminal T_2 is positioned above and substantially parallel with the lossy conducting medium 203 (e.g., the ground or Earth), and energized through a tap 233 coupled to the coil 215. An ammeter 236 located between the coil 215 and ground stake (or grounding system) 218 can be used to provide an indication of the magnitude of the current flow (I_0) at the base of the guided surface waveguide probe. Alternatively, a current clamp may be used around the conductor coupled to the ground stake (or grounding system) 218 to obtain an indication of the magnitude of the current flow (I_0).

[0145] In the example of FIG. 14, the coil 215 is coupled to a ground stake (or grounding system) 218 at a first end and the charge terminal T_1 at a second end via a vertical feed line conductor 221. In some implementations, the connection to the charge terminal T_1 can be adjusted using a tap 224 at the second end of the coil 215 as shown in FIG. 14. The coil 215 can be energized at an operating frequency by the excitation source 212 through a tap 227 at a lower portion of the coil 215. In other implementations, the excitation source 212 can be inductively coupled to the coil 215 through a primary coil. The compensation terminal T_2 is energized through a tap 233 coupled to the coil 215. An ammeter 236 located between the coil 215 and ground stake (or grounding system) 218 can be used to provide an indication of the magnitude of the current flow at the base of the guided surface waveguide probe 200f. Alternatively, a current clamp may be used around the conductor coupled to the ground stake (or grounding system) 218 to obtain an indication of the magnitude of the current flow. The compensation terminal T_2 is positioned above and substantially parallel with the lossy conducting medium 203 (e.g., the ground).

[0146] In the example of FIG. 14, the connection to the charge terminal T_1 is located on the coil 215 above the connection point of tap 233 for the compensation terminal T_2 . Such an adjustment allows an increased voltage (and thus a higher charge Q_1) to be applied to

the upper charge terminal T_1 . In other embodiments, the connection points for the charge terminal T_1 and the compensation terminal T_2 can be reversed. It is possible to adjust the total effective height (h_{TE}) of the guided surface waveguide probe 200f to excite an electric field having a guided surface wave tilt at the Hankel crossover distance R_x . The Hankel crossover distance can also be found by equating the magnitudes of Equations (20b) and (21) for $-j\gamma\rho$, and solving for R_x as illustrated by FIG. 4. The index of refraction (n), the complex Brewster angle ($\theta_{i,B}$ and $\psi_{i,B}$), the wave tilt ($|W|e^{j\psi}$) and the complex effective height ($h_{eff} = h_p e^{j\Phi}$) can be determined as described with respect to Equations (41) – (44) above.

[0147] With the selected charge terminal T_1 configuration, a spherical diameter (or the effective spherical diameter) can be determined. For example, if the charge terminal T_1 is not configured as a sphere, then the terminal configuration may be modeled as a spherical capacitance having an effective spherical diameter. The size of the charge terminal T_1 can be chosen to provide a sufficiently large surface for the charge Q_1 imposed on the terminals. In general, it is desirable to make the charge terminal T_1 as large as practical. The size of the charge terminal T_1 should be large enough to avoid ionization of the surrounding air, which can result in electrical discharge or sparking around the charge terminal. To reduce the amount of bound charge on the charge terminal T_1 , the desired elevation to provide free charge on the charge terminal T_1 for launching a guided surface wave should be at least 4-5 times the effective spherical diameter above the lossy conductive medium (e.g., the Earth). The compensation terminal T_2 can be used to adjust the total effective height (h_{TE}) of the guided surface waveguide probe 200f to excite an electric field having a guided surface wave tilt at R_x . The compensation terminal T_2 can be positioned below the charge terminal T_1 at $h_d = h_T - h_p$, where h_T is the total physical height of the charge terminal T_1 . With the position of the compensation terminal T_2 fixed and the phase delay Φ_U applied to the upper charge terminal T_1 , the phase delay Φ_L applied to the lower compensation terminal T_2 can be determined using the relationships of Equation (86), such that:

$$\Phi_U(h_d) = -\beta(h_d + y) - j \ln \left(\frac{R_x \times W - (h_p + z)e^{j(\beta h_p + \beta z + \Phi_L)}}{(h_d + y)} \right). \quad (89)$$

In alternative embodiments, the compensation terminal T_2 can be positioned at a height h_d where $\text{Im}\{\Phi_U\} = 0$. This is graphically illustrated in FIG. 15A, which shows plots 172 and 175 of the imaginary and real parts of Φ_U , respectively. The compensation terminal T_2 is positioned at a height h_d where $\text{Im}\{\Phi_U\} = 0$, as graphically illustrated in plot 172. At this fixed height, the coil phase Φ_U can be determined from $\text{Re}\{\Phi_U\}$, as graphically illustrated in plot 175.

[0148] With the excitation source 212 coupled to the coil 215 (e.g., at the 50Ω point to maximize coupling), the position of tap 233 may be adjusted for parallel resonance of the compensation terminal T_2 with at least a portion of the coil at the frequency of operation. FIG. 15B shows a schematic diagram of the general electrical hookup of FIG. 14 in which V_1 is the voltage applied to the lower portion of the coil 215 from the excitation source 212 through tap 227, V_2 is the voltage at tap 224 that is supplied to the upper charge terminal T_1 , and V_3 is the voltage applied to the lower compensation terminal T_2 through tap 233. The resistances R_p and R_d represent the ground return resistances of the charge terminal T_1 and compensation terminal T_2 , respectively. The charge and compensation terminals T_1 and T_2 may be configured as spheres, cylinders, toroids, rings, hoods, or any other combination of capacitive structures. The size of the charge and compensation terminals T_1 and T_2 can be chosen to provide a sufficiently large surface for the charges Q_1 and Q_2 imposed on the terminals. In general, it is desirable to make the charge terminal T_1 as large as practical. The size of the charge terminal T_1 should be large enough to avoid ionization of the surrounding air, which can result in electrical discharge or sparking around the charge terminal. The self-capacitance C_p and C_d of the charge and compensation terminals T_1 and T_2 respectively, can be determined using, for example, Equation (24).

[0149] As can be seen in FIG. 15B, a resonant circuit is formed by at least a portion of the inductance of the coil 215, the self-capacitance C_d of the compensation terminal T_2 , and the ground return resistance R_d associated with the compensation terminal T_2 . The parallel

resonance can be established by adjusting the voltage V_3 applied to the compensation terminal T_2 (e.g., by adjusting a tap 233 position on the coil 215) or by adjusting the height and/or size of the compensation terminal T_2 to adjust C_d . The position of the coil tap 233 can be adjusted for parallel resonance, which will result in the ground current through the ground stake (or grounding system) 218 and through the ammeter 236 reaching a maximum point. After parallel resonance of the compensation terminal T_2 has been established, the position of the tap 227 for the excitation source 212 can be adjusted to the 50Ω point on the coil 215.

[0150] Voltage V_2 from the coil 215 can be applied to the charge terminal T_1 , and the position of tap 224 can be adjusted such that the phase delay (Φ) of the total effective height (h_{TE}) approximately equals the angle of the guided surface wave tilt (W_{Rx}) at the Hankel crossover distance (R_x). The position of the coil tap 224 can be adjusted until this operating point is reached, which results in the ground current through the ammeter 236 increasing to a maximum. At this point, the resultant fields excited by the guided surface waveguide probe 200f are substantially mode-matched to a guided surface waveguide mode on the surface of the lossy conducting medium 203, resulting in the launching of a guided surface wave along the surface of the lossy conducting medium 203. This can be verified by measuring field strength along a radial extending from the guided surface waveguide probe 200.

[0151] Resonance of the circuit including the compensation terminal T_2 may change with the attachment of the charge terminal T_1 and/or with adjustment of the voltage applied to the charge terminal T_1 through tap 224. While adjusting the compensation terminal circuit for resonance aids the subsequent adjustment of the charge terminal connection, it is not necessary to establish the guided surface wave tilt (W_{Rx}) at the Hankel crossover distance (R_x). The system may be further adjusted to improve coupling by iteratively adjusting the position of the tap 227 for the excitation source 212 to be at the 50Ω point on the coil 215 and adjusting the position of tap 233 to maximize the ground current through the ammeter 236. Resonance of the circuit including the compensation terminal T_2 may drift as the

positions of taps 227 and 233 are adjusted, or when other components are attached to the coil 215.

[0152] In other implementations, the voltage V_2 from the coil 215 can be applied to the charge terminal T_1 , and the position of tap 233 can be adjusted such that the phase delay (Φ) of the total effective height (h_{TE}) approximately equals the angle (Ψ) of the guided surface wave tilt at R_x . The position of the coil tap 224 can be adjusted until the operating point is reached, resulting in the ground current through the ammeter 236 substantially reaching a maximum. The resultant fields are substantially mode-matched to a guided surface waveguide mode on the surface of the lossy conducting medium 203, and a guided surface wave is launched along the surface of the lossy conducting medium 203. This can be verified by measuring field strength along a radial extending from the guided surface waveguide probe 200. The system may be further adjusted to improve coupling by iteratively adjusting the position of the tap 227 for the excitation source 212 to be at the 50 Ω point on the coil 215 and adjusting the position of tap 224 and/or 233 to maximize the ground current through the ammeter 236.

[0153] Referring back to FIG. 12, operation of a guided surface waveguide probe 200 may be controlled to adjust for variations in operational conditions associated with the guided surface waveguide probe 200. For example, a probe control system 230 can be used to control the feed network 209 and/or positioning of the charge terminal T_1 and/or compensation terminal T_2 to control the operation of the guided surface waveguide probe 200. Operational conditions can include, but are not limited to, variations in the characteristics of the lossy conducting medium 203 (e.g., conductivity σ and relative permittivity ϵ_r), variations in field strength and/or variations in loading of the guided surface waveguide probe 200. As can be seen from Equations (41) – (44), the index of refraction (n), the complex Brewster angle ($\theta_{i,B}$ and $\psi_{i,B}$), the wave tilt ($|W|e^{j\Psi}$) and the complex effective height ($h_{eff} = h_p e^{j\Phi}$) can be affected by changes in soil conductivity and permittivity resulting from, e.g., weather conditions.

[0154] Equipment such as, e.g., conductivity measurement probes, permittivity sensors, ground parameter meters, field meters, current monitors and/or load receivers can be used to monitor for changes in the operational conditions and provide information about current operational conditions to the probe control system 230. The probe control system 230 can then make one or more adjustments to the guided surface waveguide probe 200 to maintain specified operational conditions for the guided surface waveguide probe 200. For instance, as the moisture and temperature vary, the conductivity of the soil will also vary. Conductivity measurement probes and/or permittivity sensors may be located at multiple locations around the guided surface waveguide probe 200. Generally, it would be desirable to monitor the conductivity and/or permittivity at or about the Hankel crossover distance R_x for the operational frequency. Conductivity measurement probes and/or permittivity sensors may be located at multiple locations (e.g., in each quadrant) around the guided surface waveguide probe 200.

[0155] With reference then to FIG. 16, shown is an example of a guided surface waveguide probe 200g that includes a charge terminal T_1 and a charge terminal T_2 that are arranged along a vertical axis z . The guided surface waveguide probe 200g is disposed above a lossy conducting medium 203, which makes up Region 1. In addition, a second medium 206 shares a boundary interface with the lossy conducting medium 203 and makes up Region 2. The charge terminals T_1 and T_2 are positioned over the lossy conducting medium 203. The charge terminal T_1 is positioned at height H_1 , and the charge terminal T_2 is positioned directly below T_1 along the vertical axis z at height H_2 , where H_2 is less than H_1 . The height h of the transmission structure presented by the guided surface waveguide probe 200g is $h = H_1 - H_2$. The guided surface waveguide probe 200g includes a feed network 209 that couples an excitation source 212 such as an AC source, for example, to the charge terminals T_1 and T_2 .

[0156] The charge terminals T_1 and/or T_2 include a conductive mass that can hold an electrical charge, which may be sized to hold as much charge as practically possible. The

charge terminal T_1 has a self-capacitance C_1 , and the charge terminal T_2 has a self-capacitance C_2 , which can be determined using, for example, Equation (24). By virtue of the placement of the charge terminal T_1 directly above the charge terminal T_2 , a mutual capacitance C_M is created between the charge terminals T_1 and T_2 . Note that the charge terminals T_1 and T_2 need not be identical, but each can have a separate size and shape, and can include different conducting materials. Ultimately, the field strength of a guided surface wave launched by a guided surface waveguide probe 200g is directly proportional to the quantity of charge on the terminal T_1 . The charge Q_1 is, in turn, proportional to the self-capacitance C_1 associated with the charge terminal T_1 since $Q_1 = C_1 V$, where V is the voltage imposed on the charge terminal T_1 .

[0157] When properly adjusted to operate at a predefined operating frequency, the guided surface waveguide probe 200g generates a guided surface wave along the surface of the lossy conducting medium 203. The excitation source 212 can generate electrical energy at the predefined frequency that is applied to the guided surface waveguide probe 200g to excite the structure. When the electromagnetic fields generated by the guided surface waveguide probe 200g are substantially mode-matched with the lossy conducting medium 203, the electromagnetic fields substantially synthesize a wave front incident at a complex Brewster angle that results in little or no reflection. Thus, the surface waveguide probe 200g does not produce a radiated wave, but launches a guided surface traveling wave along the surface of a lossy conducting medium 203. The energy from the excitation source 212 can be transmitted as Zenneck surface currents to one or more receivers that are located within an effective transmission range of the guided surface waveguide probe 200g.

[0158] One can determine asymptotes of the radial Zenneck surface current $J_\rho(\rho)$ on the surface of the lossy conducting medium 203 to be $J_1(\rho)$ close-in and $J_2(\rho)$ far-out, where

$$\text{Close-in } (\rho < \lambda/8): J_\rho(\rho) \sim J_1 = \frac{I_1 + I_2}{2\pi\rho} + \frac{E_\rho^{QS}(Q_1) + E_\rho^{QS}(Q_2)}{Z_\rho}, \text{ and} \quad (90)$$

$$\text{Far-out } (\rho \gg \lambda/8): J_\rho(\rho) \sim J_2 = \frac{j\gamma\omega Q_1}{4} \times \sqrt{\frac{2\gamma}{\pi}} \times \frac{e^{-(\alpha+j\beta)\rho}}{\sqrt{\rho}}. \quad (91)$$

where I_1 is the conduction current feeding the charge Q_1 on the first charge terminal T_1 , and I_2 is the conduction current feeding the charge Q_2 on the second charge terminal T_2 . The charge Q_1 on the upper charge terminal T_1 is determined by $Q_1 = C_1 V_1$, where C_1 is the isolated capacitance of the charge terminal T_1 . Note that there is a third component to J_1 set forth above given by $(E_\rho^{Q_1})/Z_\rho$, which follows from the Leontovich boundary condition and is the radial current contribution in the lossy conducting medium 203 pumped by the quasi-static field of the elevated oscillating charge on the first charge terminal Q_1 . The quantity $Z_\rho = j\omega\mu_o/\gamma_e$ is the radial impedance of the lossy conducting medium, where $\gamma_e = (j\omega\mu_1\sigma_1 - \omega^2\mu_1\varepsilon_1)^{1/2}$.

[0159] The asymptotes representing the radial current close-in and far-out as set forth by Equations (90) and (91) are complex quantities. According to various embodiments, a physical surface current $\mathbf{J}(\rho)$ is synthesized to match as close as possible the current asymptotes in *magnitude* and *phase*. That is to say close-in, $|\mathbf{J}(\rho)|$ is to be tangent to $|J_1|$, and far-out $|\mathbf{J}(\rho)|$ is to be tangent to $|J_2|$. Also, according to the various embodiments, the phase of $\mathbf{J}(\rho)$ should transition from the phase of J_1 close-in to the phase of J_2 far-out.

[0160] In order to match the guided surface wave mode at the site of transmission to launch a guided surface wave, the phase of the surface current $|J_2|$ far-out should differ from the phase of the surface current $|J_1|$ close-in by the propagation phase corresponding to $e^{-j\beta(\rho_2 - \rho_1)}$ plus a constant of approximately 45 degrees or 225 degrees. This is because there are two roots for $\sqrt{\gamma}$, one near $\pi/4$ and one near $5\pi/4$. The properly adjusted synthetic radial surface current is

$$J_\rho(\rho, \phi, 0) = \frac{I_o \gamma}{4} H_1^{(2)}(-j\gamma\rho). \quad (92)$$

Note that this is consistent with equation (17). By Maxwell's equations, such a $\mathbf{J}(\rho)$ surface current automatically creates fields that conform to

$$H_\phi = \frac{-\gamma I_o}{4} e^{-u_2 z} H_1^{(2)}(-j\gamma\rho), \quad (93)$$

$$E_\rho = \frac{-\gamma I_o}{4} \left(\frac{u_2}{j\omega\varepsilon_o} \right) e^{-u_2 z} H_1^{(2)}(-j\gamma\rho), \text{ and} \quad (94)$$

$$E_z = \frac{-\gamma I_0}{4} \left(\frac{-\gamma}{\omega \epsilon_0} \right) e^{-u_2 z} H_0^{(2)}(-j\gamma \rho). \quad (95)$$

Thus, the difference in phase between the surface current $|J_2|$ far-out and the surface current $|J_1|$ close-in for the guided surface wave mode that is to be matched is due to the characteristics of the Hankel functions in Equations (93)-(95), which are consistent with Equations (1)-(3). It is of significance to recognize that the fields expressed by Equations (1)-(6) and (17) and Equations (92)-(95) have the nature of a *transmission line mode* bound to a lossy interface, *not radiation fields* that are associated with groundwave propagation.

[0161] In order to obtain the appropriate voltage magnitudes and phases for a given design of a guided surface waveguide probe 200g at a given location, an iterative approach may be used. Specifically, analysis may be performed of a given excitation and configuration of a guided surface waveguide probe 200g taking into account the feed currents to the terminals T_1 and T_2 , the charges on the charge terminals T_1 and T_2 , and their images in the lossy conducting medium 203 in order to determine the radial surface current density generated. This process may be performed iteratively until an optimal configuration and excitation for a given guided surface waveguide probe 200g is determined based on desired parameters. To aid in determining whether a given guided surface waveguide probe 200g is operating at an optimal level, a guided field strength curve 103 (FIG. 1) may be generated using Equations (1)-(12) based on values for the conductivity of Region 1 (σ_1) and the permittivity of Region 1 (ϵ_1) at the location of the guided surface waveguide probe 200g. Such a guided field strength curve 103 can provide a benchmark for operation such that measured field strengths can be compared with the magnitudes indicated by the guided field strength curve 103 to determine if optimal transmission has been achieved.

[0162] In order to arrive at an optimized condition, various parameters associated with the guided surface waveguide probe 200g may be adjusted. One parameter that may be varied to adjust the guided surface waveguide probe 200g is the height of one or both of the charge terminals T_1 and/or T_2 relative to the surface of the lossy conducting medium 203. In addition, the distance or spacing between the charge terminals T_1 and T_2 may also be

adjusted. In doing so, one may minimize or otherwise alter the mutual capacitance C_M or any bound capacitances between the charge terminals T_1 and T_2 and the lossy conducting medium 203 as can be appreciated. The size of the respective charge terminals T_1 and/or T_2 can also be adjusted. By changing the size of the charge terminals T_1 and/or T_2 , one will alter the respective self-capacitances C_1 and/or C_2 , and the mutual capacitance C_M as can be appreciated.

[0163] Still further, another parameter that can be adjusted is the feed network 209 associated with the guided surface waveguide probe 200g. This may be accomplished by adjusting the size of the inductive and/or capacitive reactances that make up the feed network 209. For example, where such inductive reactances comprise coils, the number of turns on such coils may be adjusted. Ultimately, the adjustments to the feed network 209 can be made to alter the electrical length of the feed network 209, thereby affecting the voltage magnitudes and phases on the charge terminals T_1 and T_2 .

[0164] Note that the iterations of transmission performed by making the various adjustments may be implemented by using computer models or by adjusting physical structures as can be appreciated. By making the above adjustments, one can create corresponding “close-in” surface current J_1 and “far-out” surface current J_2 that approximate the same currents $J(\rho)$ of the guided surface wave mode specified in Equations (90) and (91) set forth above. In doing so, the resulting electromagnetic fields would be substantially or approximately mode-matched to a guided surface wave mode on the surface of the lossy conducting medium 203.

[0165] While not shown in the example of FIG. 16, operation of the guided surface waveguide probe 200g may be controlled to adjust for variations in operational conditions associated with the guided surface waveguide probe 200. For example, a probe control system 230 shown in FIG. 12 can be used to control the feed network 209 and/or positioning and/or size of the charge terminals T_1 and/or T_2 to control the operation of the guided surface waveguide probe 200g. Operational conditions can include, but are not limited to,

variations in the characteristics of the lossy conducting medium 203 (e.g., conductivity σ and relative permittivity ϵ_r), variations in field strength and/or variations in loading of the guided surface waveguide probe 200g.

[0166] Referring now to FIG. 17, shown is an example of the guided surface waveguide probe 200g of FIG. 16, denoted herein as guided surface waveguide probe 200h. The guided surface waveguide probe 200h includes the charge terminals T_1 and T_2 that are positioned along a vertical axis z that is substantially normal to the plane presented by the lossy conducting medium 203 (e.g., the Earth). The second medium 206 is above the lossy conducting medium 203. The charge terminal T_1 has a self-capacitance C_1 , and the charge terminal T_2 has a self-capacitance C_2 . During operation, charges Q_1 and Q_2 are imposed on the charge terminals T_1 and T_2 , respectively, depending on the voltages applied to the charge terminals T_1 and T_2 at any given instant. A mutual capacitance C_M may exist between the charge terminals T_1 and T_2 depending on the distance therebetween. In addition, bound capacitances may exist between the respective charge terminals T_1 and T_2 and the lossy conducting medium 203 depending on the heights of the respective charge terminals T_1 and T_2 with respect to the lossy conducting medium 203.

[0167] The guided surface waveguide probe 200h includes a feed network 209 that comprises an inductive impedance comprising a coil L_{1a} having a pair of leads that are coupled to respective ones of the charge terminals T_1 and T_2 . In one embodiment, the coil L_{1a} is specified to have an electrical length that is one-half ($1/2$) of the wavelength at the operating frequency of the guided surface waveguide probe 200h.

[0168] While the electrical length of the coil L_{1a} is specified as approximately one-half ($1/2$) the wavelength at the operating frequency, it is understood that the coil L_{1a} may be specified with an electrical length at other values. According to one embodiment, the fact that the coil L_{1a} has an electrical length of approximately one-half ($1/2$) the wavelength at the operating frequency provides for an advantage in that a maximum voltage differential is created on the charge terminals T_1 and T_2 . Nonetheless, the length or diameter of the coil

L_{1a} may be increased or decreased when adjusting the guided surface waveguide probe 200h to obtain optimal excitation of a guided surface wave mode. Adjustment of the coil length may be provided by taps located at one or both ends of the coil. In other embodiments, it may be the case that the inductive impedance is specified to have an electrical length that is significantly less than or greater than one-half ($1/2$) the wavelength at the operating frequency of the guided surface waveguide probe 200h.

[0169] The excitation source 212 can be coupled to the feed network 209 by way of magnetic coupling. Specifically, the excitation source 212 is coupled to a coil L_P that is inductively coupled to the coil L_{1a} . This may be done by link coupling, a tapped coil, a variable reactance, or other coupling approach as can be appreciated. To this end, the coil L_P acts as a primary, and the coil L_{1a} acts as a secondary as can be appreciated.

[0170] In order to adjust the guided surface waveguide probe 200h for the transmission of a desired guided surface wave, the heights of the respective charge terminals T_1 and T_2 may be altered with respect to the lossy conducting medium 203 and with respect to each other. Also, the sizes of the charge terminals T_1 and T_2 may be altered. In addition, the size of the coil L_{1a} may be altered by adding or eliminating turns or by changing some other dimension of the coil L_{1a} . The coil L_{1a} can also include one or more taps for adjusting the electrical length as shown in FIG. 17. The position of a tap connected to either charge terminal T_1 or T_2 can also be adjusted.

[0171] Referring next to FIGS. 18A, 18B, 18C and 19, shown are examples of generalized receive circuits for using the surface-guided waves in wireless power delivery systems. FIG. 18A depict a linear probe 303, and FIGS. 18B and 18C depict tuned resonators 306a and 306b, respectively. FIG. 19 is a magnetic coil 309 according to various embodiments of the present disclosure. According to various embodiments, each one of the linear probe 303, the tuned resonators 306a/b, and the magnetic coil 309 may be employed to receive power transmitted in the form of a guided surface wave on the surface of a lossy

conducting medium 203 according to various embodiments. As mentioned above, in one embodiment the lossy conducting medium 203 comprises a terrestrial medium (or Earth).

[0172] With specific reference to FIG. 18A, the open-circuit terminal voltage at the output terminals 312 of the linear probe 303 depends upon the effective height of the linear probe 303. To this end, the terminal point voltage may be calculated as

$$V_T = \int_0^{h_e} E_{inc} \cdot dl, \quad (96)$$

where E_{inc} is the strength of the incident electric field induced on the linear probe 303 in Volts per meter, dl is an element of integration along the direction of the linear probe 303, and h_e is the effective height of the linear probe 303. An electrical load 315 is coupled to the output terminals 312 through an impedance matching network 318.

[0173] When the linear probe 303 is subjected to a guided surface wave as described above, a voltage is developed across the output terminals 312 that may be applied to the electrical load 315 through a conjugate impedance matching network 318 as the case may be. In order to facilitate the flow of power to the electrical load 315, the electrical load 315 should be substantially impedance matched to the linear probe 303 as will be described below.

[0174] Referring to FIG. 18B, a ground current excited coil L_R possessing a phase delay equal to the wave tilt of the guided surface wave includes a charge terminal T_R that is elevated (or suspended) above the lossy conducting medium 203. The charge terminal T_R has a self-capacitance C_R . In addition, there may also be a bound capacitance (not shown) between the charge terminal T_R and the lossy conducting medium 203 depending on the height of the charge terminal T_R above the lossy conducting medium 203. The bound capacitance should preferably be minimized as much as is practicable, although this may not be entirely necessary in every instance.

[0175] The tuned resonator 306a also includes a receiver network comprising a coil L_R having a phase delay Φ . One end of the coil L_R is coupled to the charge terminal T_R , and the other end of the coil L_R is coupled to the lossy conducting medium 203. The receiver

network can include a vertical supply line conductor that couples the coil L_R to the charge terminal T_R . To this end, the coil L_R (which may also be referred to as tuned resonator L_R - C_R) comprises a series-adjusted resonator as the charge terminal C_R and the coil L_R are situated in series. The phase delay of the coil L_R can be adjusted by changing the size and/or height of the charge terminal T_R , and/or adjusting the size of the coil L_R so that the phase delay Φ of the structure is made substantially equal to the angle of the wave tilt Ψ . The phase delay of the vertical supply line can also be adjusted by, e.g., changing length of the conductor.

[0176] For example, the reactance presented by the self-capacitance C_R is calculated as $1/j\omega C_R$. Note that the total capacitance of the tuned resonator 306a may also include capacitance between the charge terminal T_R and the lossy conducting medium 203, where the total capacitance of the tuned resonator 306a may be calculated from both the self-capacitance C_R and any bound capacitance as can be appreciated. According to one embodiment, the charge terminal T_R may be raised to a height so as to substantially reduce or eliminate any bound capacitance. The existence of a bound capacitance may be determined from capacitance measurements between the charge terminal T_R and the lossy conducting medium 203 as previously discussed.

[0177] The inductive reactance presented by a discrete-element coil L_R may be calculated as $j\omega L$, where L is the lumped-element inductance of the coil L_R . If the coil L_R is a distributed element, its equivalent terminal-point inductive reactance may be determined by conventional approaches. To tune the tuned resonator 306a, one would make adjustments so that the phase delay is equal to the wave tilt for the purpose of mode-matching to the surface waveguide at the frequency of operation. Under this condition, the receiving structure may be considered to be “mode-matched” with the surface waveguide. A transformer link around the structure and/or an impedance matching network 324 may be inserted between the probe and the electrical load 327 in order to couple power to the load. Inserting the impedance matching network 324 between the probe terminals 321 and the

electrical load 327 can effect a conjugate-match condition for maximum power transfer to the electrical load 327.

[0178] When placed in the presence of surface currents at the operating frequencies power will be delivered from the surface guided wave to the electrical load 327. To this end, an electrical load 327 may be coupled to the tuned resonator 306a by way of magnetic coupling, capacitive coupling, or conductive (direct tap) coupling. The elements of the coupling network may be lumped components or distributed elements as can be appreciated.

[0179] In the embodiment shown in FIG. 18B, magnetic coupling is employed where a coil L_S is positioned as a secondary relative to the coil L_R that acts as a transformer primary. The coil L_S may be link-coupled to the coil L_R by geometrically winding it around the same core structure and adjusting the coupled magnetic flux as can be appreciated. In addition, while the tuned resonator 306a comprises a series-tuned resonator, a parallel-tuned resonator or even a distributed-element resonator of the appropriate phase delay may also be used.

[0180] While a receiving structure immersed in an electromagnetic field may couple energy from the field, it can be appreciated that polarization-matched structures work best by maximizing the coupling, and conventional rules for probe-coupling to waveguide modes should be observed. For example, a TE_{20} (transverse electric mode) waveguide probe may be optimal for extracting energy from a conventional waveguide excited in the TE_{20} mode. Similarly, in these cases, a mode-matched and phase-matched receiving structure can be optimized for coupling power from a surface-guided wave. The guided surface wave excited by a guided surface waveguide probe 200 on the surface of the lossy conducting medium 203 can be considered a waveguide mode of an open waveguide. Excluding waveguide losses, the source energy can be completely recovered. Useful receiving structures may be E-field coupled, H-field coupled, or surface-current excited.

[0181] The receiving structure can be adjusted to increase or maximize coupling with the guided surface wave based upon the local characteristics of the lossy conducting medium 203 in the vicinity of the receiving structure. To accomplish this, the phase delay (Φ) of the receiving structure can be adjusted to match the angle (Ψ) of the wave tilt of the surface traveling wave at the receiving structure. If configured appropriately, the receiving structure may then be tuned for resonance with respect to the perfectly conducting image ground plane at complex depth $z = -d/2$.

[0182] For example, consider a receiving structure comprising the tuned resonator 306a of FIG. 18B, including a coil L_R and a vertical supply line connected between the coil L_R and a charge terminal T_R . With the charge terminal T_R positioned at a defined height above the lossy conducting medium 203, the total phase delay Φ of the coil L_R and vertical supply line can be matched with the angle (Ψ) of the wave tilt at the location of the tuned resonator 306a. From Equation (22), it can be seen that the wave tilt asymptotically passes to

$$W = |W|e^{j\Psi} = \frac{E_\rho}{E_z} \xrightarrow{\rho \rightarrow \infty} \frac{1}{\sqrt{\epsilon_r - j\frac{\sigma_1}{\omega\epsilon_0}}}, \quad (97)$$

where ϵ_r comprises the relative permittivity and σ_1 is the conductivity of the lossy conducting medium 203 at the location of the receiving structure, ϵ_0 is the permittivity of free space, and $\omega = 2\pi f$, where f is the frequency of excitation. Thus, the wave tilt angle (Ψ) can be determined from Equation (97).

[0183] The total phase delay ($\Phi = \theta_c + \theta_y$) of the tuned resonator 306a includes both the phase delay (θ_c) through the coil L_R and the phase delay of the vertical supply line (θ_y). The spatial phase delay along the conductor length l_w of the vertical supply line can be given by $\theta_y = \beta_w l_w$, where β_w is the propagation phase constant for the vertical supply line conductor. The phase delay due to the coil (or helical delay line) is $\theta_c = \beta_p l_c$, with a physical length of l_c and a propagation factor of

$$\beta_p = \frac{2\pi}{\lambda_p} = \frac{2\pi}{v_f \lambda_0}, \quad (98)$$

where V_f is the velocity factor on the structure, λ_0 is the wavelength at the supplied frequency, and λ_p is the propagation wavelength resulting from the velocity factor V_f . One or both of the phase delays ($\theta_c + \theta_y$) can be adjusted to match the phase delay Φ to the angle (Ψ) of the wave tilt. For example, a tap position may be adjusted on the coil L_R of FIG. 18B to adjust the coil phase delay (θ_c) to match the total phase delay to the wave tilt angle ($\Phi = \Psi$). For example, a portion of the coil can be bypassed by the tap connection as illustrated in FIG. 18B. The vertical supply line conductor can also be connected to the coil L_R via a tap, whose position on the coil may be adjusted to match the total phase delay to the angle of the wave tilt.

[0184] Once the phase delay (Φ) of the tuned resonator 306a has been adjusted, the impedance of the charge terminal T_R can then be adjusted to tune to resonance with respect to the perfectly conducting image ground plane at complex depth $z = -d/2$. This can be accomplished by adjusting the capacitance of the charge terminal T_1 without changing the traveling wave phase delays of the coil L_R and vertical supply line. In some embodiments, a lumped element tuning circuit can be included between the lossy conducting medium 203 and the coil L_R to allow for resonant tuning of the tuned resonator 306a with respect to the complex image plane as discussed above with respect to the guided surface waveguide probe 200. The adjustments are similar to those described with respect to FIGS. 9A-9C.

[0185] The impedance seen “looking down” into the lossy conducting medium 203 to the complex image plane is given by:

$$Z_{in} = R_{in} + jX_{in} = Z_o \tanh(j\beta_o(d/2)), \quad (99)$$

where $\beta_o = \omega\sqrt{\mu_o\epsilon_o}$. For vertically polarized sources over the Earth, the depth of the complex image plane can be given by:

$$d/2 \approx 1/\sqrt{j\omega\mu_1\sigma_1 - \omega^2\mu_1\epsilon_1}, \quad (100)$$

where μ_1 is the permeability of the lossy conducting medium 203 and $\epsilon_1 = \epsilon_r\epsilon_o$.

[0186] At the base of the tuned resonator 306a, the impedance seen “looking up” into the receiving structure is $Z_{\uparrow} = Z_{base}$ as illustrated in FIG. 9A or $Z_{\uparrow} = Z_{tuning}$ as illustrated in FIG. 9C. With a terminal impedance of:

$$Z_R = \frac{1}{j\omega C_R}, \quad (101)$$

where C_R is the self-capacitance of the charge terminal T_R , the impedance seen “looking up” into the vertical supply line conductor of the tuned resonator 306a is given by:

$$Z_2 = Z_W \frac{Z_R + Z_W \tanh(j\beta_W h_W)}{Z_W + Z_R \tanh(j\beta_W h_W)} = Z_W \frac{Z_R + Z_W \tanh(j\theta_y)}{Z_W + Z_R \tanh(j\theta_y)}, \quad (102)$$

and the impedance seen “looking up” into the coil L_R of the tuned resonator 306a is given by:

$$Z_{base} = R_{base} + jX_{base} = Z_R \frac{Z_2 + Z_R \tanh(j\beta_P H)}{Z_R + Z_2 \tanh(j\beta_P H)} = Z_c \frac{Z_2 + Z_R \tanh(j\theta_c)}{Z_R + Z_2 \tanh(j\theta_c)}. \quad (103)$$

By matching the reactive component (X_{in}) seen “looking down” into the lossy conducting medium 203 with the reactive component (X_{base}) seen “looking up” into the tuned resonator 306a, the coupling into the guided surface waveguide mode may be maximized.

[0187] Where a lumped element tank circuit is included at the base of the tuned resonator 306a, the self-resonant frequency of the tank circuit can be tuned to add positive or negative impedance to bring the tuned resonator 306b into standing wave resonance by matching the reactive component (X_{in}) seen “looking down” into the lossy conducting medium 203 with the reactive component (X_{tuning}) seen “looking up” into the lumped element tank circuit.

[0188] Referring next to FIG. 18C, shown is an example of a tuned resonator 306b that does not include a charge terminal T_R at the top of the receiving structure. In this embodiment, the tuned resonator 306b does not include a vertical supply line coupled between the coil L_R and the charge terminal T_R . Thus, the total phase delay (Φ) of the tuned resonator 306b includes only the phase delay (θ_c) through the coil L_R . As with the tuned resonator 306a of FIG. 18B, the coil phase delay θ_c can be adjusted to match the angle (Ψ) of the wave tilt determined from Equation (97), which results in $\Phi = \Psi$. While power extraction is possible with the receiving structure coupled into the surface waveguide mode,

it is difficult to adjust the receiving structure to maximize coupling with the guided surface wave without the variable reactive load provided by the charge terminal T_R . Including a lumped element tank circuit at the base of the tuned resonator 306b provides a convenient way to bring the tuned resonator 306b into standing wave resonance with respect to the complex image plane.

[0189] Referring to FIG. 18D, shown is a flow chart 180 illustrating an example of adjusting a receiving structure to substantially mode-match to a guided surface waveguide mode on the surface of the lossy conducting medium 203. Beginning with 181, if the receiving structure includes a charge terminal T_R (e.g., of the tuned resonator 306a of FIG. 18B), then the charge terminal T_R is positioned at a defined height above a lossy conducting medium 203 at 184. As the surface guided wave has been established by a guided surface waveguide probe 200, the physical height (h_p) of the charge terminal T_R may be below that of the effective height. The physical height may be selected to reduce or minimize the bound charge on the charge terminal T_R (e.g., four times the spherical diameter of the charge terminal). If the receiving structure does not include a charge terminal T_R (e.g., of the tuned resonator 306b of FIG. 18C), then the flow proceeds to 187.

[0190] At 187, the electrical phase delay Φ of the receiving structure is matched to the complex wave tilt angle Ψ defined by the local characteristics of the lossy conducting medium 203. The phase delay (θ_c) of the helical coil and/or the phase delay (θ_y) of the vertical supply line can be adjusted to make Φ equal to the angle (Ψ) of the wave tilt (W). The angle (Ψ) of the wave tilt can be determined from Equation (86). The electrical phase delay Φ can then be matched to the angle of the wave tilt. For example, the electrical phase delay $\Phi = \theta_c + \theta_y$ can be adjusted by varying the geometrical parameters of the coil L_R and/or the length (or height) of the vertical supply line conductor.

[0191] Next at 190, the resonator impedance can be tuned via the load impedance of the charge terminal T_R and/or the impedance of a lumped element tank circuit to resonate the equivalent image plane model of the tuned resonator 306a. The depth ($d/2$) of the

conducting image ground plane 139 (FIGS. 9A-9C) below the receiving structure can be determined using Equation (100) and the values of the lossy conducting medium 203 (e.g., the Earth) at the receiving structure, which can be locally measured. Using that complex depth, the phase shift (θ_d) between the image ground plane 139 and the physical boundary 136 (FIGS. 9A-9C) of the lossy conducting medium 203 can be determined using $\theta_d = \beta_o d/2$. The impedance (Z_{in}) as seen “looking down” into the lossy conducting medium 203 can then be determined using Equation (99). This resonance relationship can be considered to maximize coupling with the guided surface waves.

[0192] Based upon the adjusted parameters of the coil L_R and the length of the vertical supply line conductor, the velocity factor, phase delay, and impedance of the coil L_R and vertical supply line can be determined. In addition, the self-capacitance (C_R) of the charge terminal T_R can be determined using, e.g., Equation (24). The propagation factor (β_p) of the coil L_R can be determined using Equation (98), and the propagation phase constant (β_w) for the vertical supply line can be determined using Equation (49). Using the self-capacitance and the determined values of the coil L_R and vertical supply line, the impedance (Z_{base}) of the tuned resonator 306 as seen “looking up” into the coil L_R can be determined using Equations (101), (102), and (103).

[0193] The equivalent image plane model of FIGS. 9A-9C also apply to the tuned resonator 306a of FIG. 18B. The tuned resonator 306a can be tuned to resonance with respect to the complex image plane by adjusting the load impedance Z_R of the charge terminal T_R such that the reactance component X_{base} of Z_{base} cancels out the reactance component of X_{in} of Z_{in} , or $X_{base} + X_{in} = 0$. Where the tuned resonator 306 of FIGS. 18B and 18C includes a lumped element tank circuit, the self-resonant frequency of the parallel circuit can be adjusted such that the reactance component X_{tuning} of Z_{tuning} cancels out the reactance component of X_{in} of Z_{in} , or $X_{tuning} + X_{in} = 0$. Thus, the impedance at the physical boundary 136 (FIG. 9A) “looking up” into the coil of the tuned resonator 306 is the conjugate of the impedance at the physical boundary 136 “looking down” into the lossy

conducting medium 203. The load impedance Z_R can be adjusted by varying the capacitance (C_R) of the charge terminal T_R without changing the electrical phase delay $\Phi = \theta_c + \theta_y$ seen by the charge terminal T_R . The impedance of the lumped element tank circuit can be adjusted by varying the self-resonant frequency (f_p) as described with respect to FIG. 9D. An iterative approach may be taken to tune the resonator impedance for resonance of the equivalent image plane model with respect to the conducting image ground plane 139. In this way, the coupling of the electric field to a guided surface waveguide mode along the surface of the lossy conducting medium 203 (e.g., Earth) can be improved and/or maximized.

[0194] Referring to FIG. 19, the magnetic coil 309 comprises a receive circuit that is coupled through an impedance matching network 333 to an electrical load 336. In order to facilitate reception and/or extraction of electrical power from a guided surface wave, the magnetic coil 309 may be positioned so that the magnetic flux of the guided surface wave, H_ϕ , passes through the magnetic coil 309, thereby inducing a current in the magnetic coil 309 and producing a terminal point voltage at its output terminals 330. The magnetic flux of the guided surface wave coupled to a single turn coil is expressed by

$$\mathcal{F} = \iint_{A_{CS}} \mu_r \mu_o \vec{H} \cdot \hat{n} dA, \quad (104)$$

where $\mathcal{F}$ is the coupled magnetic flux, μ_r is the effective relative permeability of the core of the magnetic coil 309, μ_o is the permeability of free space, $\vec{H}$ is the incident magnetic field strength vector, $\hat{n}$ is a unit vector normal to the cross-sectional area of the turns, and A_{CS} is the area enclosed by each loop. For an N-turn magnetic coil 309 oriented for maximum coupling to an incident magnetic field that is uniform over the cross-sectional area of the magnetic coil 309, the open-circuit induced voltage appearing at the output terminals 330 of the magnetic coil 309 is

$$V = -N \frac{d\mathcal{F}}{dt} \approx -j\omega \mu_r \mu_o N H A_{CS}, \quad (105)$$

where the variables are defined above. The magnetic coil 309 may be tuned to the guided surface wave frequency either as a distributed resonator or with an external capacitor across its output terminals 330, as the case may be, and then impedance-matched to an external electrical load 336 through a conjugate impedance matching network 333.

[0195] Assuming that the resulting circuit presented by the magnetic coil 309 and the electrical load 336 are properly adjusted and conjugate impedance matched, via impedance matching network 333, then the current induced in the magnetic coil 309 may be employed to optimally power the electrical load 336. The receive circuit presented by the magnetic coil 309 provides an advantage in that it does not have to be physically connected to the ground.

[0196] With reference to FIGS. 18A, 18B, 18C and 19, the receive circuits presented by the linear probe 303, the tuned resonator 306, and the magnetic coil 309 each facilitate receiving electrical power transmitted from any one of the embodiments of guided surface waveguide probes 200 described above. To this end, the energy received may be used to supply power to an electrical load 315/327/336 via a conjugate matching network as can be appreciated. This contrasts with the signals that may be received in a receiver that were transmitted in the form of a *radiated* electromagnetic field. Such signals have very low available power, and receivers of such signals do not load the transmitters.

[0197] It is also characteristic of the present guided surface waves generated using the guided surface waveguide probes 200 described above that the receive circuits presented by the linear probe 303, the tuned resonator 306, and the magnetic coil 309 will load the excitation source 212 (e.g., FIGS. 3, 12 and 16) that is applied to the guided surface waveguide probe 200, thereby generating the guided surface wave to which such receive circuits are subjected. This reflects the fact that the guided surface wave generated by a given guided surface waveguide probe 200 described above comprises a transmission line mode. By way of contrast, a power source that drives a radiating antenna that generates a radiated electromagnetic wave is not loaded by the receivers, regardless of the number of receivers employed.

[0198] Thus, together one or more guided surface waveguide probes 200 and one or more receive circuits in the form of the linear probe 303, the tuned resonator 306a/b, and/or the magnetic coil 309 can make up a wireless distribution system. Given that the distance of transmission of a guided surface wave using a guided surface waveguide probe 200 as set forth above depends upon the frequency, it is possible that wireless power distribution can be achieved across wide areas and even globally.

[0199] The conventional wireless-power transmission/distribution systems extensively investigated today include “energy harvesting” from radiation fields and also sensor coupling to inductive or reactive near-fields. In contrast, the present wireless-power system does not waste power in the form of radiation which, if not intercepted, is lost forever. Nor is the presently disclosed wireless-power system limited to extremely short ranges as with conventional mutual-reactance coupled near-field systems. The wireless-power system disclosed herein probe-couples to the novel surface-guided transmission line mode, which is equivalent to delivering power to a load by a wave-guide or a load directly wired to the distant power generator. Not counting the power required to maintain transmission field strength plus that dissipated in the surface waveguide, which at extremely low frequencies is insignificant relative to the transmission losses in conventional high-tension power lines at 60 Hz, all of the generator power goes only to the desired electrical load. When the electrical load demand is terminated, the source power generation is relatively idle.

[0200] FIG. 20 illustrates a cross sectional view of an example guided surface waveguide probe site 2100 including a boundary or propagation interface 2102 between the lossy conducting medium 203 and the second medium 206, and a probe 2110. The illustration of the guided surface waveguide probe site 2100 is provided as a representative example and is not drawn to scale. Other probe sites consistent with the concepts described herein can include additional probes similar to the probe 2110, various guided surface wave receive structures, and other equipment.

[0201] The probe 2110 may be embodied as any of the guided surface waveguide probes 200a, 200b, 200c, 200d, 200e, 200f, 200g or 200h described herein, or variations thereof. At the guided surface waveguide probe site 2100, the probe 2110 is configured to launch a guided surface wave (or waves) along the interface 2102 between the lossy conducting medium 203 and the second medium 206. Consistent with the concepts described above, the probe 2110 is configured to provide a phase delay that matches a wave tilt angle associated with a complex Brewster angle of incidence associated with the lossy conducting medium 203 in the vicinity of the probe 2110. Thus, the probe 2110 is configured to launch a guided surface wave along the propagation interface 2102 by generating an electric field having a predetermined complex wave tilt angle at or beyond a crossover distance R_x from the guided surface waveguide probe. To achieve the desired complex wave tilt angle at the crossover distance R_x , the probe 2110 can be embodied having certain structural and electrical characteristics, consistent with the description provided above. In one embodiment, for example, the probe 2110 can include a charge terminal elevated at a height over a lossy conducting medium 203, a ground stake or grounding system, and a feed network coupled between the charge terminal and the ground stake or grounding system.

[0202] In FIG. 20, the lossy conducting medium 203 may include any lossy conducting medium, such as the Earth, for example, and the second medium 206 may include the atmosphere of the Earth. It should be appreciated that the conductivity σ_1 and permittivity ϵ_1 of the lossy conducting medium 203 at the site 2100 depends upon various factors, such as the geographic location of the site 2100, the surrounding land geography (e.g., hills, mountains, rock formations, lakes, rivers, *etc.*) at the site 2100, the surrounding phytogeography (e.g., trees, plants, *etc.*) at the site 2100, the current temperature of at the site 2100, the relative humidity at the site 2100, the water content of the lossy conducting medium 203 at the site 2100, *etc.* Generally, conductivity is a measure of ability to conduct

electricity, and permittivity is a measure of resistance encountered when forming an electric field in a medium.

[0203] Because the composition of matter in the lithosphere (e.g., relative outermost surface) of the Earth varies by geographic location, the conductivity and permittivity of the Earth's surface varies by geographic location. In the context of variations in conductivity on the surface of the Earth, a map of the estimated effective ground conductivity in the United States may be found at <http://www.fcc.gov/encyclopedia/m3-map-effective-ground-conductivity-united-states-wall-sized-map-am-broadcast-stations>. The information provided in the map may be used to predict the propagation of amplitude modulated (AM) signals across the United States. For example, a higher ground conductivity indicates better AM propagation characteristics. The map shows that the conductivity in the United States ranges between about 0.5 and 30 millimhos per meter. Thus, in FIG. 20, it should be appreciated that the conductivity σ_1 of the lossy conducting medium 203 may vary, as the site 2100 may vary in location across the Earth.

[0204] The permittivity of a region is related to the amount of electric field generated per unit charge in that region. A higher electric flux exists in a region having high permittivity because of at least polarization effects. Likewise, a lower electric flux exists in a region having low permittivity. Permittivity is measured in farads per meter. The response of various materials to an electromagnetic field may depend, at least in part, on the frequency of the field. Thus, permittivity may be considered a complex function of the angular frequency of an applied field.

[0205] The response to static fields is described as the low-frequency or static limit of permittivity. While static permittivity may be a fair approximation for alternating fields of low frequencies, a measurable phase difference or shift may emerge for fields of higher frequencies. The frequency at which the phase difference or shift occurs may depend, at least in part, on the temperature the medium. Thus, in FIG. 20, it should be appreciated that the permittivity ϵ_1 of the lossy conducting medium 203 may vary over time based on the

moisture content in or temperature of the lossy conducting medium 203 at the site 2100, for example.

[0206] As noted above, the probe 2110 is configured to launch a guided surface wave along the propagation interface 2102 by generating an electric field having a predetermined complex wave tilt angle at or beyond the crossover distance R_x from the guided surface waveguide probe 2110. Thus, the probe 2110 may be designed to launch a guided surface wave for the nominal conductivity σ_1 and permittivity ϵ_1 conditions of the lossy conducting medium 203 at the site 2100. In other words, the probe 2110 may be designed to launch a guided surface wave for an average annual temperature, relative moisture content, *etc.*, of the Earth at the site 2100. In this case, because the nominal conductivity σ_1 and permittivity ϵ_1 conditions of the Earth at the site 2100 may vary over time (*i.e.*, vary from the nominal or annual average values) based at least upon changes in whether, for example, the embodiments described herein include various ways to preserve or maintain the nominal (or other desirable) conductivity σ_1 and permittivity ϵ_1 conditions in the lossy conducting medium 203 at the site 2100.

[0207] In one embodiment, if the nominal conductivity σ_1 and permittivity ϵ_1 conditions of the lossy conducting medium 203 at the site 2100 are, at least to some extent, undesirable or unsuitable, at least a portion of the lossy conducting medium 203 may be prepared to more efficiently or effectively launch the guided surface wave. The prepared portion of the lossy conducting medium 203 may extend to or beyond the propagation interface between the lossy conducting medium 203 and the second medium 206 at the crossover distance R_x .

[0208] FIG. 21A illustrates a cross sectional view of another example of a guided surface waveguide probe site 2200 in which a portion 2220 of the lossy conducting medium 203 is prepared to more efficiently launch a guided surface wave according to various embodiments of the present disclosure. In FIG. 21A, the portion 2220 of the lossy conducting medium 203 has been prepared, at least to some extent, to more efficiently

launch a guided surface wave from the probe 2110. Here, it is noted that efficiency in launching a guided surface wave may be related to a ratio of the amount of energy provided to the probe 2110 and the level of energy in the guided surface wave launched along the propagation interface 2102. Efficiency in launching a guided surface wave may additionally or alternatively be related to the propensity for a guided surface wave to launch along the propagation interface 2102. With regard to the manner in which the portion 2220 of the lossy conducting medium 203 is prepared, the portion 2220 of the Earth may be excavated and mixed with various types of materials or replaced with a different material, as described in further detail below with reference to FIG. 22.

[0209] With reference to FIG. 21A, it can be seen that the portion 2220 of the lossy conducting medium 203 extends beyond the crossover distance R_x along the propagation interface 2102. It is noted that, among embodiments, the portion 2220 of the lossy conducting medium 203 may extend along the propagation interface 2102 at least to or, in preferred embodiments, at some distance beyond the crossover distance R_x . In some embodiments, however, the portion 2220 of the lossy conducting medium 203 may not fully extend to the crossover distance R_x . Further, in various embodiments, the portion 2220 may extend down into the lossy conducting medium 203 at least to the depth “A” of the complex image of the guided surface waveguide probe 2110. The depth, size or extent of the complex image can depend in part upon the height “ h ” of the probe 2110 as described herein. As has been described, the complex image is located at a complex image depth. Thus, the depth “A” can correspond to the real portion of the complex image depth. In other embodiments, the portion 2220 of the lossy conducting medium 203 may extend down to other, shallower depths. For example, the depth “A” can correspond to the depth (or the real portion of the complex depth) of the complex image plane 130 illustrated in FIG. 3

[0210] FIG. 21B illustrates a top down view of the guided surface waveguide probe site 2200 in FIG. 21A according to various embodiments of the present disclosure. In FIG. 21B, it can be appreciated that the portion 2220 of the lossy conducting medium 203 includes an

area that extends across the propagation interface 2102, defined circularly or radially beyond the crossover distance R_x , measured from about the center of the guided surface waveguide probe 2110. Stated another way, the circular or radial distance to the edge of the portion 2220 is greater than the crossover distance. As should be appreciated, however, that the portion 2220 of the lossy conducting medium 203 need not be circular. Instead, the portion 2220 of the lossy conducting medium 203 may be formed in various sizes and shapes, preferably extending in any embodiment beyond the crossover distance R_x from the guided surface waveguide probe 2110. For example, the portion 2220 can comprise a ring encircling the guided surface waveguide probe 2110 that has an inner radius that is less than the crossover distance and an outer radius that is greater than the crossover distance.

[0211] FIG. 22 illustrates a stage in the preparation of the portion 2200 of the lossy conducting medium 203 in FIG. 21A according to various embodiments of the present disclosure. The portion 2200 of the lossy conducting medium 203 can be excavated in any suitable manner. The matter 2310 excavated from the portion 2200 can be mixed with a composition 2320 of other matter, and the aggregate composition provided back as the portion 2200 of the lossy conducting medium 203. The composition 2320 can include various compositions of matter among embodiments. For example, the composition 2320 may include a predetermined amount of salt, gypsum, sand, or gravel, for example, among other compositions of matter. According to aspects of the embodiments, the composition 2320 may be relied upon to vary the nominal conductivity σ_1 and permittivity ϵ_1 conditions of the Earth in the lossy conducting medium 203. In some embodiments, the excavated matter 2310 may be replaced entirely by (rather than being mixed with) the composition 2320. In various embodiments, the excavated matter 2310 can be replaced with another material or fluid (e.g., sea water or other liquid composition) that has different characteristics than the lossy conducting medium 203. The dimensions of the excavation can depend upon the frequency of the guided surface wave and/or the characteristics of the lossy conducting medium 203 and/or replacement material or fluid.

[0212] The depth of the excavation, and thus the depth of the prepared region 2220, can vary with different embodiments of the present disclosure. For example, the depth may depend on the excitation frequency and the characteristics of the lossy conducting medium 203 and/or the material or fluid added to prepared region 2220. In some embodiments, the depth of the excavation (or prepared region 2220) can extend a portion of the distance to the complex image plane. For instance, the excavation may be shallow or much less than the depth of the complex image plane. In other embodiments, the depth of the excavation (or prepared region 2220) can extend to the complex image plane. And in some embodiments, the depth of the excavation (or prepared region 2220) can extend beyond the complex image plane. The depth of the prepared region 2220, and the characteristics of the material or fluid it contains, can have a varying effect on whether a guided surface wave is launched in the respective direction intended.

[0213] Preparation of the boundary or propagation interface 2102 around the guided surface waveguide probes 2110 can also be used to direct the guided surface wave (or waves) launched by the probe 2110. The probe 2110 (e.g., guided surface waveguide probes 200a, 200b, 200c, 200d, 200e, 200f, 200g or 200h) can be configured to provide a wave tilt angle (Ψ) associated with a complex Brewster angle of incidence ($\theta_{i,B}$) associated with e.g., the conductivity σ_p and permittivity ϵ_p of a prepared region 2220 or the lossy conducting medium 203 in the vicinity of the probe 2110. By preparing a portion of the area surrounding the probe 2110, it is possible for the electric fields to produce a predetermined complex wave tilt angle at a crossover distance R_x that corresponds to the excitation frequency and the characteristics of the prepared region 2220 while not corresponding to the characteristics of the lossy conducting medium 203. In this way, the wave tilt is substantially mode-matched with the prepared region 2220 to launch a guided surface wave away from the probe 2110, while the wave tilt is not mode-matched with the lossy conducting medium 203. In alternative embodiments, the electric fields can produce a predetermined complex wave tilt angle at a crossover distance R_x that couples with the lossy conducting medium

203 while not coupling with the prepared region 2220. To achieve the desired complex wave tilt angle at the crossover distance R_x , the probe 2110 can be embodied having certain structural and electrical characteristics, consistent with the description provided above. The appropriate complex wave tilt angle allows the guided surface wave to be launched in a direction dictated by the prepared region or regions 2220. The effectiveness of the directional coupling will be affected by the difference in the characteristics (e.g., conductivity and permittivity as discussed above) between the prepared region 2220 and the unprepared region 2230, or between differently prepared regions.

[0214] Referring to FIGS. 23A-23D, shown are top down views illustrating examples of the guided surface waveguide probe sites 2200 with portions of the area surrounding the probe 2110 being prepared. In FIG. 23A, a prepared region 2220 is in the form of a wedge that extends radially outward from the probe 2110. By exciting electric fields that produce a complex wave tilt angle at the crossover distance R_x that matches the characteristics of the prepared region 2220, the incident electric field can be completely coupled into a guided surface waveguide mode in the direction (as indicated by arrows 2300) of the prepared region 2220. Guided surface waves that are launched by a probe 2110 will radially propagate away from the probe 2110 as illustrated by the arrows 2300. If the characteristics of the remaining area surrounding the probe 2110 are sufficiently different from those of the prepared region 2220, the guided surface wave propagates in the direction or range of directions defined by the prepared region 2220 (as indicated by the arrows 2300).

[0215] The range in which the guided surface waves can propagate along the surface of the lossy conducting medium 203 can be determined by the shape of the prepared region 2220. Since the incident electric fields provide a wave tilt angle associated with the complex Brewster angle of incidence associated with the prepared region 2220, they can completely couple into the guided surface waveguide mode around the prepared region 2220 and launch guided surface waves in the radial directions defined by the prepared region 2220. Because the incident electric field(s) do not provide a wave tilt angle associated with the

complex Brewster angle of incidence associated with an unprepared region 2230 of the lossy conducting medium 203, they do not couple (or only partially couple) into the guided surface waveguide mode of the lossy conducting medium 203 and thus do not effectively launch guided surface waves in the radial directions defined by the unprepared region 2230.

[0216] Appropriate excitation of the probe 2110 can produce fields that are substantially mode-matched to a guided surface waveguide mode on the surface of the prepared region 2220, resulting in the launching of a guided surface wave along the surface of the propagation interface in a radial direction as illustrated by the arrows 2300. The degree of coupling may be verified by measuring field strength along a radial extending from the guided surface waveguide probe 2110. The degree of coupling into the guided surface waveguide mode may be expressed based upon the ratio of the measured field strength to a baseline field strength, which can be calculated based upon the transmission frequency and the characteristics of the prepared region 2220. For example, the wave tilt may be considered effectively coupled when the measured field strength is greater than or equal to 90%, 95%, 97%, 98%, or 99% of the baseline field strength or other defined threshold. Similarly, the wave tilt may be considered to be negligible or effectively uncoupled when the measured field strength is less than or equal to 5%, 4%, 3%, 2%, or 1% of the baseline field strength or other defined threshold. Depending on the characteristics of the lossy conducting medium 203 and prepared regions 2220, the wave tilt may be partially coupled when the measured field strength falls between the two defined thresholds. Other methods for determining the degree of coupling are also possible. For example, in some embodiments, the degree of coupling may be based upon the energy transferred to a load via the guided surface wave based upon the excitation energy of the probe 2110. Defined thresholds as described above can be used to specify the degree of coupling.

[0217] The characteristics of the lossy conducting medium 203 and the prepared region 2220 can affect the directionality of the guided surface waves being launched by the probe 2110. The larger the differences between the conductivity σ_p and permittivity ϵ_p of the

prepared region 2220 and the conductivity σ_1 and permittivity ϵ_1 of the unprepared region 2230 of the lossy conducting medium 203, the larger the difference in degree of coupling between the prepared and unprepared regions 2220 and 2230. By reducing the degree of coupling of the wave tilt in the unprepared region 2230 relative to the prepared region 2220, the better the direction of the launched guided surface waves can be controlled.

[0218] While FIGS. 23A and 23B illustrate two examples of site preparation for controlling the direction of the guided surface waves generated by a probe 2110, other angular segments and/or geometries of the prepared region 2220 may be utilized. By increasing or decreasing the angle over which the prepared region 2220 extends around the probe 2110, the direction of the guided surface wave (as indicated by arrows 2300) can be broadened as illustrated by FIG. 23B, or can be narrowed (or further focused). For example, a radially distributed prepared region 2220 as illustrated in FIGS. 23A and 23B can have an angular distribution that ranges from a few degrees (e.g., 5-10 degrees wide) to 180 degrees (as shown in FIG. 23B) or more. In some implementations, such as the example of FIG. 23C, the prepared region 2220 can substantially surround the probe 2110, with a small area that is unprepared region 2230 to prevent or reduce propagation of the guided surface wave in the direction (as indicated by arrows 2300) of the unprepared region 2230.

[0219] The shape of the prepared region 2220 can also be varied to control the direction of the coupled guided surface wave. For example, the prepared region 2220 can have a rectangular or other geometric shape that extends outward from the probe 2110 to direct the launched guided surface waves. In addition, the number of prepared regions 2220 can be one or more. For example, two or more angular segments can be prepared to direct the guided surface waves in corresponding radial directions (arrows 2300), as shown in FIG. 23D. Other variations in geometry and number of prepared regions 2220 are possible, as can be understood.

[0220] Referring next to FIGS. 24A and 24B, shown are top down views illustrating examples of the guided surface waveguide probe sites 2200 with portions of the area

surrounding the probe 2110 being prepared. In these examples, the probe 2110 is configured to generate incident electric field(s) that provide a wave tilt angle associated with the complex Brewster angle of incidence associated with the lossy conducting medium 203. The prepared regions 2220 can be constructed with a conductivity σ_p and permittivity ϵ_p such that the wave tilt angle associated with the complex Brewster angle of incidence associated with the lossy conducting medium 203 does not effectively couple with the prepared region 2220. Thus, the angular range in which the guided surface waves can propagate along the surface of the lossy conducting medium 203 can be determined by the shape of the unprepared region 2230, as illustrated by the arrows 2300 in FIGS. 24A and 24B.

[0221] Since the incident electric fields provide a wave tilt angle associated with the complex Brewster angle of incidence associated with the unprepared region 2230 of the lossy conducting medium 203, they can completely couple into the guided surface waveguide mode around the unprepared region 2230 and launch guided surface waves in the radial directions (as indicated by arrows 2300) defined by the unprepared region 2230. Because the incident electric fields do not provide a wave tilt angle associated with the complex Brewster angle of incidence associated with the prepared region 2220, they do not couple (or only partially couple) into the guided surface waveguide mode of the prepared region 2220 and thus may not effectively launch guided surface waves in the radial directions defined by the prepared region 2230. For example, the prepared region 2220 can comprise an excavated area filled with water or sea water which has a conductivity σ_p and permittivity ϵ_p that is sufficiently different from the conductivity σ_1 and permittivity ϵ_1 of the lossy conducting medium 203 to allow the guided surface waves to be directed by the lossy conducting medium 203.

[0222] Appropriate excitation of the probe 2110 can produce fields that are substantially mode-matched to a guided surface waveguide mode on the surface of the unprepared region 2230, resulting in the launching of a guided surface wave along the surface of the

propagation interface in a radial direction as illustrated by the arrows 2300. The degree of coupling may be verified by measuring field strength along a radial extending from the guided surface waveguide probe 2110. The degree of coupling into the guided surface waveguide mode may be expressed based upon the ratio of the measured field strength to a baseline field strength, which can be calculated based upon the transmission frequency and the characteristics of the unprepared region 2230. For example, the wave tilt may be considered effectively coupled when the measured field strength is greater than or equal to 90%, 95%, 97%, 98%, or 99% of the baseline field strength or other defined threshold. Similarly, the wave tilt may be considered to be negligible or effectively uncoupled when the measured field strength is less than or equal to 5%, 4%, 3%, 2%, or 1% of the baseline field strength or other defined threshold. Depending on the characteristics of the lossy conducting medium 203 and prepared regions 2220, the wave tilt may be partially coupled when the measured field strength falls between the two defined thresholds. Other methods for determining the degree of coupling are also possible. For example, in some embodiments, the degree of coupling may be based upon the energy transferred to a load via the guided surface wave based upon the excitation energy of the probe 2110. Defined thresholds as described above can be used to specify the degree of coupling.

[0223] The characteristics of the lossy conducting medium 203 and the prepared region 2220 can affect the directionality of the guided surface waves being launched by the probe 2110. The larger the differences between the conductivity σ_p and permittivity ϵ_p of the prepared region 2220 and the conductivity σ_1 and permittivity ϵ_1 of the unprepared region 2230 of the lossy conducting medium 203, the larger the difference in degree of coupling between the prepared and unprepared regions 2220 and 2230. By reducing the degree of coupling of the wave tilt in the prepared region 2220 relative to the unprepared region 2230, the better the direction of the launched guided surface waves can be controlled.

[0224] While FIGS. 24A and 24B illustrate two examples of site preparation for controlling the direction of the guided surface waves generated by a probe 2110, other

angular segments and/or geometries of the prepared region 2220 may be utilized. By increasing or decreasing the angle over which the prepared region 2220 extends around the probe 2110, the direction of the guided surface wave can be broadened as illustrated by FIG. 24B, or can be narrowed (or further focused). For example, a radially distributed unprepared region 2230 can have an angular distribution that ranges from a few degrees (e.g., 5-10 degrees wide) to 180 degrees (see, e.g., the prepared region 2220 of FIG. 23A) or more. In some implementations, the unprepared region 2230 can substantially surround the probe 2110, with a small area that is a prepared region 2220 to prevent or reduce propagation of the guided surface wave in the direction of the prepared region 2220.

[0225] The shape of the unprepared region 2230 can also be varied to control the direction of the coupled guided surface wave (arrows 2300). For example, the unprepared region 2230 can have a rectangular or other geometric shape that extends outward from the probe 2110 to direct the launched guided surface waves. In addition, the number of unprepared regions 2230 can be one or more. For example, two or more angular segments can be prepared to direct the guided surface waves in radial directions (as indicated by arrows 2300) corresponding to the unprepared regions 2230. Other variations in geometry and number of unprepared regions 2230 are possible, as can be understood. It may be possible to enhance the directionality of the guided surface waves by extending the prepared regions 2220 beyond the crossover distance.

[0226] In some embodiments, the probe 2110 can be configured to launch different guided surface waves in different directions (as indicated by arrows 2300) based upon the prepared regions 2220 and the unprepared regions 2230. For example, in the examples of FIGS. 23B and 24B, the probe 2110 can be configured to launch guided surface waves at a first frequency in the directions defined by the prepared region 2220 and to launch guided surface waves at a second frequency in the directions defined by the unprepared region 2230. In this case, the probe 2110 can be adjusted to excite electric fields at the first frequency such that they produce a complex wave tilt angle at the crossover distance R_x that

matches the characteristics of the prepared region 2220. The incident electric field can then be completely coupled into a guided surface waveguide mode in the direction of the prepared region 2220, while not coupling (or only partially coupling) with the unprepared region 2230. The probe 2110 can also be adjusted to excite electric fields at the second frequency such that they produce a complex wave tilt angle at the crossover distance R_x that matches the characteristics of the unprepared region 2230 and completely couple into a guided surface waveguide mode in the direction of the unprepared region 2230, while not coupling (or only partially coupling) with the prepared region 2220. In some embodiments, there may be any number of prepared regions 2220 only limited by spacing around the probe 2110 that can be prepared such that each of the regions has different characteristics that correspond to different guided surface waveguide modes. In this way, a plurality of different guided surface waves can be launched in different directions by a single probe 2110. For example, FIG. 23D illustrates an example with two prepared regions 2220, which can be prepared with different characteristics associated with different operational frequencies. The unprepared region 2230 can also allow for coupling at a third operational frequency.

[0227] Referring next to FIGS. 25A and 25B, shown are examples of site specification for controlling the direction of the guided surface waves (arrows 2300) generated by a probe 2110 utilizing geographic features of the landscape. In the examples of FIGS. 25A and 25B, the lossy conducting medium 203 is a terrestrial medium 2503 (e.g., earth) which has a border that is defined by a body of water 2506 such as, e.g., fresh water or sea water or other treated water. In the example of FIG. 25A, a probe 2110 is positioned on a point or peninsula that is surrounded by water 2506. The water 2506 can act in the same way as the prepared regions 2220 shown in FIG. 24A. Since the incident electric fields generated by the probe 2110 provide a wave tilt angle associated with the complex Brewster angle of incidence of the terrestrial medium 2503, they can completely couple into the guided surface waveguide mode along the peninsula and launch guided surface waves in the radial directions defined by the surrounding water 2506 (as indicated by arrows 2300). By

positioning the probe 2110 on the point or peninsula, the guided surface waves that are launched are directed based upon the geography of the point or peninsula.

[0228] In the example of FIG. 25B, the probe 2110 is positioned on a coast line 2500 along the water 2506. The water 2506 can act in the same way as the prepared regions 2220 shown in FIG. 24B. The wave tilt angle produced by the electric fields of the probe 2110 allow guided surface waves to be launched in radial directions defined by the shoreline 2500 (as indicated by arrows 2300). While the examples of FIGS. 25A and 25B disclose directing guided surface waves along the surface of the terrestrial medium 2503, the probe 2110 can be configured to couple into the guided surface waveguide mode of the water 2506 to launch guided surface waves through the water 2506, while not allowing the coupling with the terrestrial medium 2503. For example, the guided surface waveguide probe 2110 in FIG. 25B can also be adjusted to excite electric fields that produce a complex wave tilt angle at the crossover distance R_x that matches the characteristics of the water 2506 and completely couple into a guided surface waveguide mode in the direction of the water 2506, while not coupling (or only partially coupling) with the terrestrial medium 2503. By positioning the probe 2110 at the inside of a bay, the guided surface waves to be launched in radial directions defined by the shorelines extending along either side of the bay. It may be possible to use other geologic features such as naturally occurring bodies of water (e.g., oceans, seas, lakes, rivers, etc.) to direct the launched guided surface waves in a desired direction.

[0229] It should be noted that as the height of the probe 2110 increases, the crossover distance R_x moves further away from the probe 2110, as illustrated in FIG. 6. As a result, as the height of the probe 2110 increases, the excavation area increases as the crossover distance R_x moves further outward.

[0230] It should be emphasized that the above-described embodiments of the present disclosure are merely possible examples of implementations set forth for a clear understanding of the principles of the disclosure. Many variations and modifications may be

made to the above-described embodiment(s) without departing substantially from the spirit and principles of the disclosure. All such modifications and variations are intended to be included herein within the scope of this disclosure and protected by the following claims. In addition, all optional and preferred features and modifications of the described embodiments and dependent claims are usable in all aspects of the disclosure taught herein. Furthermore, the individual features of the dependent claims, as well as all optional and preferred features and modifications of the described embodiments are combinable and interchangeable with one another.

CLAIMS

Therefore, the following is claimed:

1. A probe site, comprising:
a propagation interface in a surface of a lossy conducting medium, the propagation interface including a first region and a second region adjacent to the first region, the first region comprising a first lossy conducting medium and the second region comprising a second lossy conducting medium; and
a guided surface waveguide probe positioned over the propagation interface, and adjacent to the first region and the second region, the guided surface waveguide probe configured to generate at least one electrical field that synthesizes a wave front having a complex Brewster angle of incidence corresponding to the first lossy conducting medium when excited by an excitation source, where the wave front launches a guided surface wave along the propagation interface and the surface of the lossy conducting medium in a radial direction that is defined by the first region and restricted by the second region.
2. The probe site according to claim 1, wherein the wave front intersects with the propagation interface at the complex Brewster angle of incidence at a crossover distance from the guided surface waveguide probe.
3. The probe site according to claim 1, wherein the first region and the second region extend along the propagation interface from adjacent to the guided surface waveguide probe to beyond the crossover distance.

4. The probe site according to claim 1, wherein the lossy conducting medium is a terrestrial medium, and the first lossy conducting medium is the terrestrial medium.

5. The probe site according to claim 4, wherein the second region extends into the terrestrial medium at least to a depth of a complex image of the guided surface waveguide probe.

6. The probe site according to claim 4, wherein the second region extends into the terrestrial medium at least to a depth of a complex image plane of the guided surface waveguide probe.

7. The probe site according to claim 1, wherein the second lossy conducting medium is water.

8. The probe site according to claim 7, wherein the second region is a naturally occurring body of water.

9. The probe site according to claim 1, wherein the lossy conducting medium is a terrestrial medium, and the second lossy conducting medium is the terrestrial medium.

10. The probe site according to claim 9, wherein the first region is a prepared region having a conductivity and permittivity that is different from the terrestrial medium.

11. The probe site according to claim 10, wherein the prepared region comprises an excavation containing water.

12. The probe site according to claim 11, wherein the water is seawater.
13. The probe site according to claim 10, wherein the prepared region comprises an excavation containing an aggregate composition of the terrestrial medium and an added material.
14. The probe site according to claim 1, wherein the second region extends around the guided surface waveguide probe from a first side of the first region to a second side of the first region.
15. The probe site according to claim 1, wherein the propagation interface includes a third region adjacent to the first region opposite the second region.
16. The probe site according to claim 15, wherein the third region comprises the second lossy conducting medium.
17. The probe site according to claim 15, wherein the third region comprises a third lossy conducting medium.
18. The probe site according to claim 1, wherein the lossy conducting medium is a terrestrial medium.