

DESCRIPTION

Title of Invention:

GLASS COMPOSITION FOR GLASS FIBER, GLASS FIBER, GLASS FIBER
FABRIC, AND GLASS FIBER-REINFORCED RESIN COMPOSITION

Technical Field

[0001]

The present invention relates to a glass composition for glass fiber, glass fiber, a glass fiber woven fabric, and a glass fiber-reinforced resin composition.

Background Art

[0002]

Glass fiber is manufactured by melting a glass raw material prepared so as to be a glass composition for glass fiber having a desired composition in a glass melting furnace to form molten glass (a melt of the glass composition for glass fiber); discharging the molten glass from a container (bushing) having a nozzle plate on which several to thousands of nozzle tips are formed; and cooling the discharged molten glass while stretching by winding at a high speed to solidify it into fiber (hereinafter, this operation is sometimes referred to as "spinning"). The above bushing is formed from a noble metal such as platinum.

[0003]

Conventionally, glass fiber has been widely used in various applications to improve the strength of resin molded products, and the resin molded products have been used for a housing or a part of electronic devices such as a server, a smartphone, a laptop computer, and the like.

[0004]

In general, glass absorbs energy from alternating current as heat, and thus has a problem that the above resin molded product generates heat when the resin molded product is used for a housing or a part of the electronic devices.

[0005]

The dielectric loss energy absorbed by glass is proportional to the dielectric constant and the dielectric loss tangent determined by the component and the structure of the glass, and is represented by the following formula (A):

$$W = kfv^2 \times \varepsilon^{1/2} \times \tan\delta \quad (A).$$

[0006]

wherein W is a dielectric loss energy, k is a constant, f is a frequency, v^2 is a potential gradient, ε is a dielectric constant, and $\tan\delta$ is a dielectric loss tangent. From the above formula (A), it is found that the dielectric loss is larger and heat generation of the above resin molded product is larger as the dielectric constant and the dielectric loss tangent are larger and as the frequency is higher.

[0007]

In recent years, in response to the fact that the frequency (f in the above formula (A)) of the alternating current used in the above electronic devices has increased, the glass fiber used for a housing or a part of the above electronic device has been required to have a lower dielectric constant and a lower dielectric loss tangent in order to reduce dielectric loss energy. In particular, the glass fiber has been required to have a low dielectric loss tangent because the dielectric loss tangent has larger influence on the formula (A) than that of the dielectric constant, which is raised to the power of 1/2.

[0008]

In view of the above situation, the present applicant has suggested, as a glass composition for glass fiber having a low dielectric constant and a low dielectric loss tangent, suppressing the occurrence of phase separation, and having a reduced viscosity at high temperatures, a glass composition for glass fiber including SiO₂ in the range of 52.0 to 59.5% by mass, B₂O₃ in the range of 17.5 to 25.5% by mass, Al₂O₃ in the range of 9.0 to 14.0% by mass, SrO in the range of 0.5 to 6.0% by mass, MgO in the range of 1.0 to 5.0% by mass, CaO in the range of 1.0 to 5.0% by mass, and F₂ and Cl₂ in the range of 0.1 to 2.5% by mass in total, with respect to the total amount of the glass composition for glass fiber (see Patent Literature 1).

Citation List

Patent Literature

[0009]

Patent Literature 1: Japanese Patent No. 6468409

Summary of Invention

Technical Problem

[0010]

Meanwhile, there has been required a glass composition for glass fiber that enables glass fiber having a lower dielectric constant and a lower dielectric loss tangent particularly in a high-frequency region of about 10 GHz to be obtained therefrom. In order to achieve such an issue, it is contemplated that, in a glass composition for glass fiber, the contents of Al_2O_3 and alkaline earth metal oxides (CaO , MgO , and SrO) are lowered and correspondingly, the contents of SiO_2 and B_2O_3 are raised, with respect to the total amount of the glass composition for glass fiber.

[0011]

However, when the contents of SiO_2 and B_2O_3 with respect to the total amount of the glass composition for glass fiber are raised in the glass composition for glass fiber, at the cost of the content of Al_2O_3 and alkaline earth metal oxides, disadvantageously, the working temperature range, represented by the difference between the 1000 poise temperature and the liquid phase temperature, is narrowed to cause the glass fiber manufacturability to decrease, or the water resistance of the glass fiber deteriorates, and foreign matter precipitated on the glass fiber surface due to hydrolysis of the glass causes the dielectric characteristics to deteriorate or the strength of the glass fiber to markedly decrease.

[0012]

An object of the present invention is, by eliminating the disadvantage, to provide a glass composition for glass fiber that enables glass fiber having excellent water resistance and excellent dielectric characteristics (a low dielectric constant and a low dielectric loss

tangent) in a high-frequency region to be obtained therefrom, the glass composition for glass fiber per se being able to have a sufficient working temperature range.

Solution to Problem

[0013]

In order to achieve the object, the glass composition for glass fiber of the present invention includes SiO₂ in a range of 59.00 to 65.00% by mass, B₂O₃ in a range of 16.00 to 26.00% by mass, Al₂O₃ in a range of 7.00 to 14.00% by mass, CaO in a range of 0 to 5.00% by mass, MgO in a range of 0 to 4.00% by mass, SrO in a range of 0 to 6.00% by mass, TiO₂ in a range of 0.10 to 5.00% by mass, and F₂ and Cl₂ in a range of 0 to 2.00% by mass in total, with respect to the total amount of the glass composition for glass fiber, and has a content of P₂O₅ of less than 0.20% by mass and a total content of Na₂O, K₂O, and Li₂O of less than 1.00% by mass, the ratio of the content of TiO₂ (% by mass) to the total content of CaO, MgO, and SrO (% by mass) (TiO₂/(CaO + MgO + SrO)) is in a range of 0.66 to 4.00, and the content SI (% by mass) of SiO₂ and the content A (% by mass) of Al₂O₃ satisfy the following formula (1):

$$1.00 \leq 1000 \times A/SI^2 \leq 4.65 \quad (1).$$

[0014]

When the glass composition for glass fiber of the present invention includes SiO₂, B₂O₃, Al₂O₃, CaO, MgO, SrO, TiO₂, F₂ and Cl₂, P₂O₅, and Na₂O, K₂O, and Li₂O in the above range, the ratio of the content of TiO₂ (% by mass) to the total content of CaO, MgO, and SrO (% by mass) (TiO₂/(CaO + MgO + SrO)) is in the range of 0.66 to 4.00, and the content SI (% by mass) of SiO₂ and the content A (% by mass) of Al₂O₃ satisfy the formula (1), the glass composition enables glass fiber having excellent water resistance and excellent dielectric characteristics (a low dielectric constant and a low dielectric loss tangent) in a high-frequency region to be obtained therefrom and per se can have a sufficient working temperature range.

[0015]

Here, glass fiber obtained from the glass composition for glass fiber of the present invention having a low dielectric constant means that the dielectric constant is 4.2 or less at

a measurement frequency of 10 GHz, and having a low dielectric loss tangent means that the dielectric loss tangent is 0.0011 or less at a measurement frequency of 10 GHz.

[0016]

Glass fiber obtained from the glass composition for glass fiber of the present invention exhibiting excellent water resistance means that, upon evaluation of the water resistance by the following evaluation method, the mass reduction rate is 2.0% or less and the components of the glass fiber are not substantially eluted even in water.

[0017]

In the method for evaluating the water resistance, first, a glass batch, obtained by mixing glass raw materials so that the glass composition after melt-solidification has a predetermined glass composition for glass fiber, is placed in an 80 mm diameter platinum crucible, melted at 1550°C for 4 hours and at 1650°C for 2 hours, and taken out from the crucible to obtain homogeneous glass cullet. The glass cullet is placed in a small cylindrical platinum bushing having a circular nozzle tip at the bottom thereof, and the bushing is heated to a predetermined temperature to melt the glass cullet. Then, the molten glass discharged through the nozzle tip is cooled and solidified while stretched by winding on a stainless collet at a predetermined speed to thereby obtain glass fiber having a perfect circular section and a fiber diameter of 13 μm . Next, about 1 g of the obtained glass fiber (glass fiber for test) is collected from the collet and dried at 120°C for an hour, and the mass (mass before operation) is measured. Subsequently, the glass fiber for test is allowed to stand in 100 ml of distilled water at 80°C for 24 hours. Then, the glass fiber for test is taken on metal mesh perforated with eyes of about 150 μm , washed with distilled water, then dried at 120°C for an hour, and the mass (mass after operation) is measured. Then, the mass reduction rate ($100 \times (1 - (\text{mass after operation} / \text{mass before operation}))$) is calculated from the mass before operation and mass after operation.

[0018]

The glass composition for glass fiber of the present invention having sufficient working temperature range means that the working temperature range is 20°C or more. The upper limit of the working temperature range is not particularly limited, and for example, is 500°C or less, preferably, 450°C or less, and more preferably 400°C or less.

[0019]

In the glass composition for glass fiber of the present invention, the content SI (% by mass) of SiO₂, the content B (% by mass) of B₂O₃, the content A (% by mass) of Al₂O₃, the content C (% by mass) of CaO, the content M (% by mass) of MgO, the content SR (% by mass) of SrO, the content T (% by mass) of TiO₂, and the total content F (% by mass) of F₂ and Cl₂ preferably satisfy the following formula (2), more preferably satisfy the following formula (3), still more preferably satisfy the following formula (4), and particularly preferably satisfy the following formula (4):

$$204.00 \leq Si \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 422.40 \quad (2);$$

$$244.00 \leq Si \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 410.00 \quad (3);$$

$$308.50 \leq Si \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 400.50 \quad (4);$$

$$339.60 \leq Si \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 377.80 \quad (5).$$

[0020]

The present invention also consists in glass fiber formed of any of the above glass compositions for glass fiber, a glass fiber woven fabric including the glass fiber, or a glass fiber-reinforced resin composition including the glass fiber.

[0021]

The glass fiber of the present invention can be obtained by, for example, melting the above glass composition for glass fiber of the present invention, discharging the obtained melt from a bushing having a nozzle plate with 1 to 8000 nozzle tips or holes formed therein, and cooling the melt while stretching by winding at a high speed to solidify it into a fiber. Accordingly, the glass fiber of the present invention comprises the glass composition identical to that of the above glass composition for glass fiber of the present invention.

Description of Embodiments

[0022]

Hereinafter, embodiments of the present invention will be described in detail.

[0023]

The glass composition for glass fiber of the present embodiment includes SiO₂ in the range of 59.00 to 65.00% by mass, B₂O₃ in the range of 16.00 to 26.00% by mass, Al₂O₃ in the range of 7.00 to 14.00% by mass, CaO in the range of 0 to 5.00% by mass, MgO in the range of 0 to 4.00% by mass, SrO in the range of 0 to 6.00% by mass, TiO₂ in the range of 0.10 to 5.00% by mass, and F₂ and Cl₂ in the range of 0 to 2.00% by mass in total, with respect to the total amount of the glass composition for glass fiber, and has a content of P₂O₅ of less than 0.20% by mass and a total content of Na₂O, K₂O, and Li₂O of less than 1.00% by mass, the ratio of the content of TiO₂ (% by mass) to the total content of CaO, MgO, and SrO (% by mass) (TiO₂/(CaO + MgO + SrO)) is in the range of 0.66 to 4.00, and the content SI (% by mass) of SiO₂ and the content A (% by mass) of Al₂O₃ satisfy the following formula (1):

$$1.00 \leq 1000 \times A/SI^2 \leq 4.65 \quad (1).$$

[0024]

When the glass composition for glass fiber of the present embodiment includes SiO₂, B₂O₃, Al₂O₃, CaO, MgO, SrO, TiO₂, F₂ and Cl₂, P₂O₅, and Na₂O, K₂O, and Li₂O in the above range, the ratio of the content of TiO₂ (% by mass) to the total content of CaO, MgO, and SrO (% by mass) (TiO₂/(CaO + MgO + SrO)) is in the range of 0.66 to 4.00, and the content SI (% by mass) of SiO₂ and the content A (% by mass) of Al₂O₃ satisfy the formula (1), glass fiber having excellent water resistance and excellent dielectric characteristics (a low dielectric constant and a low dielectric loss tangent) in a high-frequency region can be obtained, and the glass composition per se can have a sufficient working temperature range.

[0025]

When the glass composition for glass fiber of the present embodiment has a content of SiO₂ of less than 59.00% by mass with respect to the total amount of the glass composition for glass fiber, the mechanical strength of the glass fiber obtained from the glass composition for glass fiber is greatly reduced, and the function of the glass fiber as a

reinforcing material in the glass fiber-reinforced resin composition is impaired. In addition, the glass fiber tends to deteriorate when placed in an acidic environment. On the other hand, when the content of SiO_2 is more than 65.00% by mass with respect to the total amount of the glass composition for glass fiber, the viscosity at high temperatures increases. Thus, the temperature at which the glass raw material is melted rises, and from the viewpoint of production cost, the glass composition for glass fiber of the present embodiment will be not suitable for industrial glass fiber production.

[0026]

The glass composition for glass fiber of the present embodiment has a content of SiO_2 with respect to the total amount of the glass composition for glass fiber preferably in the range of 59.20 to 64.50% by mass, more preferably in the range of 59.30 to 64.00% by mass, still more preferably in the range of 59.40 to 63.50% by mass, particularly preferably in the range of 59.50 to 63.00% by mass, especially preferably in the range of 59.60 to 62.80% by mass, and most preferably in the range of 60.10 to 62.60% by mass.

[0027]

When the glass composition for glass fiber of the present embodiment has a content of B_2O_3 of less than 16.00% by mass with respect to the total amount of the glass composition for glass fiber, the dielectric loss tangent of the glass fiber obtained from the glass composition for glass fiber cannot be sufficiently reduced. On the other hand, when the content of B_2O_3 is more than 26.00% by mass with respect to the total amount of the glass composition for glass fiber, phase separation occurs in the glass fiber obtained from the glass composition for glass fiber, and the chemical durability of the glass fiber may decrease.

[0028]

The glass composition for glass fiber of the present embodiment has a content of B_2O_3 with respect to the total amount of the glass composition for glass fiber of preferably in the range of 18.00 to 24.90% by mass, more preferably in the range of 19.00 to 24.50% by mass, still more preferably in the range of 19.60 to 24.00% by mass, particularly preferably in the range of 20.10 to 23.50% by mass, and most preferably in the range of 20.50 to 23.00% by mass.

[0029]

When the glass composition for glass fiber of the present embodiment has a content of Al_2O_3 of less than 7.00% by mass with respect to the total amount of the glass composition for glass fiber, phase separation occurs in the glass fiber obtained from the glass composition for glass fiber, and the chemical durability of the glass fiber may decrease. On the other hand, when the content of Al_2O_3 is more than 14.00% by mass with respect to the total amount of the glass composition for glass fiber, the dielectric loss tangent of the glass fiber obtained from the glass composition for glass fiber cannot be sufficiently reduced.

[0030]

The glass composition for glass fiber of the present embodiment has a content of Al_2O_3 with respect to the total amount of the glass composition for glass fiber preferably in the range of 7.20 to 13.50% by mass, more preferably in the range of 7.40 to 13.00% by mass, still more preferably in the range of 7.60 to 12.50% by mass, particularly preferably in the range of 7.80 to 12.00% by mass, especially preferably in the range of 8.00 to 11.80% by mass, and most preferably in the range of 8.20 to 9.90% by mass.

[0031]

When the glass composition for glass fiber of the present embodiment has a content of CaO of more than 5.00% by mass with respect to the total amount of the glass composition for glass fiber, the dielectric loss tangent of the glass fiber obtained from the glass composition for glass fiber cannot be sufficiently reduced.

[0032]

The glass composition for glass fiber of the present embodiment has a content of CaO with respect to the total amount of the glass composition for glass fiber preferably in the range of 0.60 to 4.80% by mass, more preferably in the range of 1.10 to 4.60% by mass, still more preferably in the range of 1.60 to 4.40% by mass, particularly preferably in the range of 1.80 to 4.20% by mass, especially preferably in the range of 2.00 to 4.00% by mass, and most preferably in the range of 2.10 to 3.60% by mass.

[0033]

When the glass composition for glass fiber of the present embodiment has a content of MgO of more than 4.00% by mass with respect to the total amount of the glass composition for glass fiber, striae occurs in a melt of the glass composition for glass fiber, cut of glass fiber during spinning may easily occur, and additionally the water resistance of the glass fiber obtained from the glass composition for glass fiber may deteriorate.

[0034]

The glass composition for glass fiber of the present embodiment has a content of MgO with respect to the total amount of the glass composition for glass fiber preferably in the range of less than 3.00% by mass, more preferably in the range of less than 2.00% by mass, still more preferably in the range of less than 1.50% by mass, particularly preferably in the range of less than 1.00% by mass, especially preferably in the range of less than 0.95% by mass, and most preferably in the range of less than 0.50% by mass.

[0035]

When the glass composition for glass fiber of the present embodiment has a content of SrO with respect to the total amount of the glass composition for glass fiber of more than 6.00% by mass, the dielectric characteristics of glass fiber obtained from the glass composition for glass fiber deteriorates, and target dielectric characteristics cannot be satisfied.

[0036]

The glass composition for glass fiber of the present embodiment has a content of SrO with respect to the total amount of the glass composition for glass fiber preferably in the range of less than 4.00% by mass, more preferably in the range of less than 3.00% by mass, still more preferably in the range of less than 2.00% by mass, particularly preferably in the range of less than 1.00% by mass, especially preferably in the range of less than 0.50% by mass, and most preferably in the range of less than 0.45% by mass.

[0037]

When the glass composition for glass fiber of the present embodiment has a content of TiO₂ with respect to the total amount of the glass composition for glass fiber of less than 0.10% by mass, the viscosity at high temperatures increases. Thus, the temperature at which the glass raw material is melted rises, and from the viewpoint of

production cost, the glass composition for glass fiber of the present embodiment will be unsuitable to industrial glass fiber production. On the other hand, when the content of TiO_2 with respect to the total amount of the glass composition for glass fiber is more than 5.00% by mass, the dielectric loss tangent of the glass fiber obtained from the glass composition for glass fiber cannot be sufficiently reduced, and the liquid phase temperature of the glass composition for glass fiber greatly increases. Thus, stable manufacturing of glass fiber cannot be conducted.

[0038]

The glass composition for glass fiber of the present embodiment has a content of TiO_2 with respect to the total amount of the glass composition for glass fiber preferably in the range of 0.60 to 4.90% by mass, more preferably in the range of 1.60 to 4.70% by mass, still more preferably in the range of 2.10 to 4.60% by mass, particularly preferably in the range of 2.50 to 4.50% by mass, and most preferably in the range of 2.80 to 4.40% by mass.

[0039]

When the glass composition for glass fiber of the present embodiment has a content of F_2 and Cl_2 in total with respect to the total amount of the glass composition for glass fiber of more than 2.00% by mass, the chemical durability of glass fiber obtained from the glass composition for glass fiber decreases.

[0040]

The glass composition for glass fiber of the present embodiment has a content of F_2 and Cl_2 in total with respect to the total amount of the glass composition for glass fiber preferably in the range of 0.10 to 1.80% by mass, more preferably in the range of 0.30 to 1.60% by mass, and still more preferably in the range of 0.50 to 1.50% by mass.

[0041]

When the glass composition for glass fiber of the present embodiment has a content of P_2O_5 of more than 0.20% by mass and a content of SiO_2 in the above range, with respect to the total amount of the glass composition for glass fiber, containing P_2O_5 does not contribute to increase in the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber. On the other hand, occurrence of phase

separation of the glass fiber cannot be suppressed, and thus the chemical durability of the glass fiber deteriorates.

[0042]

The glass composition for glass fiber of the present embodiment has a content of P_2O_5 with respect to the total amount of the glass composition for glass fiber preferably in the range of less than 0.10% by mass and more preferably in the range of less than 0.05% by mass.

[0043]

When the glass composition for glass fiber of the present embodiment has a total content of Na_2O , K_2O , and Li_2O with respect to the total amount of the glass composition for glass fiber of more than 1.00% by mass, the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber greatly deteriorate, and target dielectric characteristics cannot be satisfied.

[0044]

The glass composition for glass fiber of the present embodiment has a total content of Na_2O , K_2O , and Li_2O with respect to the total amount of the glass composition for glass fiber preferably in the range of less than 0.80% by mass, more preferably in the range of less than 0.50% by mass, still more preferably in the range of less than 0.20% by mass, particularly preferably in the range of less than 0.10% by mass, and most preferably in the range of less than 0.05% by mass.

[0045]

When the glass composition for glass fiber of the present embodiment has a ratio of the content of TiO_2 (% by mass) to the total content of CaO , MgO , and SrO (% by mass) ($TiO_2/(CaO + MgO + SrO)$) of less than 0.66, deterioration in the dielectric loss tangent caused by containing alkaline earth metal oxides cannot be sufficiently suppressed. Thus, the dielectric loss tangent of the glass fiber obtained from the glass composition for glass fiber cannot be sufficiently reduced, and the water resistance of the glass fiber may deteriorate. When the glass composition for glass fiber of the present embodiment has a ratio of more than 4.00, occurrence of striae in the glass cannot be suppressed, and the

liquid phase temperature greatly increases. Thus, stable manufacturing of glass fiber cannot be conducted.

[0046]

The glass composition for glass fiber of the present embodiment has a ratio of the content of TiO_2 (% by mass) to the total content of CaO , MgO , and SrO (% by mass) ($\text{TiO}_2/(\text{CaO} + \text{MgO} + \text{SrO})$) preferably in the range of 0.67 to 2.15, more preferably in the range of 0.85 to 2.00, still more preferably in the range of 0.90 to 1.80, particularly preferably in the range of 0.95 to 1.70, and most preferably in the range of 0.98 to 1.60.

[0047]

Here, the ratio of the content of TiO_2 (% by mass) to the total content of CaO , MgO , and SrO (% by mass) is presumed to represents the balance between deterioration in the glass fiber manufacturing stability and reduction in the dielectric loss tangent in association with increase in the liquid phase temperature of the glass composition for glass fiber caused by containing TiO_2 , which is an intermediate oxide, and increase in the glass fiber manufacturing stability and deterioration in the water resistance and the dielectric loss tangent in association with decrease in the liquid phase temperature of the glass composition for glass fiber caused by containing alkaline earth metal oxides, which are network modifying oxides.

[0048]

When the glass composition for glass fiber of the present embodiment has a value of the formula (1) of less than 1.00, it is not possible to suppress deterioration in the water resistance of the glass fiber obtained from the glass composition for glass fiber, and increase in glass fiber production cost and deterioration in the glass fiber manufacturability due to increase in the number of fuzz occurrences in the glass fiber manufacturing process in association with increase in the viscosity of the glass composition for glass fiber at high temperatures. On the other hand, when the glass composition for glass fiber has a value of the formula (1) of more than 4.65, it is not possible to suppress deterioration in the glass fiber manufacturing stability in association with increase in the liquid phase temperature of the glass composition for glass fiber, and deterioration in the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber.

[0049]

The glass composition for glass fiber of the present embodiment has a value of the formula (1) preferably in the range of 1.50 to 4.50, more preferably in the range of 1.80 to 4.20, still more preferably in the range of 2.00 to 4.00, particularly preferably in the range of 2.05 to 3.80, especially preferably in the range of 2.10 to 3.60, and most preferably in the range of 2.11 to 3.35.

[0050]

Here, in the formula (1), a higher content A of Al_2O_3 tends to allow the viscosity of the glass composition for glass fiber at high temperatures to be reduced, leading to reduction in the glass fiber production cost. However, when this value becomes excessively high, occurrence of mullite-based crystals is facilitated, and there is a tendency in which deterioration in the glass fiber manufacturing stability in association with increase in the liquid phase temperature of the glass composition for glass fiber, and deterioration in the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber cannot be suppressed. On the other hand, as this value is lower, there is a tendency in which increase in the glass fiber manufacturing stability in association with decrease in the liquid phase temperature of the glass composition for glass fiber, and increase in the dielectric characteristics of glass composition for glass fiber are obtained. However, when this value is excessively low, there is a tendency in which the water resistance of the glass fiber obtained from the glass composition for glass fiber deteriorates, and fuzz easily occurs, which fuzz becomes an obstacle to glass fiber manufacturing, in association with decrease in the strength of the glass fiber. As the content SI of SiO_2 is higher, the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber are improved, but there is a tendency in which the viscosity of the glass composition for glass fiber at high temperatures increases to cause the glass fiber production cost to increase. On the other hand, as this value is lower, the viscosity of the glass composition for glass fiber at high temperatures is reduced to thereby lead to reduction in the glass fiber production cost, but the dielectric characteristics of the glass fiber obtained from the glass composition for glass fiber tend to deteriorate. Accordingly, the formula (1) is presumed to represent a balance between the

comprehensive glass fiber manufacturability of the glass composition for glass fiber and the dielectric characteristics obtained from the glass composition for glass fiber. The tendency for fuzz to easily occur becomes an obstacle also upon processing the glass fiber into glass fiber products (e.g., glass fiber woven fabrics, chopped strands, and rovings). [0051]

In the glass composition for glass fiber of the present embodiment, the content SI (% by mass) of SiO₂, the content B (% by mass) of B₂O₃, the content A (% by mass) of Al₂O₃, the content C (% by mass) of CaO, the content M (% by mass) of MgO, the content SR (% by mass) of SrO, the content T (% by mass) of TiO₂, and the total content F (% by mass) of F₂ and Cl₂ preferably satisfy the following formula (2), more preferably satisfy the following formula (3), still more preferably satisfy the following formula (4) and particularly preferably satisfy the following formula (5):

$$204.00 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 422.40 \quad (2);$$

$$244.00 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 410.00 \quad (3);$$

$$308.50 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 400.50 \quad (4);$$

$$339.60 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 377.80 \quad (5).$$

[0052]

When the SI, B, A, C, M, SR, T, and F satisfy the formula (2), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a sufficient working temperature range.

[0053]

When the SI, B, A, C, M, SR, T, and F satisfy the formula (3), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and more excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a sufficient working temperature range. Here,

the glass fiber having more excellent dielectric characteristics means that the dielectric constant is 4.1 or less and the dielectric loss tangent is 0.0010 or less at a measurement frequency of 10 GHz.

[0054]

When the SI, B, A, C, M, SR, T, and F satisfy the formula (4), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and more excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have an excellent working temperature range of 120°C or more.

[0055]

When the SI, B, A, C, M, SR, T, and F satisfy the formula (5), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and extremely excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a more excellent working temperature range of 200°C or more. Here, the glass fiber having extremely excellent dielectric characteristics means that the dielectric constant is 4.0 or less and the dielectric loss tangent is less than 0.0010 at a measurement frequency of 10 GHz.

[0056]

When the ratio of content of MgO (% by mass) to the total content of CaO and SrO (% by mass) ($\text{MgO}/(\text{CaO} + \text{SrO})$) is in the range of less than 0.60, for example, the glass composition for glass fiber of the present embodiment lowers the viscosity of the glass composition for glass fiber at high temperatures while suppressing the occurrence of phase separation in the glass fiber obtained from the glass composition for glass fiber, which phase separation is facilitated by MgO, and can contribute to improvement in comprehensive glass fiber manufacturability of the glass composition for glass fiber by lowering the liquid phase temperature of the glass composition for glass fiber. The glass composition for glass fiber of the present embodiment has a ratio of the content of MgO (% by mass) to the total content of CaO and SrO (% by mass) ($\text{MgO}/(\text{CaO} + \text{SrO})$) preferably in the range of less than 0.40, more preferably in the range of less than 0.30, still

more preferably in the range of less than 0.20, particularly preferably in the range of less than 0.10, and most preferably in the range of less than 0.05.

[0057]

When the ratio of the content of TiO_2 (% by mass) to the content of Al_2O_3 (% by mass) ($\text{TiO}_2/\text{Al}_2\text{O}_3$) is in the range of 0.24 to 0.72, for example, the glass composition for glass fiber of the present embodiment can achieve both the effect of reducing the dielectric loss tangent by containing TiO_2 and the effect of improving the water resistance by containing Al_2O_3 while suppressing increase in the liquid phase temperature of glass composition for glass fiber, in association with occurrence of crystals facilitated by TiO_2 . The glass composition for glass fiber of the present embodiment has a ratio of the content of TiO_2 (% by mass) to the content of Al_2O_3 (% by mass) ($\text{TiO}_2/\text{Al}_2\text{O}_3$) preferably in the range of 0.28 to 0.56, more preferably in the range of 0.29 to 0.50, still more preferably in the range of 0.30 to 0.45, and most preferably in the range of 0.35 to 0.44.

[0058]

When the B, A, C, M, SR, T, F, and the content P (% by mass) of P_2O_5 satisfy the following formula (6), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a sufficient working temperature range:

$$1.08 \leq \{2 \times (0.72 \times C + M + 0.39 \times \text{SR}) - 1.06 \times F\} \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \leq 2.34 \quad (6).$$

[0059]

In the glass composition for glass fiber of the present embodiment, the B, A, C, M, SR, T, F, and P preferably satisfy the following formula (7), still more preferably satisfy the following formula (8), and particularly preferably satisfy the following formula (9):

$$1.47 \leq \{2 \times (0.72 \times C + M + 0.39 \times \text{SR}) - 1.06 \times F\} \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \leq 2.33 \quad (7);$$

$$1.47 \leq \{2 \times (0.72 \times C + M + 0.39 \times \text{SR}) - 1.06 \times F\} \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \leq 2.32 \quad (8);$$

$$2.14 \leq \{2 \times (0.72 \times C + M + 0.39 \times SR) - 1.06 \times F\} \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \leq 2.32 \quad (9).$$

[0060]

When the B, A, C, M, SR, T, F, and P satisfy the formula (7), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and more excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a sufficient working temperature range.

[0061]

When the B, A, C, M, SR, T, F, and P satisfy the formula (8), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and more excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have an excellent working temperature range of 120°C or more.

[0062]

When the B, A, C, M, SR, T, F, and P satisfy the formula (9), the glass composition for glass fiber of the present embodiment enables glass fiber having excellent water resistance and extremely excellent dielectric characteristics in a high-frequency region to be obtained therefrom and per se can have a more excellent working temperature range of 200°C or more.

[0063]

The glass composition for glass fiber of the present embodiment may include ZnO in the range of 0 to 3.00% by mass with respect to the total amount of the glass composition for glass fiber. When the glass composition for glass fiber of the present embodiment includes ZnO and the content of ZnO is more than 3.00% by mass, a devitrified product tends to occur, and stable glass fiber manufacturing cannot be performed.

[0064]

When the glass composition for glass fiber of the present embodiment includes ZnO, the content of ZnO with respect to the total amount of the glass composition for

glass fiber is preferably 2.50% by mass or less, more preferably 1.50% by mass or less, and still more preferably 0.50% by mass or less.

[0065]

The glass composition for glass fiber of the present embodiment may include MnO_2 in the range of 0 to 3.00% by mass with respect to the total amount of the glass composition for glass fiber. When the glass composition for glass fiber of the present embodiment includes MnO_2 and the content of MnO_2 is more than 3.00% by mass, the dielectric characteristics deteriorate, and desired dielectric characteristics cannot be obtained.

[0066]

When the glass composition for glass fiber of the present embodiment includes MnO_2 , the content of MnO_2 with respect to the total amount of the glass composition for glass fiber is preferably 2.50% by mass or less, more preferably 1.50% by mass or less, and still more preferably 0.50% by mass or less.

[0067]

The glass composition for glass fiber of the present embodiment may include Fe_2O_3 in the range of 0% by mass or more and 1.00% by mass or less with respect to the total amount of the glass composition for glass fiber. When the glass composition for glass fiber of the present embodiment includes Fe_2O_3 , it is effective to set the content of Fe_2O_3 to 0.10% by mass or more and 0.60% by mass or less from the viewpoint of suppressing the bubble included in the glass fiber.

[0068]

The glass composition for glass fiber of the present embodiment may include SnO_2 in the range of 0% by mass or more and 1.00% by mass or less with respect to the total amount of the glass composition for glass fiber. When the glass composition for glass fiber of the present embodiment includes SnO_2 , it is effective to set the content of SnO_2 to 0.10% by mass or more and 0.60% by mass or less from the viewpoint of suppressing the bubble included in the glass fiber.

[0069]

In the glass composition for glass fiber of the present embodiment, when the content of ZrO_2 is less than 0.50% by mass with respect to the total amount of the glass composition for glass fiber, ZrO_2 may be included. When the content of ZrO_2 is 0.50% by mass or more with respect to the total amount of the glass composition for glass fiber, the devitrified product tends to occur, and stable glass fiber manufacturing cannot be conducted.

[0070]

When the glass composition for glass fiber of the present embodiment includes ZrO_2 , the content of ZrO_2 with respect to the total amount of the glass composition for glass fiber is preferably in the range of less than 0.45% by mass, more preferably in the range of less than 0.40% by mass, still more preferably in the range of less than 0.20% by mass, particularly preferably in the range of less than 0.10% by mass, and most preferably in the range of less than 0.05% by mass.

[0071]

In the glass composition for glass fiber of the present embodiment, when the content of Cr_2O_3 is less than 0.05% by mass with respect to the total amount of the glass composition for glass fiber, Cr_2O_3 may be included. When the content of Cr_2O_3 is 0.05% by mass or more with respect to the total amount of the glass composition for glass fiber, the devitrified product tends to occur, and stable glass fiber manufacturing cannot be conducted.

[0072]

The glass composition for glass fiber of the present embodiment may include, as impurities attributable to raw materials, less than 1.00% by mass of oxides of Ba, Co, Ni, Cu, Mo, W, Ce, Y, La, Bi, Gd, Pr, Sc, or Yb in total with respect to the total amount of the glass composition for glass fiber. Particularly when the glass composition for glass fiber of the present embodiment includes BaO, CeO_2 , Y_2O_3 , La_2O_3 , Bi_2O_3 , Gd_2O_3 , Pr_2O_3 , Sc_2O_3 , or Yb_2O_3 as impurities, the content of each of the impurities is independently preferably less than 0.40% by mass, more preferably less than 0.20% by mass, still more preferably less than 0.10% by mass, particularly preferably less than 0.05% by mass, and most preferably less than 0.01% by mass.

[0073]

Regarding the content of each component described above in the glass composition for glass fiber of the present embodiment, the content of Li as the light element can be measured with an ICP emission spectroscopic analyzer, and the contents of the other elements can be measured with a wavelength dispersive X-ray fluorescence analyzer.

[0074]

The measurement method is as follows. First, a glass batch (prepared by mixing glass raw material) or glass fiber (when organic matter adheres to the surface of the glass fiber, or when glass fiber is mainly included as a reinforcing material in organic matter (resin), the glass fiber is used after the organic matter is removed by, for example, heating for about 0.5 to 24 hours in a muffle furnace at 300 to 650°C) is placed in a platinum crucible, and in an electric furnace, melted with stirring while being held at 1550°C for 4 hours and 1650°C for 2 hours for the glass batch or melted with stirring while being held at a temperature of 1550°C for 6 hours for the glass fiber to obtain a homogeneous molten glass. Next, the obtained molten glass is poured onto a carbon plate to produce a glass cullet, and then pulverized and powdered into glass powder. Regarding Li as a light element, the resulting glass powder is thermally decomposed with an acid and then quantitatively analyzed using an ICP emission spectroscopic analyzer. Regarding other elements, the glass powder is molded into a disc shape by a pressing machine and then quantitatively analyzed using a wavelength dispersive X-ray fluorescence analyzer. For the quantitative analysis using a wavelength dispersive X-ray fluorescence analyzer, specifically, specimens for calibration curve are prepared based on the measurement results from the fundamental parameter method, and the analysis can be performed by the calibration curve method. The content of each component in the specimens for calibration curve can be quantitatively analyzed by an ICP emission spectroscopic analyzer. These quantitative analysis results are converted in terms of oxides to calculate the content of each component and the total amount, and the above content of each component can be determined from these numerical values.

[0075]

The glass composition for glass fiber of the present embodiment can be obtained by melting a glass raw material prepared to have the above composition after melt-solidification (glass batch) and then cooling to be solidified.

[0076]

When the glass fiber of the present embodiment is formed from the glass composition for glass fiber of the present embodiment, at first, the glass raw material prepared as described above is supplied to a glass melting furnace, and is melted at a temperature range of 1000 poise temperature or more, specifically, a temperature range of 1400 to 1700°C. The molten glass melted at the above temperature is then discharged from 1 to 8000 nozzle tips or holes controlled at a predetermined temperature and cooled while stretched by winding at high speed to be solidified into glass fiber.

[0077]

Glass single fiber (glass filament) discharged from one nozzle tip or hole, cooled and solidified typically has a perfect circle cross-sectional shape and has a diameter of 3.0 to 35.0 μm . In applications that require low dielectric properties, the glass filament preferably has a diameter of 3.0 to 6.0 μm and more preferably a diameter of 3.0 to 4.5 μm . On the other hand, when the above nozzle tip has a non-circular shape and has a protrusion or a notch for rapidly cooling the molten glass, controlling the temperature condition can provide a glass filament having a non-circular (for example, elliptical and long-oval) cross-sectional shape. When the glass filament has an elliptical or long-oval cross-sectional shape, the ratio of the major axis to the minor axis of the cross-sectional shape (major axis/minor axis) is, for example, in the range of 2.0 to 10.0 and the fiber diameter (converted fiber diameter) when the cross-sectional area is converted to a perfect circle is in the range of 3.0 to 35.0 μm .

[0078]

The glass fiber of the present embodiment typically has a shape of a glass fiber bundle (glass strand) in which 10 to 8000 glass filaments above are bundled, and has a weight in the range of 1 to 10000 tex (g/km). Glass filaments discharged from a plurality of nozzle tips or holes may be bundled into one glass fiber bundle or may be bundled into a plurality of glass fiber bundles.

[0079]

The glass fiber of the present embodiment can have various forms, which are obtained by further processing the above glass strands, such as yarns, woven fabrics, knitted fabrics, non-woven fabrics (including chopped strand mats and multiaxial non-woven fabrics), chopped strands, rovings, and powders.

[0080]

The glass fiber of the present embodiment may be coated with an organic matter on the surface thereof for the purposes such as improvement of glass filament convergence, improvement of adhesiveness between glass fiber and a resin, and improvement of uniform dispersibility of glass fiber in a mixture of glass fiber and resin or inorganic material. Examples of such an organic matter can include starch, urethane resins, epoxy resins, vinyl acetate resins, acrylic resins, modified polypropylene (particularly carboxylic acid-modified polypropylene), and a copolymer of (poly)carboxylic acid (particularly maleic acid) and an unsaturated monomer. The glass fiber of the present embodiment may be coated with the resin composition including a silane coupling agent, a lubricant, surfactant, and the like in addition to these resins. The glass fiber of the present embodiment may be coated with the treating agent composition not including the above resins and including a silane coupling agent, surfactant, and the like. Such a resin composition or treating agent composition covers the glass fiber at a rate of 0.03 to 2.0% by mass based on the mass of the glass fiber of the present embodiment in a state where it is not coated with the resin composition or the treating agent composition. The glass fiber can be coated with an organic matter by applying a resin solution or a resin composition solution to the glass fiber using a known method such as a roller applicator, for example, in the manufacturing process of the glass fiber and then drying the glass fiber to which the resin solution or the resin composition solution is applied. The glass fiber can be coated with an organic matter by immersing the glass fiber of the present embodiment in the form of a woven fabric in the treating agent composition solution and then drying the glass fiber to which the treating agent composition is applied.

[0081]

Here, examples of the silane coupling agent include aminosilanes, chlorosilanes, epoxysilanes, mercaptosilanes, vinylsilanes, and (meth)acrylsilanes.

[0082]

Examples of the aminosilane include γ -aminopropyltriethoxysilane, N- β -(aminoethyl)- γ -aminopropyltrimethoxysilane, N- β -(aminoethyl)-N'- β -(aminoethyl)- γ -aminopropyltrimethoxysilane, and γ -anilinopropyltrimethoxysilane.

[0083]

Examples of the chlorosilane include γ -chloropropyltrimethoxysilane.

[0084]

Examples of the epoxysilane include (β -(3,4-epoxycyclohexyl)ethyltrimethoxysilane and γ -glycidoxypropyltrimethoxysilane.

[0085]

Examples of the mercaptosilane can include γ -mercaptotrimethoxysilane.

[0086]

Examples of the vinylsilane include vinyl trimethoxysilane and N- β -(N-vinylbenzylaminoethyl)- γ -aminopropyltrimethoxysilane.

[0087]

Examples of the (meth)acrylsilane include γ -methacryloxypropyltrimethoxysilane.

[0088]

In the present embodiment, the silane coupling agents may be used singly or in combination of two or more.

[0089]

Examples of the lubricant include modified silicone oils, animal oils and hydrogenated products thereof, vegetable oils and hydrogenated products thereof, animal waxes, vegetable waxes, mineral waxes, condensates of a higher saturated fatty acid and a higher saturated alcohol, polyethyleneimine, polyalkylpolyamine alkylamide derivatives, fatty acid amides, and quaternary ammonium salts.

[0090]

Examples of the animal oil include beef tallow.

[0091]

Examples of the vegetable oil include soybean oil, coconut oil, rapeseed oil, palm oil, and castor oil.

[0092]

Examples of the animal wax include beeswax and lanolin.

[0093]

Examples of the vegetable wax include candelilla wax and carnauba wax.

[0094]

Examples of the mineral wax include paraffin wax and montan wax.

[0095]

Examples of the condensate of a higher saturated fatty acid and a higher saturated alcohol include stearates such as lauryl stearate.

[0096]

Examples of the fatty acid amide include dehydrated condensates of a polyethylenepolyamine such as diethylenetriamine, triethylenetetramine, or tetraethylenepentamine and a fatty acid such as lauric acid, myristic acid, palmitic acid, or stearic acid.

[0097]

Examples of the quaternary ammonium salt include alkyltrimethylammonium salts such as lauryltrimethylammonium chloride.

[0098]

In the present embodiment, the lubricants may be used singly or in combination of two or more.

[0099]

Examples of the surfactant can include nonionic surfactants, cationic surfactants, anionic surfactants, and amphoteric surfactants. In the present embodiment, the surfactants may be used singly or in combination of two or more.

[0100]

Examples of the nonionic surfactant can include ethylene oxide propylene oxide alkyl ether, polyoxyethylene alkyl ether, polyoxyethylene-polyoxypropylene-block copolymer, alkyl polyoxyethylene-polyoxypropylene block copolymer ether,

polyoxyethylene fatty acid ester, polyoxyethylene fatty acid monoester, polyoxyethylene fatty acid diester, polyoxyethylene sorbitan fatty acid ester, glycerol fatty acid ester ethylene oxide adduct, polyoxyethylene castor oil ether, hydrogenated castor oil ethylene oxide adduct, alkylamine ethylene oxide adduct, fatty acid amide ethylene oxide adduct, glycerol fatty acid ester, polyglycerol fatty acid ester, pentaerythritol fatty acid ester, sorbitol fatty acid ester, sorbitan fatty acid ester, sucrose fatty acid ester, polyhydric alcohol alkyl ether, fatty acid alkanolamide, acetylene glycol, acetylene alcohol, ethylene oxide adduct of acetylene glycol, and ethylene oxide adduct of acetylene alcohol.

[0101]

Examples of the cationic surfactant can include alkyl dimethylbenzylammonium chloride, alkyltrimethylammonium chloride, alkyl dimethyl ethyl ammonium ethyl sulfate, higher alkylamine salts (such as acetate and hydrochloride), adduct of ethylene oxide to a higher alkylamine, condensate of a higher fatty acid and polyalkylene polyamine, a salt of an ester of a higher fatty acid and alkanolamine, a salt of higher fatty acid amide, imidazoline cationic surfactant, and alkyl pyridinium salt.

[0102]

Examples of the anionic surfactant can include higher alcohol sulfate salts, higher alkyl ether sulfate salts, α -olefin sulfate salts, alkylbenzene sulfonate salts, α -olefin sulfonate salts, reaction products of fatty acid halide and N-methyl taurine, dialkyl sulfosuccinate salts, higher alcohol phosphate ester salts, and phosphate ester salts of higher alcohol ethylene oxide adduct.

[0103]

Examples of the amphoteric surfactant can include amino acid amphoteric surfactants such as alkali metal salts of alkylaminopropionic acid, betaine amphoteric surfactants such as alkyl dimethylbetaine, and imidazoline amphoteric surfactants.

[0104]

The glass fiber woven fabric of the present embodiment includes the above glass fiber of the present embodiment. Specifically, the glass fiber woven fabric of the present embodiment can be obtained by weaving the above glass fiber of the present embodiment as at least a part of warp yarns or weft yarns with a loom known per se. Examples of the

loom may include jet looms such as air jet or water jet looms, shuttle looms, and rapier looms. Examples of weaving with the loom may include plain weaving, satin weaving, mat weaving, and twill weaving. From the viewpoint of production efficiency, plain weaving is preferred. In the glass fiber woven fabric of the present embodiment, the above glass fiber of the present embodiment is preferably used as warp yarns and weft yarns.

[0105]

In the glass fiber woven fabric of the present embodiment, the above glass fiber of the present embodiment is preferably formed by bundling 35 to 400 glass filaments each having a filament diameter of 3.0 to 9.0 μm , has a number of twists of 0 to 1.0 twist/25 mm, and has a mass of 0.9 to 69.0 tex (g/km).

[0106]

In the glass fiber woven fabric of the present embodiment, when the above glass fiber of the present embodiment is employed as warp yarns or weft yarns, the warp yarn weaving density is preferably 40 to 120 yarns/25 mm, and the weft yarn weaving density is preferably 40 to 120 yarns/25 mm.

[0107]

The glass fiber woven fabric of the present embodiment, after woven, may be subjected to desizing treatment, surface treatment, and opening treatment.

[0108]

An example of the desizing treatment is a treatment including placing the glass fiber woven fabric in a heating oven having an atmosphere temperature of 350°C to 400°C for 40 to 80 hours to thereby pyrolytically decompose organic matter adhering to the glass fiber.

[0109]

An example of the surface treatment is a treatment including immersing the glass fiber woven fabric in a solution including the silane coupling agent or including the silane coupling agent and the surfactant, squeezing extra water therefrom, and heat-drying the woven fabric in a temperature range of 80 to 180°C for 1 to 30 minutes.

[0110]

An example of the opening treatment is a treatment in which the warp yarns of the glass fiber woven fabric are subjected to opening by means of water flow pressure, opening by means of high-frequency vibration using a liquid as a medium, opening by means of the pressure of a fluid having a surface pressure, opening by means of pressing with a roll, or the like under a tension of 30 to 200 N to thereby widen the width of the warp yarns and weft yarns.

[0111]

The glass fiber woven fabric of the present embodiment preferably has a mass per unit area in the range of 7.0 to 190.0 g/m² and preferably has a thickness in the range of 8.0 to 200.0 μm.

[0112]

The yarn width of the warp yarns of the glass fiber woven fabric of the present embodiment is preferably 110 to 600 μm and the yarn width of the weft yarns thereof is preferably 110 to 600 μm.

[0113]

The glass fiber woven fabric of the present embodiment may comprise a surface treatment layer including the silane coupling agent or the silane coupling agent and the surfactant. When the glass fiber woven fabric of the present embodiment includes the surface treatment layer, the surface treatment layer can have a mass in the range of 0.03 to 1.50% by mass, for example, with respect to the total amount of the glass fiber woven fabric including the surface treatment layer.

[0114]

The glass fiber-reinforced resin composition of the present embodiment includes the above glass fiber of the present embodiment. Specifically, the glass fiber-reinforced resin composition of the present embodiment includes 10 to 90% by mass of glass fiber with respect to the total amount of the glass fiber-reinforced resin composition, as the glass fiber-reinforced resin composition including resin (thermoplastic resin or thermosetting resin), glass fiber, and other additives. The glass fiber-reinforced resin composition of the present embodiment includes 90 to 10% by mass of a resin and includes other

additives in the range of 0 to 40% by mass with respect to the total amount of the glass fiber-reinforced resin composition.

[0115]

Examples of the above thermoplastic resin can include polyethylene, polypropylene, polystyrene, styrene/maleic anhydride resins, styrene/maleimide resins, polyacrylonitrile, acrylonitrile/styrene (AS) resins, acrylonitrile/butadiene/styrene (ABS) resins, chlorinated polyethylene/acrylonitrile/styrene (ACS) resins, acrylonitrile/ethylene/styrene (AES) resins, acrylonitrile/styrene/methyl acrylate (ASA) resins, styrene/acrylonitrile (SAN) resins, methacrylic resins, polyvinyl chloride (PVC), polyvinylidene chloride (PVDC), polyamide, polyacetal, polyethylene terephthalate (PET), polybutylene terephthalate (PBT), polytrimethylene terephthalate (PTT), polycarbonate, polyarylene sulfide, polyethersulfone (PES), polyphenylsulfone (PPSU), polyphenylene ether (PPE), modified polyphenylene ether (m-PPE), polyaryl etherketone, liquid crystal polymer (LCP), fluororesins, polyetherimide (PEI), polyarylate (PAR), polysulfone (PSF), polyamideimide (PAI), polyaminobismaleimide (PABM), thermoplastic polyimide (TPI), polyethylene naphthalate (PEN), ethylene/vinyl acetate (EVA) resins, ionomer (IO) resins, polybutadiene, styrene/butadiene resins, polybutylene, polymethylpentene, olefin/vinyl alcohol resins, cyclic olefin resins, cellulose resins, and polylactic acid.

[0116]

Specific examples of the polyethylene can include high density polyethylene (HDPE), medium density polyethylene, low density polyethylene (LDPE), linear low density polyethylene (LLDPE), and ultra high molecular weight polyethylene.

[0117]

Examples of the polypropylene can include isotactic polypropylene, atactic polypropylene, syndiotactic polypropylene, and mixtures thereof.

[0118]

Examples of the polystyrene can include general-purpose polystyrene (GPPS), which is an atactic polystyrene having an atactic structure, high impact polystyrene (HIPS) with a rubber component added to GPPS, and syndiotactic polystyrene with syndiotactic structure.

[0119]

Examples of the methacrylic resin can include polymers obtained by homopolymerizing one of acrylic acid, methacrylic acid, styrene, methyl acrylate, ethyl acrylate, ethyl methacrylate, butyl acrylate, butyl methacrylate, and fatty acid vinyl ester, or polymers obtained by copolymerizing two or more of these.

[0120]

Examples of the polyvinyl chloride can include a vinyl chloride homopolymer, a copolymer of a vinyl chloride monomer and a copolymerizable monomer, or a graft copolymer obtained by graft polymerization of a vinyl chloride monomer to polymer polymerized by a conventionally known method such as emulsion polymerization method, suspension polymerization method, micro suspension polymerization method, or bulk polymerization method.

[0121]

Examples of the polyamide can include one of components such as polycaproamide (nylon 6), polyhexamethylene adipamide (nylon 66), polytetramethylene adipamide (nylon 46), polytetramethylene sebacamide (nylon 410), polypentamethylene adipamide (nylon 56), polypentamethylene sebacamide (nylon 510), polyhexamethylene sebacamide (nylon 610), polyhexamethylene dodecamide (nylon 612), polydecamethylene adipamide (nylon 106), polydecamethylene sebacamide (nylon 1010), polydecamethylene dodecamide (Nylon 1012), polyundecanamide (Nylon 11), polyundecamethylene adipamide (Nylon 116), polydodecanamide (Nylon 12), polyxylylene adipamide (nylon XD6), polyxylylene sebacamide (nylon XD10), polymetaxylylene adipamide (nylon MXD6), polyparaxylylene adipamide (nylon PXD6), polytetramethylene terephthalamide (nylon 4T), polypentamethylene terephthalamide (nylon 5T), polyhexamethylene terephthalamide (nylon 6T), polyhexamethylene isophthalamide (nylon 6I), polynonamethylene terephthalamide (nylon 9T), polydecamethylene terephthalamide (nylon 10T), polyundecamethylene terephthalamide (nylon 11T), polydodecamethylene terephthalamide (nylon 12T), polytetramethylene isophthalamide (nylon 4I), polybis(3-methyl-4-aminohexyl) methane terephthalamide (nylon PACMT), polybis(3-methyl-4-aminohexyl) methane isophthalamide (nylon PACMI), polybis(3-methyl-4-aminohexyl)

methane dodecamide (nylon PACM12), and polybis(3-methyl-4-aminohexyl) methane tetradecamide (nylon PACM14) or copolymers or mixtures of two or more of the components.

[0122]

Examples of the polyacetal can include a homopolymer with oxymethylene units as the main repeating unit, and a copolymer mainly consisting of oxymethylene units and containing oxyalkylene units having 2 to 8 adjacent carbon atoms in the main chain.

[0123]

Examples of the polyethylene terephthalate can include a polymer obtained by polycondensation of terephthalic acid or a derivative thereof with ethylene glycol.

[0124]

Examples of the polybutylene terephthalate can include a polymer obtained by polycondensation of terephthalic acid or a derivative thereof with 1,4-butanediol.

[0125]

Examples of the polytrimethylene terephthalate can include polymers obtained by polycondensation of terephthalic acid or a derivative thereof with 1,3-propanediol.

[0126]

Examples of the polycarbonate can include polymers obtained by a transesterification method in which a dihydroxydiaryl compound is reacted with a carbonate such as diphenyl carbonate in a molten state; or polymers obtained by phosgene method in which a dihydroxyaryl compound is reacted with phosgene.

[0127]

Examples of the polyarylene sulfide can include linear polyphenylene sulfide, cross linked polyphenylene sulfide having a high molecular weight obtained by performing a curing reaction after polymerization, polyphenylene sulfide sulfone, polyphenylene sulfide ether, and polyphenylene sulfide ketone.

[0128]

Examples of the polyphenylene ether can include poly(2,3-dimethyl-6-ethyl-1,4-phenylene ether), poly(2-methyl-6-chloromethyl-1,4-phenylene ether), poly(2-methyl-6-hydroxyethyl-1,4-phenylene ether), poly(2-methyl-6-n-butyl-1,4-phenylene ether), poly(2-

ethyl-6-isopropyl-1,4-phenylene ether), poly(2-ethyl-6-n-propyl-1,4-phenylene ether), poly(2,3,6-trimethyl-1,4-phenylene ether), poly[2-(4'-methylphenyl)-1,4-phenylene ether], poly(2-bromo-6-phenyl-1,4-phenylene ether), poly(2-methyl-6-phenyl-1,4-phenylene ether), poly(2-phenyl-1,4-phenylene ether), poly(2-chloro-1,4-phenylene ether), poly(2-methyl-1,4-phenylene ether), poly(2-chloro-6-ethyl-1,4-phenylene ether), poly(2-chloro-6-bromo-1,4-phenylene ether), poly(2,6-di-n-propyl-1,4-phenylene ether), poly(2-methyl-6-isopropyl-1,4-phenylene ether), poly(2-chloro-6-methyl-1,4-phenylene ether), poly(2-methyl-6-ethyl-1,4-phenylene ether), poly(2,6-dibromo-1,4-phenylene ether), poly(2,6-dichloro-1,4-phenylene ether), poly(2,6-diethyl-1,4-phenylene ether), and poly(2,6-dimethyl-1,4-phenylene ether).

[0129]

Examples of the modified polyphenylene ether can include: a polymer alloy of poly(2,6-dimethyl-1,4-phenylene)ether and polystyrene; a polymer alloy of poly(2,6-dimethyl-1,4-phenylene)ether and a styrene/butadiene copolymer; a polymer alloy of poly(2,6-dimethyl-1,4-phenylene)ether and a styrene/maleic anhydride copolymer; a polymer alloy of poly(2,6-dimethyl-1,4-phenylene)ether and polyamide; a polymer alloy of poly(2,6-dimethyl-1,4-phenylene)ether and styrene/butadiene/acrylonitrile copolymer; one obtained by introducing a functional group such as an amino group, an epoxy group, a carboxy group, a styryl group, or the like at the polymer chain end of the polyphenylene ether; and one obtained by introducing a functional group such as an amino group, an epoxy group, a carboxy group, a styryl group, a methacryl group, or the like at the polymer chain side chain of the polyphenylene ether.

[0130]

Examples of the polyaryl etherketone can include polyetherketone (PEK), polyetheretherketone (PEEK), polyetherketoneketone (PEKK), and polyetheretherketoneketone (PEEKK).

[0131]

Examples of the liquid crystal polymer (LCP) can include a polymer (copolymer) consisting of one or more structural units selected from aromatic hydroxycarbonyl units

which are thermotropic liquid crystal polyesters, aromatic dihydroxy units, aromatic dicarbonyl units, aliphatic dihydroxy units, aliphatic dicarbonyl units, and the like.

[0132]

Examples of the fluororesin can include polytetrafluoroethylene (PTFE), perfluoroalkoxy resins (PFA), fluorinated ethylene propylene resins (FEP), fluorinated ethylene tetrafluoroethylene resins (ETFE), polyvinyl fluoride (PVF), polyvinylidene fluoride (PVDF), polychlorotrifluoroethylene (PCTFE), and ethylene/chlorotrifluoroethylene resin (ECTFE).

[0133]

Examples of the ionomer (IO) resin can include copolymers of an olefin or a styrene and an unsaturated carboxylic acid, wherein a part of carboxyl groups is neutralized with a metal ion.

[0134]

Examples of the olefin/vinyl alcohol resin can include ethylene/vinyl alcohol copolymers, propylene/vinyl alcohol copolymers, saponified products of ethylene/vinyl acetate copolymers, and saponified products of propylene/vinyl acetate copolymers.

[0135]

Examples of the cyclic olefin resin can include monocyclic compounds such as cyclohexene, polycyclic compounds such as tetracyclopentadiene, and polymers of cyclic olefin monomers.

[0136]

Examples of the polylactic acid can include poly-L-lactic acid which is a homopolymer of L-form, poly-D-lactic acid which is a homopolymer of D-form, or a stereocomplex polylactic acid which is a mixture thereof.

[0137]

Examples of the cellulose resin can include methylcellulose, ethyl cellulose, hydroxycellulose, hydroxymethylcellulose, hydroxyethyl cellulose, hydroxyethyl methylcellulose, hydroxypropylmethylcellulose, cellulose acetate, cellulose propionate, and cellulose butyrate.

[0138]

Examples of the above thermosetting resin can include unsaturated polyester resins, vinyl ester resins, epoxy (EP) resins, melamine (MF) resins, phenol resins (PF), urethane resins (PU), polyisocyanate, polyisocyanurate, polyimide (PI), urea (UF) resins, silicone (SI) resins, furan (FR) resins, benzoguanamine (BR) resins, alkyd resins, xylene resins, bismaleimide triazine (BT) resins, and diallyl phthalate resin (PDAP).

[0139]

Specific examples of the unsaturated polyester resin can include resin obtained by esterification reaction of aliphatic unsaturated dicarboxylic acid and aliphatic diol.

[0140]

Examples of the vinyl ester resin can include bis vinyl ester resins and novolac vinyl ester resins.

[0141]

Examples of the epoxy resin can include bisphenol A epoxy resins, bisphenol F epoxy resins, bisphenol E epoxy resins, bisphenol S epoxy resins, bisphenol M epoxy resins (4,4'-(1,3-phenylenediisopropylidene)bisphenol epoxy resins), bisphenol P epoxy resins (4,4'-(1,4-phenylenediisopropylidene)bisphenol epoxy resins), bisphenol Z epoxy resins (4,4'-cyclohexylidene bisphenol epoxy resins), phenol novolac epoxy resins, cresol novolac epoxy resins, tetraphenol group ethane novolac type epoxy resins, novolac epoxy resins having a condensed ring aromatic hydrocarbon structure, biphenyl epoxy resins, aralkyl epoxy resins such as xylylene epoxy resins and phenyl aralkyl epoxy resins, naphthylene ether epoxy resins, naphthol epoxy resins, naphthalene diol epoxy resins, bifunctional or tetrafunctional epoxy naphthalene resins, binaphthyl epoxy resins, naphthalene aralkyl epoxy resins, anthracene epoxy resins, phenoxy epoxy resins, dicyclopentadiene epoxy resins, norbornene epoxy resins, adamantane epoxy resins, and fluorene epoxy resins.

[0142]

Examples of the melamine resin can include a polymer formed by polycondensation of melamine (2,4,6-triamino-1,3,5-triazine) and formaldehyde.

[0143]

Examples of the phenolic resin can include novolac phenolic resins such as phenol novolac resins, cresol novolac resins, and bisphenol A novolac resins, resol phenol resins such as methylol resole resins and dimethylene ether resole resins, or aryl alkylene phenol resins, and include one of these or combinations of two or more.

[0144]

Examples of the urea resin can include a resin obtained by condensation of urea and formaldehyde.

[0145]

The above thermoplastic resin or the above thermosetting resin may be used singly or in combinations of two or more.

[0146]

The glass fiber-reinforced resin composition of the present embodiment is used in applications that require low dielectric properties. Thus, as the resin, preferred are epoxy resins, modified polyphenylene ethers, polybutylene terephthalate, polypropylene, fluorine resins, and liquid crystal polymer (LCP).

[0147]

Examples of the above other additives can include reinforcing fiber other than glass fiber (for example, carbon fiber and metal fiber), a filler other than glass fiber (for example, glass powder, talc, and mica), a flame retardant, an UV absorber, a heat stabilizer, an antioxidant, an antistatic agent, a fluidity improver, an anti-blocking agent, a lubricant, a nucleating agent, an antibacterial agent, and pigment.

[0148]

The glass fiber-reinforced resin composition of the present embodiment may be prepreg obtained by impregnating the glass fiber woven fabric of the present embodiment with the resin by a known method per se and semi-curing the woven fabric.

[0149]

The glass fiber-reinforced resin composition of the present embodiment can be molded by known molding methods such as injection molding method, injection compression molding method, two-color molding method, hollow molding method, foam molding method (including supercritical fluid), insert molding method, in-mold coating

molding method, extrusion molding method, sheet molding method, thermoforming method, rotational molding method, laminate molding method, press molding method, blow molding method, stamping molding method, infusion method, hand lay-up method, spray-up method, resin transfer molding method, sheet molding compound method, bulk molding compound method, pultrusion method, and filament winding method to obtain various glass fiber-reinforced resin molded products. Curing the prepreg can also provide glass fiber-reinforced resin molded products.

[0150]

Examples of applications of such molded products can include electronic device housing, electronic components, vehicle exterior members, vehicle interior members, vehicle engine members, muffler members, and high pressure tanks.

[0151]

Examples of the electronic components include printed wiring boards.

[0152]

Examples of the vehicle exterior members include bumpers, fenders, bonnets, air dams, and wheel covers.

[0153]

Examples of the vehicle interior members include door trims and ceiling materials.

[0154]

Examples of the vehicle engine members include oil pans, engine covers, intake manifolds, and exhaust manifolds.

[0155]

Examples of the muffler members include silencers.

[0156]

The glass fiber of the present embodiment can be suitably used as a reinforcing material for inorganic materials such as gypsum and cement, in addition to the glass fiber-reinforced resin composition of the present embodiment. For example, when used as a reinforcing material for gypsum (especially, gypsum board having a thickness of 4 to 60 mm), the glass fiber comprising the glass composition in the above range can be included in a range of 0.1 to 4.0% by mass with respect to the total mass of gypsum.

[0157]

Examples and Comparative Examples of the present invention will be shown.

Examples

[0158]

At first, glass raw material was mixed to obtain a glass batch so that the glass composition after melt-solidification was the composition of Examples 1 to 4 shown in Table 1 or Comparative Examples 1 to 10 shown in Tables 2 and 3.

[0159]

Next, the glass batch corresponding to the glass composition for glass fiber of Examples 1 to 4 or Comparative Examples 1 to 10 was placed in an 80 mm diameter platinum crucible, melted at 1550°C for 4 hours and at 1650°C for 2 hours, and taken out of the crucible to obtain homogeneous glass bulk or glass cullet. The obtained glass bulk or glass cullet was then annealed at 620°C for 8 hours to obtain a test piece. The dielectric constant and dielectric loss tangent of the obtained test piece were evaluated by the following methods. Additionally, the glass cullet obtained in the process of forming the test piece was used to evaluate the water resistance by the following method. The glass cullet obtained in the process of forming the test piece was used to calculate the working temperature range by the following method. The results of Examples 1 to 4 are shown in Table 1, the results of Comparative Examples 1 to 5 are shown in Table 2, and the results of Comparative Examples 6 to 10 are shown in Table 3.

[0160]

[Evaluation method of water resistance]

The glass cullet obtained as mentioned above was placed in a small cylindrical platinum bushing having a circular nozzle tip at the bottom thereof, and the bushing was heated to a predetermined temperature to melt the glass cullet. Then, the molten glass discharged through the nozzle tip was cooled and solidified while stretched by winding on a stainless collet at a predetermined speed to thereby obtain glass fiber comprising a perfect circular section and a fiber diameter of 13 μm . About 1 g of the obtained glass fiber (glass fiber for test) was collected from the collet and dried at 120°C for an hour, and

the mass (mass before operation) was measured. Then, the glass fiber for test was allowed to stand in distilled water of 100 ml at 80°C for 24 hours. Thereafter, the glass fiber for test was taken on metal mesh perforated with eyes of about 150 μm, washed with distilled water, and then dried at 120°C for an hour, and the mass (mass after operation) was measured.

[0161]

The mass reduction rate ($100 \times (1 - (\text{mass after operation} / \text{mass before operation}))$) was calculated from the mass before operation and mass after operation. Glass fiber of which the mass reduction rate was 2.0% or less and of which the components were not substantially eluted even in water was considered OK, and glass fiber of which the mass reduction rate was more than 2.0% and of which the components were greatly eluted in water was considered No Good.

[0162]

[Measurement method of dielectric constant and dielectric loss tangent]

The test piece was polished to prepare an 80 mm × 3 mm (1 mm thickness) polished test piece. The obtained polished test piece was completely dried and then stored in a room at 23°C and a humidity of 60% for 24 hours. Subsequently, for each of the obtained polished test pieces, according to JIS C 2565: 1992, the permittivity (dielectric constant Dk) and dielectric loss tangent (dissipation factor Df) at 10 GHz were measured using a cavity resonator method dielectric constant measuring apparatus ADMS01Oc1 (trade name), manufactured by AET, Inc.

[0163]

[Calculation method of working temperature range]

First, the glass cullet was melted in a platinum crucible using a high temperature electric furnace equipped with a rotational viscometer (manufactured by Shibaura Systems Co., Ltd.), and the viscosity of the molten glass was continuously measured using a Brookfield rotational viscometer while the melt temperature was varied. The temperature at which the rotational viscosity was 1000 poise was measured to determine the 1000 poise temperature.

[0164]

Then, the glass cullet was pulverized, 40 g of glass particles having a particle diameter of 0.5 to 1.5 mm was placed in a platinum boat of $180 \times 20 \times 15$ mm and heated in a tubular electric furnace provided with a temperature gradient of 1000 to 1400°C for 8 hours or more, then taken out of the tubular electric furnace, and observed with a polarized light microscope to identify the point at which crystals derived from glass (devitrification) began to precipitate. The temperature inside the tubular electric furnace was actually measured using a type B thermocouple to determine the temperature of the point at which the crystals began to precipitate, which temperature was taken as the liquid phase temperature.

[0165]

Then, from the difference between the 1000 poise temperature and the liquid phase temperature, the working temperature range was calculated.

[0166]

[Table 1]

	Example 1	Example 2	Example 3	Example 4
SiO ₂ (% by mass; SI)	62.20	60.50	59.30	59.70
B ₂ O ₃ (% by mass; B)	22.30	22.20	22.20	21.70
Al ₂ O ₃ (% by mass; A)	8.30	9.80	12.40	10.10
CaO (% by mass; C)	3.10	2.60	1.50	0
MgO (% by mass; M)	0	0	0	0
SrO (% by mass; SR)	0	0	0	4.60
TiO ₂ (% by mass; T)	3.10	4.10	4.10	3.10
F ₂ (% by mass)	1.00	0.80	0.50	0.80
Cl ₂ (% by mass)	0	0	0	0
F ₂ +Cl ₂ (% by mass; F)	1.00	0.80	0.50	0.80
P ₂ O ₅ (% by mass; P)	0	0	0	0
Na ₂ O+K ₂ O+Li ₂ O	0	0	0	0
ZrO ₂	0	0	0	0
Total	100.00	100.00	100.00	100.00
TiO ₂ /(CaO+MgO+SrO)	1.00	1.58	2.73	0.67
1000×A/SI ²	2.15	2.68	3.53	2.83
MgO/(CaO+SrO)	0	0	0	0
TiO ₂ /Al ₂ O ₃	0.37	0.42	0.33	0.31
$SI \times B^2 \times T^2 / [C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F]^{(1/2)} \times A^3]$	358.74	396.93	257.67	229.47
$\{2 \times (0.72 \times C + M + 0.39 \times SR - 1.06 \times F) \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7)\}$	2.32	1.95	1.09	1.85
Water resistance	OK	OK	OK	OK
Working temperature range (°C)	376	173	26	113
Dielectric constant	4.0	4.1	4.1	4.2
Dielectric loss tangent	0.0009	0.0010	0.0010	0.0011

[0167]

[Table 2]

	Comparative Example 1	Comparative Example 2	Comparative Example 3	Comparative Example 4	Comparative Example 5
SiO ₂ (% by mass; SI)	56.00	54.40	58.10	52.30	57.00
B ₂ O ₃ (% by mass; B)	33.70	31.20	26.50	31.20	26.50
Al ₂ O ₃ (% by mass; A)	6.20	6.20	6.20	6.20	9.30
CaO (% by mass; C)	3.10	3.10	1.00	3.10	2.90
MgO (% by mass; M)	0	0	1.00	0	0.20
SrO (% by mass; SR)	0	0	2.10	0	0
TiO ₂ (% by mass; T)	0	4.10	4.10	6.20	2.10
F ₂ (% by mass)	1.00	1.00	1.00	1.00	1.00
Cl ₂ (% by mass)	0	0	0	0	0
F ₂ +Cl ₂ (% by mass; F)	1.00	1.00	1.00	1.00	1.00
P ₂ O ₅ (% by mass; P)	0	0	0	0	0
Na ₂ O+K ₂ O+Li ₂ O	0	0	0	0	0
ZrO ₂	0	0	0	0	1.00
Total	100.00	100.00	100.00	100.00	100.00
TiO ₂ /(CaO+MgO+SrO)	0.00	1.32	1.00	2.00	0.68
1000×A/SI ²	1.98	2.10	1.84	2.27	2.86
MgO/(CaO+SrO)	0	0	0.32	0	0.07
TiO ₂ /Al ₂ O ₃	0.00	0.66	0.66	1.00	0.23
$SI \times B^2 \times T^2 / \{ [C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F]^{(1/2)} \times A^3 \}$	0.00	2577.45	-	5666.43	175.15
$\{ 2 \times (0.72 \times C + M + 0.39 \times SR - 1.06 \times F) \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \}$	2.40	2.37	2.78	2.36	2.41
Water resistance	No Good	No Good	No Good	No Good	No Good
Working temperature range (°C)	489	267	297	Not measurable due to occurrence of crystallization	226
Dielectric constant	3.8	3.9	4.0		3.8
Dielectric loss tangent	0.0007	0.0008	0.0010		0.0009

[0168]

[Table 3]

	Comparative Example 6	Comparative Example 7	Comparative Example 8	Comparative Example 9	Comparative Example 10
SiO ₂ (% by mass; SI)	57.40	58.80	59.30	59.70	60.50
B ₂ O ₃ (% by mass; B)	23.10	26.20	20.20	20.20	22.30
Al ₂ O ₃ (% by mass; A)	15.40	10.30	14.40	11.60	8.30
CaO (% by mass; C)	0	0.70	1.50	3.60	3.10
MgO (% by mass; M)	0	0	0	0	1.70
SrO (% by mass; SR)	0	1.40	0	0	0
TiO ₂ (% by mass; T)	4.10	2.10	4.10	4.10	3.10
F ₂ (% by mass)	0.00	0.50	0.50	0.50	1.00
Cl ₂ (% by mass)	0	0	0	0	0
F ₂ +Cl ₂ (% by mass; F)	0.00	0.50	0.50	0.50	1.00
P ₂ O ₅ (% by mass; P)	0	0	0	0.30	0
Na ₂ O+K ₂ O+Li ₂ O	0	0	0	0	0
ZrO ₂	0	0	0	0	0
Total	100.00	100.00	100.00	100.00	100.00
TiO ₂ /(CaO+MgO+SrO)	-	1.00	2.73	1.14	0.65
1000×A/SI ²	4.67	2.98	4.09	3.25	2.27
MgO/(CaO+SrO)	-	0	0	0	0.55
TiO ₂ /Al ₂ O ₃	0.27	0.20	0.28	0.35	0.37
$SI \times B^2 \times T^2 / \{ [C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F]^{(1/2)} \times A^3 \}$	-	177.64	136.22	149.00	-
$\{ 2 \times (0.72 \times C + M + 0.39 \times SR - 1.06 \times F) \times (B/1.2 + A/1.7 + P/1.3 + T/4.7) / (1.37 \times B/1.2 + 1.77 \times A/1.7 + 1.63 \times P/1.3 + 1.96 \times T/4.7) \}$	0.00	1.07	1.07	3.10	4.64
Water resistance	No Good	No Good	OK	OK	No Good
Working temperature range (°C)	Not measurable due to occurrence of phase separation	119	-36	228	218
Dielectric constant	4.0	3.9	4.2	4.3	4.1
Dielectric loss tangent	0.0010	0.0009	0.0012	0.0014	0.0012

[0169]

As can be seen from Table 1, according to the glass compositions for glass fiber of Examples 1 to 4, which include SiO₂ in the range of 59.00 to 65.00% by mass, B₂O₃ in the range of 16.00 to 26.00% by mass, Al₂O₃ in the range of 7.00 to 14.00% by mass, CaO in the range of 0 to 5.00% by mass, MgO in the range of 0 to 4.00% by mass, SrO in the range of 0 to 6.00% by mass, TiO₂ in the range of 0.10 to 5.00% by mass, and F₂ and Cl₂ in the range of 0 to 2.00% by mass in total, with respect to the total amount of the glass composition for glass fiber, and have a content of P₂O₅ of less than 0.20% by mass, a total content of Na₂O, K₂O, and Li₂O of less than 1.00% by mass and in which the ratio of the content of TiO₂ (% by mass) to the total content of CaO, MgO, and SrO (% by mass)

($\text{TiO}_2/(\text{CaO} + \text{MgO} + \text{SrO})$) is in the range of 0.66 to 4.00, and the content SI (% by mass) of SiO_2 and the content A (% by mass) of Al_2O_3 satisfy the formula (1), glass fiber having excellent water resistance and excellent dielectric characteristics, that is, a dielectric constant of 4.2 or less and a dielectric loss tangent of 0.0011 or less in a high-frequency region at a measurement frequency of 10 GHz can be obtained, and the glass compositions per se can have a sufficient working temperature range of 26°C or more.

[0170]

In contrast, as can be seen from Table 2, according to the glass composition for glass fiber of Comparative Example 1, in which the content of SiO_2 is less than 59.00% by mass, the content of B_2O_3 is more than 26.00% by mass, the content of Al_2O_3 is less than 7.00% by mass, and the content of TiO_2 is less than 0.10% by mass, with respect to the total amount of the glass composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained.

[0171]

It is clear that, also in the glass composition for glass fiber of Comparative Example 2, in which the content of SiO_2 is less than 59.00% by mass, the content of B_2O_3 is more than 26.00% by mass, and the content of Al_2O_3 is less than 7.00% by mass, with respect to the total amount of the glass composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained.

[0172]

It is clear that, also in the glass composition for glass fiber of Comparative Example 3, in which the content of SiO_2 is less than 59.00% by mass, the content of B_2O_3 is more than 26.00% by mass, and the content of Al_2O_3 is less than 7.00% by mass, with respect to the total amount of the glass composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained.

[0173]

It is clear that, in the glass composition for glass fiber of Comparative Example 4, in which the content of SiO_2 is less than 59.00% by mass, the content of B_2O_3 is more than 26.00% by mass, the content of Al_2O_3 is less than 7.00% by mass, and the content of TiO_2 is more than 5.00% by mass, with respect to the total amount of the glass

composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained, and moreover, crystallization occurs.

[0174]

It is clear that, also in the glass composition for glass fiber of Comparative Example 5, in which the content of SiO_2 is less than 59.00% by mass and the content of B_2O_3 is more than 26.00% by mass, with respect to the total amount of the glass composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained.

[0175]

As can be seen from Table 3, in the glass composition for glass fiber of Comparative Example 6, in which the content of SiO_2 is less than 59.00% by mass and the content of Al_2O_3 is more than 14.00% by mass with respect to the total amount of the glass composition for glass fiber, and the value of the formula (1) is more than 4.65, glass fiber having sufficient water resistance cannot be obtained, and moreover, phase separation occurs.

[0176]

It is clear that, also in the glass composition for glass fiber of Comparative Example 7, in which the content of SiO_2 is less than 59.00% by mass and the content of B_2O_3 is more than 26.00% by mass with respect to the total amount of the glass composition for glass fiber, glass fiber having sufficient water resistance cannot be obtained.

[0177]

It is clear that, according to the glass composition for glass fiber of Comparative Example 8, in which the content of Al_2O_3 is more than 14.00% by mass with respect to the total amount of the glass composition for glass fiber, the glass composition does not have a sufficient working temperature range, and glass fiber having a sufficiently low dielectric loss tangent in a high-frequency region at a measurement frequency of 10 GHz cannot be obtained.

[0178]

It is clear that, according to the glass composition for glass fiber of Comparative Example 9, in which the content of P_2O_5 is more than 0.20% by mass with respect to the total amount of the glass composition for glass fiber, glass fiber having a sufficiently low dielectric constant and a sufficiently low dielectric loss tangent in a high-frequency region at a measurement frequency of 10 GHz cannot be obtained.

[0179]

It is clear that, according to the glass composition for glass fiber of Comparative Example 10, in which the ratio of the content of TiO_2 (% by mass) to the total content of CaO , MgO , and SrO (% by mass) with respect to the total amount of the glass composition for glass fiber ($TiO_2/(CaO + MgO + SrO)$) is less than 0.66, glass fiber having sufficient water resistance and having a sufficiently low dielectric loss tangent in a high-frequency region at a measurement frequency of 10 GHz cannot be obtained.

Claims

[Claim 1]

A glass composition for glass fiber comprising:

SiO₂ in a range of 59.00 to 65.00% by mass,

B₂O₃ in a range of 16.00 to 26.00% by mass,

Al₂O₃ in a range of 7.00 to 14.00% by mass,

CaO in a range of 0 to 5.00% by mass,

MgO in a range of 0 to 4.00% by mass,

SrO in a range of 0 to 6.00% by mass,

TiO₂ in a range of 0.10 to 5.00% by mass, and

F₂ and Cl₂ in a range of 0 to 2.00% by mass in total, with respect to the total amount of the glass composition for glass fiber, and

having a content of P₂O₅ of less than 0.20% by mass and a total content of Na₂O, K₂O, and Li₂O of less than 1.00% by mass, wherein

a ratio of a content of TiO₂ (% by mass) to a total content of CaO, MgO, and SrO (% by mass) (TiO₂/(CaO + MgO + SrO)) is in a range of 0.66 to 4.00, and

a content SI (% by mass) of SiO₂ and a content A (% by mass) of Al₂O₃ satisfy following formula (1):

$$1.00 \leq 1000 \times A/SI^2 \leq 4.65 \quad (1).$$

[Claim 2]

The glass composition for glass fiber according to claim 1, wherein the content SI (% by mass) of SiO₂, a content B (% by mass) of B₂O₃, the content A (% by mass) of Al₂O₃, a content C (% by mass) of CaO, a content M (% by mass) of MgO, a content SR (% by mass) of SrO, a content T (% by mass) of TiO₂, and a total content F (% by mass) of F₂ and Cl₂ satisfy following formula (2):

$$204.00 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 422.40 \quad (2).$$

[Claim 3]

The glass composition for glass fiber according to claim 1, wherein the content SI (% by mass) of SiO₂, a content B (% by mass) of B₂O₃, the content A (% by mass) of

Al₂O₃, a content C (% by mass) of CaO, a content M (% by mass) of MgO, a content SR (% by mass) of SrO, a content T (% by mass) of TiO₂, and a total content F (% by mass) of F₂ and Cl₂ satisfy following formula (3):

$$244.00 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 410.00 \quad (3).$$

[Claim 4]

The glass composition for glass fiber according to claim 1, wherein the content SI (% by mass) of SiO₂, a content B (% by mass) of B₂O₃, the content A (% by mass) of Al₂O₃, a content C (% by mass) of CaO, a content M (% by mass) of MgO, a content SR (% by mass) of SrO, a content T (% by mass) of TiO₂, and a total content F (% by mass) of F₂ and Cl₂ satisfy following formula (4):

$$308.50 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 400.50 \quad (4).$$

[Claim 5]

The glass composition for glass fiber according to claim 1, wherein the content SI (% by mass) of SiO₂, a content B (% by mass) of B₂O₃, the content A (% by mass) of Al₂O₃, a content C (% by mass) of CaO, a content M (% by mass) of MgO, a content SR (% by mass) of SrO, a content T (% by mass) of TiO₂, and a total content F (% by mass) of F₂ and Cl₂ satisfy following formula (5):

$$339.60 \leq SI \times B^2 \times T^2 / [\{ C + (40.1/87.6) \times SR - (40.1/24.3) \times M - F \}^{1/2} \times A^3] \leq 377.80 \quad (5).$$

[Claim 6]

Glass fiber formed from the glass composition for glass fiber according to any one of claim 1 to claim 5.

[Claim 7]

A glass fiber woven fabric comprising the glass fiber according to claim 6.

[Claim 8]

A glass fiber-reinforced resin composition comprising the glass fiber according to claim 6.