

DESCRIPTION

Title of Invention

CEMENT ADMIXTURE, EXPANSION MATERIAL, AND CEMENT COMPOSITION

Technical Field

[0001]

The present invention relates to a cement admixture, an expansive material (an expansive additive), and a cement composition, which are, for example, used in the engineering and construction fields.

Background Art

[0002]

Reduction in crack of cement/concrete is important from the viewpoint of reliability, durability, beauties, etc., and more development of technologies regarding a cement admixture having an effect for improving them, namely a cement-based expansive material is desired.

[0003]

Some proposals have been offered of a concrete expansive material capable of developing excellent expansion characteristics in small amounts (PTL 1), an expansive material for cement in which the surface of free lime is coated with calcium carbonate (PTL 2), and so on. In addition, in recent years, a proposal has been offered of joint use of an expansive material and a shrinkage reducer (PTL 3).

Meanwhile, a proposal has been offered of a slaking-resistance calcia clinker composed of a solid solution of calcia and strontium oxide (PTL 4). Meanwhile, an expansive material capable of producing ettringite as an expansive component through reaction of tricalcium aluminate, gypsum, and water is known (NPL 1).

Citation List

Patent Literature

[0004]

PTL 1: Japanese Patent No. 4244261

PTL 2: JP 54-93020 A

PTL 3: JP 2003-12352 A

PTL 4: JP 57-205363 A

Non-Patent Literature

[0005]

NPL 1: "Symposium Committee Report on the High Performance/High Durability of Structures with Expanded Concrete (September 19, 2003)"

Summary of Invention

Technical Problem

[0006]

A conventional expansive material has a characteristic feature of expanding until a material age of 7 days. But, there was involved such a problem that the drying shrinkage behavior does not change much compared to the case of not admixing with the expansive material. In addition, though the joint use of the expansive material and the shrinkage reducer is effective for inhibition of drying shrinkage, there was involved such a problem that long-term strength development properties are decreased.

The slaking-resistant calcia clinker described in PTL 4 is aimed at use as a basic refractory raw material, but PTL 4 does not describe at all that it is used as an expansive material for the purpose of inhibiting crack of cement/concrete.

[0007]

From the above, an object of the present invention is to provide a cement admixture, an expansive material, and a cement composition, each permitting to give a large expansion to the cement/concrete over an initial material age after cement/concrete placement (for example, a material age of 2 to 7 days), to inhibit a drying shrinkage strain, and to inhibit a decrease of the long-term strength development properties.

Solution to Problem

[0008]

In view of the aforementioned problem, the present inventors made extensive and intensive investigations. As a result, it has been found that the foregoing problem can be solved by a cement admixture containing free lime

and a hydraulic compound and also containing SrO as a chemical component, thereby leading to accomplishment of the present invention. Specifically, the present invention is as follows.

[0009]

[1] A cement admixture containing free lime and a hydraulic compound and also containing SrO as a chemical compound, wherein

the content of the free lime is 10 to 98 parts by mass based on 100 parts by mass of the cement admixture.

[2] The cement admixture as set forth in [1], wherein the content of the SrO is 0.001 to 5.0 parts by mass based on 100 parts by mass of the cement admixture.

[3] The cement admixture as set forth in [1] or [2], further containing anhydrous gypsum.

[4] The cement admixture as set forth in any of [1] to [3], wherein the content of the free lime is 10 to 95 parts by mass based on 100 parts by mass of the cement admixture.

[5] The cement admixture as set forth in any of [1] to [4], further containing ZrO_2 as the chemical component.

[6] The cement admixture as set forth in [5], wherein the content of the ZrO_2 is 0.0001 to 5.0 parts by mass based on 100 parts by mass of the cement admixture.

[7] The cement admixture as set forth in any of [1] to [6], wherein a Braine's specific surface area is 2,000 to 6,000 cm^2/g .

[8] The cement admixture as set forth in any of [1] to [7], wherein the content rate of particles of 10 μm or less is 30 to 60% by volume on a basis of volume, and the ratio of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less (A/B) is 1.5 to 4.0.

[9] The cement admixture as set forth in any of [1] to [8], containing, as the hydraulic compound, one or more selected from the group consisting of $3\text{CaO}\cdot\text{Al}_2\text{O}_3$, $3\text{CaO}\cdot 3\text{Al}_2\text{O}_3\cdot\text{CaSO}_4$, $3\text{CaO}\cdot\text{SiO}_2$, $2\text{CaO}\cdot\text{SiO}_2$, $4\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, $6\text{CaO}\cdot 2\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, $6\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, and $2\text{CaO}\cdot\text{Fe}_2\text{O}_3$.

[10] The cement admixture as set forth in [9], wherein $3\text{CaO}\cdot\text{Al}_2\text{O}_3$ is contained as the hydraulic compound.

[11] An expansive material composed of the cement admixture as set forth in any of [1] to [10].

[12] A cement composition containing the cement admixture as set forth in any of [1] to [10].

Advantageous Effects of Invention

[0010]

In accordance with the present invention, it is possible to aim at providing a cement admixture, an expansive material, and a cement composition, each permitting to give a large expansion to the cement/concrete over an initial material age after cement/concrete placement (for example, a material age of 2 to 7 days), to inhibit a drying shrinkage strain, and to inhibit a decrease of the long-term strength development properties.

Description of Embodiments

[0011]

The cement admixture, the expansive material, and the cement composition according to the embodiments of the present invention are hereunder described.

The terms "parts" and "%" used in this specification are on a mass basis unless specifically prescribed. In addition, the "cement/concrete" as referred to in the present invention is a general term of cement pastes, cement mortars, and cement concretes.

[0012]

[1. Cement Admixture and Expansive Material]

The cement admixture according to an embodiment of the present invention contains free lime and a hydraulic compound and also contains SrO as a chemical component. Alternatively, the cement mixture according to an embodiment of the present invention contains free lime, a hydraulic compound, and anhydrous gypsum and also contains SrO as a chemical component. In the case of referring to "100 parts of the cement admixture" on the occasion of describing the content of each component, it basically refers to "100 parts of the total of the free lime and the hydraulic compound", and on the occasion of containing the anhydrous gypsum, it refers to "100 parts of the total of the free lime, the hydraulic compound, and the anhydrous gypsum".

[0013]

(Free Lime)

The free lime is one typically called "f-CaO (free lime)". In view of the fact that the free lime is contained in the cement admixture according to an embodiment of the present invention, the expansion characteristics are given, and as a result, the drying shrinkage is inhibited.

The content of the free lime is preferably 10 to 98 parts, more preferably 10 to 95 parts, and still more preferably 40 to 90 parts based on 100 parts of the cement admixture. When the content of the free lime is 10 to 98 parts, the effect for inhibiting the drying shrinkage can be developed without causing a decrease of the long-term strength development properties.

In firing on the occasion of preparing the cement admixture, by increasing the firing temperature, or appropriately adjusting the blending amounts and particle sizes of charged raw materials other than the CaO raw material, the crystal particle diameter of the free lime in the cement admixture can be made large, or the content of the free lime can be increased.

[0014]

(Hydraulic Compound)

The hydraulic compound according to an embodiment of the present invention refers to $3\text{CaO}\cdot\text{Al}_2\text{O}_3$ (abbreviated as " C_3A "), ye'elinite expressed by $3\text{CaO}\cdot 3\text{Al}_2\text{O}_3\cdot\text{CaSO}_4$, $3\text{CaO}\cdot\text{SiO}_2$ (abbreviated as " C_3S "), calcium silicate expressed by $2\text{CaO}\cdot\text{SiO}_2$ (abbreviated as " C_2S "), $4\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$ (abbreviated as " C_4AF "), $6\text{CaO}\cdot 2\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$ (abbreviated as " $\text{C}_6\text{A}_2\text{F}$ "), calcium aluminoferrite expressed by $6\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, (abbreviated as " C_6AF "), calcium ferrite expressed by $2\text{CaO}\cdot\text{Fe}_2\text{O}_3$ (abbreviated as " C_2F "), or the like. Of these, one or more of thereof are preferably contained. Above all, one or more of C_3A , ye'elinite (especially $3\text{CaO}\cdot 3\text{Al}_2\text{O}_3\cdot\text{CaSO}_4$), C_4AF , and C_2S are preferably contained, and C_3A is more preferably contained.

In particular, when C_3A is contained, sintering of f-CaO can be promoted. From the viewpoint of promoting the sintering, the content of C_3A in the hydraulic compound is preferably 0.5 to 60% by mass, and more preferably 1 to 55% by mass. Although the C_3A includes cubic- C_3A and orthorhombic- C_3A which are different from each other in the crystal structure due to a difference of the alkali content, the C_3A in this specification means both or either one of cubic- C_3A and orthorhombic- C_3A .

[0015]

The content of the hydraulic compound is preferably 2 to 45 parts, more

preferably 5 to 30 parts, and still more preferably 7 to 20 parts based on 100 parts of the cement admixture. When the content of the hydraulic compound is 2 to 45 parts, high expansion characteristics can be given.

[0016]

(Anhydrous Gypsum)

Although the anhydrous gypsum is an arbitrary component, when added, the content of the anhydrous gypsum is preferably 3 to 50 parts, more preferably 10 to 40 parts, and still more preferably 20 to 30 parts based on 100 parts of the cement admixture.

In the case where the content of the anhydrous gypsum in the cement admixture is small, anhydrous gypsum can be separately added in an amount ranging from 3 to 50 parts based on 100 parts of the cement admixture.

[0017]

(SrO)

The cement admixture according to an embodiment of the present invention contains SrO as the chemical component. When a fixed amount of SrO is solid-solved in the cement admixture (or the expansive material), it is possible to reduce the drying shrinkage (on or after a material age of 7 days). In addition, it is also possible to improve the storage stability.

[0018]

The content of SrO is preferably 0.001 to 5.0 parts by mass, more preferably 0.001 to 0.5 parts by mass, and still more preferably 0.005 to 0.5 parts by mass based on 100 parts by mass of the cement admixture. In particular, when the content of SrO is 0.001 to 0.5 parts by mass, the effect for reducing the drying shrinkage becomes more favorable.

[0019]

(Other Component)

It is preferred that the cement admixture according to an embodiment of the present invention further contains ZrO_2 as the chemical component. The content of ZrO_2 is preferably 0.0001 to 5.0 parts by mass, more preferably 0.0001 to 0.1 parts by mass, and still more preferably 0.0003 to 0.05 parts by mass. In particular, when the content of ZrO_2 is 0.0001 to 0.1 parts by mass, the fluidity can be improved.

[0020]

A Braine's specific surface area of the cement admixture according to an

embodiment of the present invention is preferably 2,000 to 6,000 cm²/g, and more preferably 2,500 to 5,000 cm²/g. When the Braine's specific surface area is 2,000 to 6,000 cm²/g, the breakdown of the concrete structure to be caused due to expansion over an extended period of time can be prevented from occurring, and the expansion performance can be maintained favorable.

The Braine's specific surface area value in this specification can be determined in conformity with JIS R5201 (Physical Test Method for Cement).
[0021]

From the viewpoint of reduction of a slump loss, assurance of the amount of expansion with a small addition amount, and prevention of pop-out prevention, it is preferred that the content rate of particles of 10 μm or less is 30 to 60% by volume on a basis of volume, and the ratio of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less (A/B) is 1.5 to 4.0. It is more preferred that the content rate of particles of 10 μm or less is 20 to 60% by mass, and the ratio of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less (A/B) is 1.8 to 3.0.

The content rate of particles in this specification is calculated on the basis of particle size distribution resulting from ultrasonically dispersing the cement admixture in ethanol for 1 minute by using a laser diffraction/scattering particle size distribution measuring device and then performing the measurement on a volume basis under conditions at a sample refractive index of 1.770 and at a dispersion medium refractive index of 1.360.

The cement admixture of the present invention is obtained by appropriately mixing a CaO raw material, an Al₂O₃ raw material, an Fe₂O₃ raw material, an SiO₂ raw material, a CaSO₄ raw material, an SrO raw material, and a ZrO₂ raw material and then firing the mixture.

[0022]

Examples of the CaO raw material include lime stone and slaked lime; examples of the Al₂O₃ raw material include bauxite and aluminum ashes; examples of the Fe₂O₃ raw material include copper slag and commercially available iron oxide; examples of the SiO₂ raw material include silica stone; and examples of the CaSO₄ raw material include gypsum dihydrate, gypsum hemihydrate, and anhydrous gypsum.

[0023]

Although the SrO raw material is not particularly restricted, examples thereof include celestite, strontianite, strontium oxide, and strontium carbonate.

Although the ZrO₂ raw material is not particularly restricted, examples thereof include zirconium oxide, zirconium hydroxide, zirconium carbonate, zirconium oxychloride, zirconium sulfate, zirconium acetate, organic acid zirconium, and zircon sand.

In the case where SrO or ZrO₂ is contained in the CaO raw material, the Al₂O₃ raw material, the SiO₂ raw material, or the CaSO₄ raw material, it is not needed to newly add the SrO raw material or the ZrO₂ raw material.

[0024]

Although impurities are occasionally contained in these raw materials, such does not matter within a range where the effects of the present invention are not impaired. Examples of the impurities include MgO, TiO₂, MnO, P₂O₅, Na₂O, K₂O, Li₂O, sulfur, fluorine, and chlorine.

[0025]

The cement admixture can be produced by blending the aforementioned raw materials so as to attain the desired mineral composition and also the desired chemical composition regarding SrO and appropriately performing pulverization, etc., followed by firing.

Although the firing method is not particularly restricted, the firing is performed using an electric furnace, a kiln, or the like at a temperature of preferably 1,100 to 1,600°C, and more preferably 1,200 to 1,500°C. When the firing temperature is lower than 1,100°C, the expansion performance is not satisfactory, whereas when it is higher than 1,600°C, the anhydrous gypsum is occasionally decomposed.

In the case of performing the pulverization, it is preferred to perform the pulverization by a known method such that the Braine's specific surface area is 2,000 to 6,000 cm²/g.

[0026]

The content of the minerals in the thus prepared cement admixture can be confirmed by a conventionally general analysis method. For example, the minerals can be quantitatively determined by setting a pulverized sample on a powder X-ray diffraction device, thereby confirming the produced minerals and also analyzing data by the Rietveld method. In addition, the amounts of the

minerals can be determined through calculation on the basis of the identification results of the chemical components and the powder X-ray diffraction analyst. In an embodiment of the present invention, it is preferred to determine the amounts of the minerals through calculation on the basis of the identification results of the chemical components and powder X-ray diffraction analysis.

The contents of the chemical components can be determined with fluorescent X-rays.

[0027]

The cement admixture according to an embodiment of the present invention preferably contains particles in which the free lime, the hydraulic compound, the anhydrous gypsum, and SrO are present in the same particle. In addition, in the case where the cement admixture contains ZrO_2 , it is also preferred that this is present in the same particle.

Whether or not the free lime, the hydraulic compound, the anhydrous gypsum, and SrO, and further ZrO_2 are present in the same particle can be confirmed with an electron microscope or the like. Specifically, whether or not the free lime, the hydraulic compound, the anhydrous gypsum, and SrO, and further ZrO_2 are present in the same particle can be confirmed by wrapping and embedding the cement admixture with a resin, performing a surface treatment with an argon ion beam, and not only observing the structure of the cross section of the particle but also performing an elemental analysis.

[0028]

The foregoing cement admixture according to an embodiment of the present invention is preferably used as, for example, an expansive material. That is, the expansive material according to an embodiment of the present invention is composed of the already-mentioned cement admixture. According to this, it is permitted to give a large expansion to the concrete over an initial material age after concrete placement (for example, a material age of 2 to 7 days), to inhibit a drying shrinkage strain, and to inhibit a decrease of the long-term strength development properties.

[0029]

[3. Cement Composition]

The cement composition according an embodiment of the present invention is one containing the already-mentioned cement admixture. Here,

examples of the cement to be used in the cement composition include various Portland cements, such as normal, high-early-strength, ultra-high-early-strength, low heat, and moderate heat Portland cements; various mixed cements having blast furnace slag, fly ash, or silica mixed in such a Portland cement; filler cements having a limestone powder, an air-cooled blast furnace slag fine powder, etc. mixed therein; and Portland cements, such as an environmentally friendly cement (eco-cement) produced using, as the raw material, an urban refuse incineration ash or a sewage sludge incineration ash. These can be used alone or in combination of two or more thereof. The cement admixture may be the expansive material according to an embodiment of the present invention.

[0030]

In an embodiment according to the present invention, the cement and the cement admixture as well as fine aggregate, such as sand, and coarse aggregates, such as gravel, may be used in combination with one or more selected from the group consisting of a high-early strengthening agent, a rapid-hardening mortar-accelerator, a water-reducing agent, an AE water-reducing agent, a high-performance water-reducing agent, a high-performance AE water-reducing agent, a fluidizing agent, a defoaming agent, a thickening agent, a rustproofing agent, an anti-freezing agent, a shrinkage-reducing agent, a coagulation-reducing agent, an inhibitor for heat of hydration, a polymer emulsion, a clay mineral, such as bentonite, an anion exchanger such as hydrotalcite, a slag, such as a granulated blast furnace slag fine powder and an air-cooled blast furnace slag fine powder, and an admixture, such as a limestone fine powder, a siliceous fine powder, gypsum, and calcium silicate, within a range where the object of the present invention is not substantially impaired. In addition, it is possible to use, as an organic material, fibrous materials, such as a vinylon fiber, an acrylic fiber, and a carbon fiber, in combination.

[0031]

Since the use amount (blending amount) of the cement admixture (or the expansive material) varies depending upon blending of the concrete, it is not particularly restricted. However, in general, it is preferably 3 to 12 parts by mass, and more preferably 4 to 7 parts by mass in 100 parts by mass of the cement composition containing the cement and the cement admixture (or the

expansive material). When it is 3 parts by mass or more, a sufficient expansion performance is obtained. In addition, when it is 12 parts by mass or less, over-expansion is not caused, and the generation of expansive cracks in the concrete can be prevented from occurring.

Examples

[0032]

[Experimental Example A-1]

A CaO raw material, an Al₂O₃ raw material, an Fe₂O₃ raw material, an SiO₂ raw material, a CaSO₄ raw material, and an SrO raw material were blended in a mineral proportion and a proportion as the chemical component as shown in Table 1, and after mixing and pulverizing, the resultant was fired at 1,350°C to synthesize a clinker. The clinker was then pulverized using a ball mill to an extent of a Braine's specific surface area of 3,000 cm²/g to prepare a cement admixture.

Using this cement admixture, 7 parts by mass of the cement admixture was used in 100 parts by mass of a cement composition composed of cement and the cement admixture, to prepare a mortar having a water/cement composition ratio of 50% by mass and a cement composition/sand ratio of 1/3 (mass ratio) in a room at 20°C. Then, the mortar was measured in terms of a percent length change and compressive strength.

In addition, with respect to the cement admixture, a ratio (A/B) of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less was determined.

[0033]

(Used Materials)

CaO raw material: Limestone

Al₂O₃ raw material: Bauxite

Fe₂O₃ raw material: Iron oxide

SiO₂ raw material: Silica stone

CaSO₄ raw material: Gypsum dihydrate

SrO raw material: Strontianite

ZrO₂ raw material: Zircon sand

Sand: JIS standard sand

Cement: Commercially available normal Portland cement

[0034]

(Test Method)

Chemical composition: Determined with fluorescent X-ray.

Ratio (A/B) of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less: A laser diffraction/scattering particle size distribution measuring device, LA-920, manufactured by HORIBA, Ltd. was used. The cement admixture was ultrasonically dispersed in ethanol for 1 minute, and the particle size distribution on a volume basis under conditions at a sample refractive index of 1.770 and at a dispersion medium refractive index of 1.360 was measured. From such particle size distribution, the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less were determined, and the ratio A/B was calculated.

Mineral composition: Determined from calculation on a basis of the identification results of the chemical composition and the powder X-ray diffraction.

Compressive strength: A test piece of $4 \times 4 \times 16$ cm was prepared and measured for the compressive strength at the material ages of 7 days (7d) and 28 days (28d) in conformity with JIS R5201.

[0035]

Table 1

Experiment No.	Cement admixture											Addition ratio of expansive material (parts)	Percent length change (μ)			Compressive strength (N/mm ²)		Remarks
	Mineral composition (parts)					Chemical composition		Braine's specific surface area (cm ² /g)	A/B	0d	7d		28d	Difference from 7d until 28d	7d	28d		
	Hydraulic compound					SrO												
	Free lime	Ye'elimite	C4AF	C2S	Total		CaSO ₄											
1-1	10	31	5	4	40	50	0.010	3000	2.1	7	0	190	-50	-240	34.2	51.4	Example	
1-2	10	32	7	11	50	45	0.010	3000	2.1	7	0	190	-50	-240	34.2	51.4	Example	
1-3	20	30	2	3	35	45	0.010	3000	2.1	7	0	245	0	-245	33.9	51.0	Example	
1-4	40	20	5	5	30	30	0.010	3000	2.1	7	0	435	300	-135	32.8	50.2	Example	
1-5	50	10	5	5	20	30	0.001	3000	2.1	7	0	455	240	-215	32.7	49.2	Example	
1-6	50	10	5	5	20	30	0.010	3000	2.1	7	0	452	300	-152	32.7	49.4	Example	
1-7	50	10	5	5	20	30	0.500	3000	2.1	7	0	445	330	-115	32.8	49.3	Example	
1-8	50	5	0	25	30	20	0.010	3000	2.1	7	0	423	350	-73	32.8	48.7	Example	
1-9	60	5	0	5	10	30	0.010	3000	2.1	7	0	522	400	-122	32.3	48.3	Example	
1-10	90	1	2	2	5	5	0.010	3000	2.1	7	0	1000	780	-220	29.1	48.4	Example	
1-11	95	0	1	1	2	3	0.010	3000	2.1	7	0	1200	900	-300	27.7	48.1	Example	
1-12	95	0	2	2	4	1	0.010	3000	2.1	7	0	1271	1000	-271	27.2	48.2	Example	
1-13	56	2	2	10	14	30	0.010	3000	2.1	7	0	452	300	-152	32.7	49.2	Example	
1-14	100	0	0	0	0	0	0.000	3000	2.1	4	0	449	0	-449	32.7	42.0	Comparative Example	
1-15	100	0	0	0	0	0	0.000	3000	2.1	7	0	2005	1000	-1005	21.4	39.3	Comparative Example	
1-16	100	0	0	0	0	0	0.010	3000	2.1	4	0	475	100	-375	32.5	34.5	Comparative Example	
1-17	100	0	0	0	0	0	0.010	3000	2.1	7	0	2800	1400	-1400	14.1	31.9	Comparative Example	
1-18	10	32	7	11	50	45	0.000	3000	2.1	7	0	183	-150	-333	34.2	51.4	Comparative Example	
1-19	20	30	2	3	35	45	0.000	3000	2.1	7	0	245	0	-245	33.9	51.0	Comparative Example	
1-20	50	10	5	5	20	30	0.000	3000	2.1	7	0	456	140	-316	32.7	47.0	Comparative Example	
1-21	70	10	5	5	20	10	0.000	3000	2.1	7	0	1250	250	-1000	27.4	40.8	Comparative Example	
1-22	50	10	5	5	20	30	0.000	3000	2.1	7	0	493	170	-323	32.4	47.1	Comparative Example	

[0036]

[Experimental Example A-2]

The same experiment as in Experiment 1 was performed, except that in Experiment No. 1-6, a ZrO_2 raw material was used, and the amount of SrO was adjusted, thereby changing the SrO amount and the ZrO_2 amount in the clinker as shown in the following Table 2. The results are shown in Table 2.

(Test Method)

Flow test: The mortar was kneaded in conformity with JIS R5201-2015 "Physical Test Method for Cement", and just after kneading, 15-point flow values were measured. Temperature, humidity, and mortar blending were the same as those in the compressive strength testing. Standard sand was used for testing.

[0037]

Table 2

Experiment No.	Cement admixture										Addition ratio of expansive material (parts)	Evaluation						Remarks		
	Mineral composition (parts)					Braine's specific surface area (cm ² /g)	A/B	Flow test		Percent length change (μ)										
	Hydraulic compound																			
	Free lime	Ye'elimitite	C4AF	C2S	Total									CaSO ₄	Chemical composition					
												</								

[0038]

[Experimental Example B-1]

A CaO raw material, an Al₂O₃ raw material, an Fe₂O₃ raw material, an SiO₂ raw material, and an SrO raw material were blended in a mineral proportion and a proportion as the chemical component as shown in Table 3, and after mixing and pulverizing, the resultant was fired at 1,350°C to synthesize a clinker. The clinker was then pulverized using a ball mill to an extent of a Braine's specific surface area of 3,500 cm²/g to prepare a cement admixture.

Using this cement admixture, 4 or 7 parts by mass of the cement admixture was used in 100 parts by mass of a cement composition composed of cement and the cement admixture, to prepare a mortar having a water/cement composition ratio of 50% by mass and a cement composition/sand ratio of 1/3 (mass ratio) in a room at 20°C. Then, the mortar was measured in terms of a percent length change and compressive strength.

In addition, with respect to the cement admixture, a ratio (A/B) of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less was determined.

[0039]

(Used Materials)

CaO raw material: Limestone

Al₂O₃ raw material: Bauxite

Fe₂O₃ raw material: Iron oxide

SiO₂ raw material: Silica stone

CaSO₄ raw material: Natural anhydrous gypsum

SrO raw material: Strontianite

ZrO₂ raw material: Zircon sand

Sand: JIS standard sand

Cement: Commercially available normal Portland cement

[0040]

(Test Method)

Chemical composition: Determined with fluorescent X-ray

Ratio (A/B) of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less: A laser diffraction/scattering particle size distribution measuring device, LA-920, manufactured by HORIBA,

Ltd. was used. The cement admixture was ultrasonically dispersed in ethanol for 1 minute, and the particle size distribution on a volume basis under conditions at a sample refractive index of 1.770 and at a dispersion medium refractive index of 1.360 was measured. From such particle size distribution, the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less were determined, and the ratio A/B was calculated.

Mineral composition: Determined from calculation on a basis of the identification results of the chemical composition and the powder X-ray diffraction.

Percent length change: Measured at the material ages of 7 days (7d) and 28 days (28d) in conformity with JIS A6202.

Compressive strength: A test piece of $4 \times 4 \times 16$ cm was prepared and measured for the compressive strength at the material ages of 7 days (7d) and 28 days (28d) in conformity with JIS R5201.

[0041]

Table 3

Experiment No.	Cement admixture											Addition ratio of expansive material (parts)	Percent length change (× 10 ⁻⁶)				Compressive strength (N/mm ²)		Remarks
	Mineral composition (parts)					Chemical composition		Braine's specific surface area (cm ² /g)	A/B	0d	7d		28d	Difference from 7d until 28d	7d	28d			
	Hydraulic compound					SrO													
	Ye'elite	C3A	C2S	Total	CaSO ₄														
1-1	20	62	10	8	80	0	0.010	3,500	2.1	7	0	240	-10	-250	34.2	51.4	Example		
1-2	17	53	12	18	83	0	0.010	3,500	2.1	7	0	243	-10	-253	34.2	51.4	Example		
1-3	36	55	4	5	64	0	0.010	3,500	2.1	7	0	288	40	-248	33.9	51.0	Example		
1-4	57	29	7	7	43	0	0.010	3,500	2.1	7	0	479	340	-139	32.8	50.2	Example		
1-5	71	14	7	7	29	0	0.001	3,500	2.1	7	0	500	280	-220	32.7	49.2	Example		
1-6	71	14	7	7	29	0	0.010	3,500	2.1	7	0	494	345	-156	32.7	49.4	Example		
1-7	71	14	7	7	29	0	0.500	3,500	2.1	7	0	499	371	-128	32.8	49.3	Example		
1-8	63	6	0	31	38	0	0.010	3,500	2.1	7	0	460	390	-70	32.8	48.7	Example		
1-9	86	7	0	7	14	0	0.010	3,500	2.1	7	0	574	442	-132	32.3	48.3	Example		
1-10	95	1	2	2	5	0	0.010	3,500	2.1	7	0	1,040	820	-220	29.1	48.4	Example		
1-11	98	0	1	1	2	0	0.010	3,500	2.1	7	0	1,242	843	-399	27.7	48.1	Example		
1-12	90	0	5	5	10	0	0.010	3,500	2.1	7	0	1,400	1,045	-355	27.2	48.2	Example		
1-13	80	3	3	14	20	0	0.010	3,500	2.1	7	0	501	341	-160	32.7	49.2	Example		
1-14	100	0	0	0	0	0	0.000	3,500	2.1	4	0	500	40	-460	32.7	42.0	Comparative Example		
1-15	100	0	0	0	0	0	0.000	3,500	2.1	7	0	2,050	1,042	-1,008	21.4	39.3	Comparative Example		
1-16	100	0	0	0	0	0	0.010	3,500	2.1	4	0	510	141	-369	32.5	34.5	Comparative Example		
1-17	100	0	0	0	0	0	0.010	3,500	2.1	7	0	2,850	1,442	-1,408	14.1	31.9	Comparative Example		
1-18	10	32	7	11	50	45	0.000	3,500	2.1	7	0	220	-111	-333	34.2	51.4	Comparative Example		
1-19	20	30	2	3	35	45	0.000	3,500	2.1	7	0	300	41	-259	33.9	51.0	Comparative Example		
1-20	50	10	5	5	20	30	0.000	3,500	2.1	7	0	496	181	-315	32.7	47.0	Comparative Example		
1-21	70	10	5	5	20	10	0.000	3,500	2.1	7	0	1,300	291	-1,009	27.4	40.8	Comparative Example		
1-22	50	10	5	5	20	30	0.000	3,500	2.1	7	0	530	210	-320	32.4	47.1	Comparative Example		

[0042]

[Experimental Example B-2]

The same experiment as in Experiment B-1 was performed, except that in Experiment No. 1-12, a ZrO_2 raw material was used, and the amount of SrO was adjusted, thereby changing the SrO amount and the ZrO_2 amount in the clinker as shown in the following Table 4. The results are shown in Table 4.

[0043]

(Test Method)

Flow test: The mortar was kneaded in conformity with JIS R5201-2015 "Physical Test Method for Cement", and just after kneading (0 min) and 60 minutes elapsing after kneading, 15-point flow values were measured. Temperature, humidity, and mortar blending were the same as those in the compressive strength testing. Standard sand was used for testing.

[0044]

Table 4

Experiment No.	Cement admixture										Addition ratio of expansive material (parts)	Evaluation					Remarks		
	Mineral composition (parts)					Chemical composition						Flow test (mm)	Percent length change ($\times 10^{-6}$)			Compressive strength (N/mm ²)			
	Hydraulic compound					Total	SiO ₂	ZrO ₂	Braine's specific surface area (cm ² /g)	A/B									
	Free lime	Ye'elimite	C3A	C2S															
1-12	90	0	5	5	10	10	0.010	0.0000	2.1	3.500	7	180	160	1400	1045	-355	7d	28d	Example
2-1	90	0	5	5	10	10	0.001	0.0001	2.1	3.500	7	185	175	1402	1066	-336	27.4	49.2	Example
2-2	90	0	5	5	10	10	0.010	0.0001	2.1	3.500	7	190	185	1398	1090	-308	27.1	48.7	Example
2-3	90	0	5	5	10	10	0.010	0.0500	2.1	3.500	7	200	200	1401	1101	-300	26.9	49.2	Example

Industrial Applicability

[0045]

The cement admixture of the present invention can be widely used in the engineering and construction fields because it is able to give a large expansion to the concrete over an initial material age of 2 days to 7 days after concrete placement and to inhibit a drying shrinkage strain, and it is free from a decrease of the long-term strength development properties.

CLAIMS

[Claim 1]

A cement admixture comprising free lime and a hydraulic compound and also comprising SrO as a chemical compound, wherein

the content of the free lime is 10 to 98 parts by mass based on 100 parts by mass of the cement admixture.

[Claim 2]

The cement admixture according to claim 1, wherein the content of the SrO is 0.001 to 5.0 parts by mass based on 100 parts by mass of the cement admixture.

[Claim 3]

The cement admixture according to claim 1 or 2, further comprising anhydrous gypsum.

[Claim 4]

The cement admixture according to any one of claims 1 to 3, wherein the content of the free lime is 10 to 95 parts by mass based on 100 parts by mass of the cement admixture.

[Claim 5]

The cement admixture according to any one of claims 1 to 4, further comprising ZrO₂ as the chemical component.

[Claim 6]

The cement admixture according to claim 5, wherein the content of the ZrO₂ is 0.0001 to 5.0 parts by mass based on 100 parts by mass of the cement admixture.

[Claim 7]

The cement admixture according to any one of claims 1 to 6, wherein a Braine's specific surface area is 2,000 to 6,000 cm²/g.

[Claim 8]

The cement admixture according to any one of claims 1 to 7, wherein the content rate of particles of 10 μm or less is 30 to 60% by volume on a basis of volume, and the ratio of the content rate A of particles of 100 μm or less and the content rate B of particles of 10 μm or less (A/B) is 1.5 to 4.0.

[Claim 9]

The cement admixture according to any one of claims 1 to 8, containing,

as the hydraulic compound, one or more selected from the group consisting of $3\text{CaO}\cdot\text{Al}_2\text{O}_3$, $3\text{CaO}\cdot 3\text{Al}_2\text{O}_3\cdot\text{CaSO}_4$, $3\text{CaO}\cdot\text{SiO}_2$, $2\text{CaO}\cdot\text{SiO}_2$, $4\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, $6\text{CaO}\cdot 2\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, $6\text{CaO}\cdot\text{Al}_2\text{O}_3\cdot\text{Fe}_2\text{O}_3$, and $2\text{CaO}\cdot\text{Fe}_2\text{O}_3$.

[Claim 10]

The cement admixture according to claim 9, containing, as the hydraulic compound, $3\text{CaO}\cdot\text{Al}_2\text{O}_3$.

[Claim 11]

An expansive material comprising the cement admixture according to any one of claims 1 to 10.

[Claim 12]

A cement composition comprising the cement admixture according to any one of claims 1 to 10.