

METHOD FOR LOW TEMPERATURE LAMINATION OF METALS TO POLYIMIDES

BACKGROUND OF THE INVENTION

FIELD OF THE INVENTION

5 Polyimides and derivatives of polyimides are of great importance to the microelectronics packaging and encapsulation industries. This invention relates to a method for the low temperature lamination of metals, especially copper, to the surface of polyimides and derivatives of polyimides.

10 When thermally induced grafting or graft copolymerization occurs on the pristine or the pre-activated surface and interface of polyimides or derivatives of polyimides in contact with a metal surface, lamination occurs simultaneously. The surface and interfacial polymerization or graft copolymerization with concurrent lamination of the metal are carried out under atmospheric conditions, and in the complete absence of an added polymerization initiator or system degassing. Polymerization initiators may also be used to
15 enhance the graft copolymerization reaction. The process and properties can be imparted on surfaces of pristine or pre-activated polyimides and derivatives of polyimides in contact with a preferred metal.

Thermal grafting or graft copolymerization with concurrent lamination can be carried out in the presence of one or more functional monomers including, but not limited to, 1-vinyl
20 imidazole (VIDZ), 1-allyl imidazole (AIDZ), 2-vinyl pyridine (2VP), 4-vinyl pyridine (4VP), 2,4,6-trialloxy-1,3,5-triazine, triallyl-1,3,5-benzenetricarboxylate, epoxide-containing monomers, monomers of polyelectrolyte and polyampholyte.

The lap shear adhesion strength of the so-laminated polyimide-copper interface can readily exceed the fracture strength of the substrate polyimide film. The T-peel adhesion strengths
25 of the so-laminated polyimide-copper interfaces are greater than 16 N/cm, with delamination occurs via cohesive failure in the polymer film. The strong adhesion between the polymer and the metal arises from the strong adhesion/adsorption of the functional chains and the covalent tethering of the grafted functional chains on the surfaces of polyimides or derivatives of polyimide on one hand, and the strong adhesion, with or

without charge transfer interaction, of the grafted functional chains to the metal surface on the other. Strong adhesion of the metal to the polymer depends on the proper annealing of the polyimide-copper interface after thermal grafting, interfacial polymerization and lamination.

- 5 The present invention distinguishes itself from prior art lamination of metals to polyimides in that the one-step grafting/lamination process is carried out at temperature substantially below the melt processing and curing temperatures of the polyimides, does not involve the polyamic acid precursor and no adhesive is required to affect the lamination process.

DESCRIPTION OF RELATED ARTS

- 10 Polyimides are considered specialty plastics because of their outstanding, high performance engineering properties particularly suited for the microelectronics packaging industries and composite applications. Polyimides offer good thermal and mechanical stability, low dielectric constants and chemical resistance. Polyimides for electronic applications have been reviewed by P. K. Mukerji and G. Demet in *Polym. Adv. Technol.*
- 15 4, 309 (1992). Good adhesion of polyimides to metals, copper in particular, is essential for applications in microelectronics. Depending on the configuration of the particular assembly, the copper metal is either introduced onto the polyimide surface through vacuum evaporation/deposition, or by means of the direct lamination of the metal foil, films or sheet to the polymer surface.
- 20 The strategies of surface chemical and physical modification have been widely implemented in polyimides and other polymers for adhesion improvement with metals and with other polymer substrates. They have been described, for example in, E. Sacher, J. J. Pireaux and S. P. Kowalczyk (Eds.), *Metallization of Polymers*, ACS Symposium Series 440, Am. Chem. Soc., Washington, DC (1990); in M. Strobel, C. S. Lyons and K. L. Mittal
- 25 (Eds.), *Plasma Surface Modification of Polymers: Relevance to Adhesion*, VSP, Zeist, The Netherlands (1994); and in K. L. Mittal (Ed.), *Polymer Surface Modification: Relevance to Adhesion*, VSP, Zeist, The Netherlands (1995).

The patent literature contains numerous disclosures of surface modification of polyimides for adhesion enhancement. However, most of the prior art is related to plasma or chemical

30 surface treatment. A few of the prior art disclosures are related to surface modification via

graft copolymerization. Almost no prior art is directed to the modification of polyimides via surface graft copolymerization for the improvement of adhesion to metals. Throughout our exhaustive patent literature search, there is no relevant process which involves the simultaneous modification of polyimide surface via grafting or graft copolymerization and the lamination of a metal in the complete absence of an adhesive.

For further background reading, reference is made to the following patent publications:-

- European Patent Nos. 310803, 388888, 419845, 456972 and 478975;
- US Patent Nos. 4382101, 4755449 and 4842946;
- British Patent publication No. 9004392;
- 10 - Japanese Patent Publication Nos. 1132772, 3150392, 4072070, 5001160, 7070335, 61-111531, 90-025779, 04-359585, 04-064280, 06-316759, 06-279996, 07-186324, 07-317776, 08-230108, 08-325713; and
- Russian Patent Publication Nos. 262015, 315079 and 339042.

SUMMARY OF THE INVENTION

15 It is an object of the present invention to provide a new method for the low temperature direct lamination of a metal, such as copper, to surfaces of polyimides under atmospheric conditions. It is also an object of the present invention to effect the said lamination in the absence of an added adhesive. These and other objects and advantages of the present invention are obtained by providing a method for modification of pristine, pretreated, or
20 preactivated polyimide surfaces via low temperature thermal graft copolymerization or interfacial polymerization of an appropriate functional monomer in the presence of the contacting metal. A desirable low grafting/lamination temperature is selected to be substantially below the melting or curing temperature of the polyimides. Desirable radio frequency gas plasma with low plasma power is selected for the pretreatment of the
25 polyimides to minimize the undesirable over-oxidation, etching or sputtering of the polyimide surface. The surfaces of the polyimides can also be activated by corona discharge, ozone treatment, UV irradiation and electron beam bombardment.

The objects and advantages of the present invention can be achieved when the monomer used for the surface graft copolymerization or interfacial polymerization with concurrent
30 lamination are selected from a group of vinyl monomers which contain nitrogen heteroatoms or nitrogen functionalities in the pendent group or groups. The monomers are

also selected from the family containing multiple vinyl group functionalities, which can also promote chain crosslinking, as well as from the family which contains epoxide functional groups.

5 The objects and advantages of the present invention can be achieved when the monomer concentrations used for graft copolymerization or interfacial polymerization range from 2 to 100 weight per cent. Desirable solvents are selected from the group which provide good solubility for the vinyl monomer, and which promote free radical polymerization.

10 The objects and advantages of the present invention are obtained when the monomers used for the simultaneous interfacial polymerization grafting and lamination process also contains a small quantity of a polymerization initiator. The initiators are selected from the families of organic peroxides, hydroperoxides, azo and diazo compounds, and the like.

The objects and advantages of the present invention are obtained when the metals for lamination are preferably selected from copper metal and its alloys.

15 The objects and advantages of the present invention are obtained when the polymers for lamination are selected from polyimides and their derivatives.

The objects and advantages of the present invention are best achieved when the polyimide-metal interfaces from the thermal graft copolymerization and interfacial polymerization with concurrent lamination are returned to room temperature via a slow cooling or annealing process.

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DESCRIPTION OF PREFERRED EMBODIMENTS

25 The present invention is directed to a method of direct lamination of a metal, such as copper, to polyimides in the absence of an applied adhesive and at temperature substantially below the glass transition temperature or melting point of polyimides. The lamination strengths, as measured in terms of T-peel strength, of the polyimides-metal interfaces can exceed the fracture strength of a 75 μm thick Kapton[®] HN film. While not wishing to be bound by any theory, it is believed that the functional groups of the physicochemically adsorbed and covalently grafted polymer chains on the polyimide surface charge transfer interact with the contacting metal surface to give rise to the strong adhesion between the metal and the polymer. The lamination temperature in the present

invention is thus governed by the optimum temperature for thermally induced surface graft copolymerization and interfacial polymerization. More precisely, the simultaneous interfacial polymerization, grafting and lamination process at the polyimides-metal interface is affected by the thermal decomposition of the peroxides and hydroxyl peroxides at the polymer surface and interface, and the initiators in the monomer phase.

In the preferred method, the polyimides surface is preactivated by gas plasma treatment, ozone treatment, corona discharge treatment, or ultra-violet irradiation, although pristine polyimides can also be used. The pristine and preactivated polyimides are then subjected to thermally induced graft copolymerization and interfacial polymerization with reactive vinyl monomers in the presence of a contacting metal. The graft copolymerization and interfacial polymerization are also enhanced by the presence of an initiator at the polymer-metal interface or in the monomer solution

The preferred monomers are selected from the family of vinyl polymers with functional groups which are capable of undergoing charge transfer interactions with the contacting metal. Thus, the monomers are selected from the family containing the imidazole, epoxide, anionic, cationic or amphoteric functional groups. The concentration of monomers used for the grafting/lamination process typically range from 2 to 100 weight percent. The graft copolymerization with concurrent lamination process is aided by the presence of a small amount, typically in the range of 0.1 wt. % to 5 wt. %, of a crosslinking agent for vinyl polymerization. The preferred crosslinking agents are selected from the family containing multiple vinyl groups or functionalities.

The preferred application and the best advantages of the present invention are obtained from polyimide films or sheets, as well as from copper foils, films, thin sheets or plates. Thus, in the preferred method, the surface of the polyimides is pretreated with a radio frequency gas plasma, corona discharge or ozone. Pristine (untreated) polyimide surface is grafted/laminated at lower efficiency than its pretreated counter-parts. The efficiency, however, can be improved by the presence of an initiator. The initiators are selected from the families of organic peroxides, hydroperoxides, azo and diazo compound. The selection of frequency and gas type (in the case of plasma treatment) and treatment time for all treatments are important. Long pretreatment time can result in excessive etching or degradation of the polymer surface. The preferred temperature for the present interfacial polymerization, grafting and lamination process is usually less than 130 °C under

atmospheric conditions and either in the presence or in the complete absence of an added polymerization initiator.

EXAMPLES

5 The following specific examples are provided to illustrate this invention and the manner in which it may be carried out. It will be understood, however, that the specific details given in each example have been selected for purpose of illustration and are not to be constructed as a limitation on the invention. Example 1 provides more details on the conduct of the simultaneous surface graft copolymerization, interfacial polymerization and lamination experiment.

10 EXAMPLE 1

In a preferred experimental scale process, an Ar plasma pretreated polyimide film, e.g. a Kapton® HN film, of 0.5 cm × 0.25 cm in size and 75 μm in thickness and a 0.1 mm thick copper foil of similar size was lapped together in the presence of a small quantity of 1-vinyl imidazole (VIDZ). The surface of the copper metal was cleaned with a mixture of
15 aqueous 0.01 M HCl/0.01 M HNO₃/0.01 M H₂SO₄ in the volume proportion of 6:1:1, respectively, before use. The polyimide/VIDZ/Cu assembly was sandwiched between two stainless steel plates and subjected to an equivalent pressure of no less than 10 N/cm² in an hydraulic press. The assembly under pressure was also subjected to thermal graft copolymerization, interfacial polymerization and lamination at 120 °C for 2-4 h, with the
20 heat being provided by a pair of heating plates. After the grafting, polymerization and lamination process at 120 °C, the assembly was allowed to returned to room temperature slowly between the two heating plates over a period of no less than 6 h. The polyimide-Cu joint so prepared exhibited a T-peel strength exceeding 16 N/cm or exceeding the fracture strength of the 75 μm thick Kapton® HN film.

25 EXAMPLE 2

In a preferred lamination experiment, a polyimide/VIDZ/Cu assembly is similarly prepared as illustrated in Example 1, except the VIDZ monomer also contains a small quantity of a crosslinking agent, e.g. 2 vol. % of triallyl-1,3,5-benzenetricarboxylate. In the presence of the crosslinking agent, a T-peel strength exceeding the fracture strength of a 75 μm thick

Kapton[®] HN film is achieved at a lamination temperature of 100 °C or less.

EXAMPLE 3

5 A similar lamination experiment as that illustrated in Example 2, except that the crosslinking agent is replaced by 2,4,6-triallyloxy-1,3,5-triazine is also carried out. In the presence of the crosslinking agent, a T-peel strength exceeding 16 N/cm or exceeding the fracture strength of a 75 µm thick Kapton[®] HN film is achieved at a lamination temperature of 100 °C or less. Furthermore, in the presence of the crosslinking agent, the adhesion strength of the polyimide-Cu joint remains practically unchanged even after prolonged (> 10 days) immersing/soaking in water.

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EXAMPLE 4

In another preferred experiment, a pristine polyimide film is lapped together with a Cu foil of similar size in the presence of a small quantity of pure VIDZ, VIDZ plus 2 vol. % triallyl-1,3,5-benzenetricarboxylate, or VIDZ plus 2 vol. % of 2,4,6-triallyloxy-1,3,5-triazine. For lamination carried out at 120 °C, T-peel strengths exceeding 4, 9, and 11
15 N/cm are obtained, respectively, for the three cases.

EXAMPLE 5

In yet another preferred experiment, a pristine polyimide film is lapped together with a Cu foil of similar size in the presence of a small quantity of the VIDZ monomer, containing also 0.5 to 1 wt. % of a peroxide initiator, such as the benzoyl peroxide. For lamination
20 carried out at 100 °C, T-peel strength exceeding the fracture strength of a 75 µm thick Kapton[®] HN film is achieved.

EXAMPLE 6

In another preferred experiment, an Ar plasma pretreated polyimide film is lapped together with Cu foil of similar size in the presence of a small quantity of VIDZ containing 2 vol. %
25 triallyl-1,3,5-benzenetricarboxylate. For lamination carried out at 80 °C, a T-peel strength of no less than 12 N/cm is obtained even at this low lamination temperature.

EXAMPLE 7

In yet another preferred lamination experiment, an Ar plasma pretreated polyimide film is lapped together with a Cu foil of similar size in the presence of a small quantity of 4-vinyl pyridine. The lamination, grafting and interfacial polymerization is allowed to proceed at
5 120 °C for 2-4 h in a hot press. A T-peel strength of no less than 3 N/cm is obtained. The T-peel strength is increased to more than 6 N/cm in the presence of a small quantity of a crosslinking agent, e.g. in the presence of 2 vol. % 2,4,6-triallyoxy-1,3,5-triazine.

EXAMPLE 8

In yet another preferred lamination experiment, an Ar plasma pretreated polyimide film is
10 lapped together with a Cu foil of similar size in the presence of a small quantity of acryloyl morpholine. The lamination, grafting and interfacial polymerization are allowed to proceed at 120 °C for 2-4 h in a hot press. A T-peel strength of no less than 3 N/cm is obtained. The T-peel strength is increased to more than 6 N/cm in the presence of a small quantity of a crosslinking agent, e.g. in the presence of 2 vol. % 2,4,6-triallyoxy-1,3,5-
15 triazine.

EXAMPLE 9

In still another preferred lamination experiment, an Ar plasma pretreated polyimide film is lapped together with an aluminium foil of 0.1 mm in thickness in the presence of a small quantity of glycidyl methacrylate (GMA). The lamination, grafting and interfacial
20 polymerization are allowed to proceed at 120 °C for 2-4 h in a hot press. A T-peel strength of no less than 2 N/cm is obtained. The T-peel strength is increased to more than 6 N/cm when the monomer composition also include a small quantity of a crosslinking agent, e.g. 2 vol. % trially-1,3,5-benzenetricarboxylate.

EXAMPLE 10

25 In still another preferred lamination experiment, an Ar plasma pretreated polyimide film is lapped together with Cu foil of similar size in the presence of a small quantity of 1-allyl imidazole. The lamination, grafting and interfacial polymerization are allowed to proceed at 120 °C for 2-4 h in a hot press. A T-peel strength of no less than 8 N/cm is obtained.

The T-peel strength is increased to more than 12 N/cm when the monomer composition also include a small quantity of a crosslinking agent, such a 2 vol. % trially-1,3,5-benzenetricarboxylate or 2 vol. % 2,4,6-triallyoxy-1,3,5-triazine.

5 To those skilled in the art to which this invention relates, many changes in construction and widely differing embodiments and applications of the invention will suggest themselves without departing from the spirit and scope of the invention. The disclosures and the description herein are purely illustrative and are not intended to be in any sense limiting.



CLAIMS

1. A method for the lamination of a metal to a polyimide or polyimide derivative at a temperature substantially below the glass transition temperature, melting point or curing temperature thereof, wherein the said polyimide or polyimide derivative is
5 subjected to thermal graft copolymerization and interfacial polymerization in the presence of the contacting metal, with concurrent lamination of the metal in the presence of an appropriate functional monomer.
2. The method according to Claim 1, wherein lamination is affected by the simultaneous surface graft copolymerization and interfacial polymerization at the
10 lapped junction between polyimide and metal.
3. The method according to Claim 1 and Claim 2, wherein the lamination and interfacial reactions are carried out under atmospheric conditions and at temperature below 130°C.
4. The method according to any one of the preceding claims, wherein the polyimide is
15 in the form of film, sheet, slab, fiber or porous substrate.
5. The method according to any one of the preceding claims, wherein the polyimide is pretreated with a gas plasma, ozone, corona discharge, UV irradiation, electron beam bombardment or is used in its pristine form.
6. The method according to any one of the preceding claims, wherein the interfacial
20 reactions are carried out in the complete absence of an added polymerization initiator.
7. The method according to any one of the preceding claims, wherein the interfacial reactions are carried out in the presence of a polymerization initiator.
8. The method according to any one of the preceding claims, wherein the
25 polyimide/metal assembly after the lamination process is returned to room temperature in an annealing process.
9. The method according to any one of the preceding claims, wherein the metals are selected from copper, aluminium, gold, palladium, nickel, or the like, in the form of



film, foil or thin slab.

10. The method according to any one of the preceding claims, wherein the monomers are selected from vinyl monomers which contain nitrogen heteroatoms or nitrogen functionalities in the pendent group or groups, or which contain epoxide functional groups.
11. The method according to any one of the preceding claims, wherein the monomers are selected from the family of vinyl monomers consisting of 1-vinyl imidazole, 1-allyl imidazole, 2-vinyl pyridine, 4-vinyl pyridine, acryloyl morpholine, glycidyl methacrylate, allyl glycidyl ether, and the like.
12. The method according to any one of Claims 2 to 11, wherein the crosslinking agent is selected from triallyl-1,3,5-benzenecarboxylate, 2,4,6-trialloxy-1,3,5-triazine, and 1,2,4-trivinylcyclohexane.
13. The method according to any one of the preceding claims, wherein the T-peel strength exceeds the fracture strength of the 75 μ m thick Kapton[®]HN film.
14. The method according to any one of the preceding claims, wherein the monomer concentrations used for graft copolymerization or interfacial polymerization range from 2 to 100 weight percent.
15. The method according to any one of the preceding claims, wherein the monomers also contain a polymerization initiator, preferably selected from organic peroxides, hydroperoxides, azo and diazo compounds and the like.
16. The method according to any one of the preceding claims, substantially as hereinbefore described with reference to the examples.
17. A metal laminated polyimide when produced by a method as claimed in any one of the preceding claims.