

1 Shell-and-Tube Heat Exchanger with Wear-resistant Tube Plate Lining

The invention pertains to a shell-and-tube heat exchanger (THE) which contains a wear-resistant tube plate lining for application in thermal cracking equipment.

5 Shell-and-tube heat exchangers of this type are used, for example, in ethylene equipment to produce ethylene through thermal cracking downstream from the transfer line of a cracking furnace and are referred to as quench coolers (transfer line exchangers, or TLE's).

10 Quench coolers must conform to unusually high standards of construction and material characteristics. The hot reaction mixture discharged from a cracking furnace after pyrolysis of hydrocarbon materials such as naphtha, LPG, ethane, or even hydrocracking residue (unconverted oil, waxy), which can reach
15 temperatures of approximately 850° C, must be cooled quickly in the quench coolers in order to avoid undesirable side reactions. The quench cooler, or THE, functions as a waste heat boiler in which high steam pressure can be created through evaporation of feed water introduced to the casing side.

20 Coking retardation occurs in cracking furnaces during this process, which must be removed at specific intervals (60-80 days) through oxidation with air. In order to remove the coking, the furnace is heated to minimal operating levels and a mixture of air and steam is introduced into the tubes of the cracking furnace. The carbon residues are burned off with this mixture. Particles of coking are loosened
25 at the same time, and they are carried with the gasses along the cracked gas pathways through the quench cooler and into the coking removal conduits.

The cracked gas or coking removal gas, which is discharged at high velocity from the cracking furnace, generally crosses a transfer line into an axial gas entry
30 chamber and then, from below, into the quench cooler, where it collides against

1 the lower tube plates before it is fed into the remainder of the process after its journey through the heat exchanging tubes of the quench cooler.

5 In spite of short exposure periods, the cracking gas contains coking particles which become highly corrosive at the high velocities reached by the cracking gas. In order to cool the hot reaction mixture created in the cracking furnace quickly, the distance between cracking furnace and the cooling tubes must be traversed as quickly as possible. This necessitates that the gas entry chamber design be compressed, which would normally broaden out in diameter of the transfer line
10 leading to the cooler, with the result that the stream of gas containing coking particulate is concentrated on the middle region of the tube plate and the cooling tubes, which are affected particularly severely. The weight-bearing wall elements are weakened, which creates the necessity of significant maintenance costs, and maintenance downtimes result in production downtimes.

15 Various solutions have been proposed to this and similar problems. These are based on using of ceramic, fireproof materials as linings, structural members, or emulsions:

20 EP-A-0 567 674 introduces heat exchangers for the cooling of synthetic gas created in coal gasification equipment. In this application, the tube plate on the gas inlet side is covered by cuboid-based nozzles which are positioned adjacent to and abutting one another on the outer edges. Each of these nozzles has a conical opening which narrows to a section of tubing which in turn is inserted into
25 a heat exchanger tube. This solution offers no gastight closure between the individual cuboid-based elements. This would lead to buildup of coking residue in the empty spaces within the quench coolers of an olefin processor and destroy the materials. In addition, the ends of the nozzles which are used would form a tearing edge within the tube which, considering the high flow velocities within the
30 quench coolers, would result in heavy turbulences. This would result in additional erosion.

1 In DE-C-44 04068 a ceramic lining is revealed, which is comprised of fireproof
molded elements. These can in some instances be hexagonal in shape and
contain perforations through which pins or hooks can be inserted which are
5 welded to the underside of the tube plate. The molded element can be attached
to the tube plate in this fashion. This construction does not accomplish the goal of
having a seamless emulsion or lamination.

In addition, it is widely accepted that a cooling tube installed within a reactor must
be equipped with a fireproof lining which is resistant to erosion (see US 4 124
10 068), in order to reduce the risk of tube failure and the resulting penetration of
cooling water into the surrounding reaction mixture at elevated temperatures.

The suggestion is made in DE 195 34 823 A 1 that tube plates on the gas inlet
side be coated or lined with a chemically hardened, erosion-resistant, fireproof
15 product. This coating should initially be formed from a castable substance,
applied in a pliable format, and finally fired to achieve its final format as a
fireproof mass.

What these applications have in common is that they all combine ceramic—in
20 other words, non-metallic—materials with the metallic apparatus material,
principally steel. Practical experience has taught that combining ceramic and
metallic components results in increased time, effort, and expense during
manufacture, assembly, and repair and often creates problems because of the
differences in material characteristics such as thermal expansion coefficients and
25 varying levels of elasticity (brittle vs. ductile). In addition to these issues, inserted
ceramic nozzles also have the problem of turbulence and the accompanying
particular stresses to the materials at the rear end of the nozzle (from the
perspective of flow direction) associated with the tearing edge located there.
Contrary to the design laid out in DE 195 34 823, installing a lining consisting of a
30 fireproof mass positioned solely in the focal area in the center of the tube plate
has been shown to be impractical because the resulting inconsistent surface of
the tube plate, in conjunction with the variations in material characteristics,

1 results in the occurrence of particular problems in the transition range, i.e., at the
outer edge of the fireproof form, possibly through chipping or spalling of the form
or through particularly heavy erosion caused by turbulence at the edge. It should
also be noted that installation of a lining made of a fireproof material only protects
5 the tube plate as such. There is a distinct advantage to providing protection for at
least the front part of each cooling tube (viewed from the perspective of flow
direction). This can only be accomplished by applying a protective nozzle or
sleeve.

10 The problem of a significantly stronger flow rate and stress on the focal area as
compared to the peripheral areas was also investigated. One proposed solution
incorporated cone-shaped fittings (see US-PS 35 52 487). Another proposed
installing diffuser-type diversion fixtures which could be free-standing within the
entry chamber (see DE-PS 21 60 372).

15 For the purposes of equalizing the flow through the entry chamber and also
protecting the tube plate from erosion, an additional suggestion has been made
that the THE be fitted out with inserted elements made of small rods bent into the
shape of rings. The rings would be aligned along the surface of a cone, and the
20 point of the cone would be directed toward the gas inlet (see EP 037 089 A1).

The intention here is that the coking particles carried along in the focal range of
the high-velocity gas flow would be decelerated and in part deflected outward in a
radial pattern, so that they would then no longer contribute to erosion damage on
25 the tube plate and the tubes. However, an undesirable differential pressure and
the associated increased exposure time would result with fittings of this type,
meaning that there would be a yield loss.

30 This invention takes a different approach, in that it attempts to provide an
effective wear protection by applying a metallic lining to the tube plate and to the
entry space of the cooling tubes. Erosion at the inlet side tube plate and in the
cooling tubes made it necessary to periodically shut down the quench cooler for

1 purposes of inspection and maintenance. In the past, people attempted to correct
the problem by welding material onto the tube plates in order to return them to
the required wall thickness and periodically replacing the cooling tubes. This
process is very complicated and costly and is also unsatisfactory in terms of the
5 resistance capabilities of the replacement materials, since these might very well
have the same characteristics as the materials that were originally used.

It has been established that the material erosion in the gas inlet region is not
caused solely by mechanical erosion, but by the combined effects of high-
10 temperature corrosion (scaling) and mechanical erosion of the corrosion product
that has been formed (iron oxide).

Thus, one of the objectives of the invention is to apply a metallic lining which is
highly resistant to high-temperature corrosion to the tube plates and the inlet
15 region of the cooling tubes. All other characteristics of the lining must have
similar material characteristics to the rest of the equipment material (ductility,
heat expansion coefficient). It must be possible to add a partial lining without
causing any negative side effects. In addition, the lining should be easy to install
and easy to remove or replace.

20 These objectives were met by developing a shell-and-tube heat exchanger (THE)
equipped with a tube plate lining which is resistant to the wear occurring in these
conditions for use in thermal cracking equipment which contains cooling tubes (1)
through which the gas to be cooled is circulated, each tube being secured by a
25 tube plate at both ends of the tube and enclosed in a casing through which a
coolant material is circulated. (2) The surface of the tube plate on the gas inlet
side which is impacted by gas as it enters the shell-and-tube heat exchanger
should be faced, at least partially, by a protective layer which is created by
aligning individual sleeves side-to-side and end-to-end at the outer edges and
30 inserting the tube ends into them (Fig.1), typified by the fact that the insert
sleeves are created from a heat-resistant metallic material.

1 In principle (Fig. 2), the insert sleeves are simply constructed; the most basic
application consists of a tube (4) and a plate (5). One end of the tube is attached
to the plate such that the surface of the plate is positioned at a 90° angle to the
length axis of the tube. In other words, one could say that the tube stands
5 vertically on top of the plate. The plate (Fig. 3) is perforated to allow the inflowing
gas to pass through the plate into the tube. In the most basic application of this
principle, a hole would simply be drilled in the plate. Preferably, the diameter of
the drilled opening should be similar or equal to the internal diameter of the tube.
The insert tubes can be manufactured either by welded construction, by
10 machining processes, by casting, or by precision cold forging.

Ideally, the plate should be aligned with the center of the tube cross section. The
tube's length axis is then threaded through the center of the plate surface.
Logically, the drilled hole mentioned above is also located in the center of the
15 plate surface.

The plate itself is designed with a shape that allows the outer edges of the plate
to abut the outer edges of the plates of adjoining sleeves in such a manner as to
provide at least a partial continuous, gapless covering for the tube plate on the
20 inlet side (Fig. 1).

The choice of which geometric shape is best suited for the plates depends upon
the geometric relationship in which the individual cooling tubes are positioned
relative to one another. Suitable individual geometric shapes which would create
25 a solid, continuous larger surface when positioned next to each other would
include, for example, triangular surfaces (especially isosceles, where all sides are
the same length), rectangular surfaces (especially squares, but diamonds or
rhombuses would be appropriate), and hexagons (especially those where all
angles and sides are identical). If the tubes in the shell are positioned such that
30 the top view looks like a grid network, where each tube marks a grid intersection
and where the grid is square, then it would be preferable that the plates of all the
sleeves would be square.

1 Conveniently, the sleeve in the tube has an outer diameter which is equal to or
only slightly smaller than the inner diameter measurement of the cooling tube.
This is the only way that the insert sleeves, with their attached tubes, be fitted
exactly into the cooling tubes. It has been established through practical
5 application that the optimal length for tubes on the insert sleeves lies somewhere
in the area of between 50 and 200 mm; tubes measuring between 70 and 150
mm in length are especially suitable. Tubes measuring between 100 and 120 mm
are especially optimal, because this measurement is equal to the length of the
tube section of the cooling tube which is subject to the greatest impact under
10 operating conditions.

The material thickness of the tubes and the plate of the insert sleeves are
adapted to the rest of the dimensions of the THE and particular operating
conditions. Generally, a tube wall thickness of about 1 mm is optimal. The
15 preferred thickness of the plate is between 2 mm and 10 mm.

As mentioned above, material erosion in the gas inlet region, especially in the
highly impacted central region of the tube plate, by the combined effects of high-
temperature corrosion (scaling) and mechanical erosion of the corrosion product
20 that has been formed (iron oxide). As such, this is a new awareness that has not
previously been considered in the industry, where it has always been accepted
that material erosion has been caused solely, or at least primarily, by mechanical
abrasion. This assumption has prevented the experts in the field from considering
installing metallic linings instead of linings created from ceramic or other fireproof
25 masses, especially since common methods of welding in earlier times were
difficult and expensive and did not result in satisfactorily long operating times.

This invention is also based upon the realization that metallic materials which
have been adequately tempered against high temperature corrosion through
30 specific conditions—in other words, on which corrosion products are not
constantly being formed on the surface—are then also sufficiently resistant to the
purely mechanical stresses of abrasion. Because of this, the preferred materials

1 are high-temperature, corrosion-resistant alloys, especially steels containing
chrome and nickel-based alloys. Because of their durability under the process
conditions outlined here, austenitic steels are especially preferable for use in
manufacture of the insert tubes.

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In order to achieve an optimal gas flow, this inlet in the sleeves is shaped
conically or rounded off (6).

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In order to prevent a tearing edge from forming at the rear end of the sleeve as it
has been inserted into the cooling tube, which might result in turbulence and
material erosion within the cooling tube, the end of the tube which is placed
against the plate is attached to the insert sleeve (7).

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An additional advantage of the insert sleeves as they are employed in this
invention is in the formability of the metallic materials out of which they are
constructed. This makes it possible to attach the sleeves to the cooling tube in a
secure and continuous seam using a simple, common procedure such as rolling.
In addition to rolling, the process of hydraulic fastening can be used.

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The material characteristics of the insert sleeves make it possible to produce the
sleeves with a thin wall, which further minimizes the formation of tearing edge at
the opposite end of the tube from the face. Also, a very thin wall which is firmly
attached to the cooling tubes will have only a very minimal effect on heat transfer
and the cooling operation of the THE will not be impacted at this point.

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In comparison with the current state-of-the-art technology, this invention exhibits
the following advantages:

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- Compared to ceramic, the elements or insert sleeves, are very robust and
do not need any special protection against bumping or falling.

- 1 - The stability of the cooling tubes and of the sleeves is not placed under as much strain as when ceramic is used. Among other reasons, this is because permanent connection between cooling tube and sleeve tube is not completed until the rolling or hydraulic fastening takes place.
- 5 means that the process is applicable for repairs or modifications to previously-used coolers with cooling tubes which have been increased in internal diameter by removal. On machines such as these that have previously been damaged, it becomes necessary to make an additional expansion because of the material removal that has already taken place,
- 10 but with the materials used it becomes easily do-able. The insert sleeves are then attached by rolling or hydraulic fastening and widened slightly more than they would be on comparable undamaged cooling tubes.
- Low manufacturing costs due to use of common materials and processes, automatable mass production.
- 15 - Installation of a cooler requires only minimal preliminary work, such as sandblasting, but no additional treatment of the outer surface and no closing of tubes as would be necessary, for example, when applying a pliable mass.
- Assembly costs are minimal, since tools required for this assembly are all
- 20 commonly-used standard tools.
- Installation period is comparatively short, since no anchors, screws, or similar attachments must be installed. Likewise, there is no need for welding or firing, as there would be, for example, with a pliable mass.
- Another very important aspect is the quick and easy disassembly of the
- 25 installed insert sleeves, with no danger of damage to the cooler. Preferably, a suitable tool (such as an internal pipe cutter, milling cutter, or drill) would be used to make a split cut between the plate and the tube. After removal of the plate, an arbor would be inserted between the cooling tube and the sleeve tube, onto which the sleeve tube would be manually pulled.
- 30 - The plates of the insert sleeves can be chamfered at the edges, meaning where the sleeve edges form the outer rim of the total formed surface and do not abut adjoining insert sleeves, so that they do not form a sharp ridge

1 between the insert sleeve plate and the tube plate.

Application of the shell-and-tube heat transfer exchanger as outlined in this invention is not limited to thermal cracking equipment. In fact, it can be applied to
5 other processes where similar stresses impact the materials because of the operating conditions such as, for example, downstream from fluidized bed combustion or combustion turbines.

Shell-and-tube heat exchangers as outlined in this invention can be designed to
10 accommodate all common construction formats, including fixed plate, floating head, and U-bend heat exchangers. Fixed-plate heat exchangers are commonly used in cracking facilities.

Figure 1 shows a cross-section drawing through a tube plate (2) with, in this
15 instance, 2 exemplary cooling tubes (1) which are connected to the base plate by means of a tube weld (3). A single sleeve consisting of a sleeve tube (4) and a sleeve plate (5) is inserted in each cooling tube. The plates attached to the sleeves of neighboring tubes (1) share a common edging rim (8), against which they all abut, fitting precisely. This makes it possible to completely cover the tube
20 plate (2). The inflowing cracking gas is thus prevented from striking the plate, instead striking the face of the insert sleeve plate.

Figure 2 depicts the longitudinal section of an insert sleeve, and Figure 3 depicts the top view of the same sleeve. The sleeve consists of the sleeve tube (4) and
25 the sleeve plate (5). The rounded entry region (6) and the chamfered tube end (7) are also clearly recognizable.

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1 Reference Key List

- 5 (1) Cooling tube
(2) Tube plate
(3) Tube weld
(4) Sleeve tube
(5) Sleeve plate
(6) Rounded entry region
10 (7) Chamfered tube end
(8) Edging rim

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Claims

1. A shell-and-tube heat exchanger (RWUE) for cooling gas from a thermal cracking plant, comprising
- 5 a) tube plates having a lining that is resistant to wear due to scaling;
- b) cooling tubes (1), through which gas to be cooled flows, each cooling tube being held at both ends by one tube plate;
- c) a shell through which coolant for cooling the gas flows, and
- d) a plurality of sleeves formed from tubes (4) and plates (5) provided at
- 10 one end of the tubes, with the plates facing at 90° with respect to a longitudinal axis of the tubes, and having holes formed therein so that gas that flows therein passes through the plates (5) and flows inside the tubes,
- wherein, at a side where gas entering the shell-and-tube heat exchanger flows, at least part of a gas inlet side tube plate (2) is covered by a plate (5) of the
- 15 sleeves, with sleeves being arranged individually side by side, and outer edges of the plates (5) that face each other are inserted into tube ends so as to abut against each other, and wherein
- insertion sleeves are formed from austenitic steel.
- 20 2. The shell-and tube heat exchanger of claim 1, wherein the plates (5) are centered about a center of a tube cross section.
3. The shell-and-tube heat exchanger of claim 1 or claim 2, wherein the plates (5) are formed in such a shape that outer edges of plates of adjacent
- 25 sleeves abut each other, and such that at least a part of an inlet side tube plate is covered with no gap.

4. The shell-and tube heat exchanger of any one of claims 1 to 3, wherein the plates (5) are quadrilateral, preferably square.
- 5 5. The shell-and-tube heat exchanger of any one of claims 1 to 4, wherein an outer diameter of the tubes (4) of the sleeves is equal to, or slightly smaller than, the inner diameter of the cooling tubes (1).
6. The shell-and-tube heat exchanger of any one of claims 1 to 5, wherein
10 length of the tubes (4) of the insertion sleeves is 50-200 mm, preferably 70-150 mm, and most preferably, 100-120 mm.
7. The shell-and-tube heat exchanger of any one of claims 1 to 6, wherein wall thickness of the tubes (4) of the insertion sleeves is 1 mm.
- 15 8. The shell-and-tube heat exchanger of any one of claims 1 to 7, wherein thickness of the plates (5) of the insertion sleeves is 2-110 mm.
9. The shell-and-tube heat exchanger of any one of claims 1 to 8, wherein
20 tube ends are chamfered at opposite ends to the plates (5) of the insertion sleeves.
10. The shell-and tube heat exchanger of any one of claims 1 to 9, wherein the insertion sleeves are fixed to respective cooling tubes by roll joints, or
25 hydraulic tube expansion.

11. A method of providing a lining in the shell-and-tube heat exchanger of claim 1, comprising inserting a sleeve, made up of tubes (4) and plates (5), into heat exchange pipes, and fixing insertion tubes (4) of the sleeves to the heat exchange pipes using roll joints or hydraulic joints.