

Process for treating gasoline

Technical field

5 The present application relates to a process for treating gasoline, and particularly to a process for the desulfurization of gasoline.

Background art

10 Air pollution caused by vehicle exhaust emissions is getting worse. With the increasing emphasis on environmental protection, countries around the world have accelerated the pace of upgrading the quality of fuel for vehicles. For example, the Chinese national standard GB17930-2016 requires the sulfur content of gasoline to be not more than 10 $\mu\text{g/g}$, and the volume fraction of olefin in gasoline to be not more than 24%.

15 Catalytic cracking gasoline is a major component of motor gasoline, accounting for about 75% in gasoline pools, and is characterized by high olefin and sulfur content. It is not difficult to achieve deep desulfurization of gasoline and reduce the olefin contents in catalytic cracking gasoline by hydrogenation technology. However, since olefin is a high-octane component, a great reduce of its content will lead to a great loss of the octane number of gasoline, thereby affecting the performance of gasoline in automobiles and the economic benefits of refineries. Thus, techniques for deep desulfurization of gasoline while maintaining
20 the octane number of gasoline has become a hot spot in clean gasoline production.

At present, the deep desulfurization of gasoline is mainly performed by hydrodesulfurization or adsorption desulfurization.

25 Selective hydrodesulfurization is one of the main ways to remove thiophene-based sulfides, but the saturation reaction of olefins and other reactions may also occur in large quantities, resulting in a great loss of the octane number. In addition, the deep hydrogenation process for restoring octane number is also approved by practitioners, which comprises providing a second reactor to promote the cracking, isomerization and alkylation reactions of low-octane hydrocarbons while performing deep desulfurization and olefin saturation, so as to achieve the goal of restoring the octane number.

30 Chinese patent application No. CN101845322A discloses a process for reducing the content of sulfur and olefin in gasoline, in which the catalytic cracking gasoline feedstock is firstly treated in a prehydrogenation reactor to remove dienes, and then split by fractionation in

a fractionation column into light and heavy gasolines; the light gasoline is subjected to adsorption desulfurization in the presence of hydrogen; the heavy gasoline is subjected to hydrodesulfurization in a selective hydrogenation reactor, the resulting reaction effluent is subjected to hydro-upgrading in a hydro-upgrading reactor to reduce the olefin content, and the
5 upgraded heavy gasoline is blended with the product resulted from the adsorption desulfurization of the light gasoline to obtain clean gasoline that meets the standard requirements. The adsorption desulfurization catalyst may show a good effect in the removal of sulfides in gasoline, but the adsorption desulfurization is carried out in the presence of hydrogen, which would result in the saturation of olefins in the catalytic cracking gasoline.
10 Especially when the light gasoline is subjected to adsorption desulfurization, there would be a great loss of the octane number, as the olefin component of the light gasoline has a higher octane number.

In adsorption processes for the removal of sulfur-containing compounds in fuel oil, light oils are subjected to reaction and adsorption in the presence of hydrogen using adsorbents,
15 producing metal sulfides or removing sulfur by means of the polarity of sulfides, with a low hydrogen consumption and a high desulfurization efficiency. Gasoline with a sulfur content below 10 µg/g can be produced. Although deep desulfurization of gasoline can be achieved using adsorption processes with a low hydrogen consumption, there is still a slight loss of the octane number of the gasoline product. Especially when dealing with a gasoline feedstock with
20 high olefin content and high sulfur content, a large loss of the octane number of gasoline would still be encountered.

For most catalytic cracking units, in order to increase the production of propylene and butene and increase the octane number of the gasoline, an effective way is to use a catalyst or adjuvant containing a molecular sieve having an MFI structure. U.S. Patent No. US 3,758,403
25 discloses the addition of ZSM-5 molecular sieves to a catalytic cracking catalyst to increase the octane number of gasoline and increase the yield of C3 to C4 olefins. However, as is known to those skilled in the art, the increase of the production of propylene and butene is at the expense of gasoline production.

Accordingly, there remains a need in the art for a process for treating gasoline that is
30 capable of effectively reducing the sulfur and olefin content of gasoline while maintaining or even increasing the yield and the octane number of gasoline.

Summary of the invention

It is an object of the present application to provide a process and a system for treating gasoline that are capable of reducing sulfur and olefin content of gasoline, and at the same time increasing the octane number of gasoline while maintaining a high gasoline yield.

5 In order to achieve the above object, in one aspect, the present application provides a process for treating gasoline, comprising:

1) splitting a gasoline feedstock into a light gasoline fraction and a heavy gasoline fraction;

10 2) subjecting at least a portion of the resulting light gasoline fraction to etherification to obtain an etherified oil; and

3) contacting the resulting heavy gasoline fraction with a mixed catalyst and subjecting it to desulfurization and aromatization in the presence of hydrogen to obtain a heavy gasoline product;

15 wherein the mixed catalyst comprises an adsorption desulfurization catalyst and an aromatization catalyst, and the aromatization catalyst is selected from the group consisting of a fresh aromatization catalyst, a passivated aromatization catalyst, an aged aromatization catalyst, or any combination thereof.

In another aspect, the present application provides a process for treating gasoline, comprising:

20 1) splitting a gasoline feedstock into a light gasoline fraction and a heavy gasoline fraction;

2) optionally, subjecting at least a portion of the resulting light gasoline fraction to etherification to obtain an etherified oil; and

25 3) contacting the resulting heavy gasoline fraction with a mixed catalyst and subjecting it to desulfurization and aromatization in the presence of hydrogen to obtain a heavy gasoline product;

30 wherein the mixed catalyst comprises an adsorption desulfurization catalyst and an aromatization catalyst, and at least about 50 wt%, preferably at least about 80 wt%, more preferably at least about 90 wt%, particularly preferably at least about 95 wt%, and most preferably about 100 wt% of the aromatization catalyst has undergone a passivation and/or aging treatment.

In still another aspect, the present application provides a system for treating gasoline,

comprising a gasoline feedstock fractionation column and a desulfurization-aromatization reactor, wherein the gasoline feedstock fractionation column is provided with a gasoline feedstock inlet, a heavy gasoline fraction outlet, and a light gasoline fraction outlet; the desulfurization-aromatization reactor is provided with a heavy gasoline fraction inlet, a hydrogen inlet, and a desulfurization-aromatization product outlet; the heavy gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with the heavy gasoline fraction inlet of the desulfurization-aromatization reactor,

wherein a gasoline feedstock is introduced into the gasoline feedstock fractionation column through the gasoline feedstock inlet, and subjected to fractionation therein to obtain a light gasoline fraction and a heavy gasoline fraction; the heavy gasoline fraction is introduced into the desulfurization-aromatization reactor through the heavy gasoline fraction inlet, and subjected to desulfurization and aromatization in the presence of hydrogen to obtain a desulfurization-aromatization product.

In certain preferred embodiments, the system further comprises a high pressure separator and a mixer, wherein the desulfurization-aromatization product outlet of the desulfurization-aromatization reactor is in fluid communication with an inlet of the high pressure separator; an outlet of the high pressure separator is in fluid communication with an inlet of the mixer; and the light gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with an inlet of the mixer, wherein the desulfurization-aromatization product is separated in the high pressure separator into an olefin-containing tail gas and a heavy gasoline product, and the light gasoline fraction is mixed with the heavy gasoline product in the mixer to obtain a gasoline product.

In certain preferred embodiments, the system further comprises an etherification unit, wherein the light gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with an inlet of the etherification unit, and the light gasoline fraction is subjected to etherification in the etherification unit to obtain an etherified product.

The present application has at least one of the following advantageous effects as compared with the prior arts:

1. In the process of the present application, a gasoline feedstock with high sulfur and olefin contents is split into a light gasoline fraction and a heavy gasoline fraction, and then the heavy gasoline fraction is subjected to desulfurization and aromatization using an adsorption desulfurization catalyst and an aromatization catalyst, so that the sulfur in the gasoline can be

reduced and the olefins in the gasoline can be aromatized at the same time, thereby reducing the olefin content of the gasoline, and increasing the octane number of the gasoline while maintaining a high yield of gasoline.

2. The desulfurization and aromatization of the present application can be carried out using existing adsorption desulfurization reactors with no need to modify them.

3. The desulfurization and aromatization of the present application are carried out in one reactor by using two kinds of catalysts, and thus the need for a separate aromatization reactor and its ancillary system in stepwise treatment processes (i.e. desulfurization and then aromatization or aromatization and then desulfurization) for gasoline can be avoided. Meanwhile, the problem associated with the modification of existing processes for producing difunctional catalysts for gasoline desulfurization and aromatization and the low wear strength of the catalyst can also be avoided. This provides not only an improvement in the reaction efficiency, but also a reduction in the investment cost.

4. Preferably, the aromatization catalyst of the present application has undergone a passivation and/or aging treatment to impart a moderate activity to the aromatization catalyst, thereby facilitating the aromatization process.

5. In the present application, the light gasoline fraction is preferably subjected to etherification, which can not only reduce the olefin content thereof, but also produce a high-octane etherified oil, and increase the octane number of the gasoline product.

6. The etherification preferably employed in the present application can further reduce light components in the gasoline product and thus reduce the vapor pressure of gasoline.

Other features and advantages of the present application will be described in detail in the Detailed Description section below.

Brief description of the drawings

The drawings are provided to help the understanding of the present application, and should be considered as a part of the present description. The present invention will be illustrated with reference to the drawings and the embodiments described herein below, which should not be considered to be limiting. In the drawings:

Figure 1 is a schematic illustration of a preferred embodiment of the process and system of the present application.

Description of the reference numerals

1	Gasoline feedstock	2	Gasoline feedstock fractionation column
3	Heavy gasoline fraction	4	Hydrogen
5	Desulfurization-aromatization reactor		
6	Desulfurization-aromatization product		
7	High pressure separator	8	Olefin-containing tail gas
9	Heavy gasoline product	10	Light gasoline fraction
11	Pretreatment unit	12	Pre-etherification light gasoline
13	Alcohol-containing stream	14	Etherification unit
15	Etherification product	16	Etherification product fractionation column
17	Alcohol-containing tail gas	18	Etherified oil
19	Mixer	20	Gasoline product
21	Cracking gas separation unit	22	Recycle hydrogen
23	Olefin-containing liquid hydrocarbon		

Detailed description of the invention

Embodiments of the present application will be described in detail below with reference to the drawings. It should be understood that the embodiments described herein are merely illustrative and not restrictive.

Any numerical values (including the endpoints of the numerical ranges) disclosed herein are not limited to the precise value thereof, but should be understood to cover all values close to said precise value. Moreover, for the numerical ranges disclosed herein, one or more new numerical ranges can be obtained by combining the endpoints of the ranges, combining the endpoints with specific values within the ranges, or combining specific values within the ranges, and such new numerical ranges are also considered to be specifically disclosed herein.

The RIPP test methods involved in the present application can be found in "Petrochemical analysis methods", edited by Cuiding YANG et al., Science Press, September 1990, pages 263-268 and 303-304, ISBN: 7-03-001894-X.

In a first aspect, the present application provides a process for treating gasoline, comprising:

1) splitting a gasoline feedstock into a light gasoline fraction and a heavy gasoline fraction;

2) subjecting at least a portion of the resulting light gasoline fraction to etherification to obtain an etherified oil; and

3) contacting the resulting heavy gasoline fraction with a mixed catalyst and subjecting it to desulfurization and aromatization in the presence of hydrogen to obtain a heavy gasoline product;

wherein the mixed catalyst comprises an adsorption desulfurization catalyst and an aromatization catalyst, and the aromatization catalyst is selected from the group consisting of a fresh aromatization catalyst, a passivated aromatization catalyst, an aged aromatization catalyst, or any combination thereof.

In a second aspect, the present application provides a process for treating gasoline, comprising:

1) splitting a gasoline feedstock into a light gasoline fraction and a heavy gasoline fraction;

2) optionally, subjecting at least a portion of the resulting light gasoline fraction to etherification to obtain an etherified oil; and

3) contacting the resulting heavy gasoline fraction with a mixed catalyst and subjecting it to desulfurization and aromatization in the presence of hydrogen to obtain a heavy gasoline product;

wherein the mixed catalyst comprises an adsorption desulfurization catalyst and an aromatization catalyst, and at least about 50 wt%, preferably at least about 80 wt%, more preferably at least about 90 wt%, particularly preferably at least about 95 wt%, and most preferably about 100 wt% of the aromatization catalyst has undergone a passivation and/or aging treatment.

In certain preferred embodiments, the process for treating gasoline further comprises: 4) mixing at least a portion of the light gasoline fraction and/or at least a portion of the etherified oil with at least a portion of the heavy gasoline product to provide a gasoline product.

As used herein, the term "desulfurization and aromatization" refers to a process in which a gasoline feedstock is subjected to desulfurization and the conversion of olefins to aromatic hydrocarbons by the combined action of an adsorption desulfurization catalyst and an aromatization catalyst in the presence of hydrogen, which may be accompanied by a cracking reaction. In certain preferred embodiments, the desulfurization and aromatization are carried out under conditions including: a reaction temperature within a range from about 350 to about

500 °C, preferably from about 380 to about 420 °C; and a weight hourly space velocity within a range from about 2 h⁻¹ to about 50 h⁻¹, preferably from about 5 h⁻¹ to about 20 h⁻¹; a reaction pressure within a range from about 0.5 MPa to about 3.0 MPa, preferably from about 1.5 MPa to about 2.5 MPa; and a volume ratio of hydrogen to the heavy gasoline fraction (under standard conditions (STP) 0 °C (273 K), 1.01 × 10⁵ Pa) within a range from about 1 to about 500, preferably from about 50 to about 200.

The adsorption desulfurization catalyst used in the present application is not particularly limited, and may be any catalyst known to those skilled in the art that is suitable for used in the adsorption desulfurization of gasoline. In some preferred embodiments, the adsorption desulfurization catalyst comprises silica, alumina, zinc oxide, and a desulfurization active metal, and the desulfurization active metal is at least one selected from the group consisting of cobalt, nickel, copper, iron, manganese, molybdenum, tungsten, silver, tin and vanadium.

In certain preferred embodiments, on the basis of oxides, the zinc oxide is present in an amount ranging from about 10% to about 90% by weight, the silica is present in an amount ranging from about 5% to about 85% by weight, and the alumina is present in an amount ranging from about 5% to about 30% by weight based on the dry weight of the adsorption desulfurization catalyst; and on the elemental basis, the desulfurization active metal is present in the adsorption desulfurization catalyst in an amount ranging from about 5% to about 30% by weight based on the dry weight of the adsorption desulfurization catalyst.

In a preferred embodiment, the adsorption desulfurization catalyst may further comprise about 1% to about 10% by weight of a coke-like material. Industrial practice shows that the carbon content on the adsorption desulfurization catalyst has an influence on the desulfurization efficiency of the adsorption desulfurization catalyst and the loss of the octane number of gasoline. With the increase of carbon content of the adsorption desulfurization catalyst, the desulfurization efficiency of the adsorption desulfurization catalyst is gradually decreased, and the loss of the octane number of gasoline is gradually reduced accordingly. Likewise, it is highly preferable that the adsorption desulfurization catalyst has a certain sulfur content. The practice shows that the sulfur content of a spent adsorption desulfurization catalyst is in a range from about 9% to about 10% by weight, the sulfur content of a regenerated adsorption desulfurization catalyst is in a range from about 5% to about 6% by weight, and it is most preferable that the difference in sulfur content between the spent adsorption desulfurization catalyst and the regenerated adsorption desulfurization catalyst is

about 4% by weight.

As used herein, the term "aromatization catalyst" refers to a catalyst capable of converting a hydrocarbon such as an olefin or the like in a gasoline feedstock into an aromatic hydrocarbon, which generally comprises a molecular sieve, and preferably comprises a
5 molecular sieve, a support, and a metal. In certain preferred embodiments, on dry basis, the aromatization catalyst comprises about 10% to about 30% by weight of a molecular sieve, about 0% to about 20% by weight of an aromatization active metal oxide and about 50% to about 90% by weight of a support, based on the total weight of the aromatization catalyst.

In certain further preferred embodiments, the molecular sieve comprises a Y molecular
10 sieve and/or an MFI structural molecular sieve, preferably a five-membered high silica molecular sieve, which may be of the hydrogen type or may be modified by a rare earth metal and/or phosphorus, preferably having a silica-alumina ratio of greater than 100, more preferably greater than 150.

In certain further preferred embodiments, the aromatization active metal may show some
15 desulfurization or hydrocarbon conversion capability, and may, for example, be at least one selected from the group consisting of metal elements of Group IVB, metal elements of Group VB, metal elements of Group VIB, metal elements of Group VIII, metal elements of Group IB, metal elements of Group IIB, and metal elements of Group IIIA. In certain still further preferred embodiments, the metal element of Group IVB is Zr or/and Ti, the metal element of
20 Group VB is V, the metal element of Group VIB is Mo or/and W, the metal element of Group VIII is one or more selected from the group consisting of Fe, Co, and Ni, the metal element of Group IB is Cu, the metal element of Group IIB is Zn, and the metal element of Group IIIA is Ga. In some particularly preferred embodiments, the aromatization active metal is at least one selected from the group consisting of Fe, Zn and Ga, and its content is preferably within a
25 range from about 0.5% to about 5% by weight.

In certain further preferred embodiments, the support comprises silica and/or alumina.

In certain preferred embodiments, the aromatization catalyst typically has a particle size within a range from 20 to 120 microns, which is comparable to the particle size of the adsorption desulfurization catalyst. Preferably, in the present application, the adsorption
30 desulfurization catalyst and the aromatization catalyst are separately formed (for example, by spray drying) and then mixed before use.

The ratio of the adsorption desulfurization catalyst to the aromatization catalyst in the

mixed catalyst of the present application may vary depending on the olefin and sulfur content of the gasoline feedstock. In certain preferred embodiments, the percentage by weight of the aromatization catalyst in the mixed catalyst is within a range from about 1% to about 30% by weight, preferably from about 3% to about 15% by weight.

5 In certain preferred embodiments, the aromatization catalyst of the present application can be prepared in accordance with the following steps: mixing the starting material for preparing the aromatization catalyst with water to make a slurry, and then subjecting the slurry to spray-drying and calcination; wherein the starting material comprises about 15% to about 60% by weight of a natural mineral, about 10% to about 30% by weight of a precursor of an
10 inorganic oxide binder, and about 20% to about 80% by weight of a MFI structural molecular sieve containing phosphorus and supported metal, based on the dry weight of the starting material.

 In a further preferred embodiment, the starting material comprises about 20% to about 55% by weight of the natural mineral, about 12% to about 28% by weight of the precursor of
15 the inorganic oxide binder and about 35% to about 70% by weight of the MFI structural molecular sieve containing phosphorus and supported metal, based on the dry weight of the starting material.

 As used herein, the term "natural mineral" refers to a natural element or compound formed under the combined action of various substances in the earth's crust (called geological
20 action), which has a characteristic and relatively fixed chemical composition that can be expressed by a chemical formula. For example, it may comprise at least one selected from the group consisting of kaolin clay, halloysite, montmorillonite, diatomaceous earth, attapulgite, sepiolite, indianite, hydrotalcite, bentonite, and rectorite.

 As used herein, the term "inorganic oxide binder" refers to an inorganic oxide that acts as
25 a binder in the catalyst, and may, for example, comprise at least one selected from the group consisting of silica, alumina, zirconia, titania and amorphous silica-alumina.

 As used herein, the term "precursor of an inorganic oxide binder" refers to a starting material for preparing a catalytic cracking catalyst, which is generally used for producing an inorganic oxide binder in the catalytic cracking catalyst, and may, for example, comprise at
30 least one selected from the group consisting of silica sol, alumina sol, peptized pseudo-boehmite, silica-alumina sol, and phosphorus-containing alumina sol.

 As used herein, the term "supported metal" refers to a metal supported on a molecular

sieve by a loading method, excluding aluminum and alkali metals such as sodium or potassium. The supported metal used in the present application is not particularly limited and may be zinc, gallium and/or iron, and may also include other metals.

In certain further preferred embodiments, the supported metal is zinc and/or gallium, and the natural mineral comprises at least one selected from the group consisting of kaolin clay, halloysite, montmorillonite, diatomaceous earth, attapulgite, sepiolite, indianite, hydrotalcite, bentonite, and rectorite, and the inorganic oxide binder comprises at least one selected from the group consisting of silica, alumina, zirconia, titania, and amorphous silica-alumina.

In certain still further preferred embodiments, the MFI structural molecular sieve is at least one selected from the group consisting of ZSM-5, ZSM-8, and ZSM-11.

In certain preferred embodiments, the MFI structural molecular sieve in the aromatization catalyst has a $n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)$ ratio of greater than about 100; the molecular sieve has a phosphorus content, on the basis of P_2O_5 , within a range from about 0.1% to about 5% by weight, based on the dry weight of the molecular sieve; the molecular sieve has a supported-metal content, on the basis of oxides, within a range from about 0.5% to about 5% by weight, based on the dry weight of the molecular sieve; the Al distribution parameter $D(\text{Al})$ of the molecular sieve satisfies: $0.6 \leq D(\text{Al}) \leq 0.85$, wherein $D(\text{Al}) = \text{Al}(\text{S})/\text{Al}(\text{C})$, and $\text{Al}(\text{S})$ denotes the aluminum content in any region of greater than 100 square nanometers within an inward distance H from the edge of the crystal face of the molecular sieve grain determined by the TEM-EDS method (where TEM means transmission electron microscope, EDS means X-ray energy spectrum, and TEM-EDS means transmission electron microscope with X-ray energy spectrum); $\text{Al}(\text{C})$ denotes the aluminum content in any region of greater than 100 square nanometers within an outward distance H from the geometric center of the crystal face of the molecular sieve grain determined by the TEM-EDS method, wherein H denotes 10% of the distance from a certain point at the edge of the crystal face to the geometric center of the crystal face; the supported-metal distribution parameter $D(\text{M})$ of the molecular sieve satisfies: $2 \leq D(\text{M}) \leq 10$, where $D(\text{M}) = \text{M}(\text{S})/\text{M}(\text{C})$, and $\text{M}(\text{S})$ denotes the supported-metal content in any region of greater than 100 square nanometers within an inward distance H from the edge of the crystal face of the molecular sieve grain determined by the TEM-EDS method, $\text{M}(\text{C})$ denotes the supported-metal content in any region of greater than 100 square nanometers within an outward distance H from the geometric center of the crystal face of the molecular sieve grain determined by the TEM-EDS method; the molecular sieve has a mesopore volume percentage

within a range from about 40% to about 80% relative to the total pore volume thereof, with the volume percentage of mesopores having a pore diameter within a range from about 2 nm to about 20 nm relative to the total mesopore volume being preferably greater than about 90%; and the molecular sieve has a percentage of strong acid content relative to the total acid content within a range from about 60% to about 80%, with a ratio of the Bronsted acid (B acid) content to the Lewis acid (L acid) content being within a range from about 15 to about 80.

In certain further preferred embodiments, the MFI structural molecular sieve has a $n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)$ ratio of greater than about 120; the molecular sieve has a phosphorus content, on the basis of P_2O_5 , within a range from about 0.2% to about 4% by weight, based on the dry weight of the molecular sieve; the molecular sieve has a supported-metal content, on the basis of oxides, within a range from about 0.5% to about 3% by weight, based on the dry weight of the molecular sieve; the Al distribution parameter $D(\text{Al})$ of the molecular sieve satisfies: $0.65 \leq D(\text{Al}) \leq 0.8$; the supported-metal distribution parameter $D(\text{M})$ of the molecular sieve satisfies: $3 \leq D(\text{M}) \leq 6$; the molecular sieve has a mesopore volume percentage within a range from about 50% to about 70% relative to the total pore volume thereof, with the volume percentage of mesopores having a pore diameter within a range from about 2 nm to about 20 nm relative to the total mesopore volume being greater than about 92%; and the molecular sieve has a percentage of strong acid content relative to the total acid content within a range from about 65% to about 75%, with the ratio of the B acid content to the L acid content being within a range from about 20 to about 50.

The TEM-EDS method used in the present application for determining the aluminum content and the supported-metal content of the molecular sieve is well known to those skilled in the art, wherein the determination of the geometric center is also well known to those skilled in the art and can be calculated according to a formula, which will not be described herein in detail. The geometric center of a symmetrical figure is generally the intersection of the lines connecting the opposite vertices thereof. For example, the geometric center of the hexagonal crystal face of a conventional hexagonal ZSM-5 molecular sieve is at the intersection of the three lines connecting the opposite vertices thereof, where the crystal face is one face of a regular grain, and the inward and outward directions refer to the inward and outward directions on the crystal face.

According to the present application, the mesopore volume percentage of the molecular sieve relative to the total pore volume thereof is determined by the nitrogen adsorption BET

specific surface area measuring method, wherein the mesopore volume refers to the volume of pores having a pore diameter greater than about 2 nm and less than about 100 nm; the percentage of strong acid content to the total acid content of the molecular sieve is determined by the NH₃-TPD method, wherein the acid center of the strong acid is specified as the acid center having a corresponding NH₃ desorption temperature of greater than 300 °C; the ratio of the B acid content to the L acid content is determined by the pyridine adsorption infrared acidity measuring method.

In certain preferred embodiments, the MFI structural molecular sieve containing phosphorus and supported metal can be prepared in accordance with the following steps:

a. subjecting a crystallized MFI structural molecular sieve slurry to filtration and washing, to obtain a water-washed molecular sieve, wherein the water-washed molecular sieve has a sodium content, on the basis of sodium oxide, of less than 3% by weight, based on the total dry weight of the water-washed molecular sieve;

b. subjecting the water-washed molecular sieve obtained in step a to desiliconization in an alkaline solution, and then to filtration and washing, to obtain a desiliconized molecular sieve;

c. subjecting the desiliconized molecular sieve obtained in step b to ammonium ion-exchange to obtain an ammonium ion-exchanged molecular sieve, wherein the ammonium ion-exchanged molecular sieve has a sodium content, on the basis of sodium oxide, of less than 0.2% by weight, based on the total dry weight of the ammonium ion-exchanged molecular sieve;

d. subjecting the ammonium ion-exchanged molecular sieve obtained in step c to dealumination in a composite acid dealuminant solution consisting of a fluorosilicic acid, an organic acid and an inorganic acid, and then to filtration and washing, to obtain a dealuminated molecular sieve;

e. subjecting the dealuminated molecular sieve obtained in the step d to phosphorus modification and loading of the supported metal, to obtain a modified molecular sieve; and

f. subjecting the modified molecular sieve obtained in the step e to hydrothermal calcination to obtain the MFI structural molecular sieve containing phosphorus and supported metal.

The "crystallized MFI structural molecular sieve slurry" used in the step a of the present application can be obtained by methods well known to those skilled in the art, and will not be

described herein in detail. In addition, the MFI structural molecular sieve is also well known to those skilled in the art, and may be obtained by amine-free crystallization, or may be a molecular sieve prepared by a templating method. The molecular sieve obtained by amine-free crystallization does not need to be calcined, while the molecular sieve prepared by the templating method needs to be calcined in air after drying, and the ZSM-5 molecular sieve normally has a silica-alumina ratio of less than 100.

The desiliconization performed using an alkaline solution in the step b of the present application is well known to those skilled in the art. For example, the alkaline solution used in the step b may be selected from the group consisting of sodium hydroxide solution and/or potassium hydroxide solution, preferably sodium hydroxide solution. The desiliconization conditions may include: a weight ratio on dry basis of the molecular sieve to the alkali in the alkaline solution within a range of about 1:(0.1-1), preferably about 1:(0.15-0.4); a desiliconization temperature within a range from room temperature to about 100 °C, preferably from about 50 to about 85 °C, a desiliconization time within a range from about 15 minutes to about 8 hours, preferably from about 30 minutes to about 4 hours.

The ammonium ion-exchange carried out in the step c of the present application is well known to those skilled in the art. For example, in step c, the alkali-treated desiliconized molecular sieve can be subjected to ion exchange at a temperature within a range from room temperature to about 100 °C for about 0.5 to about 2 hours with a weight ratio of the molecular sieve: ammonium salt: H₂O within a range of about 1: (0.1-1): (5-10), and then to filtration, so as to provide a Na₂O content of the zeolite of less than about 0.2% by weight. The ammonium salt may be any commonly used inorganic ammonium salt, for example, at least one selected from the group consisting of ammonium chloride, ammonium sulfate, and ammonium nitrate.

The "dealumination" treatment involved in the step d of the present application is known per se to those skilled in the art, but it has not been reported to use a combination of an inorganic acid, an organic acid and a fluorosilicic acid in the dealumination as in the step d of the present application. The dealumination may be carried out in one or more stages, in which the organic acid may be firstly mixed with the ammonium ion-exchanged molecular sieve, and then the fluorosilicic acid and the inorganic acid may be mixed with the ammonium ion-exchanged molecular sieve, that is, the organic acid may be firstly added into the ammonium ion-exchanged molecular sieve, and the fluorosilicic acid and the inorganic acid may then be slowly added in a co-current manner, or alternatively the fluorosilicic acid and the

inorganic acid may be added successively, preferably the fluorosilicic acid and the inorganic acid are slowly added in a co-current manner. The dealumination can be carried out under the following conditions: a weight ratio on dry basis of the molecular sieve : fluorosilicic acid : organic acid : inorganic acid within a range of about 1: (0.02-0.5): (0.05-0.5): (0.05-0.5),
5 preferably about 1: (0.05-0.3): (0.1-0.3): (0.1-0.3); a treatment temperature within a range from about 25 to about 100 °C, and a treatment time within a range from about 0.5 to about 6 hours.

It has been proved via experimentation that, by using the composite acid system in the dealumination of the present application, the silica-alumina ratio of the molecular sieve can be effectively improved, the aluminum distribution can be adjusted, and the acid distribution can
10 be improved while maintaining the crystal structure of the molecular sieve and the integrity of its pore structure of mesopores, under the synergistic action of the three acids.

The organic acid and the inorganic acid used in the step d of the present application may be those conventionally used in the art. For example, the organic acid may be at least one selected from the group consisting of ethylenediamine tetraacetic acid, oxalic acid, citric acid,
15 and sulfosalicylic acid, preferably oxalic acid; and the inorganic acid may be at least one selected from the group consisting of hydrochloric acid, sulfuric acid and nitric acid, preferably hydrochloric acid.

The washing carried out in the step d of the present application is well known to those skilled in the art, and may be carried out, for example, by rinsing the filtered molecular sieve
20 with about 5-10 times of water at about 30-60 °C.

The phosphorus modification and the loading of the supported metal carried out in the step e of the present application are well known to those skilled in the art. For example, the phosphorus modification in the step e may comprise the step of subjecting the molecular sieve to impregnation and/or ion exchange with at least one phosphorus-containing compound
25 selected from the group consisting of phosphoric acid, ammonium hydrogen phosphate, ammonium dihydrogen phosphate and ammonium phosphate; and the loading of the supported metal in the step e may comprise the steps of: dissolving a soluble salt containing at least one supported metal selected from the group consisting of zinc and gallium in deionized water, adjusting the pH with ammonia water to precipitate the supported metal in the form of
30 hydroxide, and then mixing the resulting precipitate uniformly with the molecular sieve.

The hydrothermal calcination of the molecular sieve carried out in the step f of the present application is well known to those skilled in the art. For example, the hydrothermal

calcination in the step f can be carried out under the following conditions: a calcination atmosphere of steam, a calcination temperature within a range from about 400 to about 800 °C and a calcination time within a range from about 0.5 to about 8 hours.

In certain preferred embodiments, the inventors of the present application have surprisingly found that a better effect can be obtained by using an aromatization catalyst having a micro-activity within a range from about 20 to about 55, which can be determined according to the test method of RIPP 92-90 in catalytic cracking field for determining the micro-activity of equilibrium catalysts, for which the details can be referred to the working examples. Generally, commercially available or self-made qualified fresh aromatization catalysts normally have a micro-activity above 60, and thus show a higher activity and a stronger cracking performance. Therefore, prior to use in the desulfurization and aromatization, such fresh aromatization catalysts are preferably subjected to a pre-treatment to reduce the acid content and increase the acid strength, thereby facilitating the reduction of the hydrogen transfer reaction.

In certain preferred embodiments, the aromatization catalyst has been subjected to passivation prior to use in the desulfurization and aromatization. Preferably, the passivation comprises the step of contacting the aromatization catalyst, such as a fresh aromatization catalyst, with a compound containing carbon, sulfur and/or nitrogen to conduct a passivation reaction.

In certain further preferred embodiments, the passivated aromatization catalyst comprises about 0.1% to about 5.0% by weight of passivated species, wherein the passivated species comprises at least one element selected from the group consisting of carbon, sulfur, and nitrogen.

In certain preferred embodiments, the passivation can be carried out in a reactor located outside of the desulfurization-aromatization reactor, or in the pre-lift segment of a fluidized reactor used as the desulfurization-aromatization reactor. The compound containing carbon, sulfur and/or nitrogen used for the passivation may be gasoline, hydrogen sulfide, carbon disulfide, ammonia, anilines, pyridines or quinolines, etc. The gasoline may be the gasoline feedstock used, or other gasoline from the outside, such as catalytic cracking gasoline, steam cracking gasoline or other olefin-containing gasoline.

In certain preferred embodiments, the aromatization catalyst is subjected to an aging treatment prior to use in the desulfurization and aromatization. As used herein, the term "aging"

refers to a process in which the aromatization catalyst, such as a fresh aromatization catalyst, is subjected to a treatment at elevated temperature in the presence of steam to reduce its activity. In certain further preferred embodiments, the aging treatment is carried out under the following conditions: a temperature within a range from about 500 to about 800 °C, preferably from about 600 to about 800 °C, more preferably from about 700 to about 800 °C; an ageing time within a range from about 1 to about 360 hours, preferably from about 2 to about 48 hours, more preferably from about 4 to about 24 hours; and an aging atmosphere containing steam, preferably an atmosphere comprising about 100% steam.

In certain preferred embodiments of the aging treatment, the fresh aromatization catalyst is contacted with steam or an aging medium containing steam, and aged in a hydrothermal environment at a temperature within a range from about 500 °C to about 800 °C for about 1 hour to about 360 hours, to obtain an aged aromatization catalyst. In certain further preferred embodiments, the aging medium may comprise air, dry gas, regenerated flue gas, gas obtained after the combustion of a dry gas in air, gas obtained after the combustion of burning oil in air, or other gases such as nitrogen. Preferably, the weight fraction of steam in the aging medium containing steam is within a range from about 0.2 to about 0.9, more preferably from about 0.40 to about 0.60. Preferably, the regenerated flue gas may come from the catalyst regeneration unit of the present application or may come from a regeneration unit of other processes.

In certain preferred embodiments, the aging treatment is carried out in an aging reactor, preferably a dense phase fluidized bed. In certain further preferred embodiments, the aging treatment comprises the step of subjecting the fresh aromatization catalyst to aging at 800 °C under the condition of 100% steam for a time period within a range from 4 h to 17 h.

In certain preferred embodiments, at least about 50 wt%, preferably at least about 80 wt%, more preferably at least about 90 wt%, particularly preferably at least about 95 wt%, and most preferably about 100 wt% of the aromatization catalyst has undergone a passivation and/or aging treatment.

The desulfurization and aromatization of the present application are preferably carried out in a fluidized reactor to facilitate a rapid regeneration of the aromatization catalyst. In certain preferred embodiments, the fluidized reactor is selected from the group consisting of fluidized bed reactors, riser reactors, downer reactors, composite reactors composed of a riser reactor and a fluidized bed reactor, composite reactors composed of a riser reactor and a

downer reactor, composite reactors composed of two or more riser reactors, composite reactors composed of two or more fluidized bed reactors, and composite reactors composed of two or more downer reactors, preferably a riser reactor, a fluidized bed reactor or a combination thereof. Preferably, each of the above reactors may be divided into two or more reaction zones.

- 5 In certain preferred embodiments, the fluidized bed reactor is one or more selected from the group consisting of fixed fluidized bed, particulate fluidized bed, bubbling bed, turbulent bed, fast bed, transport bed, and dense phase fluidized bed reactors. The riser reactor is one or more selected from the group consisting of equal-diameter riser reactors, equal-linear-speed riser reactors, and various unequal-diameter riser reactors. In a particularly preferred embodiment,
10 the fluidized reactor is a dense phase fluidized reactor.

The gasoline feedstock used in the present application may be any conventional gasoline feedstock commonly used in the art. In certain preferred embodiments, the gasoline feedstock may be at least one selected from the group consisting of catalytic cracking gasoline, deep catalytic cracking gasoline, coker gasoline, thermal cracking gasoline, and straight-run gasoline,
15 or a fraction thereof. In certain preferred embodiments, the gasoline feedstock is a gasoline having a high olefin and sulfur content, of which the olefin volume fraction is generally greater than about 20% by volume, preferably greater than about 30% by volume, more preferably greater than about 40% by volume, and even more preferably greater than about 50% by volume; and the sulfur content is generally about 10 $\mu\text{g/g}$ or above, preferably greater than
20 about 50 $\mu\text{g/g}$, more preferably greater than about 100 $\mu\text{g/g}$, further preferably greater than about 500 $\mu\text{g/g}$, still more preferably greater than about 1000 $\mu\text{g/g}$. The organic sulfide in the gasoline feedstock is not particularly limited, and may be, for example, mercaptan, thioether, thiophene, alkylthiophene, benzothiophene, and/or methylbenzothiophene.

The split point between the light gasoline fraction and the heavy gasoline fraction
25 adopted in the present application may be varied as needed. In certain preferred embodiments, the split point between the light gasoline fraction and the heavy gasoline fraction is within a range from 60 to 80 $^{\circ}\text{C}$, more preferably from about 65 to about 70 $^{\circ}\text{C}$. In certain further preferred embodiments, the gasoline feedstock is split in the fractionation column in accordance with the distillation range from low to high. More preferably, the fractionation
30 column for splitting the gasoline is operated under the following conditions: an overhead temperature within a range from about 60 to about 80 $^{\circ}\text{C}$, a bottom temperature within a range from about 120 to about 160 $^{\circ}\text{C}$ and an operating pressure within a range from about 0.05 to

about 0.3 MPa.

As used herein, the term "etherification" refers to a process in which a lower hydrocarbon (e.g., isopentene and cyclopentene) below C5 in the light gasoline fraction is subjected to an etherification reaction with an alcohol to produce a high-octane etherified oil.

5 In certain preferred embodiments, the etherification comprises the step of contacting the light gasoline fraction with an alcohol to subject the olefin in the light gasoline fraction to an etherification reaction with the alcohol in the presence of an etherification catalyst, to obtain the etherified oil, wherein the etherification is carried out under the following conditions: a temperature within a range from about 20 to about 200 °C, a pressure within a range from
10 about 0.1 to about 5 MPa, a weight hourly space velocity within a range from about 0.1 to about 20 h⁻¹, and a molar ratio of the alcohol to the light gasoline fraction within a range of about 1: (0.1-100). In certain further preferred embodiments, the etherification catalyst comprises at least one selected from the group consisting of resins, molecular sieves, and heteropolyacids. In certain still further preferred embodiments, the alcohol is at least one
15 selected from the group consisting of methanol, ethanol, and propanol.

In certain preferred embodiments of the etherification, a strongly acidic cation-exchange resin catalyst is charged in a one-stage etherification and/or two-stage etherification fixed bed reactor, and a light gasoline fraction that has undergone a pre-treatment such as desulfurization and removal of dienes is passed into the etherification fixed bed reactor to conduct an
20 etherification reaction under the following conditions: a reaction temperature within a range from about 50 to about 90 °C, a liquid hourly space velocity within a range from about 1.0 to about 3.0 h⁻¹, and a molar ratio of methanol to active olefins in the light gasoline fraction within a range from about 1 to about 2, the etherified product is sent to a rectification column for separation, an etherified oil is obtained at the bottom of the column, and unreacted light
25 hydrocarbons and methanol are recycled. As used herein, the term "active olefin" refers to an olefin having a double bond at a tertiary carbon atom.

In certain further preferred embodiments, the etherification is carried out under the following conditions: a reaction temperature comprising an inlet temperature within a range from about 55 to about 60 °C and an outlet temperature of less than about 90 °C, a space
30 velocity within a range from about 1 to about 2 h⁻¹, and a molar ratio of methanol to active olefins in the light gasoline fraction within a range from about 1.2 to about 1.4. In some embodiments, the olefin content in one-stage etherification is relatively high, and a

mixed-phase bed reactor is suitable for use therein; while the olefin content in two-stage etherification is relatively low, and an adiabatic fixed-bed reactor is suitable for use therein. In certain preferred embodiments, an isomerization unit can also be employed in the light gasoline etherification process. Light gasoline etherification has many advantages, such as reducing the olefin content of gasoline, increasing the octane number, lowering the vapor pressure, increasing the added value and enhancing the blending efficiency. The etherified oil can be used as a blending component for adjusting the octane number of gasoline, or can be mixed with the heavy gasoline fraction to provide a full-range gasoline product.

In certain preferred embodiments, the light gasoline fraction has been subjected to a pre-treatment prior to the etherification to remove impurities such as sulfur compounds and/or dienes, thereby prolonging the service life of the etherification catalyst. In certain further preferred embodiments, the pretreatment is at least one selected from the group consisting of alkaline liquid extraction, mercaptan conversion, and selective hydrotreatment. In certain still further preferred embodiments, the alkaline liquid extraction is used to remove mercaptan from the light gasoline fraction using an alkaline solution by extracting the mercaptan into the alkaline solution; the mercaptan conversion is used to remove small-molecule mercaptan by converting it into other sulfides, which can be carried out by a conventional alkali-free deodorization process, a pre-hydrogenation process, etc., wherein the catalyst and the cocatalyst used can be catalysts commonly used in the art. The selective hydrotreatment is well known to those skilled in the art, and is used to remove dienes from gasoline and allow the isomerization of 3-methyl-1-butene to 2-methyl-1-butene.

In a third aspect, the present application provides a system for treating gasoline, comprising a gasoline feedstock fractionation column and a desulfurization-aromatization reactor, wherein the gasoline feedstock fractionation column is provided with a gasoline feedstock inlet, a heavy gasoline fraction outlet, and a light gasoline fraction outlet; the desulfurization-aromatization reactor is provided with a heavy gasoline fraction inlet, a hydrogen inlet, and a desulfurization-aromatization product outlet; the heavy gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with the heavy gasoline fraction inlet of the desulfurization-aromatization reactor,

wherein a gasoline feedstock is introduced into the gasoline feedstock fractionation column through the gasoline feedstock inlet, and subjected to fractionation therein to obtain a light gasoline fraction and a heavy gasoline fraction; the heavy gasoline fraction is introduced

into the desulfurization-aromatization reactor through the heavy gasoline fraction inlet, and subjected to desulfurization and aromatization in the presence of hydrogen to obtain a desulfurization-aromatization product.

In certain preferred embodiments, the system further comprises a high pressure separator and a mixer, the high pressure separator being provided with a desulfurization-aromatization product inlet, an olefin-containing tail gas outlet, and a heavy gasoline product outlet, wherein the desulfurization-aromatization product outlet of the desulfurization-aromatization reactor is in fluid communication with the desulfurization-aromatization product inlet of the high pressure separator; the heavy gasoline product outlet of the high pressure separator is in fluid communication with an inlet of the mixer and the light gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with an inlet of the mixer, wherein the desulfurization-aromatization product is separated in the high pressure separator to produce an olefin-containing tail gas and a heavy gasoline product, and the light gasoline fraction is mixed with the heavy gasoline product in the mixer to obtain a gasoline product.

In certain preferred embodiments, the system further comprises an etherification unit, wherein the light gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with an inlet of the etherification unit, and the light gasoline fraction is subjected to etherification in the etherification unit to obtain an etherified product.

In certain further preferred embodiments, the system further comprises a pretreatment unit, wherein the light gasoline fraction outlet of the gasoline feedstock fractionation column is in fluid communication with the inlet of the etherification unit via the pretreatment unit.

In certain further preferred embodiments, the system further comprises a cracking gas separation unit, the olefin-containing tail gas outlet of the high pressure separator being in fluid communication with an inlet of the cracking gas separation unit, wherein the olefin-containing tail gas is separated in the cracking gas separation unit to obtain a recycle hydrogen and an olefin-containing liquid hydrocarbon, and the olefin-containing liquid hydrocarbon is sent to the etherification unit for etherification.

In certain further preferred embodiments, the system further comprises an etherification product fractionation column, wherein the etherification product fractionation column is provided with an etherification product inlet, an alcohol-containing tail gas outlet, and an etherified oil outlet; an outlet of the etherification unit is in fluid communication with the etherification product inlet of the etherification product fractionation column, and the etherified

oil outlet of the etherification product fractionation column is in fluid communication with an inlet of the mixer;

wherein the etherification product is introduced into the etherification product fractionation column through the etherification product inlet, and subjected to fractionation therein to obtain an alcohol-containing tail gas and an etherified oil, and the light gasoline fraction and/or the etherified oil is mixed with the heavy gasoline product in the mixer to obtain a gasoline product.

In certain preferred embodiments, the heavy gasoline fraction inlet and the hydrogen inlet of the desulfurization-aromatization reactor are the same inlet.

A preferred embodiment of the process and system of the present application is described herein below with reference to the drawings, with no limitation to the present application.

As shown in FIG. 1, in a preferred embodiment, the gasoline treating system of the present application comprises a gasoline feedstock fractionation column 2, a desulfurization-aromatization reactor 5, a high pressure separator 7, a pretreatment unit 11, an etherification unit 14, an etherification product fractionation column 16, a mixer 19 and a cracking gas separation unit 21, the gasoline feedstock fractionation column 2 being provided with a gasoline feedstock inlet, a heavy gasoline fraction outlet, and a light gasoline fraction outlet, the desulfurization-aromatization reactor 5 being provided with a heavy gasoline fraction inlet, a hydrogen inlet, and a desulfurization-aromatization product outlet, the high pressure separator 7 being provided with a desulfurization-aromatization product inlet, an olefin-containing tail gas outlet, and a heavy gasoline product outlet, the etherification product fractionation column 16 being provided with an etherification product inlet, an alcohol-containing tail gas outlet, and an etherified oil outlet; wherein the light gasoline fraction outlet of the gasoline feedstock fractionation column 2 is in fluid communication with the etherification product inlet of the etherification product fractionation column 16 through the pretreatment unit 11 and the etherification unit 14 successively, the etherified oil outlet of the etherification product fractionation column 16 is in fluid communication with an inlet of the mixer 19; the heavy gasoline fraction outlet of the gasoline feedstock fractionation column 2 is in fluid communication with the heavy gasoline fraction inlet of the desulfurization-aromatization reactor 5, the desulfurization-aromatization product outlet of the desulfurization-aromatization reactor 5 is in fluid communication with the desulfurization-aromatization product inlet of the high pressure separator 7, the heavy gasoline product outlet

of the high pressure separator 7 is in fluid communication with an inlet of the mixer 19, and the olefin-containing tail gas outlet of the high pressure separator 7 is in fluid communication with an inlet of the cracking gas separation unit 21.

In the preferred embodiment illustrated in Fig. 1, the process of the present application comprises the step of feeding a gasoline feedstock 1 with a high olefin and sulfur content to a gasoline feedstock fractionation column 2 for fractional distillation, to obtain a light gasoline fraction 10 and a heavy gasoline fraction 3. The light gasoline fraction 10 is introduced into the pretreatment unit 11 and subjected to a pretreatment such as mercaptan removal to obtain a pre-etherification light gasoline 12, which is mixed with the alcohol-containing stream 13 and reacted in the etherification unit 14, the resulting etherified product 15 is fractionated in the etherification product fractionation column 16 to obtain an etherified oil 18 and an alcohol-containing tail gas 17. The heavy gasoline fraction 3 is mixed with a hydrogen gas 4 and then introduced into the desulfurization-aromatization reactor 5, and is contacted with an adsorption desulfurization catalyst and an aromatization catalyst for adsorption desulfurization and aromatization, and the desulfurization-aromatization product 6 is introduced into the high pressure separator 7 for separation to obtain an olefin-containing tail gas 8 and a heavy gasoline product 9. The olefin-containing tail gas 8 is separated in the cracking gas separation unit 21 to obtain a recycle hydrogen 22 and an olefin-containing liquid hydrocarbon 23, which is combined into the pre-etherification light gasoline 12 from the pretreatment unit 11. The heavy gasoline product 9 is combined with the etherified oil 18 obtained after etherification in the mixer 19 to provide a high-octane clean gasoline product 20.

Examples

The present application will be further illustrated with reference to the following working examples, without however limiting the present application.

Methods for Measurement

In the present application, the degree of crystallinity is determined according to the standard method of ASTM D5758-2001 (2011) e1.

In the present application, the silica-alumina ratio, $n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)$, is calculated based on the contents of silica and alumina, and the contents of silica and alumina are determined according to the standard method of GB/T 30905-2014.

In the present application, the phosphorus content is determined according to the standard method of GB/T 30905-2014, the content of the supported metal is determined according to the standard method of GB/T 30905-2014, and the sodium content is determined according to the standard method of GB/T 30905-2014.

5 For the TEM-EDS measurement method used in the present application, see "Research Technique for Solid Catalysts", Yongfang XUE, Petrochemicals, 29(3), 2000: pages 227-235.

In the present application, the total specific surface area (S_{BET}), the mesopore volume, the total pore volume, and the volume of mesopores having a diameter of 2-20 nm are determined as follows.

10 The AS-3, AS-6 Static Nitrogen Adsorbers manufactured by Quantachrome Instruments were used for measurement.

Instrument parameters: The sample was placed in a sample treating system, evacuated to 1.33×10^{-2} Pa at 300 °C, and kept at the temperature and pressure for 4 h to purify the sample. The adsorption amount and desorption amount of nitrogen in the purified sample at a liquid
15 nitrogen temperature of -196 °C under different specific pressure P/P_0 conditions were tested, and an N_2 adsorption-desorption isotherm curve was obtained. Then, the two-parameter BET equation was used to calculate the total specific surface area, the specific surface area of micropores and the specific surface area of mesopores. The adsorption amount under the specific pressure $P/P_0=0.98$ was recorded as the total pore volume of the sample, and the pore
20 size distribution of mesopores was calculated according to the BJH equation and the mesopore volume (2-100 nm) and the volume of mesopores having a diameter of 2-20 nm were calculated using the integral method.

In the present application, the method for determining the B acid content and the L acid content is as follows.

25 The FTS3000 type Fourier Infrared Spectrometer manufactured by American BIO-RAD company was used for measurement.

Test conditions: The sample was compressed into tablets and placed in an in-situ bath of the infrared spectrometer and sealed, evacuated to 10^{-3} Pa at 350 °C, and held for 1 h to allow a complete desorption of the gas molecules on the surface of the sample, and then cooled to
30 room temperature. Pyridine vapor at a pressure of 2.67 Pa was introduced into the in-situ bath, equilibrated for 30 min, warmed to 200 °C, evacuated again to 10^{-3} Pa, held for 30 min, cooled to room temperature, and scanned within the wavenumber range of 1400-1700 cm^{-1} . The

infrared spectrum of the pyridine adsorption at 200 °C was recorded. The sample in the infrared absorption cell was moved to a heat treatment zone, heated to 350 °C, evacuated to 10^{-3} Pa, held for 30 min, and cooled to room temperature. The infrared spectrum of the pyridine adsorption at 350 °C was recorded. The B acid content and the L acid content can be
5 obtained via automatic integration by the instrument.

In the present application, the method for determining the total acid content and the strong acid content is as follows.

The Autochem II2920 Temperature Programming Desorber of Micromeritics Instrument Corporation, USA, was used for measurement.

10 Test conditions: 0.2 g of the sample to be tested was weighed into a sample tube, placed in a thermal conductivity cell heating device, with He gas being used as the carrier gas (50 mL/min), heated up to 600 °C at a heating rate of 20 °C/min, and purged for 60 min to drive off impurities adsorbed on the surface of the catalyst. Then, the sample was cooled to 100 °C, kept at the temperature for 30 min, switched to a NH₃-He gas mixture (10.02 % NH₃ + 89.98 %
15 He) for adsorption for 30 min, and then purged with He gas for 90 min until the baseline was stable to desorb the physically adsorbed ammonia gas. The sample was heated to 600 °C at a heating rate of 10 °C/min for desorption, and held for 30 min. Then, the desorption was stopped. The TCD detector was used to detect the change of the gas composition, and the total acid content and the strong acid content were obtained via automatic integration by the
20 instrument. The acid center of the strong acid was specified as the acid center having a corresponding NH₃ desorption temperature of greater than 300 °C.

In the present application, the D value is calculated as follows.

In the TEM, a crystal grain was selected, which had a crystal face forming a polygon that had a geometric center, an edge, and a distance H that was 10% of the distance from the
25 geometric center to a certain point at the edge (i.e. different points at the edge having different H values). A region of greater than 100 square nanometers within an inward distance H from the edge of the crystal face, and another region of greater than 100 square nanometers within an outward distance H from the geometric center of the crystal face were arbitrarily selected, the aluminum content therein was determined, respectively, as Al(S1) and Al(C1), and a
30 calculation was conducted according to the equation $D(Al) = Al(S1)/Al(C1)$. Five different crystal grains were selected and measured, and the average value was calculated and recorded

as D(Al). The method for determining D(M) is similar to the above method for determining D(Al).

In the present application, the dry weight is determined as follows.

The molecular sieve or catalyst to be tested was placed in a muffle furnace and calcined in an air atmosphere at 600 °C for 3 hours, and the resulting calcined product was cooled to room temperature in a closed drying dish, and then weighed.

The adsorption desulfurization catalysts used in the following examples and comparative examples were produced by the Catalyst Branch of China Petroleum & Chemical Corporation under the trade name FCAS. The aromatization catalysts used included a laboratory-made catalyst, named OTAZ-C-3, and a commercial aromatization catalyst available from the Catalyst Branch of China Petroleum & Chemical Corporation under the trade name MP051. The properties of each catalyst used in the examples are shown in Table 1.

Table 1 Properties of each catalyst used in the examples

Catalyst	FCAS	OTAZ-C-3	MP051
Chemical composition, wt%			
Alumina	13	50.3	50.8
Sodium oxide	/	/	/
Nickel oxide	21	/	/
Zinc oxide	52	/	/
Gallium oxide	/	1.5	/
Silica	14	48.14	48.7
Apparent density, kg/m ³	1010	800	790
Pore volume, mL/g	/	0.27	0.23
Specific surface area, m ² /g	/	218	215
Abrasion index, wt%·h ⁻¹	/	1.5	1.4
Size distribution, wt%			
0-40 μm	14.5	13.9	15
40-80 μm	51.9	49.5	50.5
>80 μm	33.6	36.6	34.5
Micro-activity	/	80	80

The process for preparing the aromatization catalyst OTAZ-C-3 is as follows.

The starting materials used included kaolin clay (available from China Kaolin Clay Co., Ltd of Suzhou, solid content: 75% by weight), and pseudo-boehmite (available from Shandong Aluminum Co., Ltd., solid content: 65% by weight, peptized with a hydrochloric acid solution having a concentration of 31% by weight before use, the molar ratio of hydrochloric acid to the pseudo-boehmite, on the basis of alumina, being 0.20).

The crystallized ZSM-5 molecular sieve (available from Qilu Catalyst Branch, produced by amine-free method, $n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)=27$) was filtered off the mother liquor, washed with water until the Na_2O content was less than 3.0% by weight, and filtered to obtained a filter cake. 100 g (dry basis) of the above molecular sieve was added to 1000 g of 2.0% NaOH solution, heated to 65 °C, reacted for 30 min, rapidly cooled to room temperature, filtered, and washed until the filtrate was neutral. Then, the filter cake was added to 800 g of water to make a slurry, to which 40 g of NH_4Cl was added, and the mixture was heated to 75 °C. After 1 hour of ion exchange, an Na_2O content less than 0.2% by weight was obtained. The resultant was filtered, and washed to obtain a molecular sieve filter cake. 50 g (dry basis) of the above molecular sieve was added with water to produce a molecular sieve slurry with a solid content of 10% by weight. 11 g of oxalic acid was added with stirring, and then 110 g of hydrochloric acid (10% by mass) and 92 g of fluorosilicic acid (3% by mass) were added co-currently within 30 min. The resultant was heated to 65 °C and stirred at a constant temperature for 1 h, filtered and washed with water until the filtrate was neutral. The filter cake was added with water to make a molecular sieve slurry having a solid content of 45% by weight. 1.2 g of H_3PO_4 (having a concentration of 85% by weight) and 3.3 g of $\text{Zn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ were dissolved in 10g of water, added with ammonia water to provide a pH of 6, and then added to the molecular sieve slurry and mixed uniformly. The mixture was dried, and calcined at 550 °C for 2 h under 100% steam atmosphere to obtain a molecular sieve A, the properties of which are listed in Table 2.

The pseudo-boehmite was mixed with the kaolin clay and formulated into a slurry having a solid content of 30% by weight with deionized water, and stirred uniformly, and the pH of the slurry was adjusted to 2.5 with hydrochloric acid. The mixture was held at the pH and allowed to stand at 50 °C for 1 hour for aging, and stirred for another 1 hour to form a colloid. The prepared molecular sieve A and water were added to form a catalyst slurry (solid content of 35% by weight). The stirring was continued, followed by spray drying to obtain a

microsphere catalyst. The microsphere catalyst was then calcined at 500 °C for 1 hour to obtain the aromatization catalyst OTAZ-C-3 used in the present application, which had a dry basis composition of 25% by weight of kaolin clay, 25% by weight of pseudo-boehmite and 50% by weight of the molecular sieve A.

Table 2 Properties of the molecular sieve A

Item	Molecular sieve A
Degree of crystallinity/%	90
$n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)$	110
P_2O_5 content/%	1.5
Content of supported metal oxide/%	1.6
$\text{S}_{\text{BET}}/(\text{m}^2/\text{g})$	440
$(V_{\text{mesopore}}/V_{\text{total pore}})/\%$	60
$(V_{2\text{nm}-20\text{nm}}/V_{\text{mesopore}})/\%$	99
(Strong acid content/total acid content)/%	70
B acid content/L acid content	35
$\text{D}(\text{Al})$	0.77
$\text{D}(\text{M})$	3.6

The passivation of the aromatization catalyst is performed as follows.

1. The fresh aromatization catalyst OTAZ-C-3 was charged into a dense-phase fluidized bed reactor, and contacted with stabilized gasoline A at a passivation temperature of 410 °C for 2 hours to obtain a passivated OTAZ-C-3 catalyst having a content of passivated species of 0.5% by weight and a micro-activity of 35.

2. The fresh aromatization catalyst MP051 was charged into a dense-phase fluidized bed reactor, and contacted with stabilized gasoline A at a passivation temperature of 410 °C for 2 hours to obtain a passivated MP051 catalyst having a content of passivated species of 0.5% by weight and a micro-activity of 35.

The aging treatment of the aromatization catalyst is performed as follows.

1. The fresh aromatization catalyst OTAZ-C-3 was charged into a dense-phase fluidized bed reactor, and continuously aged for 8 hours under an aging temperature of 780 °C and 100% steam atmosphere to obtain an aged OTAZ-C-3 catalyst with a micro-activity of 35.

2. The fresh aromatization catalyst MP051 was charged into a dense-phase fluidized bed reactor and continuously aged for 8 hours under an aging temperature of 780 °C and 100%

steam atmosphere to obtain an aged MP051 catalyst with a micro-activity of 35.

In each example and comparative example of the present application, the contents of Na₂O, NiO, ZnO, Ga₂O₃, Al₂O₃, and SiO₂ in the catalysts were determined by the X-ray fluorescence method according to GB/T 30905-2014.

In each example and comparative example of the present application, the content of the passivated species in the passivated aromatization catalyst was determined according to the RIPP 107-90 method, of which the steps are summarized as follows: the sample was burned in a high frequency furnace to generate CO₂ and CO gases, and the gases were introduced into an infrared detector through a filter drier to obtain a total carbon content expressed in percentage. Since the catalyst itself had no induction effect, it was necessary to add a sensing agent, a fluxing agent to promote the burning of the sample; and since the sample was porous and had a water absorption capability, it was necessary to be pretreated before the test. Particularly, the test procedure included:

1. Test preparation: Preheating, cleaning, leak testing and checking of the circuit were performed according to the operation procedures of CS-46 Carbon Sulfur Tester (manufactured by American LECO company). The catalyst sample was baked at 110 °C for 2-3 hours and then cooled to room temperature in a desiccator.

2. Testing: A standard copper sample was burned, the C% value was checked, and the reading was adjusted to be within the error range. A crucible was placed on an electronic balance, and the reading was reset to zero. 0.3-0.4 g of the baked catalyst sample was added, and the sample weight was automatically input to the tester. The crucible was removed, added with a tin foil and then put back on the electronic balance, and the reading was reset to zero. 1.5-1.6g of copper flux (available from Shandong Metallurgical Research Institute) was added. The crucible was removed and covered with a cap, and then put on a burning seat with crucible tongs. After burning for 30 seconds, the reading indicator light was on, and the C% value was recorded. Each sample was assayed for two times. The carbon blank value for this test was determined by the same procedure. The carbon content of the catalyst was calculated as follows: C% = C% of the sample – the blank C%.

In each example and comparative example of the present application, the micro-activity of the aromatization catalyst was determined according to the RIPP 92-90 method, using the same equipment and test procedure as ASTM D3907-2013, under the following conditions:

feedstock oil: Dagang straight-run diesel having a relative density d_4^{20} of 0.8419, an initial boiling point of 235 °C, a dry point of 337 °C; reaction conditions: an oil intake of 1.56 g, a reaction temperature of 460 °C, a catalyst-to-oil mass ratio of 3.2, a weight hourly space velocity of the feedstock oil of 16 h⁻¹ and a feed time of 70 seconds.

5 In each example and comparative example of the present application, the octane number RON and MON of gasoline were determined according to the standard methods of GB/T 5487-1995 and GB/T 503-1995, respectively, and the antiknock index was calculated by (MON+RON)/2, the PONA of gasoline was analyzed by simulated distillation and the hydrocarbon composition analysis of gasoline (determined according to the test methods of
10 ASTM D2887 and ASTM D6733-01 (2011), respectively), and the sulfur content of gasoline was determined according to SH/T0689-2000.

Examples I-II Splitting of Gasoline Feedstock and Etherification of Light Gasoline Fraction

15 The full-range gasoline feedstocks used in Example I and Example II were stabilized gasolines A and B, respectively, and their properties are listed in Table 3.

The stabilized gasolines A and B were separately distilled in a fractionation column, split into light fractions and heavy fractions, and the light fractions were controlled to have a final boiling point of 65-70 °C (according to ASTM D86 standard). The light gasoline fraction
20 obtained by the distillation of the stabilized gasoline A was designated as LCN-A, and the heavy gasoline fraction thus obtained was designated as HCN-A. The light gasoline fraction obtained by the distillation of the stabilized gasoline B was designated as LCN-B, and the heavy gasoline fraction thus obtained was designated as HCN-B. The properties of the light gasoline fractions and the heavy gasoline fractions obtained by the distillation of the stabilized
25 gasolines A and B are shown in Table 4.

The light gasoline fractions LCN-A and LCN-B were separately subjected to a pretreatment including desulfurization and removal of dienes in the presence of hydrogen in a refining reactor, so that the sulfur content and the diene content of the light gasoline fractions were all reduced to below 10 ppm, and then mixed with methanol (analytically pure) and sent
30 into an etherification reactor for etherification. The etherification conditions included a reaction temperature of 55-80 °C, a space velocity of 1.2 h⁻¹, a molar ratio of methanol to active olefins in the light gasoline fraction of 1.2, and an etherification catalyst of strongly acidic

cation-exchange resin (732 type, styrene-based). After the etherification reaction, the resulting oil and gas were introduced into an etherification product fractionation column for separation. A methanol-containing tail gas comprising residual C5 compounds and the alcohol was obtained at the top of the column, and an etherified oil was obtained at the bottom of the column. The temperature at the top of the etherification product fractionation column was 60-80 °C, and the temperature at the bottom was 110-140 °C. The corresponding etherified oils obtained were designated as LCN-A-M and LCN-B-M, respectively, and their properties are also shown in Table 4.

Table 3 Properties of the gasoline feedstocks used in the examples

Gasoline feedstock	Stabilized gasoline A	Stabilized gasoline B
Density at 20°C, kg/m ³	737.3	743.9
Refractive index at 20°C	1.4212	1.4229
Vapor pressure (RVPE), kPa	49	50
Carbon content, % (w)	86.36	86.37
Hydrogen content, % (w)	13.64	13.63
Sulfur content, mg/L	421	138
Nitrogen content, mg/L	139	35
Induction period, min	667	>1000
Group composition (FIA method)		
Aromatics, % (by volume)	15.4	20.2
Olefins, % (by volume)	54.9	30.9
Saturated hydrocarbons, % (by volume)	29.7	48.9
Measured RON	90.9	88.6
Measured MON	78.9	78.7
(RON+MON)/2	84.9	83.7
Distillation range under normal pressure, °C		
IBP	44	44
5% (φ)	59	56
10% (φ)	63	63
30% (φ)	80	82
50% (φ)	106	108
70% (φ)	139	140
90% (φ)	175	174
FBP	204	199

Table 4 Properties of the fractions and etherified oils obtained in Examples I-II

Experimental scheme	Example I		Example II	
Name of the fraction	LCN-A	HCN-A	LCN-B	HCN-B
Percentage relative to the full-range stabilized gasoline, %	22	78	20.5	79.5
Density at 20°C, kg/m ³	647.7	760.7	653.5	767.5
Total sulfur content, mg/L	23	527	18	189
Group composition (FIA method)				
Aromatics, % (by volume)	0	22.6	0	30.2
Olefins, % (by volume)	65.1	45.1	60.8	27.9
Saturated hydrocarbons, % (by volume)	34.9	32.3	38.2	41.9
Name of the etherified oil	LCN-A-M	/	LCN-B-M	/
Percentage relative to the full-range stabilized gasoline, %	25.5	/	23.3	/
Group composition (FIA method)				
Aromatics, % (by volume)	0	/	0	/
Olefins, % (by volume)	13.0	/	15.2	/
Saturated hydrocarbons, % (by volume)	32.5	/	33.3	/

The following Examples I-1 to I-10 are working examples in which the heavy gasoline fraction HCN-A was used as the feedstock, and various types of catalysts were used for the desulfurization and aromatization, and the results are shown in Table 5.

Example I-1

The heavy gasoline fraction HCN-A was contacted with a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the passivated OTAZ-C-3 catalyst in a small continuous fluidized bed reactor for adsorption desulfurization and aromatization, in which the OTAZ-C-3 catalyst was present in an amount of 7% by weight based on the total weight of the mixed catalyst.

The operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 2.1 MPa, a weight hourly space velocity of the heavy gasoline fraction of 6 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 75. The desulfurization-aromatization product obtained from the top of the reactor was cooled to about 10 °C, and separated to obtain an off-gas and a heavy gasoline product (designated as HCN-A heavy gasoline product, the same below, the properties are shown in Table 5). The regeneration temperature of the mixed catalyst was 550 °C, and, after the regeneration, the mixed catalyst was returned to the reactor for recycling.

Example I-2

The heavy gasoline fraction HCN-A was contacted with a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aged OTAZ-C-3 catalyst in a small continuous fluidized bed reactor to carry out adsorption desulfurization and aromatization, in which the OTAZ-C-3 catalyst is present in an amount of 7% by weight based on the total weight of the mixed catalyst.

The operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 2.1 MPa, a weight hourly space velocity of the heavy gasoline fraction of 6 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 75. The desulfurization-aromatization product obtained from the top of the reactor was cooled to about 10 °C, and separated to obtain an off-gas and a heavy gasoline product (designated as HCN-A heavy gasoline product, the same below, the properties are shown in Table 5). The regeneration temperature of the mixed catalyst was 550 °C, and, after the regeneration, the mixed catalyst was returned to the reactor for recycling.

Example I-3

The operation was substantially the same as in Example I-1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of fresh OTAZ-C-3 catalyst, and the properties of the resulting HCN-A heavy gasoline product are listed in Table 5.

Example I-4

The operation was substantially the same as in Example I-1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of a mixed OTAZ-C-3 catalyst

(comprising 5% by weight of fresh catalyst and 95% by weight of passivated catalyst, based on the weight of the aromatization catalyst), and the properties of the resulting HCN-A heavy gasoline product are listed in Table 5.

5 Example I-5

The operation was substantially the same as in Example I-2, except that the aged OTAZ-C-3 catalyst was replaced with an equivalent weight of a mixed OTAZ-C-3 catalyst (comprising 5% by weight of fresh catalyst and 95% by weight of aged catalyst, based on the weight of the aromatization catalyst), and the properties of the resulting HCN-A heavy gasoline
10 product are listed in Table 5.

Example I-6

The operation was substantially the same as in Example I-1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of the passivated MP051 catalyst,
15 and the properties of the resulting HCN-A heavy gasoline product are listed in table 5.

Example I-7

The operation was substantially the same as in Example I-2, except that the aged OTAZ-C-3 catalyst was replaced with an equivalent weight of the aged MP051 catalyst, and
20 the properties of the resulting HCN-A heavy gasoline product are listed in Table 5. .

Example I-8

The operation was substantially the same as in Example I-1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of fresh MP051 catalyst, and the
25 properties of the resulting HCN-A heavy gasoline product are listed in Table 5. .

Example I-9

The operation was substantially the same as in Example I-1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of mixed MP051 catalyst
30 (comprising 5% by weight of fresh catalyst and 95% by weight of passivated catalyst, based on the weight of the aromatization catalyst), and the properties of the resulting HCN-A heavy gasoline product are listed in Table 5.

Example I-10

The operation was substantially the same as in Example I-2, except that the aged OTAZ-C-3 catalyst was replaced with an equivalent weight of mixed MP051 catalyst (comprising 5% by weight of fresh catalyst and 95% by weight of aged catalyst, based on the weight of the aromatization catalyst), and the properties of the resulting HCN-A heavy gasoline product are listed in Table 5.

Comparative Example I-1

The operation was substantially the same as in Example 1, except that the passivated OTAZ-C-3 catalyst was replaced with an equivalent weight of the adsorption desulfurization catalyst FCAS, and the properties of the resulting HCN-A heavy gasoline product are shown in Table 5.

Table 5 Results of Examples I-1 to I-10 and Comparative Example I-1

Example Nos.	Heavy gasoline fraction HCN-A	I-1	I-2	I-3	I-4	I-5
Name of the aromatization catalyst	/	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3
Type of the aromatization catalyst	/	Passivated	Aged	Fresh	Mixed	Mixed
Micro-activity of the aromatization catalyst	/	35	35	80	38	38
PONA * of gasoline, wt%						
nP	4.13	7.09	7.21	9.06	7.21	7.16
iP	22.45	25.39	26.32	28.06	26.32	26.37
O	37.74	27.42	27.01	23.12	27.01	27.21
N	6.99	9	8.9	8.8	8.9	8.9
A	28.27	30.82	30.4	30.76	30.4	30.2
Total	99.58	99.72	99.84	99.8	99.84	99.84
Measured RON	87.2	87.5	87.2	86.1	87.1	87.1

Measured MON	77.3	77.8	77.7	76.6	77.7	77.7
(RON+MON)/2	82.3	82.7	82.5	81.4	82.4	82.4
Change in antiknock index	/	0.4	0.2	-0.9	0.1	0.1
Sulfur content, ppm	692	9	9	9	9	9

*Note: The meaning of each symbol shown in the PONA of gasoline is as follows:

nP - normal paraffin; iP - isoparaffin; O - olefin; N - naphthene; A - aromatics.

Table 5 (cont.) Results of Examples I-1 to I-10 and Comparative Example I-1

Example Nos.	I-6	I-7	I-8	I-9	I-10	Comp. Ex. I-1
Name of the aromatization catalyst	MP051	MP051	MP051	MP051	MP051	None
Type of the aromatization catalyst	Passivated	Aged	Fresh	Mixed	Mixed	/
Micro-activity of the aromatization catalyst	35	35	80	38	38	/
PONA of gasoline, wt%						
nP	7.39	7.51	9.36	7.51	7.46	7.27
iP	26.99	26.88	29.06	27.32	27.37	28.04
O	26.42	26.6	22.12	26.01	26.21	26.45
N	9	9	8.8	8.9	8.9	9.4
A	29.92	29.74	30.46	30.1	29.9	28.62
Total	99.72	99.72	99.8	99.84	99.84	99.78
Measured RON	87	87	85.7	86.8	86.8	85.6
Measured MON	77.6	77.6	76.4	77.5	77.5	76.2
(RON+MON)/2	82.3	82.3	81.1	82.2	82.2	80.9

Change in antiknock index	0	0	-1.2	-0.1	-0.1	-1.4
Sulfur content, ppm	9	9	9	9	9	9

As shown in Table 5, in Comparative Example I-1, when the heavy gasoline fraction HCN-A was treated using the adsorption desulfurization catalyst FCAS only, that is, only adsorption desulfurization was carried out, the octane number (antiknock index) of the resulting HCN-A heavy gasoline product was significantly lower than that of the heavy gasoline fraction HCN-A. In Examples I-6 to I-10, when the heavy gasoline fraction was treated using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst MP051, that is, both adsorption desulfurization and aromatization were carried out, the octane number of the resulting HCN-A heavy gasoline product was improved as compared to Comparative Example I-1. Particularly, when an aromatization catalyst comprising a passivated or aged MP051 catalyst was used, the improvement was more remarkable. Further, in Examples I-1 to I-5, when the heavy gasoline fraction was treated using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst OTAZ-C-3, the octane number of the resulting HCN-A heavy gasoline product was further improved as compared to Examples I-6 to I-10. Similarly, when an aromatization catalyst comprising a passivated or aged OTAZ-C-3 catalyst was used, the improvement was more remarkable.

The following Examples II-1 to II-10 are working examples in which the heavy gasoline fraction HCN-B was used as the feedstock, and various types of catalysts were used for the desulfurization and aromatization, and the results are shown in Table 6.

Example II-1

The operation was substantially the same as in Example I-1, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

Example II-2

The operation was substantially the same as in Example I-2, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the

operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-3

The operation was substantially the same as in Example I-3, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-4

The operation was substantially the same as in Example I-4, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-5

The operation was substantially the same as in Example I-5, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-6

The operation was substantially the same as in Example I-6, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the

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operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-7

The operation was substantially the same as in Example I-7, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-8

The operation was substantially the same as in Example I-8, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-9

The operation was substantially the same as in Example I-9, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Example II-10

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The operation was substantially the same as in Example I-10, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the

operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Comparative Example II-1

The operation was substantially the same as in Comparative Example I-1, except that the heavy gasoline fraction HCN-B was used in place of the heavy gasoline fraction HCN-A, and the operating conditions were as follows: a reaction temperature of 400 °C, a reactor pressure of 1.8 MPa, a weight hourly space velocity of the heavy gasoline fraction of 8 h⁻¹, and a volume ratio of hydrogen to the heavy gasoline fraction of 60. The properties of the resulting HCN-B heavy gasoline product are listed in Table 6.

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Table 6 Results of Examples II-1 to II-10 and Comparative Example II-1

Example Nos.	Heavy gasoline fraction HCN-B	II-1	II-2	II-3	II-4	II-5
Name of the aromatization catalyst	/	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3
Type of the aromatization catalyst	/	Passivated	Aged	Fresh	Mixed	Mixed
Micro-activity of the aromatization catalyst	/	35	35	80	38	38
PONA of gasoline, wt%						
nP	3.14	5.2	5.5	7.1	5.5	5.6
iP	28.83	30.39	31.46	33.06	31.46	31.36
O	24.12	17.66	16.95	13.38	16.95	17.15
N	12.28	12.23	12.13	12.13	12.13	12.13
A	31.17	34.3	33.72	34.1	33.72	33.52
Total	99.54	99.78	99.76	99.77	99.76	99.76
Measured RON	85.2	86.4	86.1	84.9	86	86
Measured MON	77.3	78.4	78.2	77.2	78.2	78.2

(RON+MON)/2	81.3	82.4	82.2	81.1	82.1	82.1
Change in antiknock index	/	1.1	0.9	-0.2	0.8	0.8
Sulfur content, ppm	246	6	6	6	6	6

Table 6 (cont.) Results of Examples II-1 to II-10 and Comparative Example II-1

Example Nos.	II-6	II-7	II-8	II-9	II-10	Comp. Ex. II-1
Name of the aromatization catalyst	MP051	MP051	MP051	MP051	MP051	None
Type of the aromatization catalyst	Passivated	Aged	Fresh	Mixed	Mixed	/
Micro-activity of the aromatization catalyst	35	35	80	38	38	/
PONA of gasoline, wt%						
nP	5.5	5.7	7.4	5.8	5.9	4.1
iP	31.99	31.78	34.06	32.46	32.36	33.05
O	16.66	16.99	12.38	15.95	16.15	16.65
N	12.23	12.2	12.13	12.13	12.13	13.65
A	33.4	33.11	33.8	33.42	33.22	32.09
Total	99.78	99.78	99.77	99.76	99.76	99.54
Measured RON	86	86	84.7	85.7	85.7	84.5
Measured MON	78.2	78.2	77	78	78	77
(RON+MON)/2	82.1	82.1	80.9	81.9	81.9	80.8
Change in antiknock	0.8	0.8	-0.4	0.6	0.6	-0.5

index										
Sulfur content, ppm	6	6	6	6	6	6	6	6	6	6

Similar to the results of Examples I-1 to I-10, as shown in Table 6, in Comparative Example II-1, when the heavy gasoline fraction HCN-B was treated using the adsorption desulfurization catalyst FCAS only, that is, only adsorption desulfurization was carried out, the octane number (antiknock index) of the resulting HCN-B heavy gasoline product was significantly lower than that of the heavy gasoline fraction HCN-B. In Examples II-6 to II-10, when the heavy gasoline fraction was treated using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst MP051, that is, both adsorption desulfurization and aromatization were carried out, the octane number of the resulting HCN-B heavy gasoline product was improved as compared to Comparative Example II-1. Particularly, when an aromatization catalyst comprising a passivated or aged MP051 catalyst was used, the improvement was more remarkable. Further, in Examples II-1 to II-5, when the heavy gasoline fraction was treated using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst OTAZ-C-3, the octane number of the resulting HCN-B heavy gasoline product was further improved as compared to Examples II-6 to II-10. Similarly, when an aromatization catalyst comprising a passivated or aged OTAZ-C-3 catalyst was used, the improvement was more remarkable.

The following Examples III-1 to III-12 are working examples in which a HCN-A or HCN-B heavy gasoline product was mixed with the corresponding etherified oil LCN-AM or LCN-BM to obtain a gasoline product, and the results are shown in Table 7.

Example III-1

The HCN-A heavy gasoline product obtained in Example I-1 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

Example III-2

The HCN-A heavy gasoline product obtained in Example I-2 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

Example III-3

The HCN-A heavy gasoline product obtained in Example I-3 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

5 Example III-4

The HCN-A heavy gasoline product obtained in Example I-4 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

10 Example III-5

The HCN-A heavy gasoline product obtained in Example I-5 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

15 Example III-6

The HCN-A heavy gasoline product obtained in Example I-6 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

20 Example III-7

The HCN-A heavy gasoline product obtained in Example I-7 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

25 Example III-8

The HCN-A heavy gasoline product obtained in Example I-8 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

30 Example III-9

The HCN-A heavy gasoline product obtained in Example I-9 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which

are shown in Table 7.

Example III-10

5 The HCN-A heavy gasoline product obtained in Example I-10 was mixed with the etherified oil LCN-A-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

Example III-11

10 The HCN-B heavy gasoline product obtained in Example II-1 was mixed with the etherified oil LCN-B-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

Example III-12

15 The HCN-B heavy gasoline product obtained in Example II-2 was mixed with the etherified oil LCN-B-M to obtain a high-octane clean gasoline product, the properties of which are shown in Table 7.

Comparative Example III-1

20 The HCN-A heavy gasoline product obtained in Comparative Example I-1 was mixed with the etherified oil LCN-A-M to obtain a gasoline product, the properties of which are shown in Table 7.

Comparative Example III-2

25 The HCN-B heavy gasoline product obtained in Comparative Example II-1 was mixed with the etherified oil LCN-B-M to obtain a gasoline product, the properties of which are shown in Table 7.

Table 7 Results of Examples III-1 to III-12 and Comparative Examples III-1 and III-2

Example Nos.	III-1	III-2	III-3	III-4	III-5
Name of the aromatization catalyst	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3	OTAZ-C-3
Type of the aromatization catalyst	Passivated	Aged	Fresh	Mixed	Mixed
Type of the gasoline feedstock	A	A	A	A	A
Etherification of the light gasoline fraction (Yes/No)	Yes	Yes	Yes	Yes	Yes
Gasoline yield relative to the feedstock, %	102.3	102.3	101	102.1	102.1
Density at 20°C, kg/m ³	740.6	740.6	740.8	740.6	740.6
Refractive index at 20°C	1.4146	1.4146	1.4131	1.4146	1.4146
Vapor pressure (RVPE), kPa	62	62	66	62	62
Carbon content, % (w)	85.84	85.84	85.95	85.84	85.84
Hydrogen content, % (w)	14.16	14.16	14.05	14.16	14.16
Sulfur content, mg/L	15	14	13	15	14
Nitrogen content, mg/L	57	55	55	57	55
Benzene, % (by volume)	0.3	0.3	0.3	0.3	0.3
Group composition (FIA method)					
Aromatics, % (by volume)	19.8	19.1	19.3	19.2	19.1
Olefins, % (by volume)	20.3	20.4	18.3	20	20.1
Saturated hydrocarbons, % (by volume)	45.5	46.4	48	46.4	46.7
Oxygen content, % (by mass)	2.3	2.3	2.2	2.3	2.3
Measured RON	90.8	90.8	89.2	90.7	90.7
Measured MON	80	80	79	80	80

(RON+MON)/2	85.4	85.4	84.1	85.35	85.35
Change in antiknock index	0.5	0.5	-0.8	0.45	0.45
Distillation range under normal pressure, °C					
IBP	35	35	35	35	35
5% (φ)	53.7	54	54	53.7	54
10% (φ)	62	62	63	62	62
30% (φ)	80.6	81	82	80.6	81
50% (φ)	99.1	99	99	99.1	99
70% (φ)	127.7	128	128	127.7	128
90% (φ)	173	173	173	173	173
FBP	205	204	204	205	204

Table 7 (1st cont.) Results of Examples III-1 to III-12 and
Comparative Examples III-1 and III-2

Example Nos.	III-6	III-7	III-8	III-9	III-10
Name of the aromatization catalyst	MP051	MP051	MP051	MP051	MP051
Type of the aromatization catalyst	Passivated	Aged	Fresh	Mixed	Mixed
Type of the gasoline feedstock	A	A	A	A	A
Etherification of the light gasoline fraction (Yes/No)	Yes	Yes	Yes	Yes	Yes
Gasoline yield relative to the feedstock, %	102	102	100.7	101.8	101.8
Density at 20°C, kg/m ³	740.6	740.6	740.8	740.6	740.6
Refractive index at 20°C	1.4146	1.4146	1.4131	1.4146	1.4146
Vapor pressure (RVPE), kPa	63	63	66	63	63
Carbon content, % (w)	85.84	85.84	85.95	85.84	85.84
Hydrogen content, % (w)	14.16	14.16	14.05	14.16	14.16
Sulfur content, mg/L	15	14	13	15	14
Nitrogen content, mg/L	57	55	55	57	55
Benzene, % (by volume)	0.3	0.3	0.3	0.3	0.3
Group composition (FIA method)					
Aromatics, % (by volume)	19.2	19.1	19.3	19.2	19.1
Olefins, % (by volume)	18.8	19.9	17.8	19.8	19.9
Saturated hydrocarbons, % (by volume)	46.6	46.9	48.5	46.6	46.9
Oxygen content, % (by	2.3	2.3	2.2	2.3	2.3

mass)					
Measured RON	90.3	90.3	89	90.2	90.2
Measured MON	79.5	79.5	79	79.5	79.5
(RON+MON)/2	84.9	84.9	84	84.85	84.85
Change in antiknock index	0	0	-0.9	-0.05	-0.05
Distillation range under normal pressure, °C					
IBP	35	35	35	35	35
5% (φ)	53.7	54	54	53.7	54
10% (φ)	62	62	63	62	62
30% (φ)	80.6	81	82	80.6	81
50% (φ)	99.1	99	99	99.1	99
70% (φ)	127.7	128	128	127.7	128
90% (φ)	173	173	173	173	173
FBP	205	204	204	205	204

Table 7 (2nd cont.) Results of Examples III-1 to III-12 and
Comparative Examples III-1 and III-2

Example Nos.	III-11	III-12	Comp. Ex. III-1	Comp. Ex. III-2
Name of the aromatization catalyst	OTAZ-C-3	OTAZ-C-3	None	None
Type of the aromatization catalyst	Passivated	Aged	/	/
Type of the gasoline feedstock	B	B	A	B
Etherification of the light gasoline fraction (Yes/No)	Yes	Yes	Yes	Yes
Gasoline yield relative to the feedstock, %	101.8	101.8	102	101.5
Density at 20°C, kg/m ³	739.5	739.5	742.1	741.5
Refractive index at 20°C	1.4153	1.4153	1.4138	1.4154
Vapor pressure (RVPE), kPa	61	61	36.3	39.3
Carbon content, % (w)	85.91	85.91	85.6	85.76
Hydrogen content, % (w)	14.09	14.09	14.4	14.24
Sulfur content, mg/L	11	10	14	10
Nitrogen content, mg/L	20	20	57	26
Benzene, % (by volume)	0.5	0.5	0.3	0.5
Group composition (FIA method)				
Aromatics, % (by volume)	22.4	21.6	17.2	19
Olefins, % (by volume)	13.2	13.5	17.1	14.5
Saturated hydrocarbons, % (by volume)	54	54.3	51	56.2

Oxygen content, % (by mass)	1.7	1.7	2.3	1.7
Measured RON	88.8	88.8	88.9	88.5
Measured MON	79.6	79.6	78.9	78.5
(RON+MON)/2	84.2	84.2	83.9	83.5
Change in antiknock index	0.5	0.5	-1.0	-0.2
Distillation range under normal pressure, °C				
IBP	32.9	33	46.2	41.2
5% (φ)	50	50	64.4	59.6
10% (φ)	55.4	56	70.4	65
30% (φ)	76	76	84.6	81.3
50% (φ)	100	100	100.9	101.4
70% (φ)	130.4	130	128.7	129.7
90% (φ)	170.4	170	171.7	169.5
FBP	203.1	203	205	203.2

As shown in Table 7, in the case where a heavy gasoline product was mixed with the etherified oil to obtain a gasoline product, only the octane number (antiknock index) of the gasoline products obtained in Comparative Examples III-1 and III-2 using the adsorption desulfurization catalyst FCAS alone was significantly lowered as compared to the gasoline feedstock. The octane number of the gasoline products obtained in Examples III-6 to III-10 using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst MP051 was improved as compared to Comparative Example III-1. Particularly, when an aromatization catalyst comprising a passivated or aged MP051 catalyst was used, the improvement was more remarkable. Further, the octane number of the gasoline products obtained in Examples III-1 to III-5 using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst OTAZ-C-3 was further improved as compared to Examples III-6 to III-10, and when an aromatization catalyst comprising a passivated or aged OTAZ-C-3 catalyst was used, the improvement was more remarkable. Similarly, as compared to Comparative Example III-2 using only the adsorption desulfurization catalyst, the gasoline products obtained in Examples III-11 and III-12 using a mixed catalyst showed a significant improved octane number.

The following Examples IV-1 to IV-5 are working examples in which a HCN-A heavy gasoline product was mixed with a light gasoline fraction LCN-A to obtain a gasoline product, and the results are shown in Table 8.

Example IV-1

The HCN-A heavy gasoline product obtained in Example I-6 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, the properties of which are shown in Table 8.

Example IV-2

The HCN-A heavy gasoline product obtained in Example I-7 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, the properties of which are shown in Table 8.

Example IV-3

The HCN-A heavy gasoline product obtained in Example I-8 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, the properties of which are shown in Table 8.

5 Example IV-4

The HCN-A heavy gasoline product obtained in Example I-9 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, and the properties are shown in Table 8.

Example IV-5

10 The HCN-A heavy gasoline product obtained in Example I-10 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, the properties of which are shown in Table 8.

Comparative Example IV-1

15 The HCN-A heavy gasoline product obtained in Comparative Example I-1 was mixed with the light gasoline fraction LCN-A to obtain a gasoline product, the properties of which are shown in Table 8.

Comparative Example IV-2

20 The HCN-B heavy gasoline product obtained in Comparative Example II-1 was mixed with the light gasoline fraction LCN-B to obtain a gasoline product, the properties of which are shown in Table 8.

Table 8 Results of Examples IV-1 to IV-5 and Comparative Examples IV-1 and IV-2

Example Nos.	IV-1	IV-2	IV-3	IV-4	IV-5	Comp. Ex. IV-1	Comp. Ex. IV-2
Name of the aromatization catalyst	MP051	MP051	MP051	MP051	MP051	None	None
Type of the aromatization catalyst	Passivated	Aged	Fresh	Mixed	Mixed	/	/
Type of the gasoline feedstock	A	A	A	A	A	A	B
Etherification of the light gasoline fraction (Yes/No)	No	No	No	No	No	No	No
Gasoline yield relative to the feedstock, %	99	99	98	98.9	98.9	99.3	99.3
Density at 20°C, kg/m ³	740.6	740.6	740.8	740.6	740.6	740.1	739.1
Refractive index at 20°C	1.4146	1.4146	1.4131	1.4146	1.4146	1.4146	1.4129
Vapor pressure (RVPE), kPa	70	70	83	71	71	60	58
Carbon content, % (w)	85.84	85.84	85.95	85.84	85.84	85.84	85.81
Hydrogen content, % (w)	14.16	14.16	14.05	14.16	14.16	14.16	14.19
Sulfur content, mg/L	15	14	13	15	14	14	11

Nitrogen content, mg/L	57	55	55	57	55	55	20
Benzene, % (by volume)	0.3	0.3	0.3	0.3	0.3	0.3	0.5
Group composition (FIA method)							
Aromatics, % (by volume)	19.2	19.1	19.3	19.2	19.1	18.7	22.15
Olefins, % (by volume)	27.5	27.8	22.8	27	27	31.45	20.65
Saturated hydrocarbons, % (by volume)	53.3	53.1	57.9	53.8	53.9	49.85	57.2
Oxygen content, % (by mass)	/	/	/	/	/	/	/
Measured RON	89.3	89.3	88.2	89.2	89.2	88	87.4
Measured MON	78.5	78.5	78.2	78.5	78.5	78.2	78.1
(RON+MON)/2	83.9	83.9	83.2	83.85	83.85	83.1	82.75
Change in antiknock index	-1	-1	-1.7	-1.05	-1.05	-1.8	-0.95
Distillation range under normal pressure, °C							
IBP	35	35	32	35	35	42	41
5% (φ)	53.7	54	52	53.7	54	55	55
10% (φ)	62	62	60	62	62	64	62

30% (φ)	80.6	81	82	80.6	81	81	75
50% (φ)	99.1	99	98	99.1	99	99	100
70% (φ)	127.7	128	126	127.7	128	128	131
90% (φ)	173	173	172	173	173	173	171
FBP	205	204	204	205	204	204	203

As shown in Table 8, in the case where a heavy gasoline product was mixed with the light gasoline fraction to obtain a gasoline product, only the octane number (antiknock index) of the gasoline products obtained in Comparative Examples IV-1 and IV-2 using the adsorption desulfurization catalyst FCAS alone was significantly lowered as compared to the gasoline feedstock. The octane number of the gasoline products obtained in Examples IV-1 to IV-5 using a mixed catalyst comprising the adsorption desulfurization catalyst FCAS and the aromatization catalyst MP051 was improved as compared to Comparative Example IV-1. Particularly, when an aromatization catalyst comprising a passivated or aged MP051 catalyst was used, the improvement was more remarkable.

In addition, when comparing the results shown in Tables 7 and 8, it can be seen that, in working examples comprising an etherification of the light gasoline fraction, the octane number of the resulting gasoline product was significantly improved, its olefin content was significantly lowered, and its vapor pressure was effectively controlled, and meanwhile the yield of gasoline was also increased to some extent, as compared to working examples that did not comprise the etherification of the light gasoline fraction. Thus, in the case where a mixed catalyst was used in combination with an etherification treatment, a gasoline product having a low sulfur content, a low olefin content, a low vapor pressure, and a high octane number can be obtained in a high yield.

In the above specification, the inventive concept of the present application has been described with reference to specific embodiments. However, it will be understood by those skilled in the art that various modifications and changes can be made without departing from the scope of the present application. Accordingly, the specification and drawings should be considered to be illustrative rather than limiting, and all such modifications and changes should be covered by the present invention.

It is to be understood that some features described herein separately in different embodiments may be combined in a single embodiment. Meanwhile, some features described herein in a single embodiment for the sake of brevity may also be provided separately or in any sub-combination in different embodiments.

Claims

1. A process for treating gasoline, comprising:

1) splitting a gasoline feedstock into a light gasoline fraction and a heavy gasoline
5 fraction;

2) optionally, subjecting at least a portion of the resulting light gasoline fraction to
etherification to obtain an etherified oil; and

3) contacting the resulting heavy gasoline fraction with a mixed catalyst and subjecting
it to desulfurization and aromatization in the presence of hydrogen to obtain a heavy gasoline
10 product;

wherein the mixed catalyst comprises an adsorption desulfurization catalyst and an
aromatization catalyst, and at least 50 wt%, preferably at least 80 wt%, more preferably at
least 90 wt%, particularly preferably at least 95 wt%, and most preferably 100 wt% of the
aromatization catalyst has undergone a passivation and/or aging treatment, so that the
15 aromatization catalyst has a micro-activity within a range from 20 to 55,

wherein the passivation comprises the step of contacting the aromatization catalyst
with a compound containing carbon, sulfur and/or nitrogen to conduct a passivation reaction
prior to the desulfurization and aromatization,

wherein the aging treatment comprises the step of treating the aromatization catalyst,
20 prior to the desulfurization and aromatization, under the following conditions: a temperature
within a range from 600 to 800 °C, an aging time within a range from 1 to 360 hours, and an
aging atmosphere containing steam.

2. The process according to claim 1, further comprising the step of:

4) mixing at least a portion of the light gasoline fraction and/or at least a portion of the
25 etherified oil with at least a portion of the heavy gasoline product to provide a gasoline
product.

3. The process according to claim 1, wherein the gasoline feedstock has at least one of
the following characteristics:

1) an olefin content of greater than 20% by volume;

2) a sulfur content of 10 µg/g or above; and

3) being at least one selected from the group consisting of catalytic cracking gasoline,

deep catalytic cracking gasoline, coker gasoline, thermal cracking gasoline, and straight-run gasoline, or a fraction thereof.

4. The process according to claim 1, wherein the split point between the light gasoline fraction and the heavy gasoline fraction is within a range from 60 to 80 °C.

5 5. The process according to claim 1, wherein the etherification comprises the step of:
contacting the light gasoline fraction with an alcohol to subject the olefin in the light gasoline fraction to an etherification reaction with the alcohol in the presence of an etherification catalyst, to obtain the etherified oil,

wherein the etherification is carried out under the following conditions: a temperature
10 within a range from 20 to 200 °C, a pressure within a range from 0.1 to 5 MPa, a weight hourly space velocity within a range from 0.1 to 20 h⁻¹, and a molar ratio of the alcohol to the light gasoline fraction within a range of 1: (0.1-100);

and the etherification catalyst comprises at least one selected from the group consisting of resins, molecular sieves, and heteropolyacids.

15 6. The process according to claim 1, wherein the desulfurization and aromatization are carried out in a fluidized reactor, wherein the fluidized reactor is at least one selected from the group consisting of riser reactors and dense phase fluidized reactors.

7. The process according to claim 1, wherein the adsorption desulfurization catalyst comprises silica, alumina, zinc oxide, and a desulfurization active metal, and the
20 desulfurization active metal is at least one selected from the group consisting of cobalt, nickel, copper, iron, manganese, molybdenum, tungsten, silver, tin and vanadium.

8. The process according to claim 7, wherein on the basis of oxides, the zinc oxide is present in an amount ranging from 10% to 90% by weight, the silica is present in an amount ranging from 5% to 85% by weight, and the alumina is present in an amount ranging from 5
25 to 30% by weight based on the dry weight of the adsorption desulfurization catalyst; and

on the elemental basis, the desulfurization active metal is present in the adsorption desulfurization catalyst in an amount ranging from 5% to 30% by weight based on the dry weight of the adsorption desulfurization catalyst.

9. The process according to claim 1, wherein, on dry basis, the aromatization catalyst
30 comprises 10% to 30% by weight of a molecular sieve, 0% to 20% by weight of an

aromatization active metal oxide and 50% to 90% by weight of a support, based on the total weight of the aromatization catalyst;

wherein the molecular sieve comprises a Y molecular sieve and/or an MFI structural molecular sieve, the aromatization active metal is at least one selected from the group consisting of metal elements of Group IVB, metal elements of Group VB, metal elements of Group VIB, metal elements of Group VIII, metal elements of Group IB, metal elements of Group IIB, and metal elements of Group IIIA, and the support comprises silica and/or alumina.

10. The process according to claim 1, wherein the aromatization catalyst can be prepared from a starting material comprising 15% to 60% by weight of a natural mineral, 10% to 30% by weight of a precursor of an inorganic oxide binder, and 20% to 80% by weight of a MFI structural molecular sieve containing phosphorus and supported metal, based on the dry weight of the starting material,

wherein the MFI structural molecular sieve has a $n(\text{SiO}_2)/n(\text{Al}_2\text{O}_3)$ ratio of greater than 100; a phosphorus content, on the basis of P_2O_5 , within a range from 0.1% to 5% by weight based on the dry weight of the molecular sieve; a supported-metal content, on the basis of oxides, within a range from 0.5% to 5% by weight based on the dry weight of the molecular sieve; an Al distribution parameter $D(\text{Al})$ satisfying $0.6 \leq D(\text{Al}) \leq 0.85$; a supported-metal distribution parameter $D(\text{M})$ satisfying $2 \leq D(\text{M}) \leq 10$; a mesopore volume percentage within a range from 40% to 80% relative to the total pore volume; a percentage of strong acid content relative to the total acid content within a range from 60% to 80%; and a ratio of the Bronsted acid (B acid) content to the Lewis acid (L acid) content within a range from 15 to 80.

11. The process according to claim 10, wherein the supported metal is at least one of zinc, gallium and iron.

12. The process according to claim 1, wherein the percentage of the aromatization catalyst relative to the mixed catalyst is within a range from 1% to 30% by weight.

13. The process according to claim 1, wherein the desulfurization and aromatization are carried out under the following conditions: a reaction temperature within a range from 350 to 500 °C, a weight hourly space velocity within a range from 2 to 50 h^{-1} , a reaction

pressure within a range from 0.5 MPa to 3.0 MPa, and a volume ratio of hydrogen to the heavy gasoline fraction within a range from 1 to 500.