This invention relates to a method and control device for controlling when to stop a compressor in a multiple chiller ~~compressor~~ refrigeration system.

Druckexemplar

~~AUTOMATIC CHILLER STOPPING SEQUENCE~~

Background of the Invention

1. Field of the Invention

The present invention relates to methods of operating and control systems for air conditioning systems and, more particularly, to a method of operating and a control system for control devices in multiple vapor compression refrigeration systems (chillers) whereby chillers can be stopped at a predetermined load in order that the remaining building load can be picked up by the remaining running chillers without exceeding set load capacities of the running chillers.

2. Description of Related Art

Generally, large commercial air conditioning systems include a chiller which consists of an evaporator, a compressor, and a condenser. Usually, a heat transfer fluid is circulated through tubing in the evaporator thereby forming a heat transfer coil in the evaporator to transfer heat from the heat transfer fluid flowing through the tubing to refrigerant in the evaporator. The heat transfer fluid chilled in the tubing in the evaporator is normally water or glycol, which is circulated to a remote location to satisfy a cooling load. The refrigerant in the evaporator evaporates as it absorbs heat from the heat transfer fluid flowing through the tubing in the evaporator, and the compressor operates to extract this refrigerant vapor from the evaporator, to compress this refrigerant vapor, and to discharge the compressed vapor to the condenser. In the condenser, the refrigerant vapor is

condensed and delivered back to the evaporator where the refrigeration cycle begins again.

To maximize the operating efficiency of a chiller plant, it is desirable to match the amount of work done by the compressor to the work needed to satisfy the cooling load placed on the air conditioning system. Commonly, this is done by capacity control means which adjust the amount of refrigerant vapor flowing through the compressor. The capacity control means may be a device for adjusting refrigerant flow in response to the temperature of the chilled heat transfer fluid leaving the coil in the evaporator. When the evaporator chilled heat transfer fluid temperature decreases, indicating a reduction in refrigeration load on the refrigeration system, a throttling device, e.g. guide vanes, closes, thus decreasing the amount of refrigerant vapor flowing through the compressor drive motor. This decreases the amount of work that must be done by the compressor thereby decreasing the amount of power draw (KW) on the compressor. At the same time, this has the effect of increasing the temperature of the chilled heat transfer fluid leaving the evaporator. In this manner, the compressor operates to maintain the temperature of the chilled heat transfer fluid leaving the evaporator at, or within a certain range of, a setpoint temperature.

Large commercial air conditioning systems, however, typically comprise a plurality of chillers, with one designated as the "Lead" chiller (i.e. the chiller that is started first) and the other chillers designated as "Lag" chillers. The designation of the chillers changes periodically depending on such things as run time, starts, etc. The total chiller plant is sized to supply maximum design load. For less than design loads, the choice of the proper number of chillers to meet the load condition has a significant impact on total plant

efficiency and reliability of the individual chillers. In order to maximize plant efficiency and reliability it is necessary to stop selected chillers under low load conditions, and insure that all remaining chillers have a balanced load. The relative electrical energy input to the compressor motors (% KW) necessary to produce a desired amount of cooling is one means of determining the loading and balancing of a plurality of running compressors. In the prior art, however, when the building load decreased and the chillers changed capacity to follow the building load, a selected chiller was manually stopped by an operator when the total load estimated by the operator on the system dropped below the total estimated capacity of the running chillers by an amount equal tc the estimated capacity of the chiller to be stopped. However, subsequent slight increases in building load required the previously stopped chiller to be started again. This stopping and starting chillers has a very detrimental effect on the efficiency and reliability of the chillers. Thus, there exists a need for a method and apparatus which determines when a chiller can be stopped so that the remaining chillers can pick up the remaining building load and which minimizes the disadvantages of the prior control methods.

~~Summary of the Invention~~

The present invention includes a chiller stopping control system for a refrigeration system characterized by having means for generating a % KW setpoint signal at which a chiller can be stopped and the remaining load picked up by the remaining chillers, without exceeding a target % KW setpoint which is below a desired % KW setpoint for starting an additional chiller, which prevents short-cycling or restarting a recently stopped chiller.

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In US-A-4 483 152 there is described a method of controlling when to stop a compressor in a multiple compressor refrigeration system according to the preamble of claim 1. More specifically, US-A-4 483 152 discloses a stopping control system by comparing the sum of the maximum operating capacities of a reduced number of chillers with the total operating capacity. In US-A-4 483 152 the operating capacity is measured as product of flow rate and temperature differential across the evaporator. A control device according to the preamble of claim 3 is also known from US-A-4 483 152.

It is a primary object of the present invention to overcome the inadequacies of the prior art proposals and to provide a method and apparatus which determines when a chiller can be stopped so that the remaining or chillers can pick up the remaining building load and which prevents the above mentioned type of failures thereby improving the efficiency and reliability of the individual chillers.

To achieve this, the method of control of the invention is characterized by the features claimed in the characterizing portion of claim 1 and the invention provides a control device according to the characterizing portion of claim 3.

Basically, the method of control according to the invention compares the reduced cooling requirement setpoint with an average power draw of all running compressors and stops the next compressor when the ~~comparison of the~~ reduced cooling requirement setpoint is greater than the average power draw of all currently running compressors.

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A Lag compressor can be stopped when the average % KW power draw (approximated by motor current) of all running compressors is at or below a calculated % KW to meet a reduced cooling requirement. The calculated Reduced Cooling Required (% KW) setpoint is the % KW at which a Lag compressor can be stopped and the building load picked up by the remaining chillers, without exceeding a target % KW setpoint below the % KW setpoint where an additional chiller would be required. The Reduced Cooling Required (% KW) setpoint is determined as follows:

$$\text{RCR (\%KW) SP} = \frac{[\text{Chiller Cap. (N-1)}] \times (\text{ACR SP} - \text{RCR Hysteresis})}{\text{Total Running Chiller Cap. (N)}}$$

where Chiller Capacity (N-1) is the capacity of the running chillers minus the next chiller to be stopped,

Total Running Chiller Capacity (N) is the capacity of the running chillers,

ACR ~~setpoint~~ is the setpoint where an additional chiller would be required and,

RCR Hysteresis is a target value below ACR setpoint.

Brief Description of the Drawings

Figure 1 is a schematic illustration of a multiple compressor chilled water refrigeration system with a control system for balancing the relative power draw on each operating compressor according to the principles of the present invention, and

Figure 2 is a flow diagram of the control system of the present invention.

Description of the Preferred Embodiment

Referring to Figure 1, a vapor compression refrigeration system 10 is shown having a plurality of centrifugal compressors 12a-n with a control system 20 for varying the capacity of the refrigeration system 10 and for stopping compressors according to the principles of the present invention. As shown in Figure 1, the refrigeration system 10 includes a condenser 14, a plurality of evaporators 15a-n and a poppet valve 16. In operation, compressed gaseous refrigerant is discharged from one or a number of compressors 12a-n through compressor discharge lines 17a-n to the condenser wherein the gaseous refrigerant is condensed by relatively cool condensing water flowing through tubing 18 in the condenser 14. The condensed liquid refrigerant from the condenser 14 passes through the poppet valve 16 in refrigerant line 19, which forms a liquid seal to keep condenser vapor from entering the evaporator and to maintain the pressure difference between the condenser and the evaporator. The liquid refrigerant in the evaporator 15a-n is evaporated to cool a heat transfer fluid, such as water or glycol, flowing through tubing 13a-n in the evaporator 15a-n. This chilled heat transfer fluid is used to cool a building or space, or to cool a process or other such purposes. The gaseous refrigerant from the evaporator 15a-n flows through the compressor suction lines 11a-n back to the compressors 12a-n under the control of compressor inlet guide vanes 22a-n. The gaseous refrigerant entering the compressor 12a-n through the guide vanes 22a-n is compressed by the compressor 12a-n through the compressor discharge line 17a-n to complete the refrigeration cycle. This refrigeration cycle is continuously repeated during normal operation of the refrigeration system 10.

Further, preferably, the Building Supervisor 30 comprises a personal computer which serves as a data entry port as well as a programming tool, for configuring the entire refrigeration system and for displaying the current status of the individual components and parameters of the system;

Still further the local control board 27a-n includes a means for controlling the inlet guide vanes for each compressor. The inlet guide vanes are controlled in response to control signals sent by the chiller system manager. Controlling the inlet guide vanes controls the KW demand of the electric motors 24 of the compressors 12. Further, the local control boards receive signals from the electric motors 23 by way of electrical line 28a-n corresponding to amount of power draw (approximated by motor current) as a percent of full load kilowatts (% KW) used by the motors.

Referring now specifically to FIG. 2 for details of the operation of the control system there is shown a flow chart of the logic used to determine when to stop a lag compressor in accordance with the present invention. The flow chart includes capacity determination 32 of the next lag chiller in the stop sequence from which the logic flows to step 34 to compute the average % KW of all running chillers (AVGKW). The logic then proceeds to step 36 to compute the Reduced Cooling Required Setpoint according to the following:

$$\text{RCR Setpoint} = \frac{\text{(Chiller Capacity N-1) X (ACR-HYS)}}{\text{Total Running Capacity}}$$

Where:

Chiller Capacity N-1 is the sum of the capacities of the currently running chillers minus the capacity of the next

CLAIMS

1. A method of controlling when to stop a compressor (12a-n) in a multiple ~~compressor~~ refrigeration system (10) including a motor (24a-n) for driving ~~each~~ compressor (12a-n), comprising the steps of:

determining the capacity of the next ~~compressor (12a-n)~~ to be stopped,

determining the capacity of all currently running ~~compressors (12a-n)~~,

determining a reduced cooling requirement (RCR) setpoint for stopping said compressor (12a-n),

characterized in further comprising the steps of:

comparing said reduced cooling requirement setpoint (RCR) with an average power draw of all running compressors (12a-n), and

stopping said next ~~compressor (12a-n)~~ when ~~the comparison of~~ said reduced cooling requirement setpoint (RCR) is greater than said average power draw of all currently running compressors (12a-n), and

in that the step of determining said reduced cooling requirement setpoint is calculated by solving the equation:

$$\text{RCR Setpoint} = \frac{\text{(Chiller Capacity N-1) X (ACR-HYS)}}{\text{Total Running Capacity}}$$

where Chiller Capacity N-1 is the sum of the capacities of the currently running chillers (12a-n, 14, 15a-n) minus the capacity of the next chiller (12a-n,14,15a-n) to be stopped,

ACR is the Additional Cooling Required which is a programmable value which the average power draw must be above before the next chiller (12a-n,14,15a-n) is started,

HYS is the Hysteresis which is a programmable value substracted from ACR to determine a

target for the average power draw after the next chiller (12a-n, 14, 15a-n) is stopped,

and Total Running Capacity is the sum of the capacities of all chillers (12a-n, 14, 15a-n) currently running.

2. A method as set forth in claim 1, characterized in that ACR and HYS is ~~the~~ power draw in kilowatts of the respective compressor motors (24a-n).

3. A control device for controlling when to stop a compressor (12a-n) of a multiple ~~compressor~~ refrigeration system (10) including a motor (24a-n) for driving ~~each~~ compressor (12a-n), comprising:

a capacity determining means for determining the capacity of the next ~~compressor (12a-n)~~ to be stopped,

a capacity measuring means for measuring the ~~output~~ of the currently running ~~compressor (12a-n)~~

a reduced cooling requirement setpoint calculation means connected to said capacity determining means and said capacity measuring means for calculating a reduced capacity (RCR) setpoint which will satisfy a space load upon stopping said next compressor (12a-n),

characterized in further comprising a comparison means for comparing the average power draw of the currently running compressors (12a-n) (AVGKW) with said reduced capacity setpoint (RCR) wherein said next compressor (12a-n) is stopped when the average power draw of the currently running compressors (12a-n) is less than or equal to said reduced capacity (RCR) setpoint, and

in that said reduced cooling requirement setpoint calculation means calculates the reduced capacity (RCR) setpoint according to the relationship:

$$\text{RCR Setpoint} = \frac{\text{(Chiller Capacity N-1) X (ACR-HYS)}}{\text{Total Running Capacity}}$$

* < chiller (12a-n, 14, 15a-n) >

** < chillers (12a-n, 14, 15a-n) >

where, Chiller Capacity N-1 is the sum of the capacities of the currently running chillers (12a-n, 14, 15a-n) minus the capacity of the next chiller (12a-n,14,15a-n) to be stopped,

ACR is the Additional Cooling Required which is a programmable value which the average power draw (AVGKW) must be above before the next chiller (12a-n,14,15a-n) is started,

HYS is the Hysteresis which is a programmable value subtracted from ACR to determine a target for the average power draw (AVGKW) after the next chiller (12a-n,14,15a-n) is stopped, and

Total Running Capacity is the sum of the capacities of all chillers (12a-n, 14, 15a-n) currently running.

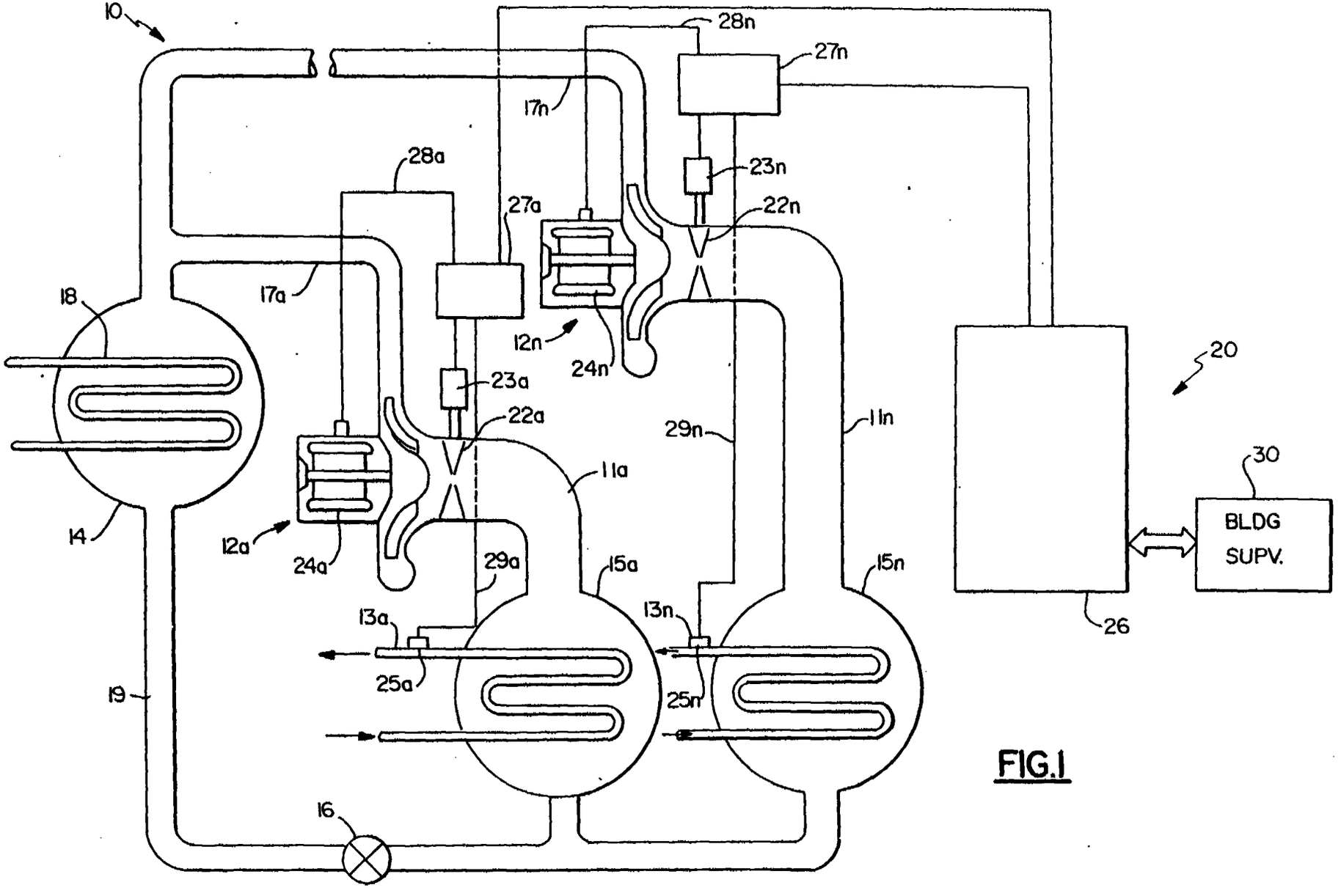

10
28n
27n
17n
28a
23n
27a
22n
18
17a
12n
24n
23a
22a
11n
29n
11a
14
12a
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BLDG
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FIG.1