

DEEP TISSUE FLOWMETRY USING DIFFUSE SPECKLE CONTRAST ANALYSIS

CROSS-REFERENCE TO RELATED APPLICATIONS

[0001] This application claims the benefit of priority to U.S. Provisional App. No. 61/755,700, filed on January 23, 2013, and to U.S. Provisional App. No. 61/830,256. The entire contents of each of these applications are hereby incorporated by reference.

BACKGROUND

Field of the Invention

[0002] This disclosure relates to systems and methods for measuring deep tissue flow, particularly via non-invasive optical approaches.

Description of the Related Art

[0003] Diffuse correlation spectroscopy (DCS), a noninvasive optical method to probe deep tissue flow. The principle of DCS is based on the fact that transmitted light intensity measured at a sufficiently small area will fluctuate primarily due to the movement of the scatterers (such as red blood cells) in the course of the diffuse light propagation. Therefore, when the autocorrelation function is calculated from the fluctuating transmission light intensity, the decay rate of the autocorrelation will be proportionally higher as flow rate increases.

[0004] Although successful in monitoring averaged microcirculation in deep tissue, DCS suffers from several disadvantages, including sophisticated hardware requirements (for example, long coherence length laser, photon-counting avalanche photodiode, fast counter, etc.), non-trivial data analysis (for example, fast autocorrelation calculation, model fit by optimization, etc.), low sampling rate, and low channel number, rendering multichannel measurements difficult. These limitations pose challenges for the application of DCS as a stable, real-time clinical monitoring device. Accordingly, there is a need for an improved method for noninvasive, real-time measurement of blood perfusion with reduced computational complexity, decreased expense, a high sampling rate, and multichannel capabilities.

SUMMARY OF THE INVENTION

[0005] Disclosed herein is a method for determining blood flow in a patient, the method comprising: directing coherent light onto a first location of the patient's skin; imaging a second location of the patient's skin, wherein a portion of the coherent light is scattered by the blood flow beneath the patient's skin such that the scattered light is at least partially detectable at the second location; and calculating the blood flow based on the image of the second location.

[0006] In some embodiments, the calculation can comprise calculating the speckle contrast. In some embodiments, calculating the speckle contrast comprises dividing the standard deviation of intensity by the average intensity of the image of the second location. In some embodiments, the blood flow can be at least 5 mm below the surface of the patient's skin. In some embodiments, the first and second locations can be on a patient's limb. In some embodiments, the first and second locations can be on a patient's foot. In some embodiments, imaging the second location can comprise capturing an image with a multi-pixel image sensor. In some embodiments, the coherent light can comprise light from a laser. In some embodiments, the first and second locations can be at least 10 mm apart. In some embodiments, the method can further comprise signaling the blood flow to an operator.

[0007] Also disclosed herein is a method for determining blood flow in a patient, the method comprising: directing coherent light onto a first location of the patient's skin; detecting time-series measurements of the light intensity at a second location of the patient's skin, wherein a portion of the coherent light is scattered by the blood flow beneath the patient's skin such that the scattered light is at least partially detectable at the second location; and calculating the blood flow based on the time-series measurements.

[0008] In some embodiments, the calculating can comprise calculating the spatial and temporal contrast. In some embodiments, calculating the temporal speckle contrast can comprise dividing the temporal standard deviation of intensity by the temporal average intensity at the second location. In some embodiments, the blood flow can be at least 5 mm below the surface of the patient's skin. In some embodiments, the first and second locations can be on a patient's foot. In some embodiments, the first and second locations can be less than 10 mm apart. In some embodiments, the first and second locations can be at least 10 mm apart. In some embodiments, the method can

further comprise signaling the blood flow an operator. In some embodiments, the signaling can comprise providing audible, visual, or tactile indicia of blood flow.

[0009] Further disclosed herein is a system for assessment of blood flow in tissue, the system comprising: a coherent light source configured to apply light to the tissue; a multi-pixel image sensor detector configured to capture an image including at least a quantity of light transmitted through the tissue, wherein the light is scattered, at least in part, by the blood flow; an analyzer configured to analyze the image to determine blood flow in the tissue; and a feedback device configured to provide a signal indicative of the blood flow determined by the analyzer.

[0010] In some embodiments, the multi-pixel image sensor can comprise a CCD camera. In some embodiments, the analyzer can be configured to calculate the spatial speckle contrast by dividing the standard deviation of intensity by the average intensity. In some embodiments, the system can be configured to provide the signal indicative of the blood flow in substantially real-time.

BRIEF DESCRIPTION OF THE DRAWINGS

[0011] FIG. 1 is a block diagram of a system for measuring flow of turbid media.

[0012] FIG. 2 is a schematic illustration of diffuse light penetration and detection in multi-layer tissue.

[0013] FIG. 3A is a schematic illustration of a diffuse correlation spectroscopy (DCS) system.

[0014] FIG. 3B is a schematic illustration of a diffuse speckle contrast analysis (DSCA) system.

[0015] FIG. 4 is a graph of DCS and DSCA measurements of blood flow over time during cuff occlusion protocol.

[0016] FIG. 5 is a schematic illustration of spatial domain DSCA.

[0017] FIG. 6A is a graph of a numerical simulation of $1/K_s^2$ as a function of αD_b .

[0018] FIG. 6B is a graph of $1/K_s^2$ plotted against measured flow rate.

[0019] FIG. 6C is a graph of $1/K_s^2$ as a function of the flow rate for three source-detector separation distances.

[0020] FIG. 6D is a graph of flow sensitivity for various source-detector separation distances.

[0021] FIG. 7 is a schematic diagram of a phantom flow experiment.

[0022] FIG. 8 is a flow diagram of a method for calculating flow rate using spatial domain DSCA.

[0023] FIG. 9 is a flow diagram of a method for calculating flow rate using time domain DSCA.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0024] Over the last decade or so, DCS technology has been developed, validated, and employed to noninvasively probe the blood flow information in deep tissue vasculature such as brain, muscle, and breast. In contrast to some other blood flow measurement techniques, such as positron emission tomography (PET), single photon emission computed tomography (SPECT), and xenon-enhanced computed tomography (XeCT), DCS uses non-ionizing radiation and requires no contrast agents. It does not interfere with commonly used medical devices such as pacemakers and metal implants. It therefore has potential in cancer therapy monitoring and bedside monitoring in clinical settings.

[0025] However, traditional DCS analysis suffers from a long integration time, high cost, and low channel number of simultaneous measurements. One factor contributing to these limitations is dependence on very sensitive photodetector and subsequent autocorrelation calculation. An improved flowmetry system provides cost-effective, real-time measurements using statistical analysis without having to rely on autocorrelation analysis on fast time-series data. This statistical analysis can be implemented either in spatial domain using a multi-pixel image sensor, or in the time domain using slow counter. A multi-pixel image sensor can also be used for time domain analysis such that single or multiple pixels act as an individual detector, which is especially suitable for multi-channel application. In various embodiments, this approach can be used to measure blood flow, either absolute, relative, or both.

[0026] FIG. 1 is a block diagram of a system for measuring flow of turbid media. A sample 102 includes a heterogeneous matrix therein. Within this matrix is an embedded flow layer with randomly ordered microcirculatory channels through which small particles 207 move in a non-ordered fashion. For example, in some embodiments

the sample may be body tissue, with a complex network of peripheral arterioles and capillaries. A source 108 injects light into the sample 102. A detector 110 can detect light scattered by the moving particles 207 in the microcirculatory channels. The detector 110 can be positioned to receive light that passes from the source into the sample, and diffuses through the sample. In some embodiments, the detector can be coupled to the sample by a single-mode optical fiber. In some embodiments, the detector may be a multi-pixel image sensor, for example a CCD camera, used to image an area of the sample. In other embodiments, the detector may be a photon-counting avalanche photodiode (APD) or photomultiplier tube (PMT). As the particles flow in random directions, the scattering of light from the source 108 will vary, causing intensity fluctuations to be detected by the detector 110.

[0027] An analyzer 112 is coupled to detector 110 and configured to receive a signal from the detector 110. The time-dependent intensity fluctuations reflect the time-dependent displacements of particles 207 within the sample 102, and accordingly the signal from the detector 110 may be used to determine the flow rate of the particles 207 within the sample 102.

[0028] The flow rate or other characteristic determined by the analyzer 112 may be output to a display 114. The measured quantity may therefore be provided to an operator via the display 114. In various embodiments, the operator may be a clinician, diagnostician, surgeon, surgical assistant, nurse, or other medical personnel. In some embodiments, the measurement may be provided via display 114 in substantially real-time. In some embodiments, the measurement may be provided via display 114 within about 1 second from measurement, *i.e.*, within about 1 second of the time that the scattered light is detected by the detector, the measurement may be provided via display 114. In various embodiments, the measurement may be provided within less than about 10 minutes, within less than about 5 minutes, within less than about 1 minute, within less than about 30 seconds, within less than about 10 seconds, or within less than about 1 second from measurement.

[0029] FIG. 2 is a schematic illustration of diffuse light penetration and detection in multi-layer tissue. As illustrated, a source 202 and a detector 204 are both positioned adjacent a portion of tissue 206. As noted above, in some embodiments optical fibers may be used to couple one or both of the source and detector to the tissue. The tissue 206 is multi-layer, including an upper layer 208 with no flow, and a deeper

layer 210 with flow. A plurality of light-scattering particles 212 flow within capillaries in flow layer 210, and may include, for example, red blood cells. As light 214 is emitted from the source 202, it diffuses as it penetrates the tissue 206. As illustrated, a portion of the light 214 is diffused such that it is incident on the detector 204. The light 214 may follow a roughly crescent-shaped path from the source 202 to the detector 204. The depth of penetration of the light 214 detected by the detector 204 depends on the separation between the source and the detector. As the distance increases, penetration depth generally increases. In various embodiments, the separation distance may be between about 0.5 cm and about 10 cm, or in some embodiments between about 0.75 cm and about 5 cm. Preferably, in other embodiments the separation distance may be between about 1 cm and about 3 cm. In various embodiments, the separation distance may be less than about 10 cm, less than about 9 cm, less than about 8 cm, less than about 7 cm, less than about 6 cm, less than about 5 cm, less than about 4 cm, less than about 3 cm, less than about 2 cm, less than about 1 cm, less than about 0.9 cm, less than about 0.8 cm, less than about 0.7 cm, less than about 0.5 cm, less than about 0.4 cm, less than about 0.3 cm, less than about 0.2 cm, or less than about 0.1 cm. The penetration depth may vary, for example in some embodiments the penetration depth of the sensor may be between about 0.5 cm and about 5 cm, or in some embodiments between about 0.75 cm and about 3 cm. Preferably, in other embodiments the penetration depth may be between about 5 mm and about 1.5 cm. Of course, the tissue optical properties of the various layers also contribute to the penetration depth of the light, as does the intensity, wavelength, or other characteristics of the light source. These variations can allow for the depth of measurement to be adjusted based on the part of the body being analyzed, the particular patient, or other considerations.

[0030] FIG. 3A is a schematic illustration of a diffuse correlation spectroscopy (DCS) system 300. As illustrated, a laser 302 directs light via an input optical fiber 304 into a sample 306. Moving particles are distributed within the sample. The incident light 308 diffuses through the sample 306, affected by the movement of the particles, and is detected via output optical fiber 310 by detector 312. In a DCS system, the detector can be, for example, a photon-counting avalanche photodiode (APD) or photomultiplier tube (PMT). An analyzer 314 is configured to receive a signal from the detector 312. For the DCS system, the analyzer 112 includes an autocorrelator, which calculates the temporal intensity autocorrelation function of light received by the

detector 312. The autocorrelation function can be used to obtain the scattering and flow characteristics of the small particles in the sample 304. The time-dependent intensity fluctuations reflect the time-dependent displacements of the scatterers of the sample 306, and accordingly the autocorrelation function can be used to determine the flow rate within the sample 306. As noted previously, the DCS system requires a precise and fast-counting detector such as an APD or PMT. Additionally, calculating the autocorrelation function is computationally intensive, and the DCS approach favors single-channel measurement.

[0031] FIG. 3B is a schematic illustration of a diffuse speckle contrast analysis (DSCA) system. The illustrated system 301 is configured for spatial domain DSCA (sDSCA). As shown, several components are similar to those in the DCS system of FIG. 3A, including laser 302, input optical fiber 304, sample 306 having moving particles therein, and light 308 diffusing through the sample 306 from the input fiber 304. However, in contrast to the output fiber and detector of the DCS system, the sDSCA system 301 uses relay optics 311 and a CCD camera 313. The relay optics 311 are optional, and may, for example, comprise one or more optical fibers, lenses, mirrors, prisms, or other optical elements. This configuration does not require a fast detector and counter, and furthermore allows simultaneous measurements on many detector positions in an area covered by CCD, compared with the single position measurement by the DCS approach. The detector is therefore greatly simplified by use of a CCD camera 313.

[0032] As shown in FIG. 3A, traditional DCS makes use of two optical fibers, an input fiber 304 to deliver source light, which is typically a multimode fiber, and an output fiber 310 for detecting fluctuation of the transmitted light on a small region. The output fiber 310 is a singlemode fiber, and the core diameter of the fiber 310 must be comparable to the speckle size to ensure detection of the relevant fluctuating signal. In contrast, the DSCAs system of FIG. 3B utilizes a CCD 313 as a detector. In use, a single image from the CCD camera with an optimized magnification and exposure time may be processed by the analyzer 315 to estimate deep tissue flow. As described in more detail below, the analysis technique in sDSCA differs significantly from that of DCS, providing a number of advantages. For example, as sDSCA does not rely on the computationally intensive autocorrelation calculation, the data analysis is vastly simplified.

[0033] **[0033]** This simplified instrumentation and data analysis can also provide better time resolution. Since the image processing can be done very quickly, the

time resolution is only limited by CCD exposure time and CCD readout time. FIG. 4 illustrates a direct comparison between DSCA and traditional DCS measurement in-vivo using a cuff occlusion protocol. Both show nearly identical trends that reflect physiological activity, including a large decrease of blood flow during cuff occlusion, and reactive hyperemia after releasing the cuff. Moreover, DSCA captures finer time data than DCS, enabling observation of fast physiological changes not possible with conventional DCS, such as the low frequency oscillation of about 0.1Hz observed by DSCA in FIG 4. In some embodiments, DSCA can achieve a sampling rate of approximately 30 Hz, compared to the approximately 1 Hz for DCS systems.

[0034] FIG. 5 is a schematic illustration of spatial domain DSCA system. Light from laser 501 is injected into the sample 503 via input optical fiber 505. The laser can provide a long coherence length. The incident light 507 diffuses through the sample 503 and creates a speckle pattern detectable on the upper surface of the sample 503. CCD camera 509 using optional relay optics 511 captures an image of the speckle pattern on the sample 503. Relay optics 511 can include one or more imaging lenses, prisms, mirrors, lens tubes to block stray light, and other optical elements configured to aid the imaging of the speckle pattern on the sample 503 with the CCD camera 509.

[0035] A representation of the obtained raw CCD image 513 is shown, along with a representation of the calculated K_s distribution 515 where 100×50 pixels were used. The raw speckle image 513 is first obtained from the sample surface. The raw speckle images may first be normalized by the smooth intensity background, which can be averaged over a number of speckle images. The speckle contrast, K_s is defined as the ratio of the standard deviation to the mean intensity across many detectors or pixels, $K_s = \sigma_s / \langle I \rangle$, where subscript s refers to the spatial, as opposed to temporal, variations. The quantity K_s is related to the field autocorrelation function $g_1(\tau)$ as follows:

$$V(T) = [K_s(T)]^2 = \frac{2}{T} \int_0^T (1 - \tau/T) [g_1(\tau)]^2 d\tau$$

where V is the intensity variance across the image, and T is the CCD exposure time. By using the known solution of the correlation diffusion equation in the semi-infinite medium, the formal relationship between the flow rate and K_s can be derived. The relationship between the flow and $1/K_s^2$ turns out to be substantially linear in the range of flow seen in body tissue, with $1/K_s^2$ increasing with increasing flow rate, as is illustrated

in FIGS. 6A and 6B. FIG. 6A shows a numerical simulation relating $1/K_s^2$ to the blood flow index (αD_b in a Brownian motion model), while FIG. 6B shows experimental results of the relationship between $1/K_s^2$ to flow rate. Data shown in Figures 6B, 6C, and 6D were measured on a flow phantom, shown in Figure 7. As illustrated in FIG. 7, a phantom 702 includes a flow channel 704, which is between 1 cm and 3.5 cm below the upper surface. A plurality of glass beads 706 is disposed within the flow channel. Intralipid fluid 708 is driven through the flow channel 704 via the peristaltic motor 710. The interstitial spaces between the glass beads 706 within the flow channel 704 simulates microcirculatory flow channels in tissue, and the movement of the intralipid fluid 708 within these interstices simulates arteriole or capillary blood flow. A multimode fiber 712 delivers light into the phantom 702, with a single-mode fiber 714 detecting light scattered by the glass beads 706.

[0036] FIG. 6C illustrates the varying linear relationships between $1/K_s^2$ and the flow rate depending on source-detector separation distance when measuring the flow phantom. At smaller source-detector separations, the measurement depth (nominally equal to half the source-detector separation) may not reach the flow channel 704. This accounts for the data associated with a 1.6cm source-detector separation being largely insensitive to the flow rate within the flow channel 704. As the source-detector separation increases, the measurement depth reaches the flow channel, and the sensitivity of the measurements to the flow rate increases, as reflected in the increased slopes of the data in Fig 6C.

[0037] By dividing the raw image obtained from CCD camera into sub-sections, these sub-sections can each provide different source-detector separation distances. The flow sensitivities calculated from ten source-detector separation distances from a single CCD image are illustrated in FIG. 6D. The use of a single CCD image allows for multi-depth measurements from a single exposure, which may enable a depth-specific measurement of deep tissue blood flow.

[0038] Another way to implement this speckle contrast rationale for flowmetry is to use statistical analysis on time series data obtained by integrating over a certain time. This temporal domain analysis is referred to herein as tDSCA. The integrating time for tDSCA can be regarded as analogous to the exposure time of CCD camera in sDSCA. In the case of tDSCA, a detector with moderate sensitivity with an integrating circuit can be used. For example, each pixel on a CCD chip can be used for

this purpose as each CCD pixel keeps accumulating photoelectrons for a given exposure time. Therefore, a number of single-mode fibers can be directly positioned on some locations on a single CCD chip, resulting in a multi-channel tDSCA system without losing any time resolution. The number of channels is only limited by the CCD chip size, pixel size, and the area of each fiber tip. In some embodiments, tDSCA can use sensitive detectors such as avalanche photodiode (APD) and/or photomultiplier tube (PMT) with a slow counter such as a counter included in a DAQ card with USB connection, but scaling this embodiment to multichannel instrument is costly and bulky. Time-series data taken either way can be obtained by repeat measurements, for example 25 measurements can be made consecutively, after which the data can be analyzed statistically to determine the flow rate. In a configuration with an exposure time of 1 ms, one flow index would be obtained every 25 ms, resulting in approximately 40 Hz operation.

[0039] The statistical analysis of the time-series data can be substantially identical to that described above with respect to sDSCA, except that the statistics (average intensity and standard deviation of intensity) are calculated in the time domain, rather than the spatial domain. As a result, tDSCA may provide lower time resolution than sDSCA. However, the detector area for tDSCA may be significantly smaller than with sDSCA. As with the spatial domain counterpart, tDSCA provides an approach with instrumentation and analysis that are significantly simpler and less computationally intensive than traditional DCS techniques.

[0040] FIG. 8 is a flow diagram of a method for calculating flow rate using spatial domain DSCA. Process 800 begins in block 802 with directing a coherent light source onto a sample. As noted above, the coherent light source can be, for example, a laser having a long coherence length (i.e., coherence length greater than about 1 mm). Next in block 804 a speckle image of the sample is obtained using a CCD camera with a selected exposure time. The position of the sample at which the image is taken is selected based on the desired penetration depth into the sample of the detected light scattered by deep tissue flow. CCD will capture the image of speckle either by using a relay optics or by placing the CCD chip directly onto the surface of the sample. Process 800 continues in block 806 with calculating the spatial speckle contrast (K_s) by dividing the standard deviation of the intensity of image pixels by the average of the intensity of image pixels. In some embodiments, a number of adjacent pixels may be grouped together for a single intensity data point, and standard deviation among the different groups of pixels can be

calculated. Similarly, the average intensity among the different groups of pixels can likewise be calculated. Process 800 continues in block 808 with calculating the flow rate using the spatial speckle contrast (K_s). As described above, $1/K_s^2$ is related to flow rate in a substantially linear fashion, allowing for computationally trivial calculation of the flow rate. In some embodiments, this approach is used to calculate relative blood flow rate only. In many clinical applications, relative blood flow measurements can be adequate for the task at hand. In other embodiments, this approach can be used to calculate absolute blood flow rate.

[0041] FIG. 9 is a flow diagram of a method for calculating flow rate using time domain DSCA. Process 900 begins in block 902 with directing a coherent light source onto a sample. This step can be performed essentially identically to spatial domain DSCA. Next, in block 904, time series data of light scattered from the sample is detected. A detector, for example a CCD camera, CMOS image sensor, an avalanche photodiode, or photomultiplier tube, may be coupled to the sample via a single-mode optical fiber. Intensity measurements may be integrated over a selected exposure time. In some embodiments, the select exposure time can be approximately 1 ms. A series of such measurements are taken sequentially to provide time-series data. Process 900 continues in block 906 with calculating the temporal speckle contrast (K_t) by dividing the standard deviation of the time series data by the average of the time series data. In block 908, the flow rate can be calculated using the temporal speckle contrast (K_t). As with the spatial speckle contrast ratio, $1/K_t^2$ is related to flow rate in a substantially linear fashion, allowing for the flow rate to be easily calculated. The blood flow rate calculated may be relative flow in some embodiments.

[0042] Whether spatial or temporal domain DSCA is selected may depend on a variety of factors. For example, sDSCA relies on the use of a CCD camera or similar imaging device, which is relatively large compared with a single-mode fiber and a photodiode. In some applications, the size difference may pose little obstacle to its use. In applications in which the size of the CCD camera is a limiting factor, a small area sensor may be used and applied directly onto the skin, or a relay optics with small magnification can be used. However, tDSCA does not face the same limitations, and accordingly the temporal domain may be more suitable when space or curvature renders sDSCA impractical. As noted previously, tDSCA provides relatively low time resolution compared to sDSCA, however the tDSCA time resolution is typically adequate for patient

monitoring applications, particularly for long-term perfusion monitoring. For short-term monitoring, when time resolution may be more important, sDSCA may be the preferred approach. In both spatial and temporal domains, DSCA provides a technique for measuring blood flow perfusion accurately and quickly, with higher time resolution and lower cost instrumentation than previous methods.

[0043] Although this application has been disclosed in the context of certain embodiments and examples, it will be understood by those skilled in the art that the present application extends beyond the specifically disclosed embodiments to other alternative embodiments and/or uses of the application and obvious modifications and equivalents thereof. Additionally, the skilled artisan will recognize that any of the above-described methods can be carried out using any appropriate apparatus. Further, the disclosure herein of any particular feature in connection with an embodiment can be used in all other disclosed embodiments set forth herein. Thus, it is intended that the scope of the present application herein disclosed should not be limited by the particular disclosed embodiments described above.

WHAT IS CLAIMED IS:

1. A method for determining blood flow in a patient, the method comprising:
 - directing coherent light onto a first location of the patient's tissue;
 - imaging a second location of the patient's tissue, wherein a portion of the coherent light is scattered by the blood flow beneath the patient's tissue such that the scattered light is at least partially detectable at the second location; and
 - calculating the blood flow based on the image of the second location.
2. The method of Claim 1, wherein the calculating comprises calculating the speckle contrast.
3. The method of Claim 2, wherein calculating the speckle contrast comprises dividing the standard deviation of intensity by the average intensity of the image of the second location.
4. The method of Claim 1, wherein the blood flow is at least 5 mm below the surface of the patient's skin.
5. The method of Claim 1, wherein the first and second locations are on a patient's limb.
6. The method of Claim 1, wherein the first and second locations are on a patient's foot.
7. The method of Claim 1, wherein imaging the second location comprises capturing an image with a CCD camera.
8. The method of Claim 1, wherein the coherent light comprises light from a laser.
9. The method of Claim 1, wherein the first and second locations are at least 10 mm apart.
10. The method of Claim 1, further comprising signaling the blood flow an operator.
11. A method for determining blood flow in a patient, the method comprising:
 - directing coherent light onto a first location of the patient's skin;
 - obtaining time-series measurements of the light intensity at a second location of the patient's skin, wherein a portion of the coherent light is scattered by the blood flow beneath the patient's skin such that the scattered light is at least partially detectable at the second location; and
 - calculating the blood flow based on the time-series measurements.

12. The method of Claim 11, wherein the calculating comprises calculating the temporal speckle contrast.

13. The method of Claim 12, wherein calculating the temporal speckle contrast comprises dividing the temporal standard deviation of intensity by the temporal average intensity at the second location.

14. The method of Claim 11, wherein the blood flow is at least 5 mm below the surface of the patient's skin.

15. The method of Claim 11, wherein the first and second locations are on a patient's foot.

16. The method of Claim 11, wherein the first and second locations are at least 10 mm apart.

17. The method of Claim 11, further comprising signaling the blood flow to an operator.

18. The method of Claim 11, wherein the signaling comprises providing audible, visual, or tactile indicia of blood flow.

19. A system for assessment of blood flow in tissue, the system comprising:
a coherent light source configured to apply light to the tissue;
a multi-pixel image sensor configured to capture optical information including at least a quantity of light transmitted through the tissue, wherein the light is scattered, at least in part, by the blood flow;
an analyzer configured to analyze the optical information to determine blood flow in the tissue; and
a feedback device configured to provide a signal indicative of the blood flow determined by the analyzer.

20. The system of Claim 19, wherein the multi-pixel image sensor comprises a CCD camera.

21. The system of Claim 19, wherein the analyzer is configured to calculate the spatial speckle contrast by dividing the spatial standard deviation of intensity by the spatial average of intensity.

22. The system of Claim 19, wherein the system is configured to provide the signal indicative of the blood flow in substantially real-time.

23. The system of Claim 19, wherein the analyzer is configured to calculate the temporal speckle contrast by dividing the temporal standard deviation of intensity by the temporal average of intensity.