

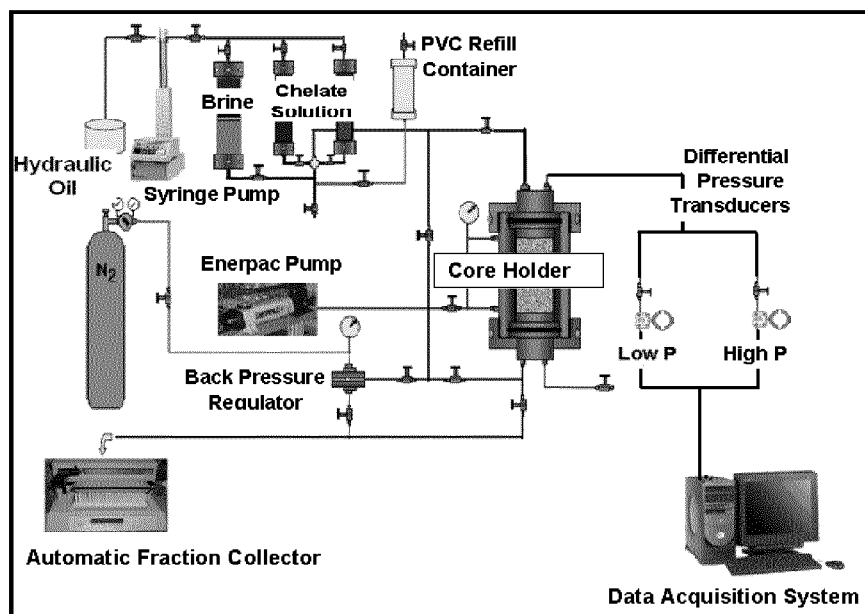


Fig. 1- Core flooding set-up.

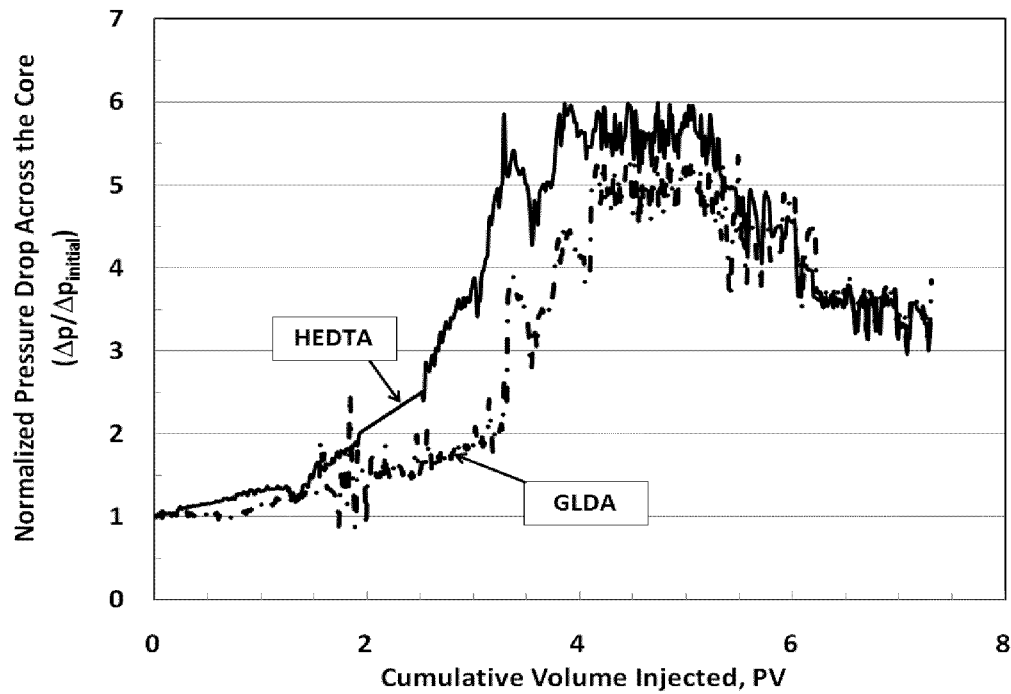


Fig. 2 - Pressure drop across the core during the core flooding experiment for 0.6M GLDA (pH = 4) and 0.6M HEDTA (pH = 4) at 300°F and 5 cm³/min using Berea sandstone cores.

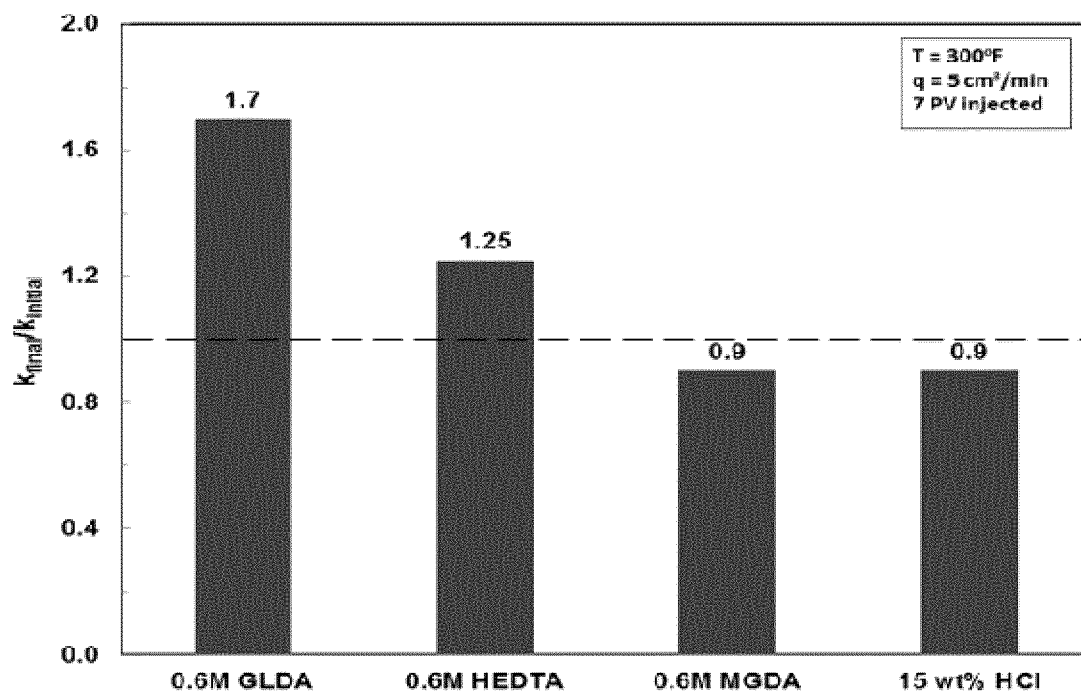


Fig. 3 - Permeability ratio for the Berea sandstone cores treated with 15 wt% HCl and 0.6M chelating agent (pH =4) at 300°F and 5 cm³/min.

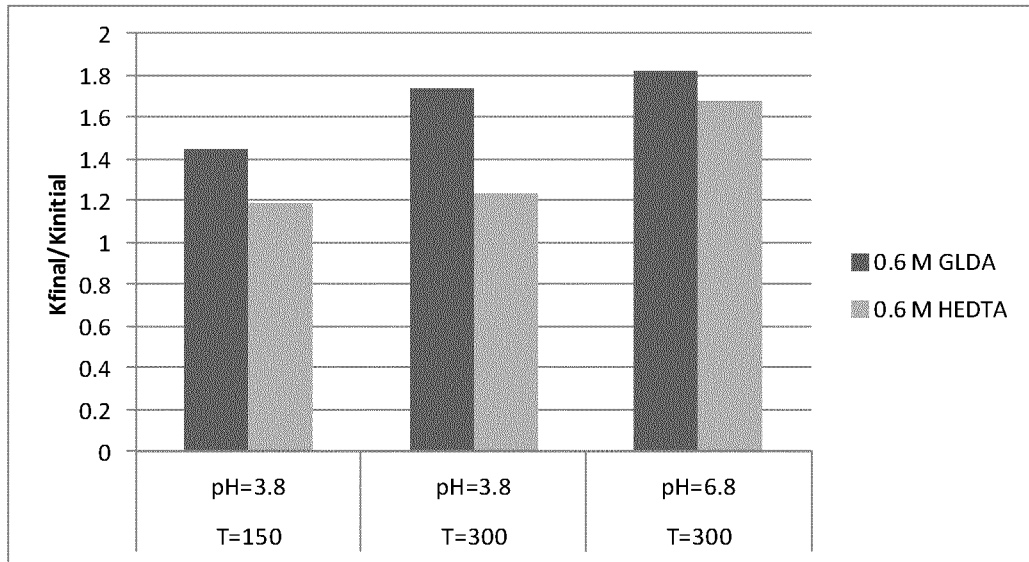


Fig. 4 - Permeability ratio for the Berea sandstone cores treated with 0.6M chelating agent at pH=3.8 or pH=6.8 and at 150 or 300°F and 5 cm³/min.

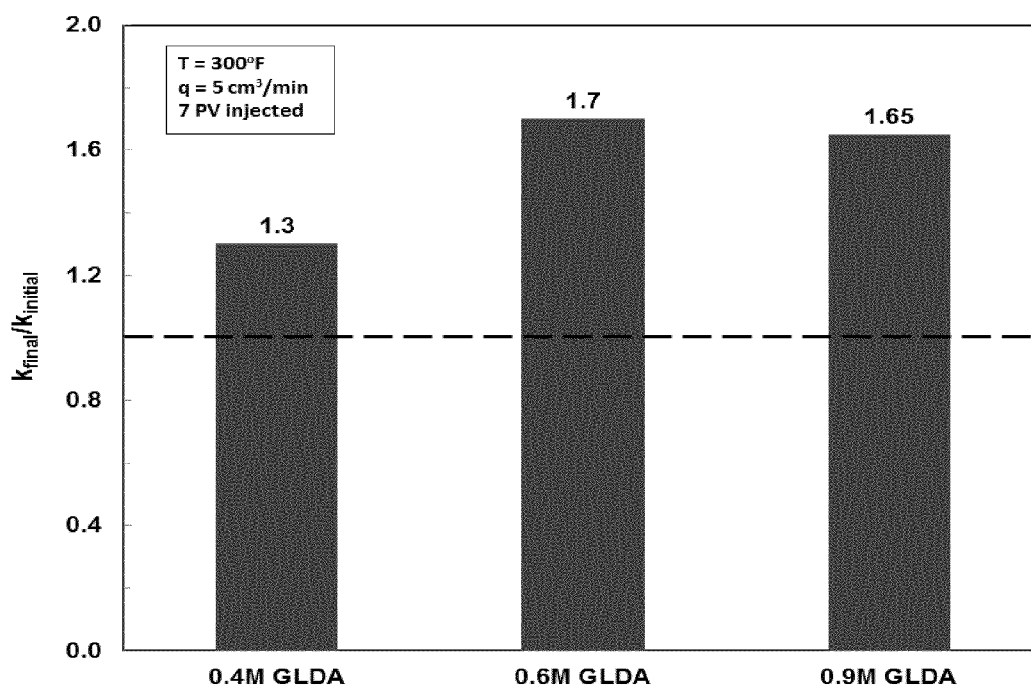


Fig. 5 - Permeability ratio for the Berea sandstone cores after treatment by different GLDA concentration.

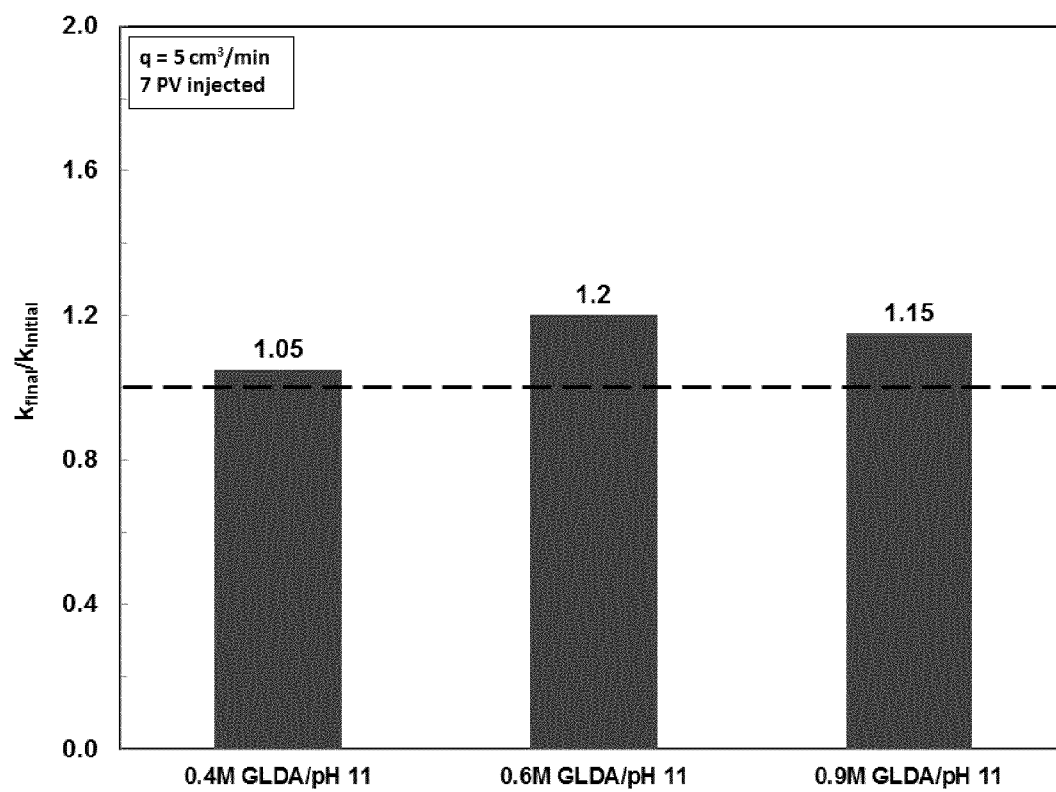


Fig. 6 - Permeability ratio for the Berea sandstone cores after treatment by different GLDA concentration.

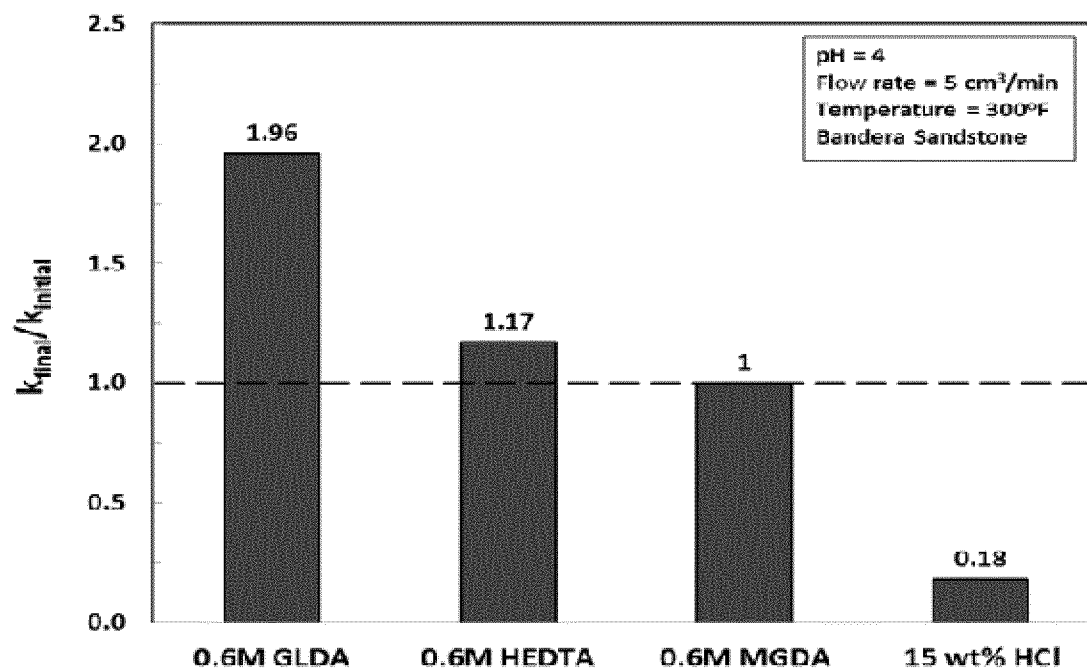


Fig. 7 - Permeability ratio for the Bandera sandstone cores treated with 15 wt% HCl and 0.6M chelate (pH =4) at 300°F and 5 cm³/min.

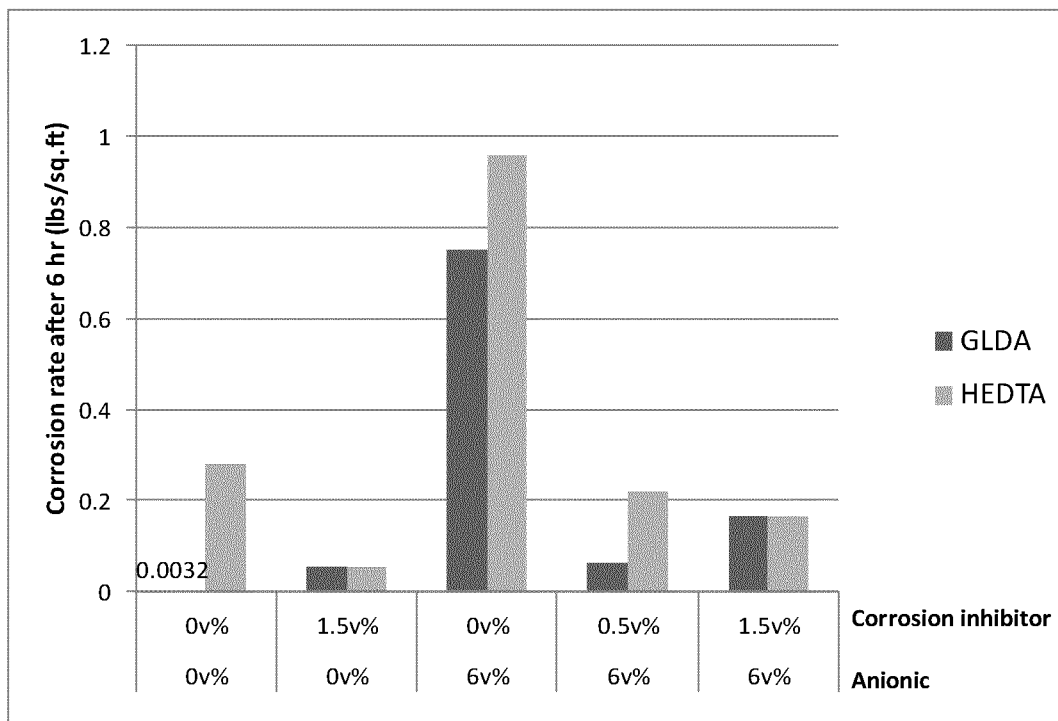


Fig. 8 - The corrosion rate after a 6-hour corrosion test at 325°F (=163°C) of 0.6 M GLDA and HEDTA at pH=3.8 and 1,000psi nitrogen (N₂) pressure, with 0-1.5 vol% corrosion inhibitor (Armohib 31; 100wt% active ingredient) and 0 or 6 vol% anionic surfactant (Witconate NAS-8; 36wt% active ingredient)

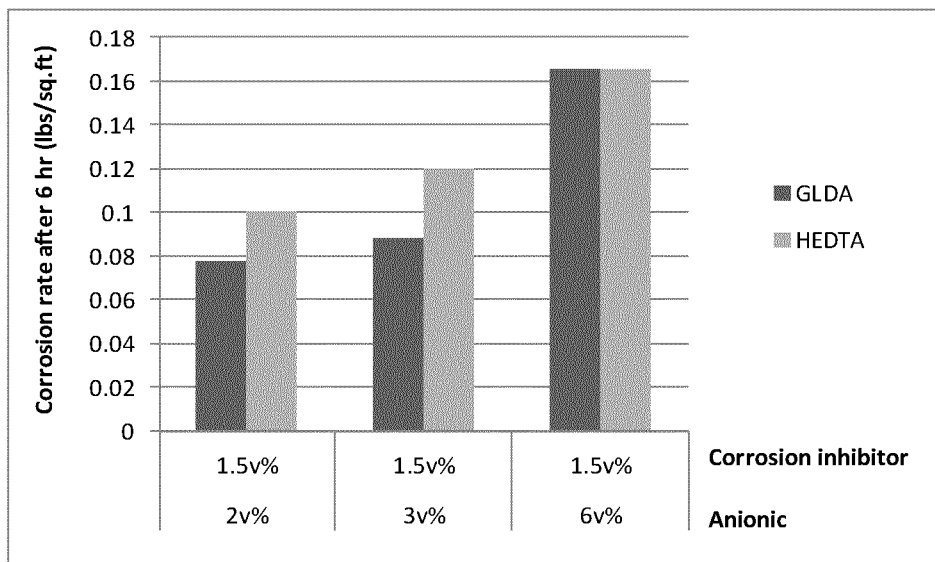


Fig. 9 - The corrosion rate after a 6-hour corrosion test at 325°F (=163°C) of 0.6 M GLDA and HEDTA at pH=3.8 and 1,000psi nitrogen (N₂) pressure, with 1.5 vol% corrosion inhibitor (Armohib 31; 100wt% active ingredient) and 2-6 vol% anionic surfactant (Witconate NAS-8; 36wt% active ingredient)