

Description

This invention relates to an apparatus for coin testing and more particularly to an improved inductive sensing arrangement for use in electronic coin testing apparatus.

There are several types of inductive coin discrimination apparatus based upon passing a coin through the electromagnetic field of an inductor which is part of an oscillator circuit. For greater accuracy of discrimination, a coin may be examined using two or more frequencies by introducing the coin into electromagnetic fields of different frequencies and determining if the interactions between the coin being tested and the fields are within predetermined tolerances anticipated for acceptable electrically conductive coins. See, for example, U.S. Patent No. 3,870,137, assigned to the assignee of the present application.

In some of the tests by apparatus as disclosed in the prior art, the coin under test is introduced through a coin entry and travels along a coin passageway past an inductor or inductors located along one side of the coin passageway or in some cases on opposing sides of the coin passageway. The inductor is part of an inductor-capacitor (LC) oscillator circuit which oscillates at an idling frequency in the absence of a coin. When a coin is present alongside the inductor, the frequency of the oscillator circuit containing the inductor shifts. The degree of interaction between the coin and the electromagnetic field of the inductor forms the basis for coin identification.

Given the natural wear which occurs during a coin's circulation and the consequential range of coin interaction for a given coin denomination, a practical coin identification apparatus must accept coins which fall within certain tolerance ranges. Accuracy of measurement of the interaction of a coin and an electromagnetic field is important and particularly so for discriminating between valid coins just within the tolerance range and invalid coins just outside the tolerance range.

The coin testing apparatus according to the present invention comprises a coin testing apparatus comprising means to subject a coin in a coin passageway to an electromagnetic field, means to produce a signal indicative of the degree of interaction of the coin with the field, and means to determine whether said signal corresponds to that for an acceptable coin, wherein the means to subject a coin to an electromagnetic field comprises an oscillator which includes an inductor adjacent the coin passageway which produces the electromagnetic field in the coin passageway, the oscillation frequency of the oscillator being a function of the effective inductance of the inductor, characterized in that the oscillator is a resistor-inductor type relaxation oscillator.

The inductive sensor circuit the present invention may operate at a frequency in the range of approximately 100 kHz to 1 MHz. The exact fre-

quency selected depends upon the balancing of greater resolution capability versus greater adverse effects of stray capacitances at the higher frequencies. The RL relaxation oscillator is an oscillator circuit which has two stable states resulting in two distinct output levels, and which switches between the two states at a rate determined by the rate of rise or decay of voltage across the storage element in the RL circuit. The RL relaxation oscillator has a linear frequency response to changes in the effective inductance in the circuit and may be easily tuned by the adjustment of a resistor whereas typical non-relaxation type LC oscillators have a non-linear frequency response and usually require tuning by adjustment of a variable capacitor. Also, the sensor circuit will operate independently of the Q of the circuit, unlike LC oscillator circuits. Other aspects of the sensor circuit are that its output signal has well defined zero crossings and can be easily translated from logic level to logic level, e.g., TTL to CMOS.

Because the RL relaxation oscillator has nearly double the frequency shift of an LC non-relaxation oscillator per unit change in effective inductance brought about by coin influence, coin interaction with the magnetic field of the inductor of an RL oscillator can be measured with greater accuracy than the interaction of the same coin with the field of the inductor of an LC oscillator can be measured. Such improved accuracy of measurement is particularly important when a frequency of oscillation of an oscillator is sampled for a very short time.

Further features of the invention, its nature, and various advantages will be more apparent upon consideration of the following detailed description of exemplary embodiments of the invention with reference to the accompanying drawings.

In the drawings:

Fig. 1 illustrates a simple RL relaxation oscillator;

Fig. 2 illustrates a simple LC oscillator (a Colpitts oscillator) for purposes of comparison;

Fig. 3 is a schematic of a first embodiment of inductive coin testing apparatus according to the invention;

Fig. 4 is a schematic of second and third embodiments of inductive coin testing apparatus according to the invention;

Fig. 5 illustrates an oscillator circuit suitable for use in determining a coin characteristic such as coin diameter in any of the disclosed embodiments of the invention; and

Fig. 6 illustrates a second oscillator circuit suitable for use in determining a coin characteristic such as coin thickness in any of the disclosed embodiments of the invention.

Although coin selector apparatus constructed in accordance with the principles of this invention may be designed to identify and accept any number of coins from the coin sets of many countries, the invention will be adequately illustrated by explanation of its application to identify the U.S. 5-, 10-, and 25-cent coins. The figures are

intended to be representational and are not necessarily drawn to scale. Throughout this specification the term "coin" is intended to include genuine coins, tokens counterfeit coins, slugs, washers, and any other item which may be used by persons in an attempt to use coin-operated devices. Furthermore, from time to time in this specification, for simplicity, coin movement is described as rotational motion; however, except where otherwise indicated, translational and other types of motion also are contemplated. Similarly, although specific types of logic circuits are disclosed in connection with the embodiments described below in detail, other logic circuits can be employed to obtain equivalent results without departing from the invention.

Fig. 1 illustrates a simple RL relaxation oscillator circuit 10 consisting of a voltage supply 1, a switch 2, a resistor 3 (R), an inductor 7 (L), a Schmitt trigger gate 9, and a diode 11. When the switch 2 is closed and voltage is initially supplied, the input to the gate 9 will be high. The gate 9 produces a low output (ground) when it receives a high input (an input above the gate's upper threshold level). The low at the output of the gate 9 provides a path for current to flow from voltage supply 1 through the resistor 3 and the inductor 7 to ground.

As the current through the inductor 7 increases, the voltage drop across the resistor 3 increases until the voltage at the input of the gate 9 drops below the gate's lower threshold level. When the input voltage level drops below the lower threshold level, the output of the gate 9 goes high interrupting the flow of current through the inductor 7. With this interruption of current, the voltage level at the output of the gate 9 rises rapidly. This rapid rise means the voltage waveform at the output of the gate 9 will have a steep slope. Diode 11 limits this rise of voltage level at the output of the gate 9 to the supply voltage plus the voltage drop across the diode 11 and provides a path for discharge of the inductor current. Inductor current discharges along a path through the diode 11 and the resistor 3 until the voltage at the input of the gate 9 again reaches the upper threshold value. When the upper threshold voltage is reached, the gate 9 again produces a low output and the cycle repeats until the switch 2 is opened. This produces an oscillation with a square waveform.

The frequency of oscillation of the RL oscillator 10 is approximately a constant times the ratio of R and L ($f_{RL} \approx K \times R/L$). The change in frequency for a change in inductance may be approximated by the following relationship: $\Delta f_{RL} \approx -f(\Delta L/L)$. For an LC oscillator such as the Colpitts oscillator of Fig. 2, containing inductor L and capacitors C of equal capacitance, the analogous relationships are $f_{LC} \approx (K/2\pi)(1/\sqrt{LC})$ and $\Delta f_{LC} \approx -f(\Delta L/2L)$.

When a coin affects the electromagnetic field of either an LC or an RL relaxation type of oscillator, it results in a change in the effective inductance in the oscillator. The RL oscillator has a linear response to changes in inductance. For a given change in effective inductance L, the change in

frequency for the RL oscillator, Δf_{RL} , is twice that for the LC oscillator Δf_{LC} .

The present invention adapts the RL relaxation oscillator for use in coin discriminating apparatus. Fig. 3 illustrates in schematic form a first embodiment of coin discriminating apparatus 60 which comprises RL oscillator circuit 40 including inductor 37, and test means 50 to establish whether the output of oscillator 40 corresponds to that expected for an acceptable coin. The mechanical structure of the apparatus 60 may be similar to the mechanical apparatus shown and described in U.S. Patent No. 3,870,137. The portion shown in Fig. 3 includes a back sidewall 36, a coin entry cup 31, a coin track 33 comprising an edge of a first energy dissipating device, and a second coin track 35 comprising an edge of a second energy dissipating device 35a, which forms the initial track section, and a terminal track section which is molded from plastic along with the sidewall 36 as a single piece. The mechanical structure of this portion of the apparatus also includes a front sidewall 38 which is spaced from and generally parallel to the back sidewall 36. The two sidewalls 36 and 38 are connected together by a hinge and spring 34 at one corner, in a manner similar to that shown in U.S. Patent No. 3,907,086, except that the retarding apparatus disclosed in that patent is not necessarily used. Together with the energy dissipating devices 33, 35a and the track 35, the sidewalls 36 and 38 form a coin passageway from the coin entry cup 31 past the coin testing inductor 37 which is located in or behind one of the sidewalls. The inductor's location with respect to the coin track is generally indicated by broken lines in Fig. 3.

The test means 50 used with this embodiment is circuitry which measures the maximum shift in frequency of the oscillator circuit 40 from normal idling frequency and determines whether this frequency shift corresponds to that produced when a genuine coin passes the inductive element in the RL oscillator circuit. Circuitry for measuring the frequency shift is known in the art. Such circuitry shown and described, for example, in U.S. Patent No. 3,918,564, see particularly Fig. 4 and text at column 3, line 60 to column 4, line 55 in that patent. Alternatively, the test means 50 can be any one of a number of suitable detector circuits which detect whether the maximum frequency of the oscillator during coin passage is within a tolerance range of the frequency for a genuine coin. See, for example, Figs. 4, 10 and 8 and the corresponding text at column 5, line 13 et seq., column 10, line 65 to column 11, line 47; and column 21, line 66 to column 23, line 47 in U.S. Patent No. 3,870,137.

A coin enters the mechanical section 30 of apparatus 60 through coin entry 31. The coin then travels along coin tracks 33 and 35 between sidewalls 36 and 38. Sidewalls 36 and 38 are parallel plates spaced apart by at least slightly more than the thickness of the thickest coin to be processed by the apparatus. In addition, sidewalls 36 and 38 are tilted slightly from the vertical so

that a face of a coin rolling down coin track 33 and later coin track 35 bears on front sidewall 38. Inductor 37, as shown in Fig. 3, is mounted alongside coin track 35 in the front sidewall 38. Alternatively, the inductor 37 may consist of two coils series connected opposite each other, one coil being mounted in each sidewall. A two coil embodiment will be discussed in conjunction with Figs. 4 and 6.

Inductor 37 is part of the RL relaxation oscillator circuit 40 such as the oscillator circuits shown in Fig. 5 and Fig. 6. When a coin passes inductor 37, the frequency of oscillation of oscillator circuit 40 will shift. Test means 50 of Fig. 3 determines in known fashion if the peak frequency shift of the oscillator circuit 40 during coin passage is indicative of an acceptable coin, i.e., whether the maximum frequency or frequency shift occurring during coin passage is within a predetermined tolerance range.

In second and third embodiments shown in Fig. 4, two oscillator circuits such as those shown in Figs. 5 and 6 are combined in a single apparatus 460 for testing two characteristics of a coin.

A coin to be tested enters the mechanical portion of the apparatus 460 through coin entry 431.

The coin then travels along coin tracks 433 and 435 between the back sidewall 436 and the front sidewall 438. The coin first reaches inductor 437 which is mounted in the front sidewall 438. The inductor 437 is of the pot core type, approximately 21.6 mm in diameter with its face approximately 0.4 mm from the passageway side of the front sidewall 438 and its center approximately 20 mm above the coin track in an embodiment for the United States coin set. Inductor 437 is part of oscillator circuit 440. Coin passage by inductor 437 will affect the frequency of oscillation of oscillator 440. Test means 450 is connected to oscillator 440 and determines if this effect is indicative of an acceptable coin. An idling frequency, the frequency of oscillation when a coin is not passing by inductor 437, of about 300 kHz for oscillator 440 is employed for coin diameter testing in this embodiment.

After passing inductor 437, the coin continues along coin track 435 toward inductors 439a and 439b. These two inductors are connected in series and are mounted opposite one another in the sidewalls. Each of inductors 439a and 439b is of the pot core type, approximately 18 mm in diameter with its face approximately 0.4 mm for the passageway side of the sidewall in which it is mounted and its center approximately 9.5 mm above the coin track in an embodiment for the United States coin set. Inductors 439a and 439b are part of oscillator 445 which, like oscillator 440, is affected by coin passage. Test means 455 is connected to oscillator 445 and determines if this effect is indicative of an acceptable coin. An idling frequency of about 850 kHz for oscillator 445 is employed for coin thickness testing in this embodiment. A signal on line 448 is employed to switch on either of the oscillators 440 and 445. An

inverter 449, shown in Fig. 4 as an inverter connected NAND gate, is connected between line 448 and one of the oscillators, so that when oscillator 445 is on, oscillator 440 is off and vice versa, thus avoiding the possibility of interference between them.

Fig. 5 illustrates an RL relaxation oscillator 140 suitable for use in coin discrimination apparatus according to either of the embodiments of my invention. The basic functioning of oscillator 140 is similar to that of the oscillator 10 of Fig. 1. Resistor 143 corresponding to resistor 3 of Fig. 1, consists of fixed value resistor 144 and adjustable resistor 145. The addition of the adjustable resistor 145 allows the frequency of oscillator 140 to be tuned by simply adjusting the adjustable resistor 145. Capacitor 152 connected between one input of a NAND gate Schmitt trigger 149 and ground is added to eliminate higher modes of oscillation resulting from stray capacitance in the circuit. The other input to the NAND gate 149 is a control line for switching the oscillator 140 on or off. Additional resistors 155 and 156 connected in series between the output of gate 149 and ground serve as an output attenuator 154 to reduce the amplitude of the signal produced at the output of gate 149 to a level compatible with the circuitry of the test means used to determine if the coin effect on the oscillator 140 is indicative of an acceptable coin.

An output signal suitably scaled by the output attenuator 154, is taken from the node connecting resistors 155 and 156 using line 157. The output signal on line 157 is digital in nature and requires no amplitude adjustment or shaping beyond that provided by attenuator 154 to be suitable for counting. The digital nature of the signal on line 157 makes the RL relaxation oscillator 140 especially suitable for use in coin discrimination apparatus employing a microprocessor or other digital circuitry.

A circuit similar in construction to the one shown in Fig. 5 is suitable for use in determining coin diameter. For diameter testing according to one embodiment of the invention, inductor 147 consists of a single coil with an inductance of 1.0 mH and the idling frequency of oscillator 140 is about 300 kHz. Table 1 below lists typical values of components for an oscillator circuit as shown in Fig. 5.

TABLE 1

Supply	141	5V DC
Resistors	144	330 Ohms
	155	1 k
	156	5.1 k
Adjustable resistor	145	0—1 k
Inductor	147	1 mH

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TABLE 1 (Continued)

Schmitt trigger	149	One section of a National Semiconductor Model No. DM 74132 four section Schmitt trigger NAND gate
Diode	151	1N4004
Capacitor	152	180 pf

A circuit similar in construction to the one shown in Fig. 6 can be used for determining coin thickness. The basic functioning of oscillator 240 is similar to that of oscillator 10 of Fig. 1 and inductor 247 consists of two coils 247a and 247b connected in series. In this embodiment, each of the coils has an inductance of 240 uH and the idling frequency of oscillator 240 is about 850 kHz. Since the coils 247a and 247b of the inductor 247 are on opposite sidewalls of the apparatus, the leads are relatively long. A resistor 246 is provided to reduce the adverse capacitive effects of these leads. A resistor 254 is provided to reduce drift of frequency shift with temperature. Table 2 below lists typical values of components for an oscillator circuit as shown in Fig. 6.

TABLE 2

Supply	241	5V DC
Resistors	244	330 Ohms
	246	43 k
	254	2.2 k
	255	1 k
	256	5.1 k
Adjustable Resistor	245	0—1 k
Inductor	247	2 coils—each 240 uH
Schmitt trigger	249	One section of a National Semiconductor Model No. DM 74132 four section Schmitt trigger NAND gate
Diode	251	1N4004
Capacitor	252	82 pF

Claims

1. A coin testing apparatus comprising means (35, 37; 435, 437, 439) to subject a coin in a coin passageway (35; 435) to an electromagnetic field, means (40; 440, 445) to produce a signal indicative of the degree of interaction of the coin with the field, and means (50; 450, 455) to determine whether said signal corresponds to that for an acceptable coin, wherein the means to subject a coin to an electromagnetic field comprises an oscillator which includes an inductor (147; 247) adjacent the coin passageway which produces the electromagnetic field in the coin passageway, the oscillation frequency of the oscillator being a function of the effective inductance of the inductor, characterised in that the oscillator is a resistor-inductor type relaxation oscillator (140; 240).
2. Apparatus as claimed in claim 1, characterised in that the means (50; 450, 455) to determine whether a signal corresponds to that for an acceptable coin include counting means for counting the oscillations of the oscillator output signal.
3. A coin testing apparatus as claimed in claim 1 or claim 2, characterised in that said resistor-inductor relaxation oscillator (140; 240) has a substantially linear frequency change with respect to change in the effective inductance in the oscillator over a range of inductance suitable for testing coins and produces an output signal which is digital in nature and requires no amplitude discrimination or shaping to be suitable for counting.
4. Apparatus as claimed in claim 1, characterised in that the resistor-inductor relaxation oscillator (140; 240) further comprises a variable resistor (145; 245) connected to the inductor.
5. Apparatus as claimed in claim 1, characterised in that the resistor-inductor relaxation oscillator (140; 240) further comprises a capacitor (152; 252) connected to eliminate higher modes of oscillation due to stray capacitance in the resistor-inductor relaxation oscillator.
6. Apparatus as claimed in any preceding claim, characterised in that the inductor comprises a single coil (147) and the normal frequency of oscillation of the oscillator (140) in the absence of a coin is approximately 300 kHz.
7. Apparatus as claimed in any preceding claim, characterised in that the coin passageway has two side-walls the inductor comprises two coils (247a, 247b) which are serially connected, the coils being mounted opposite one another on the sidewalls of the coin passageway and the normal frequency of oscillation of the resistor-inductor relaxation oscillator (240) in the absence of a coin is approximately 850 kHz.
8. Apparatus as claimed in any preceding claim, characterised in that the means (40; 440, 445) to produce a signal indicative of the degree of interaction of the coin with the electromagnetic



(14)

TABLE 1 (Continued)

Schmitt trigger	149	One section of a National Semiconductor Model No. DM 74132 four section Schmitt trigger NAND gate
Diode	151	1N4004
Capacitor	152	180 pf

A circuit similar in construction to the one shown in Fig. 6 can be used for determining coin thickness. The basic functioning of oscillator 240 is similar to that of oscillator 10 of Fig. 1 and oscillator 140 of Fig. 5. For coin thickness testing, inductor 247 consists of two coils 247a and 247b connected in series. In this embodiment, each of the coils has an inductance of 240 uH and the idling frequency of oscillator 240 is about 850 kHz. Since the coils 247a and 247b of the inductor 247 are on opposite sidewalls of the apparatus, the leads are relatively long. A resistor 246 is provided to reduce the adverse capacitive effects of these leads. A resistor 254 is provided to reduce drift of frequency shift with temperature. Table 2 below lists typical values of components for an oscillator circuit as shown in Fig. 6.

TABLE 2

Supply	241	5V DC
Resistors	244	330 Ohms
	246	43 k
	254	2.2 k
	255	1 k
	256	5.1 k
Adjustable Resistor	245	0—1 k
Inductor	247	2 coils—each 240 uH
Schmitt trigger	249	One section of a National Semiconductor Model No. DM 74132 four section Schmitt trigger NAND gate
Diode	251	1N4004
Capacitor	252	82 pF

Claims

1. A coin testing apparatus comprising means (35, 37; 435, 437, 439) to subject a coin in a coin passageway (35; 435) to an electromagnetic field, means (40; 440, 445) to produce a signal indicative of the degree of interaction of the coin with the field, and means (50; 450, 455) to determine whether said signal corresponds to that for an acceptable coin, wherein the means to subject a coin to an electromagnetic field comprises an oscillator which includes an inductor (147; 247) adjacent the coin passageway which produces the electromagnetic field in the coin passageway, the oscillation frequency of the oscillator being a function of the effective inductance of the inductor, characterised in that the oscillator is a resistor-inductor type relaxation oscillator (140; 240).
2. Apparatus as claimed in claim 1, characterised in that the means (50; 450, 455) to determine whether a signal corresponds to that for an acceptable coin include counting means for counting the oscillations of the oscillator output signal.
3. A coin testing apparatus as claimed in claim 1 or claim 2, characterised in that said resistor-inductor relaxation oscillator (140; 240) has a substantially linear frequency change with respect to change in the effective inductance in the oscillator over a range of inductance suitable for testing coins and produces an output signal which is digital in nature and requires no amplitude discrimination or shaping to be suitable for counting.
4. Apparatus as claimed in claim 1, characterised in that the resistor-inductor relaxation oscillator (140; 240) further comprises a variable resistor (145; 245) connected to the inductor.
5. Apparatus as claimed in claim 1, characterised in that the resistor-inductor relaxation oscillator (140; 240) further comprises a capacitor (152; 252) connected to eliminate higher modes of oscillation due to stray capacitance in the resistor-inductor relaxation oscillator.
6. Apparatus as claimed in any preceding claim, characterised in that the inductor comprises a single coil (147) and the normal frequency of oscillation of the oscillator (140) in the absence of a coin is approximately 300 kHz.
7. Apparatus as claimed in any preceding claim, characterised in that the coin passageway has two side-walls the inductor comprises two coils (247a, 247b) which are serially connected, the coils being mounted opposite one another on the sidewalls of the coin passageway and the normal frequency of oscillation of the resistor-inductor relaxation oscillator (240) in the absence of a coin is approximately 850 kHz.
8. Apparatus as claimed in any preceding claim, characterised in that the means (40; 440, 445) to produce a signal indicative of the degree of interaction of the coin with the electromagnetic



field comprises means responsive to the frequency of the resistor-inductor relaxation oscillator (140; 240) when the coin passes and means to produce a signal indicative of the frequency of the oscillator.

9. Apparatus as claimed in any one of claims 1, 4 or 5, characterised by two separate such oscillators (140, 240) having their inductors (147, 247) adjacent the coin passageway to subject the coin to two fields, each resistor-inductor relaxation oscillator having a linear frequency response with respect to changes in the effective inductance in the oscillator over a range of inductance suitable for testing coins and producing an output signal which is digital in nature and requires no amplitude discrimination or shaping to be suitable for counting, and means to determine if the output signals of the two oscillators correspond to those for an acceptable coin.

Patentansprüche

1. Münzprüfapparat mit einer Einrichtung (35, 37; 435, 437, 439), die eine Münze in einer Münzlaufbahn (35; 435) einem Elektromagnetfeld unterwirft, einer Einrichtung (40; 440, 445) zur Erzeugung eines Signals, das den Grad der Wechselwirkung der Münze mit dem Feld angibt, und einer Einrichtung (50; 450, 455) zur Bestimmung, ob das Signal dem für eine annehmbare Münze entspricht, wobei die Einrichtung, die die Münze einem Elektromagnetfeld unterwirft, einen Oszillator mit einem Induktor (147; 249) umfaßt, der neben der Münzlaufbahn angeordnet ist und das Elektromagnetfeld in der Münzlaufbahn erzeugt, und wobei die Schwingfrequenz des Oszillators eine Funktion der effektiven Induktivität des Induktors ist, dadurch gekennzeichnet, daß der Oszillator ein RL-Kippgenerator (140; 240) ist.

2. Apparat nach Anspruch 1, dadurch gekennzeichnet, daß die Einrichtung (50; 450, 455) zur Bestimmung, ob ein Signal dem für eine annehmbare Münze entspricht, eine Zählereinrichtung zum Zählen der Schwingungen des Oszillator-Ausgangssignal aufweist.

3. Apparat nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß der RL-Kippgenerator (140; 240) in einem zum Prüfen von Münzen geeigneten Induktivitätsbereich einen im wesentlichen linearen Frequenzgang bezüglich der effektiven Induktivität des Oszillators aufweist und ein Ausgangssignal erzeugt, das digitaler Natur ist und sich ohne Amplitudendiskriminierung oder Impulsformierung zur Zählung eignet.

4. Apparat nach Anspruch 1, dadurch gekennzeichnet, daß der RL-Kippgenerator (140; 240) ferner einen mit dem Induktor verbundenen variablen Widerstand (145; 245) umfaßt.

5. Apparat nach Anspruch 1, dadurch gekennzeichnet, daß der RL-Kippgenerator (140; 240) ferner einen Kondensator (152; 252) umfaßt, der so geschaltet ist, daß er höhere Schwingungsmoden aufgrund von Streukapazitäten in dem RL-Kippgenerator eliminiert.

6. Apparat nach einem der vorhergehenden Ansprüche, dadurch gekennzeichnet, daß der Induktor eine einzelne Spule (147) umfaßt und die normale Schwingfrequenz des Oszillators (140) bei Anwesenheit einer Münze etwa 300 kHz beträgt.

7. Apparat nach einem der vorhergehenden Ansprüche, dadurch gekennzeichnet, daß die Münzlaufbahn zwei Seitenwände aufweist, der Induktor zwei in Serie geschaltete Spulen (247a, 247b) umfaßt, die Spulen einander gegenüber an den Seitenwänden der Münzlaufbahn montiert sind und die normale Schwingfrequenz des RL-Kippgenerators (240) bei Abwesenheit einer Münze etwa 850 kHz beträgt.

8. Apparat nach einem der vorhergehenden Ansprüche, dadurch gekennzeichnet, daß die Einrichtung (40; 440, 445) zur Erzeugung eines Signals, das den Grad der Wechselwirkung der Münze mit dem Elektromagnetfeld angibt, eine Einrichtung, die auf die Frequenz des RL-Kippgenerators (140; 240) anspricht, wenn die Münze vorbeiläuft, sowie eine Einrichtung zur Erzeugung eines die Oszillatorfrequenz angegebenden Signals umfaßt.

9. Apparat nach einem der Ansprüche 1, 4 und 5, gekennzeichnet durch zwei getrennte Oszillatoren (140, 240), deren Induktoren (147, 247) neben der Münzlaufbahn angeordnet sind, um die Münze zwei Feldern zu unterwerfen, wobei jeder RL-Kippgenerator innerhalb eines zum Prüfen von Münzen geeigneten Induktivitätsbereichs einen linearen Frequenzgang bezüglich der effektiven Induktivität in dem Oszillator aufweist und ein Ausgangssignal erzeugt, das digitaler Natur ist und sich ohne Amplitudendiskriminierung oder Impulsformierung zum Zählen eignet, sowie eine Einrichtung zur Bestimmung, ob die Ausgangssignale der beiden Oszillatoren denjenigen für eine annehmbare Münze entsprechen.

Revendications

1. Appareil de vérification de pièces de monnaie comportant des moyens (35, 37; 435, 437, 439) pour soumettre une pièce de monnaie qui se trouve dans un passage (35; 435) pour pièce de monnaie à un champ électromagnétique, des moyens (40; 440, 445) pour produire un signal indicatif du degré d'interaction entre la pièce de monnaie et le champ et des moyens (50; 450, 455) pour déterminer si ledit signal correspond ou non à celui d'une pièce de monnaie acceptable, étant précisé que les moyens pour soumettre une pièce de monnaie à un champ électromagnétique comprennent un oscillateur qui inclut une bobine d'induction (147; 247) voisine du passage de la pièce de monnaie qui produit le champ électromagnétique dans le passage de la pièce de monnaie, la fréquence d'oscillation de l'oscillateur étant fonction de l'inductance efficace de la bobine d'induction, caractérisé en ce que l'oscillateur est un oscillateur à relaxation du type résistance-inductance (140; 240).

2. Appareil selon la revendication 1, caractérisé



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en ce que les moyens (50; 450, 455) pour déterminer si un signal correspond ou non à celui d'une pièce de monnaie acceptable incluent des moyens de comptage pour compter les oscillations du signal de sortie de l'oscillateur.

3. Appareil de vérification de pièces de monnaie selon la revendication 1 ou la revendication 2, caractérisé en ce que ledit oscillateur à relaxation du type à résistance-inductance (140; 240) présente un changement de fréquence sensiblement linéaire par rapport à un changement dans l'inductance efficace de l'oscillateur sur une plage d'inductance convenant pour vérifier des pièces de monnaie et produit un signal de sortie qui est de nature numérique et ne demande ni discrimination de l'amplitude, ni mise en forme pour convenir pour le comptage.

4. Appareil selon la revendication 1, caractérisé en ce que l'oscillateur à relaxation du type à résistance et à inductance (140; 240) comporte en outre une résistance variable (145; 245) connectée à la bobine d'induction.

5. Appareil selon la revendication 1, caractérisé en ce que l'oscillateur à relaxation du type à résistance-inductance (140; 240) comporte en outre un condensateur (152; 252) connecté pour éliminer les modes plus élevés d'oscillation dus à une capacité parasite dans l'oscillateur à relaxation du type résistance-inductance.

6. Appareil selon l'une quelconque des revendications précédentes, caractérisé en ce que la bobine d'induction comporte une bobine simple (147); et en ce que la fréquence normale d'oscillation de l'oscillateur (140) en l'absence d'une pièce de monnaie est environ 300 kHz.

7. Appareil selon l'une quelconque des revendications précédentes, caractérisé en ce que le passage de la pièce de monnaie présente deux

parois latérales; en ce que l'inductance comporte deux bobines (247a, 247b) qui sont connectées en série, les bobines étant montées en face l'une de l'autre sur les parois latérales du passage de la pièce de monnaie; et en ce que la fréquence normale d'oscillation de l'oscillateur à relaxation du type à résistance-inductance (240) en l'absence d'une pièce de monnaie est environ de 850 kHz.

8. Appareil selon l'une quelconque des revendications précédentes, caractérisé en ce que les moyens (40; 440, 445) pour produire un signal indicatif du degré d'interaction entre la pièce de monnaie et le champ électromagnétique comportent des moyens sensibles à la fréquence de l'oscillateur à relaxation du type à résistance-inductance (140; 240) lorsque la pièce de monnaie passe et des moyens pour produire un signal indicatif de la fréquence de l'oscillateur.

9. Appareil selon l'une quelconque des revendications 1, 4 ou 5, caractérisé par deux tels oscillations distincts (140, 240) ayant leurs bobines d'induction (147, 147) voisines du passage de la pièce de monnaie pour soumettre la pièce de monnaie à deux champs, chaque oscillateur à relaxation du type résistance-inductance présentant une réponse en fréquence linéaire par rapport aux changements de l'inductance efficace dans l'oscillateur sur une plage d'inductance convenant pour vérifier les pièces de monnaie et produire un signal de sortie qui est de nature numérique et ne demande ni discrimination de l'amplitude, ni mise en forme pour convenir pour le comptage, ainsi que par des moyens pour déterminer si les signaux de sortie des deux oscillateurs correspondent à ceux d'une pièce de monnaie acceptable.

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