

Lens element

TECHNICAL FIELD

5 The invention relates to a lens element intended to be worn in front of an eye of a person to suppress or reduce progression of abnormal refractions of the eye such as myopia or hyperopia.

BACKGROUND OF THE INVENTION

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Myopia of an eye is characterized by the fact that the eye focuses distant objects in front of its retina. Myopia is usually corrected using a concave lens and hyperopia is usually corrected using a convex lens.

15 It has been observed that some individuals when corrected using conventional single vision optical lenses, in particular children, focus inaccurately when they observe an object which is situated at a short distance away, that is to say, in near vision conditions. Because of this focusing defect on the part of a myopic child which is corrected for his far vision, the image of an object close by is also formed behind his retina, even in the foveal area.

20 Such focusing defect may have an impact on the progression of myopia of such individuals. One may observe that for most of said individual the myopia defect tends to increase over time.

25 Foveal vision corresponds to viewing conditions for which the image of an object looked at is formed by the eye in the central zone of the retina, called the foveal zone.

Peripheral vision corresponds to the perception of elements of a scene that are offset laterally relative to the object looked at, the images of said elements being formed on the peripheral portion of the retina, away from the foveal zone.

30 The ophthalmic correction with which an ametropic subject is provided is usually adapted for his foveal vision. However, as is known, the correction has to be reduced for the peripheral vision relative to the correction that is determined for the foveal vision. In particular, studies carried out on monkeys have shown that strong

defocusing of the light behind the retina, which occurs away from the foveal zone, may cause the eye to elongate and therefore may cause a myopia defect to increase.

Therefore, it appears that there is a need for a lens element that would suppress or at least slow down progression of abnormal refractions of the eye such as
5 myopia or hyperopia.

SUMMARY OF THE INVENTION

To this end, the invention proposes a lens element intended to be worn in
10 front of an eye of a wearer comprising:

- a refraction area having a refractive power based on a prescription for said eye of the wearer; and
- a plurality of at least two contiguous optical elements, at least one optical element having an optical function of not focusing an image on the retina of the eye
15 of the wearer so as to slow down the progression of the abnormal refraction of the eye.

Advantageously, having optical elements that are configured to not focus an image on the retina of the wearer reduce the natural tendency of the retina of the eye
20 to deform, in particular to extend. Therefore, the progression of the abnormal refraction of the eye is slow down.

Furthermore, having contiguous optical elements helps improving the aestheticism of the lens element in particular limiting the discontinuity degree of the lens element surface.

25 Having contiguous optical elements also makes the manufacturing to the lens element easier.

According to further embodiments which can be considered alone or in combination:

- 30 - the at least the two contiguous optical elements are independent; and/or
- the optical elements have a contour shape being inscribable in a circle having a diameter greater than or equal to 0.8 mm and smaller than or equal to 3.0 mm; and/or

- the optical elements are positioned on a network; and/or
 - the network is a structured network; and/or
 - the optical elements are positioned along a plurality of concentric rings; and/or
- 5 - the lens element further comprises at least four optical elements organized in at least two groups of contiguous optical elements; and/or
- each group of contiguous optical element is organized in at least two concentric rings having the same center, the concentric ring of each group of contiguous optical element being defined by an inner diameter corresponding to the
- 10 smallest circle that is tangent to at least one optical element of said group and an outer diameter corresponding to the largest circle that is tangent to at least one optical elements of said group; and/or
- at least part of, for example all the concentric rings of optical elements are centered on the optical center of the surface of the lens element on which said optical
- 15 elements are disposed; and/or
- the concentric rings of optical elements have a diameter comprised between 9.0 mm and 60 mm; and/or
 - the distance between two successive concentric rings of optical elements is greater than or equal to 5.0 mm, the distance between two successive concentric
- 20 rings being defined by the difference between the inner diameter of a first concentric ring and the outer diameter of a second concentric ring, the second concentric ring being closer to the periphery of the lens element; and/or
- the optical element further comprises optical elements positioned radially between two concentric rings; and/or
- 25 - the structured network is a squared network or a hexagonal network or a triangle network or an octagonal network; and/or
- the network structure is a random network, for example a Voronoid network; and/or
 - at least part, for example all, of the optical elements have a constant optical
- 30 power and a discontinuous first derivative between two contiguous optical elements; and/or

- at least part, for example all, of the optical elements have a varying optical power and a continuous first derivative between two contiguous optical elements; and/or
- at least one, for example all, of the optical element has an optical function of
5 focusing an image on a position other than the retina in standard wearing conditions and for peripheral vision; and/or
- at least one optical element has a non-spherical focused optical function in standard wearing conditions and for peripheral vision; and/or
- at least one of the optical elements has a cylindrical power is a toric
10 refractive micro-lens; and/or
- the optical elements are configured so that along at least one section of the lens the mean sphere of optical elements increases from a point of said section towards the peripheral part of said section; and/or
- the optical elements are configured so that along at least one section of the
15 lens the cylinder of optical elements increases from a point of said section towards the peripheral part of said section; and/or
- the optical elements are configured so that along the at least one section of the lens the mean sphere and/or the cylinder of optical elements increases from the center of said section towards the peripheral part of said section; and/or
- 20 - the refraction area comprises an optical center and the optical elements are configured so that along any section passing through the optical center of the lens the mean sphere and/or the cylinder of the optical elements increases from the optical center towards the peripheral part of the lens; and/or
- the refraction area comprises a far vision reference point, a near vision
25 reference, and a meridian joining the far and near vision reference points, the optical elements are configured so that in standard wearing conditions along any horizontal section of the lens the mean sphere and/or the cylinder of the optical elements increases from the intersection of said horizontal section with the meridian towards the peripheral part of the lens; and/or
- 30 - the mean sphere and/or the cylinder increase function along the sections are different depending on the position of said section along the meridian; and/or
- the mean sphere and/or the cylinder increase function along the sections are unsymmetrical; and/or

- the optical elements are configured so that in standard wearing condition the at least one section is a horizontal section; and/or
- the mean sphere and/or the cylinder of optical elements increases from a first point of said section towards the peripheral part of said section and decreases from a second point of said section towards the peripheral part of said section, the second point being closer to the peripheral part of said section than the first point; and/or
- the mean sphere and/or the cylinder increase function along the at least one section is a Gaussian function; and/or
- the mean sphere and/or the cylinder increase function along the at least one section is a Quadratic function; and/or
- the optical elements are configured so that the mean focus of the light rays passing through each optical element is at a same distance to the retina; and/or
- the refractive area is formed as the area other than the areas formed as the plurality of optical elements; and/or
- for every circular zone having a radius comprised between 2 and 4 mm comprising a geometrical center located at a distance of the framing reference that faces the pupil of the user gazing straight ahead in standard wearing conditions greater or equal to said radius + 5mm, the ratio between the sum of areas of the parts of optical elements located inside said circular zone and the area of said circular zone is comprised between 20% and 70%; and/or
- wherein at least part, for example all, of the optical elements are located on the front surface of the ophthalmic lens; and/or
- at least part, for example all, of the optical elements are located on the back surface of the ophthalmic lens; and/or
- at least part, for example all, of the optical elements are located between the front and the back surfaces of the ophthalmic lens; and/or
- at least one of the optical elements is a multifocal refractive micro-lens; and/or
- the at least one multifocal refraction micro-lens comprises a cylindrical power; and/or
- the at least one multifocal refractive micro-lens comprises an aspherical surface, with or without any rotational symmetry; and/or

- at least one of the optical elements is a toric refractive micro-lens; and/or
- the at least one multifocal refractive micro-lens comprises a toric surface; and/or
- at least one of the optical elements is made of a birefringent material; and/or
- 5 - at least one of the optical elements is a diffractive lens; and/or
- the at least one diffractive lens comprises a metasurface structure; and/or
- at least one optical elements has a shape configured so as to create a caustic in front of the retina of the eye of the person; and/or
- at least one optical element is a multifocal binary component; and/or
- 10 - at least one optical element is a pixelated lens; and/or
- at least one optical element is a π -Fresnel lens; and/or
- at least part, for example all, optical functions comprise high order optical aberrations; and/or
- the lens element comprises an ophthalmic lens bearing the refraction area and a clip-on bearing the optical elements adapted to be removably attached to the ophthalmic lens when the lens element is worn; and/or
- 15 - the refraction area is further configured to provide to the wearer in standard wearing conditions and for foveal vision a second optical power different from the first optical power; and/or
- 20 - the difference between the first optical power and the second optical power is greater than or equal to 0.5D; and/or
- at least one, for example at least 70 %, for example all optical elements are active optical element that may be activated by an optical lens controller; and/or
- the active optical element comprises a material having a variable refractive index whose value is controlled by the optical lens controller.
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BRIEF DESCRIPTION OF THE DRAWINGS

- Non-limiting embodiments of the invention will now be described with reference to
- 30 the accompanying drawing wherein:
- o figure 1 is a plan view of a lens element according to the invention;
 - o figure 2 is a general profile view of a lens element according to the invention;

- figure 3 represents an example of a Fresnel height profile;
- figure 4 represents an example of a diffractive lens radial profile;
- figure 5 illustrates a π -Fresnel lens profile;
- figures 6a to 6c illustrate a binary lens embodiment of the invention;
- 5 ○ figure 7a illustrates the astigmatism axis γ of a lens in the TABO convention;
- figure 7b illustrates the cylinder axis γ_{AX} in a convention used to characterize an aspherical surface;
- Figures 8 and 9 show, diagrammatically, optical systems of eye and
- 10 lens;
- Figures 10 to 14 illustrate different organizations of optical elements according to different embodiments of the invention; and
- Figures 15a to 16b illustrate different types of junction between optical elements according to the invention.

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Elements in the figures are illustrated for simplicity and clarity and have not necessarily been drawn to scale. For example, the dimensions of some of the elements in the figure may be exaggerated relative to other elements to help to improve the understanding of the embodiments of the present invention.

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DETAILED DESCRIPTION OF EMBODIMENTS OF THE INVENTION

The invention relates to a lens element intended to be worn in front of an eye of a wearer.

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In the reminder of the description, terms like « up », « bottom », « horizontal », « vertical », « above », « below », « front », « rear » or other words indicating relative position may be used. These terms are to be understood in the wearing conditions of the lens element.

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In the context of the present invention, the term "lens element" can refer to an uncut optical lens or a spectacle optical lens edged to fit a specific spectacle frame or an ophthalmic lens and an optical device adapted to be positioned on the ophthalmic lens. The optical device may be positioned on the front or back surface of the ophthalmic lens. The optical device may be an optical patch. The optical device may

be adapted to be removably positioned on the ophthalmic lens for example a clip configured to be clipped on a spectacle frame comprising the ophthalmic lens.

A lens element 10 according to the invention is adapted for a wearer and intended to be worn in front of an eye of said wearer.

5 As represented on figure 1, a lens element 10 according to the invention comprises:

- a refraction area 12, and
- a plurality of contiguous optical elements 14.

10 The refraction area 12 is configured to provide to the wearer in standard wearing conditions, in particular for foveal vision, a first optical power based on the prescription of the wearer for correcting an abnormal refraction of said eye of the wearer.

The wearing conditions are to be understood as the position of the lens
15 element with relation to the eye of a wearer, for example defined by a pantoscopic angle, a Cornea to lens distance, a Pupil-cornea distance, a centre of rotation of the eye (CRE) to pupil distance, a CRE to lens distance and a wrap angle.

The Cornea to lens distance is the distance along the visual axis of the eye in the primary position (usually taken to be the horizontal) between the cornea and the
20 back surface of the lens; for example equal to 12mm.

The Pupil-cornea distance is the distance along the visual axis of the eye between its pupil and cornea; usually equal to 2mm.

The CRE to pupil distance is the distance along the visual axis of the eye between its center of rotation (CRE) and cornea; for example equal to 11.5mm.

25 The CRE to lens distance is the distance along the visual axis of the eye in the primary position (usually taken to be the horizontal) between the CRE of the eye and the back surface of the lens, for example equal to 25.5mm.

The pantoscopic angle is the angle in the vertical plane, at the intersection between the back surface of the lens and the visual axis of the eye in the primary
30 position (usually taken to be the horizontal), between the normal to the back surface of the lens and the visual axis of the eye in the primary position; for example equal to -8° .

The wrap angle is the angle in the horizontal plane, at the intersection between the back surface of the lens and the visual axis of the eye in the primary position (usually taken to be the horizontal), between the normal to the back surface of the lens and the visual axis of the eye in the primary position for example equal to 0°.

An example of standard wearer condition may be defined by a pantoscopic angle of -8°, a Cornea to lens distance of 12 mm, a Pupil-cornea distance of 2 mm, a CRE to pupil distance of 11.5 mm, a CRE to lens distance of 25.5 mm and a wrap angle of 0°.

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The term “prescription” is to be understood to mean a set of optical characteristics of optical power, of astigmatism, of prismatic deviation, determined by an ophthalmologist or optometrist in order to correct the vision defects of the eye, for example by means of a lens positioned in front of his eye. For example, the prescription for a myopic eye comprises the values of optical power and of astigmatism with an axis for the distance vision.

Although the invention is not directed to progressive lenses, the wording used in this description is illustrated in figures 1 to 10 of document WO2016/146590 for a progressive lens. The skilled person can adapt the definitions for single vision lenses.

A progressive lens comprises at least one but preferably two non-rotationally symmetrical aspheric surfaces, for instance but not limited to, progressive surface, regressive surface, toric or atoric surfaces.

As is known, a minimum curvature CURVmin is defined at any point on an aspherical surface by the formula:

$$CURV_{\min} = \frac{1}{R_{\max}}$$

where Rmax is the local maximum radius of curvature, expressed in meters and CURVmin is expressed in dioptries.

Similarly, a maximum curvature CURVmax can be defined at any point on an aspheric surface by the formula:

$$CURV_{\max} = \frac{1}{R_{\min}}$$

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where Rmin is the local minimum radius of curvature, expressed in meters and CURVmax is expressed in dioptries.

It can be noticed that when the surface is locally spherical, the local minimum radius of curvature Rmin and the local maximum radius of curvature Rmax are the same and, accordingly, the minimum and maximum curvatures CURVmin and CURVmax are also identical. When the surface is aspherical, the local minimum radius of curvature Rmin and the local maximum radius of curvature Rmax are different.

From these expressions of the minimum and maximum curvatures CURVmin and CURVmax, the minimum and maximum spheres labelled SPHmin and SPHmax can be deduced according to the kind of surface considered.

When the surface considered is the object side surface (also referred to as the front surface), the expressions are the following:

$$SPH_{\min} = (n-1) * CURV_{\min} = \frac{n-1}{R_{\max}}, \text{ and } SPH_{\min} = (n-1) * CURV_{\min} = \frac{n-1}{R_{\max}}$$

where n is the index of the constituent material of the lens.

If the surface considered is an eyeball side surface (also referred to as the back surface), the expressions are the following:

$$SPH_{\min} = (1-n) * CURV_{\min} = \frac{1-n}{R_{\max}} \text{ and } SPH_{\max} = (1-n) * CURV_{\max} = \frac{1-n}{R_{\min}}$$

where n is the index of the constituent material of the lens.

As is well known, a mean sphere SPHmean at any point on an aspherical surface can also be defined by the formula:

$$SPH_{\text{mean}} = \frac{1}{2} (SPH_{\min} + SPH_{\max})$$

The expression of the mean sphere therefore depends on the surface considered:

$$SPH_{\text{mean}} = \frac{n-1}{2} \left(\frac{1}{R_{\min}} + \frac{1}{R_{\max}} \right)$$

if the surface is the object side surface,

$$SPH_{\text{mean}} = \frac{1-n}{2} \left(\frac{1}{R_{\min}} + \frac{1}{R_{\max}} \right)$$

if the surface is an eyeball side surface,

a cylinder CYL is also defined by the formula $CYL = |SPH_{\max} - SPH_{\min}|$.

The characteristics of any aspherical face of the lens may be expressed by the local mean spheres and cylinders. A surface can be considered as locally non-spherical when the cylinder is at least 0.25 diopters.

For an aspherical surface, a local cylinder axis γ_{AX} may further be defined.

5 Figure 7a illustrates the astigmatism axis γ as defined in the TABO convention and figure 7b illustrates the cylinder axis γ_{AX} in a convention defined to characterize an aspherical surface.

The cylinder axis γ_{AX} is the angle of the orientation of the maximum curvature $CURV_{max}$ with relation to a reference axis and in the chosen sense of rotation. In the above defined convention, the reference axis is horizontal (the angle of this reference axis is 0°) and the sense of rotation is counter clockwise for each eye, when looking at the wearer ($0^\circ \leq \gamma_{AX} \leq 180^\circ$). An axis value for the cylinder axis γ_{AX} of $+45^\circ$ therefore represents an axis oriented obliquely, which when looking at the wearer, extends from the quadrant located up on the right to the quadrant located
10 down on the left.

Moreover, a progressive multifocal lens may also be defined by optical characteristics, taking into consideration the situation of the person wearing the lenses.

Figures 8 and 9 are diagrammatic illustrations of optical systems of eye and lens, thus showing the definitions used in the description. More precisely, figure 8 represents a perspective view of such a system illustrating parameters α and β used to define a gaze direction. Figure 9 is a view in the vertical plane parallel to the antero-posterior axis of the wearer's head and passing through the center of rotation of the eye in the case when the parameter β is equal to 0.
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25 The center of rotation of the eye is labelled Q' . The axis $Q'F'$, shown on Figure 9 in a dot-dash line, is the horizontal axis passing through the center of rotation of the eye and extending in front of the wearer – that is the axis $Q'F'$ corresponding to the primary gaze view. This axis cuts the aspherical surface of the lens on a point called the fitting cross, which is present on lenses to enable the positioning of lenses in a frame by an optician. The point of intersection of the rear surface of the lens and the axis $Q'F'$ is the point O. O can be the fitting cross if it is located on the rear surface. An apex sphere, of center Q' , and of radius q' , is tangential to the rear surface of the lens in a point of the horizontal axis. As
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examples, a value of radius q' of 25.5 mm corresponds to a usual value and provides satisfying results when wearing the lenses.

A given gaze direction – represented by a solid line on figure 8 - corresponds to a position of the eye in rotation around Q' and to a point J of the apex sphere; the angle β is the angle formed between the axis $Q'F'$ and the projection of the straight line $Q'J$ on the horizontal plane comprising the axis $Q'F'$; this angle appears on the scheme on Figure 3. The angle α is the angle formed between the axis $Q'J$ and the projection of the straight line $Q'J$ on the horizontal plane comprising the axis $Q'F'$; this angle appears on the scheme on Figures 8 and 9. A given gaze view thus corresponds to a point J of the apex sphere or to a couple (α, β) . The more the value of the lowering gaze angle is positive, the more the gaze is lowering and the more the value is negative, the more the gaze is rising.

In a given gaze direction, the image of a point M in the object space, located at a given object distance, is formed between two points S and T corresponding to minimum and maximum distances JS and JT, which would be the sagittal and tangential local focal lengths. The image of a point in the object space at infinity is formed, at the point F' . The distance D corresponds to the rear frontal plane of the lens.

Ergorama is a function associating to each gaze direction the usual distance of an object point. Typically, in far vision following the primary gaze direction, the object point is at infinity. In near vision, following a gaze direction essentially corresponding to an angle α of the order of 35° and to an angle β of the order of 5° in absolute value toward the nasal side, the object distance is of the order of 30 to 50 cm. For more details concerning a possible definition of an ergorama, US patent US-A-6,318,859 may be considered. This document describes an ergorama, its definition and its modelling method. For a method of the invention, points may be at infinity or not. Ergorama may be a function of the wearer's ametropia or wearer's addition.

Using these elements, it is possible to define a wearer optical power and astigmatism, in each gaze direction. An object point M at an object distance given by the ergorama is considered for a gaze direction (α, β) . An object proximity ProxO is defined for the point M on the corresponding light ray in the object space as the inverse of the distance MJ between point M and point J of the apex sphere:

$$\text{ProxO} = 1/MJ$$

This enables to calculate the object proximity within a thin lens approximation for all points of the apex sphere, which is used for the determination of the ergorama. For a real lens, the object proximity can be considered as the inverse of the distance between the object point and the front surface of the lens, on the corresponding light ray.

For the same gaze direction (α, β) , the image of a point M having a given object proximity is formed between two points S and T which correspond respectively to minimal and maximal focal distances (which would be sagittal and tangential focal distances). The quantity ProxI is called image proximity of the point M:

$$\text{ProxI} = \frac{1}{2} \left(\frac{1}{JT} + \frac{1}{JS} \right)$$

By analogy with the case of a thin lens, it can therefore be defined, for a given gaze direction and for a given object proximity, i.e. for a point of the object space on the corresponding light ray, an optical power Pui as the sum of the image proximity and the object proximity.

$$Pui = \text{ProxO} + \text{ProxI}$$

With the same notations, an astigmatism Ast is defined for every gaze direction and for a given object proximity as :

$$\text{Ast} = \left| \frac{1}{JT} - \frac{1}{JS} \right|$$

This definition corresponds to the astigmatism of a ray beam created by the lens. It can be noticed that the definition gives, in the primary gaze direction, the classical value of astigmatism. The astigmatism angle, usually called axis, is the angle γ . The angle γ is measured in the frame $\{Q', x_m, y_m, z_m\}$ linked to the eye. It corresponds to the angle with which the image S or T is formed depending on the convention used with relation to the direction z_m in the plane $\{Q', z_m, y_m\}$.

Possible definitions of the optical power and the astigmatism of the lens, in the wearing conditions, can thus be calculated as explained in the article by B. Bourdoncle et al., entitled "Ray tracing through progressive ophthalmic lenses", 1990 International Lens Design Conference, D.T. Moore ed., Proc. Soc. Photo. Opt. Instrum. Eng.

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The refractive area 12 may further be configured to provide to the wearer, in particular for foveal vision, a second optical power different from the first optical power based on the prescription of the wearer.

In the sense of the invention, the two optical powers are considered different
5 when the difference between the two optical powers is greater than or equal to 0.5 D.

When the abnormal refraction of the eye of the person corresponds to myopia the second optical power is greater than the first optical power.

When the abnormal refraction of the eye of the person corresponds to hyperopia, the second optical power is smaller than the first optical power.

10 The refractive area is preferably formed as the area other than the areas formed as the plurality of optical elements. In other words, the refractive area is the complementary area to the areas formed by the plurality of optical elements.

The refractive area may have a continuous variation of optical power. For
15 example, the optical area may have a progressive addition design.

The optical design of the refraction area may comprise

- a fitting cross where the optical power is negative,
- a first zone extending in the temporal side of the refractive area when
the lens element is being worn by a wearer. In the first zone, the optical
20 power increases when moving towards the temporal side, and over the nasal side of the lens, the optical power of the ophthalmic lens is substantially the same as at the fitting cross.

Such optical design is disclosed in greater details in WO2016/107919.

Alternatively, the optical power in the refractive area may comprise at least
25 one discontinuity.

As represented on figure 1, the lens element may be divided in five complementary zones, a central zone 16 having an optical power equal to the first refractive power and four quadrants Q1, Q2, Q3, Q4 at 45°, at least one of the
30 quadrant having at least a point where the optical power is equal to the second optical power.

In the sense of the invention the “quadrants at 45°” are to be understood as equal angular quadrant of 90° oriented in the directions 45°/225° and 135°/315° according to the TABO convention as illustrated on figure 1.

Preferably, the central zone 16 comprises a framing reference point that faces
5 the pupil of the wearer gazing straight ahead in standard wearing conditions and has a diameter greater than or equal to 4 mm and smaller than or equal to 22 mm.

According to an embodiment of the invention at least the lower part quadrant Q4 has a second optical power for central vision different from the first optical
10 power corresponding to the prescription for correcting the abnormal refraction.

For example, the refractive area has a progressive addition dioptric function. The progressive addition dioptric function may extend between the upper part quadrant Q2 and the lower part quadrant Q4.

Advantageously, such configuration allows compensation of accommodative
15 lag when the person looks for example at near vision distances thanks to the addition of the lens.

According to an embodiment, at least one of the temporal Q3 and nasal Q1 quadrant has a second optical power. For example, the temporal Q3 quadrant has a variation of power with the eccentricity of the lens.

Advantageously, such configuration increases the efficiency of the abnormal
20 refraction control in peripheral vision with even more effect in horizontal axis.

According to an embodiment, the four quadrants Q1, Q2, Q3 and Q4 have a concentric power progression.

As illustrated on figure 1, the plurality of optical elements 14 comprises at
25 least two optical elements that are contiguous.

In the sense of the invention, two optical elements located on a surface of the lens element are contiguous if there is a path supported by said surface that links the two optical elements and if along said path one does not reach the basis surface on
30 which the optical elements are located.

When the surface on which the at least two optical elements are located is spherical, the basis surface corresponds to said spherical surface. In other words, two optical elements located on a spherical surface are contiguous if there is a path

supported by said spherical surface and linking them and if along said path one may not reach the spherical surface.

When the surface on which the at least two optical elements are located is non-spherical, the basis surface corresponds to the local spherical surface that best fit said non-spherical surface. In other words, two optical elements located on a non-spherical surface are contiguous if there is a path supported by said non-spherical surface and linking them and if along said path one may not reach the spherical surface that best fit the non-spherical surface.

Advantageously, having contiguous optical elements helps improving the aesthetic of the lens element and is easier to manufacture.

At least one, preferably all of the, optical element of the plurality of optical elements 14, has an optical function of not focusing an image on the retina of the eye of the wearer, in particular for peripheral vision and preferably for central and peripheral vision.

In the sense of the invention "focusing" is to be understood as producing a focusing spot with a circular section that can be reduced to a point in the focal plane.

Advantageously, such optical function of the optical element reduces the deformation of the retina of the eye of the wearer in peripheral vision, allowing to slow down the progression of the abnormal refraction of the eye of the person wearing the lens element.

According to a preferred embodiment of the invention, the at least two contiguous optical elements are independent.

In the sense of the invention, two optical elements are considered as independent if producing independent images.

In particular, when illuminated by a parallel beam "in central vision", each "independent contiguous optical element" forms on a plane in the image space a spot associated with it. In other words, when one of the "optical element" is hidden, the spot disappears even if this optical element is contiguous with another optical element.

For the classic Fresnel ring (carrying a single power) as disclosed in US7976158, said Fresnel ring produces a single spot whose position is not changed if one conceals a small part of the ring. The Fresnel ring cannot therefore be considered as a succession of "independent contiguous optical element".

According to an embodiment of the invention, the optical elements have specific sizes. In particular, the optical elements have a contour shape being inscribable in a circle having a diameter greater than or equal to 0.8 mm and smaller than or equal to 3.0 mm, preferably greater than or equal to 1.0 mm and smaller than
5 2.0 mm.

According to embodiments of the invention, the optical elements are positioned on a network.

The network on which the optical elements are positioned may be a structured
10 network as illustrated on figures 1 and 10 to 13.

In the embodiments illustrated on figures 1 and 10 to 12 the optical elements are positioned along a plurality of concentric rings.

The concentric rings of optical elements may be annular rings.

According to an embodiment of the invention, the lens element further
15 comprises at least four optical elements. The at least four optical elements are organized in at least two groups of contiguous optical elements, each group of contiguous optical element being organized in at least two concentric rings having the same center, the concentric ring of each group of contiguous optical element being defined by an inner diameter and an outer diameter.

20 The inner diameter of a concentric ring of each group of optical elements corresponds to the smallest circle that is tangent to at least one optical element of said group of optical elements. The outer diameter of a concentric ring of optical element corresponds to the largest circle that is tangent to at least one optical element of said group.

25 For example, the lens element may comprise n rings of optical elements, $f_{inner\ 1}$ referring to the inner diameter of the concentric ring which is the closest to the optical center of the lens element, $f_{outer\ 1}$ referring to the outer diameter of the concentric ring which is the closest to the optical center of the lens element, $f_{inner\ n}$ referring to the inner diameter of the ring which is the closest to the periphery of the
30 lens element, and $f_{outer\ n}$ referring to the outer diameter of the concentric ring which is the closest to the periphery of the lens element.

The distance D_i between two successive concentric rings of optical elements i and $i+1$ may be expressed as:

$$D_i = |f_{inner\ i+1} - f_{outer\ i}|,$$

wherein $f_{outer\ i}$ refers to the outer diameter of a first ring of optical elements i and $f_{inner\ i+1}$ refers to the inner diameter of a second ring of optical elements $i+1$ that is successive to the first one and closer to the periphery of the lens element.

According to another embodiment of the invention, the optical elements are organized in concentric rings centered on the optical center of the surface of the lens element on which the optical elements are disposed and linking the geometrical center of each optical element.

For example, the lens element may comprise n rings of optical elements, f_1 referring to the diameter of the ring which is the closest to the optical center of the lens element and f_n referring to the diameter of the ring which is the closest to the periphery of the lens element.

The distance D_i between two successive concentric rings of optical elements i and $i+1$ may be expressed as:

$$D_i = \left| f_{i+1} - f_i - \frac{d_{i+1}}{2} - \frac{d_i}{2} \right|,$$

wherein f_i refers to the diameter of a first ring of optical elements i and f_{i+1} refers to the diameter of a second ring of optical elements $i+1$ that is successive to the first one and closer to the periphery of the lens element, and

wherein d_i refers to the diameter of the optical elements on the first ring of optical elements and d_{i+1} refers to the diameter of the optical elements on the second ring of optical elements that is successive to the first ring and closer to the periphery of the lens element. The diameter of the optical element corresponds to the diameter of the circle in which the contour shape of the optical element is inscribed.

Advantageously, the optical center of the lens element and the center of the concentric rings of optical elements coincide. For example, the geometrical center of the lens element, the optical center of the lens element, and the center of the concentric rings of optical elements coincide.

In the sense of the invention, the term coincide should be understood as being really close together, for example distanced by less than 1.0 mm.

The distance D_i between two successive concentric rings may vary according to i . For example, the distance D_i between two successive concentric rings may vary
5 between 2.0 mm and 5.0 mm.

According to an embodiment of the invention, the distance D_i between two successive concentric rings of optical elements is greater than 2.00 mm, preferably 3.0 mm, more preferably 5.0 mm.

Advantageously, having the distance D_i between two successive concentric
10 rings of optical elements greater than 2.00 mm allows managing a larger refraction area between these rings of optical elements and thus provides better visual acuity.

Considering an annular zone of the lens element having an inner diameter greater than 9 mm and an outer diameter smaller than 57 mm, having a geometrical center located at a distance of the optical center of the lens element smaller than
15 1mm, the ratio between the sum of areas of the parts of optical elements located inside said circular zone and the area of said circular zone is comprised between 20% and 70%, preferably between 30% and 60%, and more preferably between 40% and 50%.

In other words, the inventors have observed that for a given value of the
20 abovementioned ratio, the organization of contiguous optical elements in concentric rings, where these rings are spaced by a distance greater than 2.0 mm, allows providing annular zones of refractive area easier to manufacture than the refractive area managed when optical element are disposed in hexagonal network or randomly disposed on the surface of the lens element. thereby provide a better correction of the
25 abnormal refraction of the eye and thus a better visual acuity.

According to an embodiment of the invention, the diameter d_i of all optical elements of the lens element are identical.

According to an embodiment of the invention, the distance D_i between two successive concentric rings i and $i+1$ may increase when i increases towards the
30 periphery of the lens element.

The concentric rings of optical elements may have a diameter comprised between 9 mm and 60 mm.

According to an embodiment of the invention, the lens element comprises optical elements disposed in at least 2 concentric rings, preferably more than 5, more preferably more than 10 concentric rings. For example, the optical elements may be disposed in 11 concentric rings centered on the optical center of the lens.

5 On figure 1, the optical elements are micro-lenses positioned along a set of 5 concentric rings. The optical power and/or cylinder of the micro-lenses may be different depending on their position along the concentric rings.

On figure 10, the optical elements correspond to different sectors of concentric circles.

10 On figures 11b, the optical elements correspond to part of pure cylindrical concentric rings as illustrated on figure 11a. In this example, the optical elements have constant power but a variable cylindrical axis.

According to an embodiment of the invention, for example illustrated on figure 12, the lens element may further comprise optical elements 14 positioned
15 radially between two concentric rings. In the example illustrated on figure 12, only 4 optical elements are placed between two concentric rings, however, more optical elements may be positioned between both rings.

The optical elements may be placed on a structured network that is a squared network or a hexagonal network or a triangle network or an octagonal network.

20 Such embodiment of the invention is illustrated on figure 13 where the optical elements 14 are placed on a squared network.

Alternatively, the optical elements may be placed on a random structure network such as a Voronoid network as illustrated on figure 14.

Advantageously, having the optical elements placed on a random structure
25 limits the risk of light scattering or diffraction.

Different junctions between two contiguous optical elements are possible.

For example, as illustrated on figures 15a and 15b, at least part, for example all of the optical elements have a constant optical power and a discontinuous first derivative between two contiguous optical elements. In the examples illustrated on
30 figures 15a and 15b, θ is the angular coordinate in polar reference. As one can observe in this embodiment, there is no area between the contiguous optical elements with no sphere.

Alternatively, as illustrated on figures 16a and 16b, at least part, for example all, of the optical elements have a varying optical power and a continuous first derivative between two contiguous optical elements.

To obtain such variation, here one may use two constant powers, one positive
5 and one negative. The area of the negative power is much smaller than the area of the positive power, so that globally one has a positive power effect.

An important point in this embodiment illustrated on figures 16a and 16b is that the Z coordinate is always positive compared to the refraction area.

10 As illustrated on figure 2, a lens element 10 according to the invention comprises an object side surface F1 formed as a convex curved surface toward an object side, and an eye side surface F2 formed as a concave surface having a different curvature than the curvature of the object side surface F1.

According to an embodiment of the invention, at least part, for example all, of
15 the optical elements are located on the front surface of the lens element.

At least part, for example all, of the optical elements may be located on the back surface of the lens element.

At least part, for example all, of the optical elements may be located between the front and back surfaces of the lens element. For example, the lens element may
20 comprise zones of different refractive index forming the optical elements.

According to an embodiment of the invention, at least one of the optical elements has an optical function of focusing an image for peripheral vision on a position other than the retina.

25 Preferably, at least 50%, for example at least 80%, for example all, of the optical elements have an optical function of focusing an image for peripheral vision on a position other than the retina.

According to a preferred embodiment of the invention, all of the optical elements are configured so that the mean focus of the light rays passing through each
30 optical element is at a same distance to the retina of the wearer, at least for peripheral vision.

The optical function, in particular the dioptric function, of each optical element may be optimized so as to provide a focus image, in particular in peripheral

vision, at a constant distance of the retina of the eye of the wearer. Such optimization requires adapting the dioptric function of each of the optical element depending on their position on the lens element.

In particular, the inventors have determined that the spot diagram of the beam
5 of light passing through a spherical 3D shaped micro lens analyzed in peripheral vision (30° from the pupil center) is not a point.

To obtain a point, the inventors have determined that the optical element should have a cylindrical power, for example have a toric shape.

10 According to an embodiment of the invention, the optical elements are configured so that at least along one section of the lens the mean sphere of the optical elements increases from a point of said section towards the periphery of said section.

The optical elements may further be configured so that at least along one section of the lens, for example at least the same section as the one along which the
15 mean sphere of the optical elements increases, the cylinder increases from a point of said section, for example the same point as for the mean sphere, towards the peripheral part of said section.

Advantageously, having optical elements configured so that along at least one section of the lens the mean sphere and/or mean cylinder of optical elements
20 increases from a point of said section towards the peripheral part of said section allows increasing the defocus of the light rays in front the retina in case of myopia or behind the retina in case of hyperopia.

In other words, the inventors have observed that having optical elements configured so that along at least one section of the lens the mean sphere of optical
25 elements increases from a point of said section towards the peripheral part of said section helps slow down the progression of abnormal refraction of the eye such as myopia or hyperopia.

The optical elements may be configured so that that along the at least one
30 section of the lens the mean sphere and/or the cylinder of optical elements increases from the center of said section towards the peripheral part of said section.

According to an embodiment of the invention, the optical elements are configured so that in standard wearing condition the at least one section is a horizontal section.

5 The mean sphere and/or the cylinder may increase according to an increase function along the at least one horizontal section, the increase function being a Gaussian function. The Gaussian function may be different between the nasal and temporal part of the lens so as to take into account the dissymmetry of the retina of the person.

10 Alternatively, the mean sphere and/or the cylinder may increase according to an increase function along the at least one horizontal section, the increase function being a Quadratic function. The Quadratic function may be different between the nasal and temporal part of the lens so as to take into account the dissymmetry of the retina of the person.

15 According to an embodiment of the invention, the mean sphere and/or the cylinder of optical elements increases from a first point of said section towards the peripheral part of said section and decreases from a second point of said section towards the peripheral part of said section, the second point being closer to the peripheral part of said section than the first point.

20 Such embodiment is illustrated in table 1 that provides the mean sphere of optical elements according to their radial distance to the optical center of the lens element.

25 In the example of table 1, the optical elements are micro lens placed on a spherical front surface having a curvature of 329.5 mm and the lens element is made of an optical material having a refractive index of 1.591, the prescribed optical power of the wearer is of 6 D. The optical element is to be worn in standard wearing conditions and the retina of the wearer is considered as having a defocus of 0.8 D at an angle of 30°. The optical elements are determined to have a peripheral defocus of 2D.

30

Distance to optical center (mm)	Mean sphere of optical element (D)
0	1.992
5	2.467
7.5	2.806
10	3.024
15	2.998
20	2.485

Table 1

As illustrated in table 1, starting close to the optical center of the lens element, the mean sphere of the optical elements increases towards the peripheral part of said section and then decreases towards the peripheral part of said section.

According to an embodiment of the invention, the mean cylinder of optical elements increases from a first point of said section towards the peripheral part of said section and decreases from a second point of said section towards the peripheral part of said section, the second point being closer to the peripheral part of said section than the first point.

Such embodiment is illustrated in tables 2 and 3 that provides the amplitude of the cylinder vector projected on a first direction Y corresponding to the local radial direction and a second direction X orthogonal to the first direction.

In the example of table 2, the optical elements are micro-lenses placed on a spherical front surface having a curvature of 167.81 mm and the lens element is made of an optical material having a refractive index of 1.591, the prescribed optical power of the wearer is of -6 D. The optical element is to be worn in standard wearing conditions and the retina of the wearer is considered as having a defocus of 0.8 D at an angle of 30°. The optical elements are determined to have a peripheral defocus of 2D.

In the example of table 3, the optical elements are micro-lenses placed on a spherical front surface having a curvature of 167.81 mm and the lens element is made of an optical material having a refractive index of 1.591, the prescribed optical power of the wearer is of -1 D. The optical element is to be worn in standard wearing conditions and the retina of the wearer is considered as having a defocus of 0.8 D at

an angle of 30°. The optical elements are determined to have a peripheral defocus of 2D.

gazing direction (in degree)	Px (in Diopter)	Py (in Diopter)	Cylinder (in Diopter)
0	1.987	1.987	1.987
18.581	2.317	2.431	2.374
27.002	2.577	2.729	2.653
34.594	2.769	2.881	2.825
47.246	2.816	2.659	2.7375
57.02	2.446	1.948	2.197

Table 2

5

gazing direction (in degree)	Px (in Diopter)	Py (in Diopter)	Cylinder (in Diopter)
0	1.984	1.984	1.984
18.627	2.283	2.163	2.223
27.017	2.524	2.237	2.3805
34.526	2.717	2.213	2.465
46.864	2.886	1.943	2.4145
56.18	2.848	1.592	2.22

Table 3

As illustrated in tables 2 and 3, starting close to the optical center of the lens element, the cylinder of the optical elements increases towards the peripheral part of said section and then decreases towards the peripheral part of said section.

According to an embodiment of the invention, the refraction area comprises an optical center and optical elements are configured so that along any section passing through the optical center of the lens the mean sphere and/or the cylinder of the optical elements increases from the optical center towards the peripheral part of the lens.

For example, the optical elements may be regularly distributed along circles centered on the optical center of the refraction area.

The optical elements on the circle of diameter 10 mm and centered on the optical center of the refraction area may be micro lenses having a mean sphere of 2.75 D.

The optical elements on the circle of diameter 20 mm and centered on the optical center of the refraction area may be micro lenses having a mean sphere of 4.75 D.

5 The optical elements on the circle of diameter 30 mm and centered on the optical center of the refraction area may be micro lenses having a mean sphere of 5.5 D.

The optical elements on the circle of diameter 40 mm and centered on the optical center of the refraction area may be micro lenses having a mean sphere of 5.75 D.

10 The cylinder of the different micro lenses may be adjusted based on the shape of the retina of the person.

According to an embodiment of the invention, the refraction area comprises a far vision reference point, a near vision reference, and a meridian joining the far and near vision reference points. For example, the refraction area may comprise a
15 progressive additional lens design adapted to the prescription of the person or adapted to slow down the progression of the abnormal refraction of the eye of the person wearing the lens element.

Preferably, according to such embodiment, the optical elements are configured so that in standard wearing conditions along any horizontal section of the
20 lens the mean sphere and/or the cylinder of the optical elements increases from the intersection of said horizontal section with the meridian line towards the peripheral part of the lens.

The meridian line corresponds to the locus of the intersection of the main gaze direction with the surface of the lens.

25 The mean sphere and/or the cylinder increase function along the sections may be different depending on the position of said section along the meridian line.

In particular, the mean sphere and/or the cylinder increase function along the sections are unsymmetrical. For example, the mean sphere and/or the cylinder increase function are unsymmetrical along vertical and/or horizontal section in
30 standard wearing conditions.

According to an embodiment of the invention, at least one of the optical elements has a non-focused optical function in standard wearing conditions and for peripheral vision.

Preferably at least 50%, for example at least 80%, for example all, of the optical elements 14 have a non- focused optical function in standard wearing conditions and for peripheral vision.

In the sense of the invention, a “non-focused optical function” is to be understood as not having a single focus point in standard wearing conditions and for peripheral vision.

Advantageously, such optical function of the optical element reduces the deformation of the retina of the eye of the wearer, allowing to slow down the progression of the abnormal refraction of the eye of the person wearing the lens element.

The at least one optical element having a non-focused optical function is transparent.

Advantageously, the non-contiguous optical elements are not visible on the lens element and do not affect the aesthetics of the lens element.

According to an embodiment of the invention, the lens element may comprise an ophthalmic lens bearing the refraction area and a clip-on bearing the plurality of at least three optical elements adapted to be removably attached to the ophthalmic lens when the lens element is worn.

Advantageously, when the person is in a far distance environment, outside for example, the person may separate the clip-on from the ophthalmic lens and eventually substitute a second clip-on free of any of at least three optical elements. For example, the second clip-on may comprise a solar tint. The person may also use the ophthalmic lens without any additional clip-on.

The optical element may be added to the lens element independently on each surface of the lens element.

One can add these optical elements on a defined array like square or hexagonal or random or other.

The optical element may cover specific zones of the lens element, like at the center or any other area.

According to an embodiment of the invention, the central zone of the lens corresponding to a zone centered on the optical center of the lens element does not comprise any optical element. For example, the lens element may comprise an empty

zone centered on the optical center of said lens element and having a diameter equal to 9 mm which does not comprise any optical element.

The optical center of the lens element may correspond to the fitting point of the lens.

5 Alternatively, the optical elements may be disposed on the entire surface of the lens element.

The optical element density or the quantity of power may be adjusted depending on zones of the lens element. Typically, the optical element may be positioned in the periphery of the lens element, in order to increase the effect of the
10 optical element on myopia control, so as to compensate peripheral defocus due to the peripheral shape of the retina for example.

According to a preferred embodiment of the invention, every circular zone of the lens element having a radius comprised between 2 and 4 mm comprising a geometrical center located at a distance of the optical center of the lens element
15 greater or equal to said radius + 5mm, the ratio between the sum of areas of the parts of optical elements located inside said circular zone and the area of said circular zone is comprised between 20% and 70%, preferably between 30% and 60%, and more preferably between 40% and 50%.

The optical elements can be made using different technologies like direct
20 surfacing, molding, casting or injection, embossing, filming, or photolithography etc...

According to an embodiment of the invention, at least one, for example all, of the optical elements has a shape configured so as to create a caustic in front of the retina of the eye of the person. In other words, such optical element is configured so
25 that every section plane where the light flux is concentrated if any, is located in front of the retina of the eye of the person.

According to an embodiment of the invention, the at least one, for example all, of the optical element having a non-spherical optical function is a multifocal refractive microlens.

30 In the sense of the invention, a “multifocal refractive microlens” includes bifocals (with two focal powers), trifocals (with three focal powers), progressive addition lenses, with continuously varying focal power, for example aspherical progressive surface lenses.

According to an embodiment of the invention, at least one of the optical element, preferably more than 50%, more preferably more than 80% of the optical elements are aspherical microlenses. In the sense of the invention, aspherical microlenses have a continuous power evolution over their surface.

5 An aspherical microlens may have an asphericity comprised between 0.1D and 3D. The asphericity of an aspherical microlens corresponds to the ratio of optical power measured in the center of the microlens and the optical power measured in the periphery of the microlens.

10 The center of the microlens may be defined by a spherical area centered on the geometrical center of the microlens and having a diameter comprised between 0.1 mm and 0.5 mm, preferably equal to 2.0 mm.

15 The periphery of the microlens may be defined by an annular zone centered on the geometrical center of the microlens and having an inner diameter comprised between 0.5 mm and 0.7 mm and an outer diameter comprised between 0.70 mm and 0.80 mm.

According to an embodiment of the invention, the aspherical microlenses have an optical power in their geometrical center comprised between 2.0D and 7.0D in absolute value, and an optical power in their periphery comprised between 1.5D and 6.0D in absolute value.

20 The asphericity of the aspherical microlenses before the coating of the surface of the lens element on which the optical elements are disposed may vary according to the radial distance from the optical center of said lens element.

25 Additionally, the asphericity of the aspherical microlenses after the coating of the surface of the lens element on which the optical elements are disposed may further vary according to the radial distance from the optical center of said lens element.

30 According to an embodiment of the invention, the at least one multifocal refractive micro-lens has a toric surface. A toric surface is a surface of revolution that can be created by rotating a circle or arc about an axis of revolution (eventually positioned at infinity) that does not pass through its center of curvature.

Toric surface lenses have two different radial profiles at right angles to each other, therefore producing two different focal powers.

Toric and spheric surface components of toric lenses produce an astigmatic light beam, as opposed to a single point focus.

According to an embodiment of the invention, the at least one of the optical element having a non-spherical optical function, for example all, of the optical elements is a toric refractive micro-lens. For example, a toric refractive micro-lens with a sphere power value greater than or equal to 0 diopter (δ) and smaller than or equal to +5 diopters (δ), and cylinder power value greater than or equal to 0.25 Diopter (δ).

As a specific embodiment, the toric refractive microlens may be a pure cylinder, meaning that minimum meridian power is zero, while maximum meridian power is strictly positive, for instance less than 5 Diopters.

According to an embodiment of the invention, at least one, for example all, of the optical element, is made of a birefringent material. In other words, the optical element is made of a material having a refractive index that depends on the polarization and propagation direction of light. The birefringence may be quantified as the maximum difference between refractive indices exhibited by the material.

According to an embodiment of the invention, at least one, for example all of the optical element, has discontinuities, such as a discontinuous surface, for example Fresnel surfaces and/or having a refractive index profile with discontinuities.

Figure 3 represents an example of a Fresnel height profile of a optical element that may be used for the invention.

According to an embodiment of the invention, at least one, for example all of the optical element, is made of a diffractive lens.

Figure 4 represents an example of a diffractive lens radial profile of an optical element that may be used for the invention.

At least one, for example all, of the diffractive lenses may comprise a metasurface structure as disclosed in WO2017/176921.

The diffractive lens may be a Fresnel lens whose phase function $\psi(r)$ has π phase jumps at the nominal wavelength, as seen in Figure 5. One may give these structures the name “ π -Fresnel lenses” for clarity’s sake, as opposition to unifocal Fresnel lenses whose phase jumps are multiple values of 2π . The π -Fresnel lens whose phase function is displayed in Figure 5 diffracts light mainly in two diffraction orders associated to dioptric powers 0 δ and a positive one P, for example 3 δ .

According to an embodiment of the invention, at least one, for example all of the optical element, is a multifocal binary component.

For example, a binary structure, as represented in Figure 6a, displays mainly two dioptric powers, denoted $-P/2$ and $P/2$. When associated to a refractive structure as shown in Figure 6b, whose dioptric power is $P/2$, the final structure represented in Figure 6c has dioptric powers 0 δ and P . The illustrated case is associated to $P=3 \delta$.

According to an embodiment of the invention, at least one, for example all of the optical element, is a pixelated lens. An example of multifocal pixelated lens is disclosed in Eyal Ben-Eliezer et al, APPLIED OPTICS, Vol. 44, No. 14, 10 May 2005.

According to an embodiment of the invention, at least one, for example all of the optical element, has an optical function with high order optical aberrations. For example, the optical element is a micro-lens composed of continuous surfaces defined by Zernike polynomials.

According to an embodiment of the invention, at least one, for example at least 70 %, for example all optical elements are active optical element that may be activated manually or automatically by an optical lens controller device.

The active optical element may comprise a material having a variable refractive index whose value is controlled by the optical lens controller device.

The invention has been described above with the aid of embodiments without limitation of the general inventive concept.

Many further modifications and variations will be apparent to those skilled in the art upon making reference to the foregoing illustrative embodiments, which are given by way of example only and which are not intended to limit the scope of the invention, that being determined solely by the appended claims.

In the claims, the word “comprising” does not exclude other elements or steps, and the indefinite article “a” or “an” does not exclude a plurality. The mere fact that different features are recited in mutually different dependent claims does not indicate that a combination of these features cannot be advantageously used. Any reference signs in the claims should not be construed as limiting the scope of the invention.