

Description

The present invention relates to the production of a polycrystalline body, i.e. a composite ceramic, comprised of a crystalline mullite phase and a crystalline beta spodumene phase. In a preferred embodiment, the present invention relates to the production of a polycrystalline material comprised of mullite and beta spodumene useful as a substrate for silicon with a thermal expansion coefficient identical or close to that of silicon.

To minimize stress at the silicon-substrate interface of an IC device during operation, it is desired that the substrate material have a thermal expansion coefficient which matches that of silicon as closely as possible. Such a match is expected to be especially critical in projected high power semiconductor devices where heating and cooling cycles during operation of the device are expected to subject the silicon-substrate interface to more severe thermal stresses than are encountered in present devices. Present technology utilizes alpha alumina as the substrate material. However, the thermal expansion mismatch between alumina and silicon is judged to be too great for this material to be satisfactory for future applications. In addition, high speed integrated circuits require a substrate material with a low dielectric constant. For projected high speed devices, alumina is judged to have too high a dielectric constant. A replacement substrate material for alumina is then needed whose thermal expansion coefficient provides a closer match to that of silicon and whose dielectric constant is lower than that of alumina.

Mullite composite substrate materials have been investigated in the past. Leipold and Sibold, J. Amer. Ceram. Soc., 65, C147 (1982), report making a two phase mullite based ceramic with a thermal expansion coefficient close to that of silicon by preparing a silica-rich mullite composition. After firing, this resulted in a body consisting of mullite and a silica-rich glass which contained approximately 50% glass. Fiori and Vincenzini, "Colloque Internationale sur les Nouvelles Orientations des Composants Possibles", p. 203, Paris, March 29—April 1, 1982, also report making similar mullite-silica glass compositions for use as a substrate material with a thermal expansion to match that of silicon.

Mullite is a crystalline aluminum silicate phase which has the approximate chemical formula, $3\text{Al}_2\text{O}_3 \cdot 2\text{SiO}_2$. It is a potential substrate material as its thermal expansion coefficient is a reasonable match for that of silicon ($3.3 \times 10^{-6}/^\circ\text{K}$ at 300°K for mullite vs. $2.5 \times 10^{-6}/^\circ\text{K}$ at 300°K for silicon). However, as discussed above, a closer match than this is desired for substrates for projected high power devices. Therefore, according to one aspect of the present invention, the thermal expansion coefficient of mullite is lowered to match that of silicon through the addition of a second phase having a low thermal expansion coefficient. Specifically, in accordance with the present invention, beta spodumene (a lithium aluminum silicate) is added. Beta spodumene has a thermal expansion coefficient of $0.9 \times 10^{-6}/^\circ\text{K}$ between 293°K and 1273°K .

Those skilled in the art will gain a further and better understanding of the present invention from the detailed description set forth below, considered in conjunction with the figures accompanying and forming a part of the specification, in which:

Figure 1 is a photomicrograph (magnified $750\times$) showing the polished cross-section of a composite ceramic produced in accordance with the present invention comprised of about 63.0% by weight of mullite phase (lighter phase), and about 37.0% by weight of beta spodumene phase (darker colored phase).

Figure 2 is a graph showing the calculated thermal expansion coefficient of the present polycrystalline body as a function of its beta spodumene content. Specifically, in Figure 2, using the formula for the thermal expansion coefficient for a multiphase body originally derived by Turner, J. Res. NBS, 37, 239 (1946), the thermal expansion coefficient of a mullite-beta spodumene ceramic was calculated at 300°K . Figure 2 shows the results of such a calculation compared with the thermal expansion coefficient of silicon at 300°K shown as α_{Si} in Figure 2. These calculations indicate that for the present composite ceramic to match the thermal expansion of silicon, it would need to have a content of about 37 weight % beta spodumene, and

Figure 3 shows the thermal expansion of $\text{Si}(x)$ reported in the literature at the given temperatures. All of the solid lines in Figure 3 were produced by means of a dilatometer by heating the present polycrystalline body produced in Example 11 herein from about 25°C to about 500°C , cooling back down to about 50°C and then heating back up to about 500°C , i.e. it was measured between about 298°K to about 773°K . In Figure 3, the present polycrystalline body had a density of 94.9% of its theoretical density, and X-ray diffraction analysis showed it to be comprised of about 63% by weight of mullite phase and about 37% by weight of beta spodumene phase and a trace of $\alpha\text{-Al}_2\text{O}_3$. Figure 3 shows that the present polycrystalline body had a thermal expansion coefficient at temperatures ranging from about 25°C to about 500°C which matched that of Si, or which was within about 5% of that of silicon, or which was within about 10% of that of silicon.

In accordance with the present invention, a mullite-beta spodumene ceramic can be fabricated to match the thermal expansion coefficient of silicon. An advantage of the present mullite-beta spodumene ceramic over the mullite-glass ceramics is that the present ceramic has a potentially higher thermal conductivity because of the higher thermal conductivity of the crystalline ceramics over the glass.

Briefly stated, the present process for producing a polycrystalline body comprised of from 50% by weight to 95% by weight crystalline mullite and from 5% by weight to 50% by weight crystalline beta

spodumene comprises providing a mixture comprised of mullite and/or beta spodumene and/or Al_2O_3 and/or SiO_2 and/or a precursor for Li_2O , said mixture having a composition required to produce said polycrystalline body, shaping said mixture into a compact, sintering said compact at a temperature ranging from greater than 1423°C to 1500°C at which sufficient liquid phase is generated to liquid phase sinter the compact and produce a densified body having a density greater than about 85% of the theoretical density of said body, said sintering temperature having no significant deleterious effect on said body, said sintered body containing said mullite phase and a glassy phase of said beta spodumene, nucleation-annealing said sintered body at a temperature ranging from 600°C to 800°C to nucleate said glassy beta spodumene phase, crystallization-annealing the resulting nucleated body at a temperature ranging from 1200°C to below the temperature at which liquid forms in said body to produce said polycrystalline body, said sintering, said nucleation-annealing and said crystallization-annealing being carried out in an atmosphere or vacuum which has no significant deleterious effect on said compact or body.

The % density given herein for a sintered or fired body is, unless otherwise stated, the fractional density of the theoretical density of mullite and beta spodumene based on the particular amounts of mullite and beta spodumene present.

In the present invention, the composition of the mullite phase is one which can exist in thermodynamic equilibrium with a beta spodumene phase. Likewise, the composition of the beta spodumene phase is one which can exist in thermodynamic equilibrium with the mullite phase. The present polycrystalline body, therefore, is comprised of a mullite phase composed of from 71.8 weight % to 74.0 weight % Al_2O_3 balance SiO_2 , and a beta spodumene phase comprised of a lithium aluminum silicate having a nominal formula of $\text{Li}_2\text{O} \cdot \text{Al}_2\text{O}_3 \cdot 4\text{SiO}_2$ and being composed of from 58.5 weight % to 79.4 weight % silica balance lithium aluminate ($\text{Li}_2\text{O} \cdot \text{Al}_2\text{O}_3$).

In the present invention, the specific phase composition of the present polycrystalline body depends largely on its final application. In one embodiment of the present invention, the phase composition of the present polycrystalline body is tailored to match the thermal expansion coefficient of silicon at 300°K .

In carrying out the present process, there is provided a particulate mixture comprised of the components, i.e. mullite and/or beta spodumene and/or Al_2O_3 and/or SiO_2 and/or a precursor for Li_2O , and such mixture has a composition required to produce the present polycrystalline body. For example, the mixture can be comprised of powders of Al_2O_3 , SiO_2 and a precursor for Li_2O . Alternatively, for example, the mixture can be comprised of powders of prepared beta spodumene and mullite. Also, for example, the mixture can be comprised of combinations of powders of Al_2O_3 and/or SiO_2 and/or a precursor for Li_2O and/or beta spodumene and/or mullite. The particular amounts of the components used in forming the present particulate mixture is determined by the particular phase composition desired in the present polycrystalline body. In the present process, there is no significant loss of any of the reactants, i.e. Al_2O_3 , Li_2O , SiO_2 , mullite powder or beta spodumene powder forming the mullite and beta spodumene phases in the present polycrystalline body.

The precursor for Li_2O should have no significant deleterious effect in the present invention. Specifically, it should thermally decompose completely at a temperature below 900°C , and preferably below 500°C , producing Li_2O and gaseous product or products of decomposition which vaporize away before sintering of the compact is initiated. Representative of suitable precursors for Li_2O are lithium nitrate, lithium acetate and lithium hydroxide.

The components of the mixture can be of commercial or technical grade. Specifically, they should not contain any impurities which would have a significantly deleterious effect on the properties of the resulting polycrystalline body. The larger the amount of impurities in the starting materials, the greater is the amount of glassy phase in the final product.

In carrying out the present process, a uniform or at least a substantially uniform particulate mixture or dispersion of the components is formed. The present mixture can be formed by a number of conventional techniques such as, for example, ball milling or jet milling. Representative of the mixing techniques is ball milling, preferably with balls of a material such as $\alpha\text{-Al}_2\text{O}_3$ which has low wear and which has no significant detrimental effect on the properties desired in the final product. Preferably, milling is carried out in a liquid mixing medium which is inert to the ingredients. Typical liquid mixing mediums include hydrocarbons such as benzene and chlorinated hydrocarbons. The resulting wet milled material can be dried by a number of conventional techniques to remove the liquid medium. Preferably, it is dried in an oven maintained just below the boiling point of the liquid mixing medium. Spray-drying can also be used.

The present particulate mixture should have a particle size which produces the present polycrystalline body. Preferably, the present mixture has an average particle size which is submicron. Larger particle sizes, generally greater than about 5 microns, have a tendency to lower densification. In the present mixture, components other than powders of mullite and beta spodumene should be of a size which allows the present reaction to take place, i.e. formation of mullite and beta spodumene phases.

A number of techniques can be used to shape the particulate mixture into a compact. For example, the mixture can be extruded, injection molded, die-pressed, isostatically pressed, slip cast or tape cast to produce the compact of desired shape. Any lubricants, binders or similar material used in shaping the mixture should have no significant deleterious effect on the compact or the resulting polycrystalline body. Such materials are of the type which evaporate away on heating at temperatures below the present

sintering temperature, and preferably below 200°C, leaving no significant residue or any effective contaminants.

The shaped compact can be in any desired form. For example, it can be simple, hollow and/or complex in shape. Preferably, for use as a substrate, it is in the form of a tape.

5 The compact is sintered at a temperature at which sufficient liquid phase is generated to carry out the present liquid phase sintering and such sintering temperature can range from greater than about 1423°C to about 1500°C. The sintering temperature should have no significantly deleterious effect on the compact or body, i.e., the sintering temperature should not generate so much liquid phase as to slump the compact or body. Specifically, the particular sintering temperature used depends largely on the amount of liquid phase
10 generated at such temperature for the particular composition of the compact. For the present composition, the sintering temperature is one at which beta spodumene is molten, and in such instance it ranges from higher than about 1423°C to about 1500°C. Temperatures higher than about 1500°C are not operable because they generate so much liquid phase as to slump the compact or body. With increasing temperatures, increasing amounts of mullite dissolve in the molten beta spodumene generating more
15 liquid at the higher sintering temperatures.

The present sintering is carried out to produce a sintered body having a density greater than about 85% of its theoretical density, i.e. greater than about 85% of the weighted average theoretical density for mullite and beta spodumene based on the amounts thereof present. Preferably, the present sintering is carried out to produce a sintered body having a density greater than 90%, and more preferably greater than
20 95%, of the theoretical density of said body. Sintering time is determinable empirically. Generally, a sintering time of about 30 minutes to five hours is satisfactory.

The sintered body is comprised of crystalline mullite phase and a glassy beta spodumene phase with some metastable lithium aluminum silicates also present and, depending on its composition, possibly some α -Al₂O₃ phase. Generally, the metastable lithium aluminum silicates are present in an amount
25 ranging from 10% by volume to 15% by volume of the sintered body. These metastable lithium aluminum silicates decompose into beta spodumene during the present crystallization annealing and are not present in the present polycrystalline body. The sintered body is nucleation-annealed to nucleate the glassy beta spodumene phase sufficiently to allow its crystallization to produce the present polycrystalline body. Specifically, the sintered body is annealed at a temperature ranging from 600°C to 800°C, preferably from
30 650°C to 750°C, and most preferably, it is annealed at about 700°C. At a temperature below about 600°C, the rate of nucleation is too slow to be useful whereas a temperature higher than about 800°C is not operable in the present process.

Nucleation-annealing time is determinable empirically by standard techniques such as, for example, by observations of the degree to which the final product is crystallized. Generally, a nucleation-annealing
35 time period of about two hours is satisfactory at about 700°C.

The nucleation-annealed sintered body is then crystallization-annealed to crystallize the nucleated glassy beta spodumene phase to produce the present polycrystalline body. Specifically, the nucleation-annealed sintered body is crystallization-annealed at a temperature ranging from 1200°C to a temperature at which the body remains totally solid, i.e. below 1423°C, preferably from 1200°C to 1300°C, and most
40 preferably, it is about 1300°C. There appears to be no significant advantage in using crystallization annealing temperatures higher than 1300°C.

Crystallization-annealing time is determinable empirically by standard techniques such as, for example, by observations of the degree to which the final product is crystallized. Generally, a crystallization-annealing time ranging from about two to ten hours is satisfactory. Longer annealing times
45 reduce the amount of α -Al₂O₃ phase in the final body if it is present.

The present sintering, nucleation-annealing and crystallization-annealing is carried out in an atmosphere which has no significantly deleterious effect on the compact or body. Representative of a useful atmosphere is air, hydrogen, wet hydrogen, nitrogen, argon and mixtures thereof. The sintering and annealing atmosphere is preferably at ambient pressure since there is no advantage in using a pressure
50 higher than ambient. Sintering can also be carried out in a vacuum which has no significant deleterious effect on the compact or body.

In one preferred embodiment, the present sintering, nucleation-annealing and crystallization-annealing are carried out in a single run using the same atmosphere or vacuum throughout the run.

The present polycrystalline body is a pressureless sintered ceramic body. By pressureless sintering
55 herein it is meant the densification or consolidation of the compact or shaped body at ambient pressure or under a vacuum, i.e. without the application of mechanical pressure, into a body having a density greater than 85% of its theoretical density.

The present polycrystalline body has a density greater than about 85% of its theoretical density, i.e. greater than 85% of the weighted average theoretical density for mullite and beta spodumene based on the
60 amounts thereof present in the body. Preferably, the present polycrystalline body has density greater than 90%, and more preferably greater than 95%, of the theoretical density of said body.

The present polycrystalline body has a number of uses, but because of its relatively low thermal expansion coefficient and dielectric constant, it is particularly useful as a substrate material, especially as a supporting substrate for semiconductors in information processing equipment such as computers.
65 Specifically, the present polycrystalline body has a thermal expansion coefficient of less than $3.3 \times 10^{-6}/^\circ\text{K}$

at 300°K, and its thermal expansion coefficient decreases as its content of beta spodumene increases. This is illustrated by the calculated graph of Figure 2. The present polycrystalline body containing about 5% by weight beta spodumene would have a thermal expansion coefficient of about $3.2 \times 10^{-6}/^{\circ}\text{K}$ at 300°K, and the present body containing about 50% by weight beta spodumene would have a thermal expansion coefficient of about $2.2 \times 10^{-6}/^{\circ}\text{K}$ at 300°K.

The present polycrystalline body has a dielectric constant ranging from higher than 6 to lower than 7 at 300°K. The dielectric constant is a function of the amount of beta spodumene present. The more beta spodumene present, the lower is the dielectric constant of the present body.

The present polycrystalline body is comprised of mullite and beta spodumene phases, and more specifically, it has a phase composition comprised of polycrystalline mullite in an amount ranging from 50% by weight to 95% by weight of the total weight of the body and polycrystalline beta spodumene in an amount ranging from 5% by weight to 50% by weight of the total weight of the body.

In a preferred embodiment, the present polycrystalline body has a phase composition comprised of polycrystalline mullite ranging from 60% by weight to 70% by weight of the total weight of the body, and polycrystalline beta spodumene, ranging from 30% by weight to 40% by weight of the total weight of the body, and has a thermal expansion coefficient within about 10% of that of silicon at 300°K.

In a more preferred embodiment, the present polycrystalline body has a phase composition comprised of about 63% by weight of polycrystalline mullite and about 37% by weight of polycrystalline beta spodumene, and has a thermal expansion coefficient within about 5% of that of silicon at 300°K.

The present polycrystalline body can contain a glassy phase in an amount of less than about 5% by volume, preferably less than about 2% by volume, and more preferably less than about 1% by volume, of the total volume of said body. Even more preferably, the present polycrystalline body contains only a detectable amount of glassy phase. Therefore, glassy phase in the present polycrystalline body can range from a detectable amount up to about 5% by volume of the total volume of the body. The amount of glassy phase present in the present polycrystalline body depends largely on the impurities in the starting materials.

The present polycrystalline body may contain a phase of $\alpha\text{-Al}_2\text{O}_3$ ranging up to about 11% by weight of the total weight of the body. This is due to the fact that since the mullite-beta spodumene join intersects an alumina crystallization field, alumina may precipitate at the sintering temperatures used depending largely on the SiO_2 content of the body and the relative amounts of mullite and beta spodumene phases therein. For example, when the body contains about 80% by weight mullite phase and about 20% by weight beta spodumene phase and has an SiO_2 content of about 36.0% by weight, about 4% by weight of $\alpha\text{-Al}_2\text{O}_3$ phase can form therein but when its SiO_2 content is increased to 37.0% by weight, no $\alpha\text{-Al}_2\text{O}_3$ phase will form therein. Also, when the SiO_2 content of the body is greater than about 53.6% by weight, no $\alpha\text{-Al}_2\text{O}_3$ phase will form therein.

More particularly, when the present more preferred polycrystalline body comprised of about 63% by weight mullite phase and about 37% by weight beta spodumene phase has a SiO_2 content of about 44.5% by weight of the total weight of the body, it can contain $\alpha\text{-Al}_2\text{O}_3$ phase in an amount detectable by X-ray diffraction analysis. When such more preferred polycrystalline body has a SiO_2 content of about 45.8% by weight, any $\alpha\text{-Al}_2\text{O}_3$ phase which it may contain is not detectable by X-ray diffraction analysis. However, when such more preferred polycrystalline body has a SiO_2 content of at least about 47.0% by weight and higher it does not contain $\alpha\text{-Al}_2\text{O}_3$ phase.

The SiO_2 content of the present body, i.e. sintered, annealed as well as the present polycrystalline body, ranges from 29.7% by weight to 53.8% by weight of the total weight of the body. By SiO_2 content of the present body, it is meant herein the total SiO_2 content therein, i.e. it is the total of SiO_2 contained in the mullite and beta spodumene phases and in any glassy phase. The present polycrystalline body does not contain a phase of SiO_2 .

The present polycrystalline body can be annealed at a temperature ranging from about 1200°C to below the temperature at which liquid forms in said body in the same atmosphere used for the present crystallization-annealing, to reduce its content of $\alpha\text{-Al}_2\text{O}_3$ phase.

In a preferred embodiment, alumina precipitation, i.e. formation of $\alpha\text{-Al}_2\text{O}_3$ phase in the body is reduced or eliminated by increasing the SiO_2 content of the starting particulate mixture by an amount which is determinable empirically for the particular composition. Preferably, the SiO_2 content of the particulate mixture is increased by adding silica thereto. By SiO_2 content of the present particulate mixture, it is meant herein the total SiO_2 content in the mixture in any form such as mullite powder, beta spodumene powder as well as silica powder. The present particulate mixture has an SiO_2 content ranging from about 29.7% by weight to about 53.8% by weight of the total weight of the mixture.

In the present polycrystalline body, the phases are distributed uniformly, substantially uniformly or at least significantly uniformly. Also, the present polycrystalline body has a uniform, substantially uniform or at least a significantly uniform microstructure.

The beta-spodumene phase in the present polycrystalline body can be discontinuous or continuous. Specifically, in the present polycrystalline body, when the beta-spodumene phase ranges from 5% by weight to 10% by weight of the body, it is discontinuous. As the beta-spodumene phase increases in amount from 10% by weight of the body, it exhibits some continuity, and at about 15% by weight of the

body, it is likely to be continuous and interconnecting. The beta-spodumene phase ranging in amount from in excess of 15% by weight to 50% by weight of the body is continuous and interconnecting.

The present polycrystalline body can be in any desired form. For example, it can be simple, hollow and/or complex in shape. Preferably, for use as a substrate, it is in the form of a sheet.

The invention is further illustrated by the following examples wherein the procedure was as follows unless otherwise stated:

All firing of the compact or body was carried out in a molybdenum disilicide resistance furnace.

At the end of each run, the power was switched off and the body was furnace-cooled to room temperature.

% Density of a sintered or fired body, given herein, is fractional density using 2.822 g/cm which is the theoretical density for 37% by weight beta spodumene (2.38 g/cm³) and 63% by weight mullite (3.19 g/cm³).

The weight % of mullite and of beta spodumene is based on the composition of the starting mixture since there is no significant weight loss between the green and sintered or fired forms of the body in the present process.

Density was measured by a standard immersion technique using isopropyl alcohol as the fluid.

Phase composition of the final product was determined by standard metallographic techniques such as optical microscopy and/or X-ray diffraction analysis.

Thermal expansion coefficient was measured in a calibrated alumina dilatometer at the given temperature.

Example 1

Mullite powder (99.9% pure) composed of 71.8 weight % of Al₂O₃ balance SiO₂ and having an average particle size of about 0.2 micrometer was used.

Beta spodumene powder (99.9% pure) composed of 8.0 weight % Li₂O, 27.5 weight % Al₂O₃ and 64.5 weight % SiO₂ and having an average particle size of about 0.5 micrometer was used.

About 63% by weight of the mullite powder and about 37% by weight of the beta spodumene powder were ball-milled using alumina media in acetone with a polyacrylic acid added as a dispersant. After milling for 3 hours, the solvent was removed by drying in air at about 40°C. The resulting particulate mixture was substantially uniform and had an average particle size of less than about 0.5 μm.

The particulate mixture was pressed into pellets at ambient temperature under a pressure of about 13.7980 N/mm² (20,000 psi). Each pellet was in the form of a disc of substantially the same size of about 1.27 cm (1/2 inch) in diameter and about 3.175 mm (1/8 inch) in thickness.

One disc was sintered at 1450°C for five hours. The temperature was then lowered to 700°C where it was held for 2 hours to nucleate the glassy beta spodumene phase. The temperature was then raised to 1300°C where it was held for 2 hours to crystallize the beta spodumene phase. The disc was then furnace cooled to ambient temperature. All firing, i.e. sintering, nucleation- and crystallization-annealing was carried out in oxygen at ambient pressure, and the fired disc was furnace cooled in the same atmosphere.

The fired disc, i.e. the present polycrystalline body, had a density of about 92.5% of its theoretical density. X-ray diffraction analysis showed that it was comprised of about 60% by weight of crystalline mullite, about 35% by weight of crystalline beta spodumene and about 5% by weight of α-Al₂O₃ phase.

Since the fired disc contained about 5% by weight of α-Al₂O₃ phase, the composition of its mullite and beta spodumene phases differed slightly from that of the starting mullite and beta spodumene powders, i.e. the composition of its crystalline mullite and crystalline beta spodumene phases would be within about 5% by weight of the composition of the starting mullite and beta spodumene powders.

From other experiments, it was known that this fired disc, i.e. the present polycrystalline body, had a thermal expansion coefficient within about 10% of that of silicon at 300°K and a dielectric constant higher than 6 but lower than 7 at 300°K.

This disc would be useful as a supporting substrate for a silicon chip for use in ceramic packaging for use in computers.

This example is illustrated in Table I.

Examples 2—14 of Table I were carried out in substantially the same manner as Example 1 except as noted in Table I and except as noted herein. Specifically, in Table I, all of the starting powders of beta spodumene and mullite were of the same composition and size except the mullite powder of Example 12 where the mullite powder had an average particle size from greater than 5 to 10 micrometers.

In Examples 1—5, 7, 8 and 11—14, the starting beta spodumene and mullite powders comprised 37% by weight beta spodumene and 63% by weight mullite. However, in Examples 13 and 14, excess silica was added, i.e. in Example 13 the SiO₂ was added to form a mixture of mullite, beta spodumene and silica wherein the silica was 4.5 weight % of the total mixture, and in Example 14 the SiO₂ was 7.0 weight % of the total particulate mixture.

In Table I, the starting α-Al₂O₃ powder had an average particle size of about 0.15 micrometer, the starting SiO₂ powder had an average particle size of about 1.0 micrometer, and the starting LiOH · H₂O powder had an average particle size of about 1.0 micrometer and all of these powders were greater than 99% pure.

In Examples 6, 9 and 10, the starting powders were used in proportions which produced the given composition of the particulate mixture.

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In Table I, each particulate mixture was substantially uniform and had an average particle size of less than about 0.5 micrometer except in Example 12 where it had an average particle size greater than one micron.

5 In Examples 2—14, all firing, i.e. sintering, nucleation-annealing and crystallization annealing, was carried out in air at ambient pressure, and the fired body was furnace cooled in air to ambient temperature.

In Examples 11, 13 and 14, the green disc, i.e. green body, was fired in air at ambient pressure at 1400°C for 2 hours, and then the temperature was raised to the given sintering temperature for the given time period.

10 The resulting fired discs, i.e. the final fired bodies, of Examples 1—6, 8, 11, 13 and 14 were analyzed by X-ray diffraction analysis and their phase composition is shown in Table I.

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TABLE I

Ex.	Starting powders	Composition of particulate mixture			Sintering		Nucleation annealing		Crystallization annealing		Firing Atmosphere	Density % theo.	Phase composition of final fired body by x-ray diffraction analysis (wt%)
		Al ₂ O ₃ wt%	SiO ₂ wt%	Li ₂ O wt%	Temp. °C	Time hr.	Temp. °C	Time hr.	Temp. °C	Time hr.			
1	β-spodumene, mullite	55.4	41.6	3.0	1450	5	700	2	1300	2	O ₂	92.5	~60% Mullite, ~35% beta spodumene, ~5% α-Al ₂ O ₃
2	β-spodumene mullite	55.4	41.6	3.0	1450	0.5	700	2	1200	5	Air	94.4	~60% Mullite, ~35% beta spodumene, ~5% α-Al ₂ O ₃
3	β-spodumene, mullite	55.4	41.6	3.0	1450	0.5	700	2	1100	5	Air	—	Major amount mullite, Minor amounts α-Al ₂ O ₃ , LAS**, glass
4	β-spodumene, mullite	55.4	41.6	3.0	1450	5	none	none	1300	2	Air	94.0	63% Mullite, <35% beta spodumene, ~5% α-Al ₂ O ₃ +glass
5	β-spodumene, mullite	55.4	41.6	3.0	1450	5	none	none	none	none	Air	93.2	Major amount mullite, Minor amounts α-Al ₂ O ₃ , LAS**, glass
6	β-spodumene, α-Al ₂ O ₃ , SiO ₂	55.4	41.6	3.0	1400	5	none	none	none	none	Air	89.4	Major amount mullite, Minor amounts α-Al ₂ O ₃ , LAS**, glass
7	β-spodumene, mullite	55.4	41.6	3.0	1400	5	none	none	none	none	Air	73.8	—
8	β-spodumene, mullite	55.4	41.6	3.0	1500	5	none	none	none	none	Air	92.2	Not significantly different from Example 5
9	LiOH · H ₂ O, α-Al ₂ O ₃ , SiO ₂	55.4	41.6	3.0	1450	5	none	none	none	none	Air	83.7	—
10	β-spodumene, LiOH · H ₂ O, α-Al ₂ O ₃ , SiO ₂	55.4	41.6	3.0	1450	5	none	none	none	none	Air	87.5	—
11	β-spodumene, mullite	55.4	41.6	3.0	*1450	0.5	700	2	1300	5	Air	94.9	~60% Mullite, ~35% beta spodumene, ~5% α-Al ₂ O ₃
12	β-spodumene, mullite	55.4	41.6	3.0	1450	5	none	none	none	none	Air	91.7	—
13	β-spodumene, mullite, 4.5 wt% SiO ₂	52.7	44.5	2.8	*1450	0.5	700	2	1300	5	Air	91.6	~62% Mullite, ~36% beta spodumene, ~2% α-Al ₂ O ₃ and barely detectable
14	β-spodumene, mullite, 7.0 wt% SiO ₂	51.5	45.8	2.7	*1450	0.5	700	2	1300	5	Air	90.9	~63% Mullite, ~37% beta spodumene

*Sample prefired in air at 1400°C, 2h

**LAS: Lithium aluminum silicate identified as virgilite (Li₂Al₂Si₃O₈)

Examples 1, 2, 11, 13 and 14 illustrate the present invention. The fired disc, i.e. the present polycrystalline body, produced in Examples 1, 2, 11, 13 and 14 would be useful as a supporting substrate for a silicon chip in a semiconductor device, and more particularly, as a supporting substrate for a silicon chip or other semiconductor in information processing equipment such as computers.

The present polycrystalline body produced in Example 11 had a thermal expansion coefficient measured to be 2.5×10^{-6} at 300°K and a dielectric constant of 6.5 at room temperature, i.e. about 25°C. Also, the polycrystalline body produced in Example 11 was used to produce all of the solid lines in Figure 3 which illustrates that it had a thermal expansion coefficient that closely matched that of Si over the shown temperature range.

In Example 13, the excess silica admixed with the starting powders significantly reduced the amount of α - Al_2O_3 phase in the final polycrystalline body and resulted in a beta spodumene phase which was more silica rich than the starting beta spodumene powder.

In Example 14, the excess silica admixed with the starting powders produced a polycrystalline body which did not have any α - Al_2O_3 phase detectable by X-ray diffraction analysis and resulted in a beta spodumene phase which was more silica rich than the starting beta spodumene powder.

In Example 14, a polished cross-section of the resulting fired disc, i.e. the present polycrystalline body, is shown in Figure 1. Figure 1 shows that the disc is comprised of mullite (lighter phase) and beta spodumene (darker colored phase). Figure 1 illustrates that the present body of this composition has a continuous interconnecting phase of beta spodumene.

Example 2 shows that a crystallization-annealing temperature of 1200°C was operable to produce the present product.

Example 3 shows that a crystallization-annealing temperature of 1100°C was not operable to produce the present product.

Example 4 shows that without the present nucleation-annealing, the present product was not produced. The resulting fired disc in Example 4 contained more than 5% by volume of glassy phase, and from about 40% to about 60% by volume of its beta spodumene phase was not crystalline.

Examples 5 and 8 illustrate that without the present nucleation and crystallization-annealings, the present polycrystalline body was not produced.

Although Examples 5—10 and 12 did not produce the present polycrystalline body, they do illustrate the effect of sintering temperature and starting powders on the density of the final product.

Example 15

This is a paper example.

Two pellets, i.e. green discs, are prepared according to the present invention according to the disclosure of Example 1. Each disc has the same composition as disclosed for Example 1.

Tungsten ink in the form of an X is brushed on one surface of one of the discs. A sandwich of the two discs with the deposited tungsten ink between them is formed and sintered at 1450°C for 30 minutes. The temperature is then lowered to 700°C where it is held for 2 hours to nucleate the glassy beta spodumene phase. The temperature is then raised to 1300°C where it is held for 2 hours to crystallize the beta spodumene phase. The resulting fired body is then furnace cooled to ambient temperature. All firing, i.e. sintering, nucleation- and crystallization-annealing is carried out in wet hydrogen having a dew point of 25°C at ambient pressure, and the fired body is cooled in the same atmosphere.

The resulting product, i.e. body, should have a density greater than 90% of its theoretical density.

The low oxygen partial pressure, which is necessary to prevent the oxidation of the tungsten, should result in some volatilization of SiO from the surface of the ceramic. However, this should result only in the slight depletion of beta spodumene only on the surface as should be indicated by X-ray diffraction and would not be considered significant.

In this paper example, the resulting fired ceramic product should have a high electrical resistivity on the order of 10^{13} ohms at 25°C. The tungsten interconnects should have sintered to sufficient density to provide a continuous electrical pathway through the assembly. The high resistivity of the ceramic in conjunction with the electrical continuity of the tungsten would make the present polycrystalline body useful in ceramic packaging of semiconductors.

Claims

1. A polycrystalline body characterized in that it comprises crystalline mullite in an amount ranging from 50% by weight to 95% by weight of the total weight of the body and crystalline beta spodumene in an amount ranging from 5% by weight to 50% by weight of the total weight of the body, said body having a density greater than about 85% of the theoretical density of said body.

2. The polycrystalline body of claim 1 wherein crystalline mullite ranges from 60% by weight to 70% by weight of the total weight of the body, and crystalline beta spodumene ranges from 30% by weight to 40% by weight of the total weight of the body.

3. The polycrystalline body of claim 1, characterized in that it comprises about 63% by weight of polycrystalline mullite and about 37% by weight of polycrystalline beta spodumene.

4. The polycrystalline body as set forth in any one of claims 1 to 3 in the form of a sheet.

Examples 1, 2, 11, 13 and 14 illustrate the present invention. The fired disc, i.e. the present polycrystalline body, produced in Examples 1, 2, 11, 13 and 14 would be useful as a supporting substrate for a silicon chip in a semiconductor device, and more particularly, as a supporting substrate for a silicon chip or other semiconductor in information processing equipment such as computers.

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In Example 13, the excess silica admixed with the starting powders significantly reduced the amount of $\alpha\text{-Al}_2\text{O}_3$ phase in the final polycrystalline body and resulted in a beta spodumene phase which was more silica rich than the starting beta spodumene powder.

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2. The polycrystalline body of claim 1 wherein crystalline mullite ranges from 60% by weight to 70% by weight of the total weight of the body, and crystalline beta spodumene ranges from 30% by weight to 40% by weight of the total weight of the body.

3. The polycrystalline body of claim 1, characterized in that it comprises about 63% by weight of polycrystalline mullite and about 37% by weight of polycrystalline beta spodumene.

4. The polycrystalline body as set forth in any one of claims 1 to 3 in the form of a sheet.



5. The polycrystalline body of claim 3 wherein said density is greater than 90%.

6. The polycrystalline body as set forth in claim 1 or 2, characterized in that it further comprises an α - Al_2O_3 phase ranging up to about 11% by weight of the total weight of the body and a glassy phase ranging from a detectable amount up to about 5% by volume of the total volume of said body, said body having a dielectric constant ranging from higher than 6 to lower than 7 at 300 K.

7. The polycrystalline body as set forth in claim 1, wherein said mullite phase is comprised of from 71.8 weight % of 74.0 weight % Al_2O_3 balance SiO_2 , said beta spodumene phase is comprised of from 58.5 weight % to 79.4 weight % SiO_2 balance Li_2O Al_2O_3 .

8. A process for producing a polycrystalline body comprised of from 50% by weight to 95% by weight of crystalline mullite phase and from 5% by weight to 50% by weight of crystalline beta spodumene phase which comprises providing a mixture comprised of mullite and/or beta spodumene and/or Al_2O_3 and/or SiO_2 and/or a precursor for Li_2O , said mixture having a composition required to produce said polycrystalline body, shaping said mixture into a compact, sintering said compact at a temperature ranging from greater than 1423°C to 1500°C at which sufficient liquid phase is generated to liquid phase sinter the compact and produce a densified body having a density greater than about 85% of the theoretical density of said body, said sintering temperature having no significant deleterious effect on said compact or body, said sintered body containing said mullite phase and a glassy phase of beta spodumene, nucleation-annealing said sintered body at a temperature ranging from 600°C to 800°C to nucleate said glassy beta spodumene phase, crystallization-annealing the resulting nucleated body at a temperature ranging from 1200°C to below the temperature at which liquid forms in said body to produce said polycrystalline body, said sintering, said nucleation-annealing and said crystallization-annealing being carried out in an atmosphere or vacuum which has no significant deleterious effect on said compact or body.

9. The process according to claim 8 wherein said nucleation-annealing temperature ranges from 650°C to 750°C.

10. The process according to claim 8 wherein said atmosphere is selected from the group consisting of air, hydrogen, wet hydrogen, nitrogen, argon and mixtures thereof.

11. The process according to claim 8 wherein said compact is in the form of a tape.

12. The process according to claim 8, wherein said polycrystalline body is comprised of from 60% by weight to 70% by weight of said mullite and from 30% by weight to 40% by weight of said beta spodumene.

13. The process according to claim 8 wherein said polycrystalline body is comprised of about 37% by weight of said beta spodumene and about 63% by weight of said mullite.

Patentansprüche

1. Polykristalliner Körper, dadurch gekennzeichnet, daß er kristallines Mullit in einer Menge von 50 bis 95 Gew.-% des Gesamtgewichtes des Körpers und kristallines Beta-Spodumen in einer Menge von 5 bis 50 Gew.-% des Gesamtgewichtes des Körpers umfaßt und der Körper eine Dichte von mehr als etwa 85% der theoretischen Dichte des Körpers aufweist.

2. Polykristalliner Körper nach Anspruch 1, worin das kristalline Mullit im Bereich von 60 bis 70 Gew.-% des Gesamtgewichtes des Körpers und das kristalline Beta-Spodumen im Bereich von 30 bis 40 Gew.-% des Gesamtgewichtes des Körpers vorhanden ist.

3. Polykristalliner Körper nach Anspruch 1, dadurch gekennzeichnet, daß er etwa 63 Gew.-% polykristallines Mullit und etwa 37 Gew.-% polykristallines Beta-Spodumen umfaßt.

4. Polykristalliner Körper nach irgendeinem der Ansprüche 1 bis 3 in der Form einer Platte.

5. Polykristalliner Körper nach Anspruch 3, dessen Dichte größer als 90% ist.

6. Polykristalliner Körper nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß er weiter eine α - Al_2O_3 -Phase umfaßt, die in einer Menge von bis zu etwa 11 Gew.-% des Gesamtgewichtes des Körpers vorhanden ist sowie eine glasartige Phase im Bereich von einer nachweisbaren Menge bis zu etwa 5 Vol.-% des Gesamtvolumens des Körpers, wobei der Körper eine Dielektrizitätskonstante im Bereich von mehr als 6 bis weniger als 7 bei 300°K hat.

7. Polykristalliner Körper nach Anspruch 1, worin die Mullit-Phase aus 71,8 bis 74 Gew.-% Al_2O_3 , Rest SiO_2 und die Beta-Spodumen-Phase aus 58,5 bis 79,4 Gew.-% SiO_2 , Rest Li_2O Al_2O_3 zusammengesetzt ist.

8. Verfahren zum Herstellen eines polykristallinen Körpers, der aus 50 bis 95 Gew.-% kristalliner Mullit-Phase und 5 bis 50 Gew.-% kristalliner Beta-Spodumen-Phase zusammengesetzt ist, umfassend: Herstellen einer Mischung aus Mullit und/oder Beta-Spodumen und/oder Al_2O_3 und/oder SiO_2 und/oder einem Vorläufer für Li_2O , wobei die Mischung eine Zusammensetzung aufweist, wie sie erforderlich ist, um den genannten polykristallinen Körper herzustellen, Formen der Mischung zu einem Preßling, Sintern des Preßlings bei einer Temperatur im Bereich von mehr als 1423 bis 1500°C, in dem ausreichend flüssige Phase erzeugt wird, um eine Flüssigphasen-Sinterung des Preßlings zu erhalten und einen verdichteten Körper zu erzeugen, dessen Dichte größer ist als etwa 85% der theoretischen Dichte des Körpers, wobei die Sintertemperatur keine merkliche nachteilige Wirkung auf den Preßling oder Körper hat, der gesinterte Körper die genannte Mullit-Phase und eine glasartige Phase aus Beta-Spodumen enthält, Keimbildungs-Glühen des gesinterten Körpers bei einer Temperatur im Bereich von 600 bis 800°C, um die Kristallkeimbildung der glasartigen Beta-Spodumen-Phase zu erreichen, Kristallisations-Glühen des



gebildeten, Keime enthaltenden Körpers bei einer Temperatur im Bereich von 1200°C bis unterhalb der Temperatur, bei der sich in dem Körper Flüssigkeit bildet, um den genannten polykristallinen Körper herzustellen, wobei das Sintern, das Keimbildungs-Glühen und das Kristallisations-Glühen in einer Atmosphäre oder im Vakuum ausgeführt wird, die keine merkliche nachteilige Wirkung auf den Preßling oder Körper hat.

9. Verfahren nach Anspruch 8, worin die Keimbildungs-Glühtemperatur im Bereich von 650 bis 750°C liegt.

10. Verfahren nach Anspruch 8, worin die Atmosphäre ausgewählt ist aus der Gruppe bestehend aus Luft, Wasserstoff, feuchtem Wasserstoff, Stickstoff, Argon und deren Mischungen.

11. Verfahren nach Anspruch 8, worin der Preßling in Form eines Bandes vorliegt.

12. Verfahren nach Anspruch 8, worin der polykristalline Körper aus 60 bis 70 Gew.-% Mullit und 30 bis 40 Gew.-% Beta-Spodumen zusammengesetzt ist.

13. Verfahren nach Anspruch 8, worin der polykristalline Körper aus etwa 37 Gew.-% Beta-Spodumen und etwa 63 Gew.-% Mullit zusammengesetzt ist.

Revendications

1. Élément polycristallin caractérisé en ce qu'il comprend de la mullite cristalline en une quantité comprise entre 50% en poids et 95% en poids du poids total de l'élément et du spodumène bêta cristallin en une quantité comprise entre 5% en poids du poids total de l'élément, l'élément présentant une masse volumique supérieure à environ 85% de la masse volumique théorique de l'élément.

2. Élément polycristallin selon la revendication 1, dans lequel la quantité de mullite cristalline est comprise entre 60% en poids et 70% en poids du poids total de l'élément et en ce que la quantité de spodumène bêta cristallin est comprise entre 30% en poids et 40% en poids du poids total de l'élément.

3. Élément polycristallin selon la revendication 1, caractérisé en ce qu'il comprend environ 63% en poids de mullite polycristalline et environ 37% en poids de spodumène bêta polycristallin.

4. Élément polycristallin selon l'une quelconque des revendications 1 à 3 sous forme d'une feuille.

5. Élément polycristallin selon la revendication 3, dans lequel la masse volumique est supérieure à 90%.

6. Élément polycristallin selon la revendication 1 ou 2, caractérisé en ce qu'il comprend, en outre, une phase Al_2O_3 représentant jusqu'à environ 11% en poids du poids total de l'élément et une phase vitreuse en une quantité comprise entre une quantité décelable et environ 5% en volume du volume total de l'élément, l'élément présentant une constante diélectrique comprise entre plus de 6 et moins de 7 à 300°K.

7. Élément polycristallin selon la revendication 1, dans lequel la phase mullite est composée de 71,8% en poids à 74,0% en poids d' Al_2O_3 , le reste étant SiO_2 , la phase spodumène bêta est composée de 58,5% en poids à 79,4% en poids de SiO_2 , le reste étant Li_2O Al_2O_3 .

8. Procédé de production d'un élément polycristallin composé de 50% en poids à 95% en poids de phase mullite cristalline et de 5% en poids à 50% en poids de phase spodumène bêta cristalline qui comprend l'apport d'un mélange composé de mullite et/ou de spodumène bêta et/ou d' Al_2O_3 et/ou de SiO_2 et/ou d'un précurseur de Li_2O , le mélange présentant la composition voulue pour produire l'élément polycristallin, la mise du mélange sous forme d'un comprimé, le frittage du comprimé à une température comprise entre plus de 1423°C et 1500°C à laquelle suffisamment de phase liquide se forme pour fritter par la phase liquide le comprimé et produire un élément densifié présentant une masse volumique de plus d'environ 85% de la masse volumique théorique de l'élément, la température de frittage n'ayant pas d'effet nocif important sur le comprimé ou élément, l'élément fritté contenant la phase mullite et une phase vitreuse de spodumène bêta, le recuit de nucléation de l'élément fritté à une température comprise entre 600°C et 800°C pour produire des germes dans la phase vitreuse de spodumène bêta, le recuit de cristallisation de l'élément résultant dans lequel on a produit des germes à une température comprise entre 1200°C et une température inférieure à la température à laquelle du liquide se forme dans l'élément pour produire l'élément polycristallin sachant que l'on met en oeuvre le frittage, le recuit de nucléation et le recuit de cristallisation dans une atmosphère ou sous un vide qui n'a pas d'effet nocif important sur le comprimé ou élément.

9. Procédé selon la revendication 8, dans lequel la température de recuit de nucléation est comprise entre 650°C et 750°C.

10. Procédé selon la revendication 8, dans lequel l'atmosphère est choisie dans le groupe constitué par l'air, l'hydrogène, l'hydrogène humide, l'azote, l'argon et leurs mélanges.

11. Procédé selon la revendication 8, dans lequel le comprimé est sous la forme d'un ruban.

12. Procédé selon la revendication 8, dans lequel l'élément polycristallin est composé de 60% en poids à 70% en poids de mullite et de 30% en poids à 40% en poids de spodumène bêta.

13. Procédé selon la revendication 8, dans lequel l'élément polycristallin est composé d'environ 37% en poids de spodumène bêta et d'environ 63% en poids de mullite.

