

**A method and an apparatus for measuring positions of contact
elements of an electronic component**

5 The present invention relates to a method and an apparatus for measuring respective positions of a set of N contact elements of an electronic component, whereby a first and a second image of the contact elements are recorded. The first image, being obtained by light, perpendicularly reflected on the contact elements, whereas the second image is obtained by light which is reflected over a triangulation angle with respect to the contact elements.

10 Such a method and such a device are known from PCT/BE00/00020. In the known method or device the first image is recorded by a first camera, whereas the second image is recorded by a second camera. The positions of the contact elements are then determined based on the data present in the first and second image.

15 A drawback of the known method and device is that two individual cameras are required. The first camera records the first image, whereas the second records the second image. Consequently two framegrabber channels are required to process the image data. Moreover, the two cameras have to be housed in the same apparatus thus requiring
20 a large volume.

 It is an object of the present invention to realise a method and an apparatus for measuring respective positions of contact elements of an electronic component where only a single camera is required without affecting the accuracy of the measurement.

25 A method or device according to the present invention is therefor characterised in that it comprises :

- bringing said set of contact elements in a measurement plane;
- illuminating said measurement plane by means of a substantially homogeneous first light source;

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- forming a first light path created by a first light beam produced by said first light source and reflection upon at least one of said contact elements in a direction of a first viewing angle, wherein said first light path starts from said at least one contact element and ends in an image plane of a camera;
- forming a second light path created by a second light beam obtained by reflection upon at least one of said contact elements in a direction of a second viewing angle having a different value than said first viewing angle, wherein said second light path starts from said at least one contact element and ends in said image plane of said camera;
- forming a first image of said contact element by means of said camera and by selectively opening said first light path, and forming a second image of said contact element by means of said camera by selectively opening said second light path;
- measuring said position by using said first and second image.

By creating a first and a second light path which end both in the image plane of a same camera, two different images can be formed of the same contact elements while using a single camera. The selective opening of the first and second path enables that, the light travelling along the first path, will be blocked when the second path is open and vice versa. In such a manner, the second image obtained by light of the second path will not be affected by the light travelling along the first path. Thus two different images are obtained which enable to determine the positions of the contact elements while using a single camera.

A first preferred embodiment of a device according to the invention is characterised in that it comprises a second light source provided for producing said second light beam, said second light beam being oriented in such a manner that the output second light beam is incident on said measurement plane over an angle α , wherein $20^\circ \leq \alpha \leq$

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80°. The use of a second light source enables to make a clear distinction between the light in the different light paths.

5 A second preferred embodiment of an apparatus according to the invention is characterised in that said first and second light source are provided for producing light in non-overlapping wavelength ranges. The use of non-overlapping wavelength ranges enables to even more distinguish the light travelling along the first and second light path since consequently light of different wavelength ranges travels along those paths. The light producing the first and second image will thus not
10 interfere.

Preferably selection means provided for selectively opening either said first or said second path are formed by a dichroic mirror. A dichroic mirror in combination with light of different wavelength ranges offers the advantage that for one wavelength range the dichroic mirror is
15 reflective whereas transparent for the other wavelength range.

A third preferred embodiment of an apparatus according to the invention is characterised in that at least one lateral mirror is set up over a viewing angle Ψ adjacent the measurement plane, said camera having a resolution of $nK \times mK$ where $1 \leq n \leq 2$ and $1 \leq m \leq 2$ and being
20 provided for recording light reflected by said at least one mirror. This embodiment requires a less critical set up of mirrors to construct a first and second light path.

The invention will now be described in more details with reference to the drawings. In the drawings :

25 figure 1 shows schematically an overall view of a first embodiment of an apparatus according to the present invention;

figure 2 shows the first and second light path such as formed in the apparatus as shown in figure 1;

figure 3 shows an example of a first and second image
30 recorded by the apparatus shown in figure 1;

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figure 4 shows an example of a first and second image recorded by the apparatus shown in figure 1 and using an anamorphic optical system;

figure 5 shows schematically an overall view of a second embodiment of an apparatus according to the present invention;

figure 6 illustrates the required depth-of-view when using the method of the present invention;

figure 7 shows schematically the principle of a third embodiment of an apparatus according to the present invention;

figure 8 shows the different image set ups obtained by the apparatus shown in figure 5; and

figure 9 shows an example of images recorded by the apparatus shown in figure 8.

In the drawings, a same reference sign has been assigned to a same or analogous element.

The method according to the invention is designed for the automatic computation of the coplanarity of contact elements of electronic components such as BGA (Ball Grid Array)/CSP (Chip Scale Packaging) and flip-chips devices. Other computation may be performed by the invention, including calculation of two or three dimensional size of elements, the colour and shape of elements and detection of missing or misplaced elements.

In the first embodiment of an apparatus 8 according to the present invention and shown in figure 1, the electronic component 10 is placed in a measurement plane 7, in such a manner that its N contact elements are illuminated by a first light source 3. The latter produces a homogeneous illumination of the contact elements preferably at a low incident angle, which is at the most 20°. Preferably, the first light source comprises a high-quality ring-light illumination source. Such a source is built up of a series of LED's which are disposed in a ring, square,

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hexagonal or other substantially planar geometrical arrangement situated under the plane in which the contact elements are placed. It is important that a substantially homogeneous light field is created which covers the volume in which the contact elements of the component are located. In such a manner, a substantially homogeneous illumination of different contact elements is obtained. In order to obtain a symmetrical illumination, the amount of the angle will be determined by the dimension of the component to be measured. The larger the component, the larger the angle. So, for example, for a component of 40 x 40 mm, the diameter of the ring will be 15 cm and the incident angle = 15° , whereas for a component of less than 15 x 15 mm, the incident angle = 10° .

Since the light source 3 illuminates the surface on which the contact elements are placed from the peripheral of the surface, the sides of the contact elements, generally formed by balls, are illuminated. The light produced by the source 3 is reflected according to a first viewing angle substantially perpendicular with respect to the measurement plane 7 in which the electronic component 10 is situated. That reflected light is incident on a first mirror 1, which is inclined over an angle δ defined in function of the other optical elements forming the apparatus 8.

A second illumination source 4 for example formed by a series of LED's is mounted under the measurement plane 7. The light produced by that second illumination source is incident over an angle on the measurement plane. A second mirror 5, inclined over an angle δ , catches the light produced by the second source 4 and reflected on the surface of the contact element 10. The light reflected by the second mirror 5 is oriented towards a third mirror 6 inclined over an angle φ .

A dichroic mirror 2, inclined over an angle θ reflects the light reflected by the first mirror 1 into the objective of a single camera 9 placed under the first mirror 1 and the dichroic mirror 2. The latter is transparent for the light reflected by the third mirror 6 in such a manner

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that the latter light also reaches the single camera 9. The camera is preferably a CCD or CMOS camera.

The set up of the illumination sources and the mirrors, such as shown in figure 1, enables the formation of a first and a second light path as shown also in figure 2. The first light path p1 is created by the first light beam, which is produced by the first illumination source 3 and the reflection of that light in a substantially perpendicular direction with respect to the measurement plane in which the electronic component 10 is set up. The first path p1 has an initial or first section extending between the measurement plane and the first mirror 1. A second section extends between the first mirror 1 and the dichroic mirror 2 and is obtained by the light reflected by the first mirror. A final section of the first path extends between the dichroic mirror 2 and the image plane of the camera 9. The final section is obtained by light reflected towards the camera and incident on the dichroic mirror. In the present example, the angle κ between the incident and reflected light on the dichroic mirror is : $\kappa = 31^\circ$.

The second light path p2 is created by the second light beam which is produced by the second illumination source 4 incident over an angle α , $20^\circ \leq \alpha \leq 80^\circ$ on the measurement plane. The initial or first section of the second light path p2 extends in the direction of a second viewing angle α , between the measurement plane and the second mirror 5. The angle δ upon which the second mirror is inclined is i.a. determined by the angle α and the position of the camera. In the present example $2^\circ \leq \delta \leq 15^\circ$. A second section of the second light path is obtained by the light reflected by the second mirror 5 and oriented towards the third mirror 6. The orientation of the third mirror is dependent on the one of the second mirror 5 and the camera 9. In the present example $5^\circ \leq \varphi \leq 35^\circ$. A final section of the second light path extends between the third mirror and the image plane of camera 9. That final

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section crosses the dichroic mirror and is obtained by light reflected by the third mirror.

5 The dichroic mirror enables the multiplexing of the images obtained by the light travelling on the one hand along the first path and on the other hand along the second path. A dichroic mirror has the properties that for a first wavelength range it acts as a mirror by reflecting the light, whereas for a second non-overlapping wavelength range the mirror is transparent i.e. acts as a simple glass plate. The dichroic mirror is therefor a wavelength-multiplexer. By assigning now the first
10 wavelength range to the light travelling along the first path and the second wavelength range, non-overlapping with the first range, to the second path, an optical assembly is obtained which has the property to use a single camera for forming two different images.

One possible assignment of wavelength ranges is for
15 example red light in the range of 600 nm to 720 nm for the first source and blue light in the range of 420 nm to 550 nm for the second source. The red light then travels along the first light path p1 and the dichroic mirror 4 acts as a mirror for red light, i.e. reflects the red towards the camera. On the other hand the blue light travels along the second path.
20 As the dichroic mirror 2 is transparent for blue light, the blue light crosses the dichroic mirror in order to reach camera 9.

Preferably, the first and second light source are not switched on together but alternately. Although, even if due to scattering, blue light would reach the first mirror 1 or red light the third mirror 6, this
25 scattered light would not affect the formation of the first and second image by the camera. Indeed, blue light incident on the first mirror and reflected towards the dichroic mirror will cross the latter as the dichroic mirror is transparent for blue light. Red light reaching the third mirror and thus incident on the dichroic mirror in such a manner will be reflected by
30 the latter. A clean separation of both images is thus obtained.

Figure 3 shows on the left side a first image obtained by light travelling along the first path and on the right side a second image obtained by light travelling along the second path. The first image has the typical doughnut shape, obtained by perpendicular reflection on the contact elements. The second image shows the typical moon shapes due to the lateral illumination over a triangulation angle.

Since in the second light path the optical axis in the initial section is not perpendicular to the measurement plane but makes an angle α with the measurement plane, various points on the electronic component will be at varying distance from the objective used. Consequently there is a requirement for a significant depth-of-view. Figure 6 illustrates the latter requirement. The required depth-of-view d is expressed as follows :

$$d = f \cdot \sin \alpha$$

where f is the field of view which corresponds to the lateral size of the object or electronic component considered. The required depth-of-view is obtained by using a sufficiently small aperture of the camera objective. As an example, for a field-of-view $f = 50$ mm and a viewing angle $\alpha = 60^\circ$, a total depth-of-view of 43 mm is required. The total depth-of-view is given by the wave-optical formula :

$$\text{Depth} = \lambda / (\text{aperture})^2$$

where λ is the wavelength of the used light source. Assuming the wavelength $\lambda = 500$ nm, the required aperture on the object side is 0.0034, which corresponds to an F-number of 16 for a $f = 50$ mm focal length objective.

Another constraint that must be satisfied by using a single camera is that for both views the average optical length (measured along a central axis of the light path) i.e. the distance between the object and the image plane of the camera, must be substantially the same in order to be able to generate a sharp image with only a single objective . That

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condition is satisfied by a proper set up of the different mirrors 1, 2, 5 and 6 and their correct inclination in such a manner that the first and second light path have approximately a same optical length.

Some modifications or improvements could be applied to the apparatus shown in figure 1. Within a given set up, i.e. for fixed opto-mechanical assembly of mirrors and camera, one may change the field-of-view and thereby camera resolution simply by exchanging the single objective. Objectives of different focal lengths, with suitably adjusted apertures and mounting positions, will all create sharp images filling the camera field entirely, but mapping smaller (large focal length) or larger (small focal length) fields-of-view.

Because of the angular viewing for the second image under an angle α the image height is compressed by a factor of $\cos(\alpha)$ as shown in figure 3. That is, an object square of side E is seen as a trapezoid, roughly of width E and height $E \cdot \cos(\alpha)$. Therefor, not the entire area of the image field is used. The resolution and therefor accuracy of the method could be improved by expanding the height of this image, without affecting the width. An optical system with magnifications different for the two orthogonal directions is called an anamorphic optical system. This can be generated within the second viewing path by means of employing two cylindrical mirrors for the second and third mirrors 5 and 6, replacing the two planar mirrors. The result is shown in figure 4. Alternatively, two additional cylindrical lenses could be used within the second path. These two mirrors or two lenses form a beam expander in one direction and have no optical action in the other direction. None of these elements may be part of the first path, the straight viewing path, of course, since here the object aspect ratio should remain unaffected.

It will be clear that the set up such as illustrated in the figures 1 and 2 only shows an example of a possible embodiment of an

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apparatus according to the present invention. Alternative embodiments could be used for realising the first and second light path. So, for example it is not absolutely necessary that the first path has an initial section extending perpendicularly to the measurement plane, i.e. the first viewing angle being equal to 90° . Other values for the first and second viewing angle are also admitted. Of course the set up of the different mirrors has to be adapted to the choice of the first and second viewing angle and the position of the single camera.

It is also not absolutely required that the first or second light path has different sections. For example, a different alignment of the camera 9 and/or the component 10 or first light source 3 could enable a construction of the first light beam going directly, without using a first mirror 1, towards the image plane of the camera. Further, more or less mirrors than the mirrors 1, 5 and 6 could be used to build up the light paths. What is important is that two light beams are created enabling to form the first and second light path leaving the measurement plane along a first and second viewing angle respectively, where the first and second viewing angle have different values. Each of the light beams have to create each time an image on the image plane of a single camera.

Instead of using a dichroic mirror 2, a semi-transparent mirror could also be used. In the latter embodiment filters or shutters have however to be mounted in the first and second light path. Those filters or shutters should obstruct one light path when the other is open and vice versa. So, for example, when the first light path is open, the shutter has to close the second path. As some light intensity is lost by using semi-transparent mirrors, care should be taken that enough light intensity is produced by the sources 3 and 4.

When filters 13 and 14 are used such as in the embodiment shown in figure 5, those filters have of course to be transparent for the wavelength range assigned to the light path in which they are mounted

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and filter out other wavelengths. In such a manner light from one light path can not interfere with light of the other path and disturb the respective images to be taken.

5 It is thus important that the light paths are selectively opened either by use of the dichroic mirrors or by using filters or shutters. When using shutters their opening has to be synchronised with the light sources. So, when the first light source 3 is emitting light, shutter 13 has to be open while the second light source should preferably be switched off and shutter 14 has to be closed. The opposite situation occurs when
10 the second light source 4 emits i.e. shutter 13 is closed and shutter 14 is open. The shutters are for example formed by usual diaphragms which are electrically operable or by an LCD.

When using the semi-transparent mirror, the wavelength of the light emitted by both light sources could be the same. Of course
15 when a dichroic mirror is used, it is necessary that the wavelength ranges of both light sources are different and non-overlapping. The first and the second image have to be made subsequently in order to not disturb each other.

Another embodiment of the single-camera solution is shown
20 in figure 7 and does not use wavelength multiplex but spatial composition. In this embodiment at least one lateral mirror 20 is placed adjacent to the object 10. The mirror makes an angle ψ with the measurement plane. That angle is situated between 20° and 80°. In the shown embodiment two mirrors 20 and 21, one on the east side and the
25 other on the west side, are placed. Alternatively it could also be possible to place two further mirrors, one on the north side and the other on the south side. In the latter embodiment a direct view, forming the first image, is formed in the middle of the image plane, as shown in figure 8, and four further around the direct view, forming the second image.

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In the embodiment shown in figure 7, the single camera and lens view the direct view and the side views next to each other. Figure 9 shows the images obtained with a set up having a single mirror on the east side. In order to have a same resolution as in the embodiments of figure 1 or 5, the camera needs to have more pixels in one direction. For example, with a viewing angle $\psi = 60^\circ$, the image size is compressed by a factor 2 ($\cos\psi = \frac{1}{2}$). Consequently, the camera needs to have 1.5 times as many pixels as in the other embodiments. Nevertheless, the use of mirrors adjacent to the measurement plane avoids the use of mirrors and their alignment in the light paths. As an example, if a 1 K x 1 K pixel camera is used in the embodiments of figure 1 or 5, a 1 K x 1,5 K pixel camera would be preferred for a set up with one lateral mirror in order to obtain the same resolution. The depth-of-field requirement is the same as described herebefore.

The more lateral mirrors are used, the more accurate will be the measurement. For an embodiment with 2 mirrors, a 1 K x 2 K pixel camera is preferred and a 2 K x 2 K pixel camera is preferred when four mirrors are used in order to obtain a same resolution. Generally an nK x mK resolution is preferred with $1 \leq n \leq 2$ and $1 \leq m \leq 2$.

Of course it would also be possible to use a camera with a higher or a lower resolution, depending on the required image quality. The resolution of the camera should in any way be adapted to record both images simultaneously.

By means of employing a more complex set up of normal mirrors and dichroic mirrors, these multiple side view embodiments may also be executed with a camera of smaller pixel number, using again a wavelength multiplex for the various views. Those experienced in the optical art will have no difficulty in devising a multitude of possible set ups, based on the methods outlined above.

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The determination of the position of the contact elements is determined on the basis of the recorded images in an analogous manner as described in PCT/BE00/00020 which is hereby incorporated by reference.

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CLAIMS

1. A method for measuring respective positions of a set of N contact elements of an electronic component, said method comprises :

- bringing said set of contact elements in a measurement plane;
- 5 – illuminating said measurement plane by means of a substantially homogeneous first light source;
- forming a first light path created by a first light beam produced by said first light source and reflection upon at least one of said contact elements in a direction of a first viewing angle, wherein said first light path starts from said at least one contact element and ends in an image plane of a camera;
- 10 – forming a second light path created by a second light beam obtained by reflection upon at least one of said contact elements in a direction of a second viewing angle having a different value than said first viewing angle, wherein said second light path starts from said at least one contact element and ends in said image plane of said camera;
- 15 – forming a first image of said contact element by means of said camera and by selectively opening said first light path, and forming a second image of said contact element by means of said camera by selectively opening said second light path;
- 20 – measuring said position by using said first and second image.

2. A method as claimed in claim 1, wherein said second light beam is produced by a second light source .

3. A method as claimed in claim 2, wherein said first and second light source produce light with non-overlapping wavelength.

4. A method as claimed in any one of the claims 1 to 3, wherein the first and second light path have a substantially equal average optical length.

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5. A method as claimed in anyone of the claims 1 to 4, wherein said first light source produces said first light beam with an incident angle on said elements of at the most 20° .

5 6. A method as claimed in anyone of the claims 1 to 5, wherein said first light path has an initial section starting from said contact element and extending substantially perpendicularly with respect to said measurement plane.

7. A method as claimed in anyone of the claims 1 to 6, wherein said second light path has an initial section starting from said contact element and wherein said second viewing angle α is comprised between $20^\circ \leq \alpha \leq 80^\circ$.

8. An apparatus for measuring respective positions of a set of N contact elements of an electronic component, said apparatus comprises a first light source provided for generating a substantially homogeneous light beam and illuminating a measurement plane in which said contact elements are disposed, said apparatus comprises a camera and first optical means provided for forming a first light path created by a first light beam produced by said first light source and reflection upon at least one of said contact elements in a direction of a first viewing angle, said first light path starting from said at least one contact element and ending in an image plane of said camera, said apparatus further comprising second optical means provided for forming a second light path created by a second light beam obtained by reflection upon at least one of said contact elements in a direction of a second viewing angle, having a different value than said first viewing angle, said second light path starting from said at least one contact element, said camera being connected to processing means provided for measuring said position from images recorded by said camera, characterised in that said second light path ends in said image plane of said camera and wherein said apparatus further comprises selection means mounted in said first and

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second light path and provided for selectively opening either said first or said second light path.

9. An apparatus as claimed in claim 8, characterised in that it comprises a second light source provided for producing said second light beam, said second light beam being oriented in such a manner that the output second light beam is incident on said measurement plane over an angle α , wherein $20^\circ \leq \alpha \leq 80^\circ$.

10. An apparatus as claimed in claim 9, characterised in that said first and second light source are provided for producing light in non-overlapping wavelength ranges.

11. An apparatus as claimed in claim 9, characterised in that means are provided for subsequently switching on/off the first and second light source.

12. An apparatus as claimed in anyone of the claims 8 to 11, characterised in that said selection means are formed by a dichroic mirror.

13. An apparatus as claimed in anyone of the claims 8 to 11, characterised in that said selection means are formed by a semi-transparent mirror and shutters.

14. An apparatus for measuring respective positions of a set of N contact elements of an electronic component, said apparatus comprises a first light source provided for illuminating a measurement plane in which said contact elements are disposed, said first illumination source being provided for generating a substantially homogeneous light beam, said apparatus comprises a camera provided for recording a first image of said contact elements obtained by reflection of light on the measurement plane, characterised in that a least one lateral mirror is set up over a viewing angle Ψ adjacent to the measurement plane, said camera being provided for recording light reflected by said at least one

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mirror and for forming a second image therefrom, said camera having a resolution adapted to form said first and second image simultaneously.

15. An apparatus as claimed in claim 14, characterised in that said camera has a resolution of $nK \times mK$ where $1 \leq n \leq 2$ and $1 \leq m$

5 ≤ 2 .