

Figures 4A and 4B illustrate up shifting the down-transmitter system of Figure 3B, according to various embodiments.

Figure 5 shows a physical structure equivalent to a result of a shift operation on the tool of Figure 4A, according to various embodiments.

5 Figures 6A and 6B illustrate up shifting the down-transmitter system of Figure 3B, according to various embodiments.

Figure 7 shows a physical structure equivalent to a result of a shift operation on the tool of Figure 6A, in accordance with various embodiments.

10 Figure 8 shows a physical structure equivalent to a result of shift operations on the tool of Figures 4A and 6A, in accordance with various embodiments.

Figures 9A and 9B illustrate down shifting the up-transmitter system of Figure 3A, in accordance with various embodiments.

15 Figure 10 shows a physical structure equivalent to a result of a shift operation on the tool of Figure 9A, in accordance with various embodiments.

Figures 11A and 11B illustrate down shifting the up-transmitter system of Figure 3A, in accordance with various embodiments.

Figure 12 shows a physical structure equivalent to a result of a shift operation on the tool of Figure 11A, in accordance with various embodiments.

20 Figure 13 shows a physical structure equivalent to a result of shift operations on the tool of Figures 9A and 11A, according to various embodiments.

25 Figure 14 shows a physical structure equivalent to a result of combined shift operations on the tool of Figures 4A, 6A, 9A, and 11A, according to various embodiments.

Figures 15A-15D shows examples of different physical structures that can be realized in measurement functions by a tool, having a fixed arrangement of transmitters and receivers, operated with respect to shifting positions of the transmitters relative to the receivers, according to various embodiments.

30 Figure 16A shows a physical structure whose measurements can be obtained by the tool of Figure 2A by selectively taking measurements at locations relative to a reference location such that these measurements mimic the physical structure, according to various embodiments.

Figure 16B shows a physical structure whose measurement function can be attained by the tool of Figure 2A by selectively taking measurements at locations relative to a reference location such that these measurements mimic the physical structures of Figure 16A and 15D.

5 Figure 17 shows features of an example method of operating a tool downhole in a well, according to various embodiments.

Figure 18 depicts a block diagram of features of an example system having a processing unit and a tool to operatively provide measurements to mimic different arrangements of transmitters and receivers, according to various
10 embodiments.

Figure 19 depicts an embodiment of a system at a drilling site, according to various embodiments.

Detailed Description

15 The following detailed description refers to the accompanying drawings that show, by way of illustration and not limitation, various embodiments in which the invention may be practiced. These embodiments are described in sufficient detail to enable those skilled in the art to practice these and other
20 embodiments. Other embodiments may be utilized, and structural, logical, and electrical changes may be made to these embodiments. The various embodiments are not necessarily mutually exclusive, as some embodiments can be combined with one or more other embodiments to form new embodiments. The following detailed description is, therefore, not to be taken in a limiting sense.

25 Figure 1 shows a block diagram of an embodiment of an apparatus 100 having a processing unit 120 and a tool 105 to determine properties downhole in a well 102. Tool 105 has an arrangement of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N to operate in conjunction with processing unit 120 to mimic a different arrangement of transmitters and receivers. Mimic as used
30 herein means to imitate or copy in operation. Equivalent, similar, or identical control and processing of arrangements of transmitters and receivers as disclosed in various embodiments herein provide a mechanism for these arrangements to simulate or resemble closely in operation other physical arrangements of

transmitters and receivers such as to be an imitation or imitations of these other physical arrangements.

5 In an embodiment, an arrangement of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N can operate in conjunction with processing unit 120 to mimic a desired triaxial tool, where it may not be possible to physically implement such a triaxial tool for operation in well 102. Transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N can be oriented with respect to longitudinal axis 107 of tool 105. Each of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N can be tilted with respect to longitudinal axis 107. For example, each of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N can be tilted at 45° with respect to longitudinal axis 107 with two transmitters perpendicular to each other. The two perpendicular transmitters can be disposed on tool 105 with two receivers located between the two transmitters. Each sensor element (i.e., transmitters and receivers) in arrangement of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N can be realized as a coil element, a tilted coil element, a wire element, a toroidal element, a solenoid element, an electrode type element, a transducer, or other appropriate electromagnetic based sensor. The selected sensors may operate in various frequency ranges.

20 Processing unit 120 provides signals to selectively activate transmitters and selectively acquire measurement signals at the arrangement of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N. Processing unit 120 can control activation of the transmitters of tool 105 and can acquire and process signals received from the receivers and transmitters in tool 105 with respect to a reference location about which shifting of tool 105 is correlated to the transmission and reception of signals. A selective set of measurements taken with the shifting of tool 105 can essentially mimic an ideal physical triaxial tool for measuring formation properties downhole in well. The measurements can be taken with tool 105 shifted into specific positions with respect to the arrangement of transmitters and receivers 110-1, 110-2 . . . 110-(N-1), 110-N. The measurements can be taken with tool 105 by first determining a reference location and determining a set of locations relative to the reference location at which transmitters are to be activated and a set of locations relative to the

reference location at which signals are to be acquired at receivers and transmitters with respect to the selective activation of the transmitter. With these locations stored in a machine readable storage medium accessible to processing unit 120, the firing of the relevant transmitters at their respective predetermined
5 locations and the corresponding collection of signals at relevant receivers and transmitters at their respective predetermined locations can be made as the tool reaches these locations downhole, such as with a tool moving with a downhole drilling operation.

Processing unit 120 can be located at the surface of well 102 operably in
10 communication with tool 105 via a communication mechanism. Such a communication mechanism can be realized as a communication vehicle that is standard for well operations. Processing unit 120 can be distributed along the mechanism by which tool 105 is placed downhole in well 102. Processing unit 120 can be integrated with tool 105 such that processing unit 120 is operable
15 downhole in well 102. Processing unit 120 can be distributed along tool 105 or along a structure that delivers tool 105 downhole.

In various embodiments, a processing methodology operatively transforms an array arrangement of transmitters and receivers into a triaxial tool; that is, measurements made by the (non-triaxial) tool are processed to be
20 equivalent to measurement by a tool having a desired triaxial physical structure. Such a triaxial tool can be used as a measurements-while-drilling (MWD) tool such as a logging-while-drilling (LWD) tool. In addition, the triaxial tool can be adapted as a wireline tool. The transformation can be realized by measurements taken with respect to a series of depth shifting operations. Once this
25 transformation is performed, a compensated resistivity can be obtained. In addition, the dip angle, the azimuth, vertical resistivity R_v , and the horizontal resistivity R_h of the formation can be computed.

Figures 2A and 2B show example embodiments of arrangements of transmitters and receivers that can be used in conjunction with a processing unit
30 to operate so as to mimic a different arrangement of transmitters and receivers. An arrangement of transmitters and receivers can be used in conjunction with a processing unit to operate such as to mimic a desired triaxial tool, where such

triaxial tool may not be physically realizable. Such arrangements may be used in apparatus 100 of Figure 1.

Figure 2A shows an embodiment of a tool 205-1 that includes receiver antennas 214-1 and 214-2 and transmitter antennas 212-1 and 212-2, where
5 transmitter antennas 212-1 and 212-2 are arranged symmetrically with respect to a middle location 209-1 between receiver antennas 214-1 and 214-2 with receiver antennas 214-1 and 214-2 between transmitter antennas 212-1 and 212-2 such that receiver antennas 214-1 and 214-2 are central with respect to the sensors of tool 205-1. Transmitter antenna 212-1 may be referred to as T_{UP} and
10 transmitter antenna 212-2 may be referred to as T_{DN} , indicating that T_{UP} is above T_{DN} when the tool is disposed downhole. Transmitter antennas 212-1 and 212-2 and receiver antennas 214-1 and 214-2 are tilted with respect to a longitudinal axis 207-1 of tool 205-1. With tool 205-1 having a cylindrical-like shape, longitudinal axis 207-1 is along the length of tool 205-1.

15 In the example shown in Figure 2A, receiver antennas 214-1 and 214-2 are separated from each other by $2L_R$ with each of receiver antennas 214-1 and 214-2 having centers on the longitudinal axis 207-1 separated from central point 209-1 between receiver antennas 214-1 and 214-2 by the distance L_R . Central point 209-1 may be taken as a reference point. Central point 209-1 may be
20 assigned a numerical value of zero as the point of reference for the effective shifting operations to enable the mimicking of a different arrangement of transmitter antennas and receiver antennas, such as mimicking a triaxial tool. Each of transmitter antennas 212-1 and 212-2 have a center on the longitudinal axis 207-1 separated from central point 209-1 by the distance L_T . The centers of
25 transmitter antennas 212-1 and 212-2 are separated from each other by $2L_T$. In the example shown in Figure 2A, all antennas are at the same tilt angle with respect to longitudinal axis 207-1, where the tilt angle may equal 45° with respect to longitudinal axis 207-1, with T_{UP} and T_{DN} oriented in directions perpendicular to each other.

30 Figure 2B shows an embodiment of a tool 205-2 that includes receiver antennas 214-3 and 214-4 and transmitter antennas 212-3 and 212-4, where transmitter antennas 212-3 and 212-4 are arranged symmetrically with respect to a middle location 209-2 between receiver antennas 214-3 and 214-4 with

receiver antennas 214-3 and 214-4 between transmitter antennas 212-3 and 212-4 such that receiver antennas 214-3 and 214-4 are central with respect to the sensors of tool 205-2. Transmitter antenna 212-3 may be referred to as T_{UP} and transmitter antenna 212-4 may be referred to as T_{DN} , indicating that T_{UP} is above
5 T_{DN} when the tool is disposed downhole. Transmitter antennas 212-3 and 212-4 and receiver antennas 214-3 and 214-4 are tilted with respect to a longitudinal axis 207-2 of tool 205-2. With tool 205-2 having a cylinder-like shape, longitudinal axis 207-2 is along the length of tool 205-2.

In the example shown in Figure 2B, receiver antennas 214-3 and 214-4
10 are separated from each other by $2L_R$ with each of receiver antennas 214-3 and 214-4 having centers on the longitudinal axis 207-2 separated from central point 209-2 between receiver antennas 214-3 and 214-4 by the distance L_R . Central point 209-2 may be taken as a reference point. Central point 209-2 may be assigned a numerical value of zero as the point of reference for the effective
15 shifting operations to enable the mimicking of a different arrangement of transmitter antennas and receiver antennas, such as mimicking a triaxial tool. Each of transmitter antennas 212-3 and 212-4 have a center on the longitudinal axis 207-2 separated from central point 209-1 by the distance L_T . The centers of transmitter antennas 212-3 and 212-4 are separated from each other by $2L_T$. In
20 the example shown in Figure 2B, all antennas are at the same tilt angle with respect to longitudinal axis 207-2, where the tilt angle may equal 45° with respect to longitudinal axis 207-2, with T_{UP} and T_{DN} oriented in directions perpendicular to each other.

Transmitter antennas and receiver antennas can be arranged into two
25 kinds of relative positions: parallel and perpendicular. With ϕ being the tool rotating angle and with the receiver antenna and transmitter antenna parallel to each other, the received voltage at the receiver antenna, represented with the upper index pr , is expressed as:

$$\begin{aligned}
V^{pr} = & \frac{1}{2}V_{xx} \cos^2 \phi + \frac{1}{2}V_{xy} \cos \phi \sin \phi + \frac{1}{2}V_{xz} \cos \phi \\
& + \frac{1}{2}V_{yx} \cos \phi \sin \phi + \frac{1}{2}V_{yy} \sin^2 \phi + \frac{1}{2}V_{yz} \sin \phi \\
& + \frac{1}{2}V_{zx} \cos \phi + \frac{1}{2}V_{zy} \sin \phi + \frac{1}{2}V_{zz}
\end{aligned} \tag{1a}$$

With ϕ being the tool rotating angle and with the receiver antenna and transmitter antenna perpendicular to each other, the received voltage at the receiver antenna, represented with the upper index pp , is expressed as:

$$\begin{aligned}
V^{pp} = & -\frac{1}{2}V_{xx} \cos^2 \phi - \frac{1}{2}V_{xy} \cos \phi \sin \phi - \frac{1}{2}V_{xz} \cos \phi \\
& - \frac{1}{2}V_{yx} \cos \phi \sin \phi - \frac{1}{2}V_{yy} \sin^2 \phi - \frac{1}{2}V_{yz} \sin \phi \\
& + \frac{1}{2}V_{zx} \cos \phi + \frac{1}{2}V_{zy} \sin \phi + \frac{1}{2}V_{zz}
\end{aligned} \tag{1b}$$

Figures 2A and 2B both consist of structures in which transmitters and receivers are parallel or are perpendicular relative to each other. For ease of discussion, only tool 205-1 of Figure 2A is discussed herein with respect to an embodiment implementing a tool that can mimic a different arrangement of transmitters and receivers, such as mimicking a triaxial tool. Tool 205-2 of Figure 2B can also be implemented in a manner similar to or identical to the functional implementation of tool 205-1.

Figures 3A and 3B show the structure of Figure 2A divided into two kinds of systems: an up-transmitter system (UTS) 211 and a down-transmitter system (DTS) 213. UTS 211 includes transmitter antenna 212-1 (T_{UP}), receiver antenna 214-1, and receiver antenna 214-2. DTS 213 includes transmitter antenna 212-2 (T_{DN}), receiver antenna 214-1, and receiver antenna 214-2. A reference point at position Z in the direction of measurement, such as in the direction of drilling, can be selected. With the reference point of measurement set, the shifting of UTS 211 and DTS 213 can be conducted in a process to implement the mimicking of a different arrangement of transmitter antennas and receiver antennas, such as mimicking a triaxial tool. The shifting can be simulated to determine the location of points to independently activate T_{UP} and T_{DN} and to collect signals at receiver antenna 214-1, at receiver antenna 214-2, at T_{DN} when T_{UP} is activated, and at T_{UP} when T_{DN} is activated, as tool reaches

these locations. In a logging-while-drilling configuration, the implemented tool can be operated as a triaxial LWD tool.

Figures 4A and 4B illustrate up shifting down-transmitter system 213 of Figure 3B. Figure 4A shows reference position Z located centrally between receiver antenna 214-1 and receiver antenna 214-2 on tool 205-1. DTS 213 is shifted up by distance $L_T - L_R$. L_T and L_R are positive values and the direction down from reference Z is in the positive direction. With the distance between receiver antennas 214-1 and 214-2 being $2L_R = 8$ inches, $L_R = 4$ inches. Other distances can be used for the distance $2L_R$ between receiver antennas 214-1 and 214-2. As shown in Figure 4B, up shifting this symmetrical arrangement of transmitter antennas and receiver antennas by $L_T - L_R$ operatively locates receiver antenna 214-1 at the same position as transmitter antenna 212-1, T_{UP} of UTS 211, and operatively locates transmitter antenna 212-2, T_{DN} of DTS 213 at the same position as receiver antenna 214-2 of UTS 211.

Figure 5 shows a physical structure equivalent to a result of a shift operation on tool 205-1 of Figure 4A. Up shifting a down-transmitter system 213 of tool 205-1 is conducted to operatively generate an updated up-transmitter system 211-1. Using the reciprocity theory that provides for transmitter antenna 212-2, T_{DN} , to function as a receiver, up shifting DTS 213 by $L_T - L_R$ generates an updated UTS 211-1 equivalent to a physical structure shown in Figure 5. Updated UTS 211-1 operatively includes transmitter antenna 212-1 T_{UP} , receiver antenna 214-1, and two receivers (transmitter antenna 212-2-D2 as receiver antenna R_{21} and receiver antenna 214-2 as receiver antenna R_{22}) perpendicular to each other at the position of antenna receiver 214-2 for UTS 211. The D2 with respect to transmitter 212-2 indicates a receiver antenna that is mimicked by using transmitter antenna 212-2 at a shifted location. Updated UTS 211-1 is provided by measurements taken at locations defined by the effective shifting demonstrated above along the longitudinal axis 207-1 of tool 205-1. When transmitter antenna 212-1 is activated with transmitter antenna 212-2, T_{DN} , at the selected reference point Z plus L_R (positive moving downhole from reference point Z), the voltage received at transmitter antenna 212-2, T_{DN} , as a receiver is $V_{TUP R21}$. When transmitter antenna 212-1 is activated with receiver antenna

214-2 at the selected reference point Z plus L_R , the voltage received at receiver antenna 214-2 is $V_{TUP R22}$.

Figures 6A and 6B illustrate up shifting down-transmitter system 213 of Figure 3B. Figure 6A shows reference position Z located centrally between receiver antenna 214-1 and receiver antenna 214-2 of tool 205-1. DTS 213 is shifted up by distance $L_T + L_R$. L_T and L_R are positive values and the direction down from reference Z is in the positive direction. With the distance between receiver antennas 214-1 and 214-2 being $2L_R = 8$ inches, $L_R = 4$ inches. Other distances can be used for the distance L_R between receiver antennas 214-1 and 214-2. As shown in Figure 6B, up shifting this symmetrical arrangement of transmitter antennas and receiver antennas by $L_T + L_R$ operatively locates receiver antenna 214-2 at the same position as transmitter antenna 212-1, T_{UP} of UTS 211, and operatively locates transmitter antenna 212-2, T_{DN} of DTS 213 at the same position as receiver antenna 214-1 of UTS 211.

Figure 7 shows a physical structure equivalent to a result of a shift operation on tool 205-1 of Figure 6A. Up shifting a down-transmitter system 213 of tool 205-1 is conducted to operatively generate an updated up-transmitter system 211-2. Using the reciprocity theory that provides for transmitter antenna 212-2, T_{DN} , to function as a receiver, up shifting DTS 213 by $L_T + L_R$ generates an updated UTS 211-2 equivalent to a physical structure shown in Figure 7. Updated UTS 211-2 operatively includes transmitter antenna 212-1 T_{UP} , receiver antenna 214-2, and two receivers (transmitter antenna 212-2-D1 as receiver antenna R_{12} and receiver antenna 214-1 as receiver antenna R_{11}) perpendicular to each other at the position of antenna receiver 214-1 for UTS 211. The D1 with respect to transmitter antenna 212-2 indicates a receiver that is mimicked by using transmitter antenna 212-2 at a shifted location. Updated UTS 211-2 is provided by measurements taken at locations defined by the effective shifting demonstrated above along the longitudinal axis 207-1 of tool 205-1. When transmitter antenna 212-1 is activated with transmitter antenna 212-2, T_{DN} , at the selected reference point Z minus L_R , the voltage received at transmitter antenna 212-2, T_{DN} , as a receiver is $V_{TUP R12}$. When transmitter antenna 212-1 is activated with receiver antenna 214-1 at the selected reference point Z minus L_R , the voltage received at receiver antenna 214-1 is $V_{TUP R11}$.

Figure 8 shows a physical structure equivalent to a result of shift operations on tool 205-1 of Figures 4A and 6A. Figure 8 shows an updated up-transmitter system 211-3 that combines shifting reflected in Figures 4B and 6B. Updated UTS 211-3 operatively includes tilted transmitter antenna 212-1, T_{UP} , and two sets of perpendicular receivers. One set 216-1 of perpendicular receivers is realized with transmitter antenna 212-2-D1 as receiver antenna R_{12} and receiver antenna 214-1 as receiver antenna R_{11} . The other set 216-2 of perpendicular receivers is realized with transmitter antenna 212-2-D2 as receiver antenna R_{21} and receiver antenna 214-2 as receiver antenna R_{22} . The D1 and D2 with respect to transmitter 212-2 each indicate a receiver that is mimicked by using transmitter antenna 212-2 at a shifted location. The two sets 216-1 and 216-2 of perpendicular receiver antennas maintain the symmetry of tool 205-1. The two sets 216-1 and 216-2 are separated from each other by $2L_R$. The two sets can be operatively provided by selectively activating T_{UP} and selectively collecting signals at two receiver antennas and at a transmitter antenna as tool 205-1 becomes positioned at specific distances based on shifted distances from a reference point. The reference point may be central to the two receiving antennas.

Figures 9A and 9B illustrate down shifting up-transmitter system 211 of Figure 3A. Figure 9A shows reference position Z located centrally between receiver antenna 214-1 and receiver antenna 214-2 of tool 205-1. UTS 211 is shifted down by distance $L_T - L_R$. L_T and L_R are positive values and the direction down from reference Z is in the positive direction. With the distance between receiver antennas 214-1 and 214-2 being $2L_R = 8$ inches, $L_R = 4$ inches. Other distances can be used for the distance $2L_R$ between receiver antennas 214-1 and 214-2. As shown in Figure 9B, down shifting this symmetrical arrangement of transmitter antennas and receiver antennas by $L_T - L_R$ operatively locates receiver antenna 214-2 of UTS 211 at the same position as transmitter antenna 212-2, T_{DN} of DTS 213, and operatively locates transmitter antenna 212-1, T_{UP} of UTS 211, at the same position as receiver antenna 214-1 of DTS 213.

Figure 10 shows a physical structure equivalent to a result of a shift operation on tool 205-1 of Figure 9A. Down shifting an up-transmitter system 211 of tool 205-1 is conducted to generate an updated down-transmitter system

213-1. Using reciprocity theory that provides for transmitter antenna 212-1, T_{UP} , to function as a receiver, down shifting UTS 211 by $L_T - L_R$ generates an updated DTS 213-1 equivalent to the physical structure shown in Figure 10. Updated DTS 213-1 operatively includes transmitter antenna 212-2, T_{DN} , receiver antenna 214-2, and two receivers (transmitter antenna 212-1-D1, T_{UP} , as receiver antenna R_{11} and receiver antenna 214-1 as receiver antenna R_{11}) perpendicular to each other at the position of antenna receiver 214-1 for DTS 213, since transmitter antenna 212-1 is perpendicular to transmitter 212-2. The D1 with respect to transmitter antenna 212-1 indicates a receiver that is mimicked by using transmitter antenna 212-1 at a shifted location. Updated DTS 213-1 is provided by measurements taken at locations defined by the effective shifting demonstrated above along the longitudinal axis 207-1 of tool 205-1. When transmitter antenna 212-2 is activated with transmitter antenna 212-1, T_{UP} , at the selected reference point Z minus L_R , the voltage received at transmitter 212-1, T_{UP} , as a receiver is $V_{TDN R12}$. When transmitter antenna 212-2 is activated with receiver antenna 214-1 at the selected reference point Z minus L_R , the voltage received at receiver antenna 214-1 is $V_{TUP R11}$.

Figures 11A and 11B illustrate down shifting up-transmitter system 211 of Figure 3A. Figure 11A shows reference position Z located centrally between receiver antenna 214-1 and receiver antenna 214-2. UTS 211 is shifted down by distance $L_T + L_R$. L_T and L_R are positive values and the direction down from reference Z is in the positive direction. With the distance between receiver antennas 214-1 and 214-2 being $2L_R = 8$ inches, $L_R = 4$ inches. Other distances can be used for the distance $2L_R$ between receiver antennas 214-1 and 214-2. As shown in Figure 11B, down shifting this symmetrical arrangement of transmitter antennas and receiver antennas by $L_T + L_R$ operatively locates receiver antenna 214-1 of UTS 211 at the same position as transmitter antenna 212-1, T_{DN} of DTS 213, and operatively locates transmitter antenna 212-1, T_{UP} , of UTS 211 at the same position as receiver antenna 214-2 of DTS 213.

Figure 12 shows a physical structure equivalent to a result of a shift operation on tool 205-1 of Figure 11A. Down shifting up-transmitter system 211 is conducted to generate an updated down-transmitter system 213-2. Using reciprocity theory that provides for transmitter antenna 212-1, T_{UP} , to function as

a receiver, down shifting UTS 211 by $L_T + L_R$ generates an updated DTS 213-2, shown in Figure 12. Updated DTS 213-2 operatively includes transmitter antenna 212-2, T_{DN} , receiver antenna 214-1, and two receivers (transmitter antenna 212-1, T_{UP} , as receiver antenna R_{21} and receiver antenna 214-2 as receiver antenna R_{22}) perpendicular to each other at the position of antenna receiver 214-2 for DTS 213, since transmitter antenna 212-1 is perpendicular to transmitter antenna 212-2. The D2 with respect to transmitter antenna 212-1 indicates a receiver that is mimicked by using transmitter antenna 212-1 at a shifted location. Updated DTS 213-2 is provided by measurements taken at locations defined by the effective shifting demonstrated above along the longitudinal axis 207-1 of tool 205-1. When transmitter antenna 212-2 is activated with transmitter antenna 212-1, T_{UP} , at the selected reference point Z plus L_R , the voltage received at transmitter antenna 212-1, T_{UP} , as a receiver is $V_{T_{DN} R_{21}}$. When transmitter antenna 212-2 is activated with receiver antenna 214-2 at the selected reference point Z plus L_R , the voltage received at receiver antenna 214-1 is $V_{T_{UP} R_{22}}$.

Figure 13 shows a physical structure equivalent to a result of shift operations on tool 205-1 of Figures 9A and 11A. Figure 13 shows an updated down-transmitter system 213-3 that combines shifting reflected in Figures 9B and 11B. Updated DTS 213-3 operatively includes tilted transmitter antenna 212-2, T_{DN} , and two sets of perpendicular receivers. One set 218-1 of perpendicular receivers is realized with transmitter antenna 212-1-D1 as receiver antenna R_{12} and receiver antenna 214-1 as receiver antenna R_{11} . The other set 218-2 of perpendicular receivers is realized with transmitter antenna 212-1-D2 as receiver antenna R_{21} and receiver antenna 214-2 as receiver antenna R_{22} . The D1 and D2 with respect to transmitter antenna 212-1 each indicate a receiver that is mimicked by using transmitter antenna 212-2 at a shifted location. The two sets 218-1 and 218-2 of perpendicular receivers maintain the symmetry of tool 205-1. The two sets 218-1 and 218-2 are separated from each other by $2L_R$. The two sets are operatively provided by selectively activating T_{DN} and selectively collecting signals at two receiver antennas and at a transmitter antenna as tool 205-1 becomes positioned at specific distances based on shifted distances from a

reference point. The reference point may be central to the two receiving antennas.

Figure 14 shows a physical structure 1406 equivalent to a result of combined shift operations on tool 205-1 of Figures 4A, 6A, 9A, and 11A. The physical structure of Figure 14 can be mimicked from combining the effective down shifting of up-transmitter system 211 of tool 205-1 and the up shifting of down-transmitter system 213 of tool 205-1 as reflected in Figures 4A-B, 6A-B, 9A-B, and 11A-B. The various shiftings are provided by activating one transmitter antenna with the other transmitter antenna located at each of the receiver antenna locations relative to a reference position Z. The operatively generated tool equivalent to the physical structure shown in Figure 14 can provide an updated azimuthal deep resistivity (ADR) tool with perpendicular receiver antennas. Measurements of updated tool 205-1 to the equivalent structure of Figure 14 can be transformed into a triaxial measurement. Such triaxial measurements can be made as triaxial LWD measurements using various transformations.

Figures 15A-15D shows examples of different physical structures that can be realized in measurement functions by an embodiment of a tool, having a fixed arrangement of transmitters and receivers, operated with respect to shifting positions of the transmitters relative to the receivers. The received responses at these shifted positions can be used to operatively make transformations to the tool measurements for it to function as different arrangements of transmitters and receivers. Such transformation can be accomplished through processing measurements made by the tool, having the fixed arrangement, at locations correlated to shifting the tool with respect to a reference location relative to the fixed arrangement of transmitters and receivers. Figure 15A shows an equivalent physical structure 1506-1 for obtaining measurements that can be provided by the selected measurements of tool 205-1 of Figure 2A taken at selected locations relative to a selected reference that provides the voltage measurements V_{TdnR11} , V_{TdnR12} , V_{TdnR21} , and V_{TdnR22} . The transformations $V_{TdnR11} + V_{TdnR12}$ and $V_{TdnR21} + V_{TdnR22}$ provide the measurements that could be obtained by a physical structure shown in Figure 15A.

Using reciprocity theory and considering tool's rotation, the measurements equivalent to the structure shown in Figure 15A can be made equal to measurements equivalent to structure 1506-2 shown in Figure 15B. Structure 1506-2 in Figure 15B can be physically realized using a conventional ADR tool without a process of measurements that operatively shifts the tool sensors. A conventional ADR sensor tool typically consists of two central tilted receiver antennas, and three pairs of transmitter antennas arranged symmetrically with respect to the middle of the receiver antennas. The inner transmitter antenna pairs can have a short spacing (for example, 16 inches) and are coaxial non-tilted antennas as shown in Figure 15B. However, the outer transmitter antenna pairs (not shown in Figure 15B) can have 32 and 48 inch spacing and can be tilted. With this arrangement for a conventional ADR sensor tool in a non homogenous layered medium, it generally is not possible to get an accurate compensated resistivity measurement.

The average of voltages acquired by an ADR tool, as structured in Figure 15B, is the measurement obtainable by a traditional LWD tool, which can be arranged with structure 1506-3 as shown in Figure 15C, without a process of measurements that operatively shifts the tool sensors. Figure 15D shows a physical tool structure 1506-4 that can provide measurements that are the difference of the measurement of ADR tool shown in Figure 15B and the average measurement of the traditional LWD tool shown in Figure 15C. Measurements of the physical tool shown in Figure 15D are sensitive to boundary positions. The measurements provided by the physical structures shown in Figures 15A-15D can be attained by measurements of tool 205-1 of Figure 2A appropriately shifted with the measurements transformed by adding and/or subtracting various of the measurements taken by tool 205-1.

The received voltage of structure shown in Figure 15C is

$$V = V_{zz} \quad (2)$$

The voltage of structure shown in Figure 15D is

$$V = \frac{1}{2} V_{xx} \cos \phi + \frac{1}{2} V_{yy} \sin \phi \quad (3)$$

Figure 16A shows a physical structure 1606-1 whose measurements can be obtained by tool 205-1 of Figure 2A by selectively taking measurements at

locations relative to a reference location such that these measurements can be transformed to mimic physical structure 1606-1. The measurements can be obtained by tool 205-1 resulting from selectively activating one transmitter with another transmitter located a location at which a receiver of tool 205-1 also
5 acquires a signal from another activation of the same transmitter. These measurements correlated to specific locations of the arrangement of transmitters and receivers of tool 205-1 can be referred to as shift measurements. The shift measurements of tool 205-1 can provide the voltage measurements V_{TdnR11} , V_{TdnR12} , V_{TdnR21} , and V_{TdnR22} with respect to a reference location. By making the
10 transformations $V_{TdnR11} - V_{TdnR12}$ and $V_{TdnR21} - V_{TdnR22}$, measurements are acquired that are obtainable by the physical structure 1606-1 shown in Figure 16A.

Figure 16B shows a physical structure 1606-2 whose measurement function can be attained by tool 205-1 of Figure 2A by selectively taking measurements at locations relative to a reference location such that these
15 measurements mimic the physical structures of Figure 16A and 15D. The average of voltages measured in mimicking the structure shown in Figure 16A can be obtained by a measurement using the physical structure shown in Figure 15D. The difference between the measurement of the structure shown in Figure 16A and the measurement of the structure shown in Figure 15D is the
20 measurement obtainable by the physical structure 1606-2 shown in Figure 16B, whose measurements yield

$$V = \frac{1}{2} V_{xx} \cos^2 \phi + \frac{1}{2} V_{yy} \sin^2 \phi . \quad (4)$$

Combining the measurements made to effectively copy the measurements of the physical tool structures shown in Figures 15C, 15D, and 16B and considering the
25 tool's rotation, a triaxial tool's measurement, which may be applied to LWD applications, can be obtained from ADR measurements using tilted transmitters.

After performing measurements to operatively shift tool 205-1 of Figure 2A, the collected measurements can be made to equivalently correspond to the structure of shown in Figure 14. The measurements performing the effective
30 shifting of tool 205-1 provide triaxial measurements. Such a tool can be used in LWD applications. With the azimuthal angle set to 0° , 45° , 90° , 135° , 180° , 225° , 270° , and 315° , equation (1a) and (1b) can be expressed as

$$V^{pr}(0) = \frac{1}{2}V_{xx} + \frac{1}{2}V_{zz} + \frac{1}{2}V_{xz} + \frac{1}{2}V_{zx} \quad (5a)$$

$$V^{pr}(45) = \frac{1}{4}V_{xx} + \frac{1}{4}V_{yy} + \frac{\sqrt{2}}{4}V_{xz} + \frac{1}{4}V_{yx} + \frac{1}{4}V_{zy} + \frac{\sqrt{2}}{4}V_{yz} + \frac{\sqrt{2}}{4}V_{zx} + \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (5b)$$

$$V^{pr}(90) = \frac{1}{2}V_{yy} + \frac{1}{2}V_{yz} + \frac{1}{2}V_{zy} + \frac{1}{2}V_{zz} \quad (5c)$$

$$V^{pr}(135) = \frac{1}{4}V_{xx} - \frac{1}{4}V_{yy} - \frac{\sqrt{2}}{4}V_{xz} - \frac{1}{4}V_{yx} + \frac{1}{4}V_{zy} + \frac{\sqrt{2}}{4}V_{yz} - \frac{\sqrt{2}}{4}V_{zx} + \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (5d)$$

$$5 \quad V^{pr}(180) = \frac{1}{2}V_{xx} - \frac{1}{2}V_{zz} - \frac{1}{2}V_{xz} + \frac{1}{2}V_{zx} \quad (5e)$$

$$V^{pr}(225) = \frac{1}{4}V_{xx} + \frac{1}{4}V_{yy} - \frac{\sqrt{2}}{4}V_{xz} + \frac{1}{4}V_{yx} + \frac{1}{4}V_{zy} - \frac{\sqrt{2}}{4}V_{yz} - \frac{\sqrt{2}}{4}V_{zx} - \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (5f)$$

$$V^{pr}(270) = \frac{1}{2}V_{yy} - \frac{1}{2}V_{yz} - \frac{1}{2}V_{zy} + \frac{1}{2}V_{zz} \quad (5g)$$

$$V^{pr}(315) = \frac{1}{4}V_{xx} - \frac{1}{4}V_{yy} + \frac{\sqrt{2}}{4}V_{xz} - \frac{1}{4}V_{yx} + \frac{1}{4}V_{zy} - \frac{\sqrt{2}}{4}V_{yz} + \frac{\sqrt{2}}{4}V_{zx} - \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (5h)$$

$$V^{pp}(0) = -\frac{1}{2}V_{xx} - \frac{1}{2}V_{zz} + \frac{1}{2}V_{xz} + \frac{1}{2}V_{zx} \quad (6a)$$

$$10 \quad V^{pp}(45) = -\frac{1}{4}V_{xx} - \frac{1}{4}V_{yy} - \frac{\sqrt{2}}{4}V_{xz} - \frac{1}{4}V_{yx} - \frac{1}{4}V_{zy} - \frac{\sqrt{2}}{4}V_{yz} + \frac{\sqrt{2}}{4}V_{zx} + \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (6b)$$

$$V^{pp}(90) = -\frac{1}{2}V_{yy} - \frac{1}{2}V_{yz} + \frac{1}{2}V_{zy} + \frac{1}{2}V_{zz} \quad (6c)$$

$$V^{pp}(135) = -\frac{1}{4}V_{xx} + \frac{1}{4}V_{yy} + \frac{\sqrt{2}}{4}V_{xz} + \frac{1}{4}V_{yx} - \frac{1}{4}V_{zy} - \frac{\sqrt{2}}{4}V_{yz} - \frac{\sqrt{2}}{4}V_{zx} + \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (6d)$$

$$V^{pp}(180) = -\frac{1}{2}V_{xx} + \frac{1}{2}V_{zz} - \frac{1}{2}V_{xz} + \frac{1}{2}V_{zx} \quad (6e)$$

$$V^{pp}(225) = -\frac{1}{4}V_{xx} - \frac{1}{4}V_{yy} + \frac{\sqrt{2}}{4}V_{xz} - \frac{1}{4}V_{yx} - \frac{1}{4}V_{zy} + \frac{\sqrt{2}}{4}V_{yz} - \frac{\sqrt{2}}{4}V_{zx} - \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (6f)$$

$$15 \quad V^{pp}(270) = -\frac{1}{2}V_{yy} + \frac{1}{2}V_{yz} - \frac{1}{2}V_{zy} + \frac{1}{2}V_{zz} \quad (6g)$$

$$V^{pp}(315) = -\frac{1}{4}V_{xx} + \frac{1}{4}V_{yy} - \frac{\sqrt{2}}{4}V_{xz} + \frac{1}{4}V_{yx} - \frac{1}{4}V_{zy} + \frac{\sqrt{2}}{4}V_{yz} + \frac{\sqrt{2}}{4}V_{zx} - \frac{\sqrt{2}}{4}V_{zy} + \frac{1}{2}V_{zz} \quad (6h)$$

From equations 5a-5h and 6a-6h, the tensor voltage for each transmitter and receiver position combination in Figure 14 can be solved. For example, from equations (5a), (6a), (5e), and (6e), the following linear equations are obtained:

$$\begin{bmatrix} 1 & 1 & 1 & 1 \\ -1 & -1 & 1 & 1 \\ 1 & -1 & -1 & 1 \\ -1 & 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} V_{xx} \\ V_{xx} \\ V_{zx} \\ V_{zx} \end{bmatrix} = 2 \begin{bmatrix} V^{pr}(0) \\ V^{pp}(0) \\ V^{pr}(180) \\ V^{pp}(180) \end{bmatrix} \quad (7a)$$

5

For example, from equations (5c), (6c), (5g), and (6g), the following linear equations are obtained:

$$\begin{bmatrix} 1 & 1 & 1 & 1 \\ -1 & -1 & 1 & 1 \\ 1 & -1 & -1 & 1 \\ -1 & 1 & -1 & 1 \end{bmatrix} \begin{bmatrix} V_{yy} \\ V_{yz} \\ V_{zy} \\ V_{zz} \end{bmatrix} = 2 \begin{bmatrix} V^{pr}(90) \\ V^{pp}(90) \\ V^{pr}(270) \\ V^{pp}(270) \end{bmatrix} \quad (7b)$$

- 10 Solving equations (7a) and (7b), most of the components of voltage matrix can be obtained except V_{xy} and V_{yx}

$$\bar{V} = \begin{bmatrix} V_{xx} & ? & V_{xz} \\ ? & V_{yy} & V_{yz} \\ V_{zx} & V_{zy} & V_{zz} \end{bmatrix} \quad (8)$$

The components V_{xy} and V_{yx} are not obtained, but $\frac{V_{xy} + V_{yx}}{2}$ can be obtained, if

- 15 the solved components in (8) are substituted into any equation of (5b), (5d), (5f), (5h), (6b), (6d), (6f) and (6h). The voltage matrix can be expressed as

$$\bar{V} = \begin{bmatrix} V_{xx} & \frac{V_{xy} + V_{yx}}{2} & V_{xz} \\ \frac{V_{xy} + V_{yx}}{2} & V_{yy} & V_{yz} \\ V_{zx} & V_{zy} & V_{zz} \end{bmatrix} \quad (9)$$

- Though the XY and YX components in equation (9) may not be completely
20 accurate, they are sufficient, since a coordinate system can be selected to let V_{xy} , V_{yx} , V_{zy} , and V_{yz} be 0. As such, the matrix becomes

$$\overline{V} = \begin{bmatrix} V_{xx} & 0 & V_{xz} \\ 0 & V_{yy} & 0 \\ V_{zx} & 0 & V_{zz} \end{bmatrix}. \quad (10)$$

After shifting, the voltage matrix for each transmitter and receiver position

combination, $\overline{V}_{tup}^{R_1}, \overline{V}_{tup}^{R_2}, \overline{V}_{tdn}^{R_1}$, and $\overline{V}_{tdn}^{R_2}$, can be obtained. These components can be used in the matrix to conduct a triaxial LWD interpretation to determine

- 5 horizontal resistivity, R_h , and vertical resistivity R_v .

Computation of the voltage matrix discussed above is based on the azimuthal angle being known. However, the true azimuthal angle is not obtained directly from field data. In order to obtain the azimuthal angle, measurements are taken with a full rotation partitioned into a number of bins such that
10 measurements are taken as the tool shifts from one bin to another. With a coordinate system selected such that V_{xy}, V_{yx}, V_{zy} , and V_{yz} each equal 0, equations (1a) and (1b) can be rewritten as

$$V^{prl} = \frac{V_{xx} - V_{yy}}{4} \cos 2\phi + \frac{V_{xz} + V_{zx}}{4} \cos \phi + \frac{2V_{zz} + V_{yy} + V_{xx}}{4} \quad (11a)$$

$$V^{pp} = \frac{-V_{xx} + V_{yy}}{4} \cos 2\phi - \frac{V_{xz} - V_{zx}}{4} \cos \phi + \frac{2V_{zz} - V_{yy} - V_{xx}}{4} \quad (11b)$$

- 15 Formulae (12a) and (12b) can be used to perform curve fitting to match formulae (11a) and (11b), from which a bin shift azimuthal angle can be obtained.

$$V^{prl}(i) = A^{prl} \cos(2\phi_i + 2\varphi) + B^{prl} \cos(\phi_i + \varphi) + C^{prl}, (i=1, \dots, N) \quad (12a)$$

$$V^{pp}(i) = A^{pp} \cos(2\phi_i + 2\varphi) + B^{pp} \cos(\phi_i + \varphi) + C^{pp}, (i=1, \dots, N) \quad (12b)$$

- where $A^{prl}, B^{prl}, C^{prl}, A^{pp}, B^{pp}$, and C^{pp} are the coefficients with respect to
20 formulae (11a) and (11b), φ is the bin shift angle, and N is the number of bins. In various embodiments, the number of bins N equals 32. However, the number of bins is not limited to 32.

- After depth shifting, the measurements of tool 205-1 of Figure 2A (or tool 205-2 of Figure 2B) can be transferred to the measurements equivalent to a
25 tool having the structure in Figure 14. From the measurements taken to correspond to the structure in Figure 14, two compensated measurements can be obtained directly. One compensated measurement is provided by effective

perpendicular structure $T_{UP}-R_{12}-R_{22}$ and $R_{11}-R_{21}-T_{DN}$, in which the measurements of bins separated by 180° of this structure is the same in a homogeneous anisotropic formation since ZX and XZ components cancel each other. For a bin structure of 32 bins, bins 1 and 17 are separated from each other by 180° . The bin structure can have a number of bins different from 32. The other compensated measurement is provided by effective parallel structure $T_{UP}-R_{11}-R_{21}$ and $T_{DN}-R_{12}-R_{22}$, where the difference between the measurements of the bins separated by 180° in this structure is double compared with a conventional ADR tool. From the measurement of the two effective structures, the location of anisotropic formations can be identified.

From computations of measurements of a tool shifted to operatively function as the tool in Figure 14, measurements equivalent to a conventional physical ADR tool as shown in Figure 15B, a traditional LWD tool as shown in Figure 15C, ZX component as shown in Figure 15D, and horizontal transmitter and receiver structure as shown in Figure 16B can be obtained. As a result, the measurements of tool 205-1 of Figure 2A (or tool 205-2 of Figure 2B), configured to function as the structure in Figure 14, can provide all the data that can be provided by a physical ADR tool and a traditional physical LWD tool. Tool 205-1 of Figure 2A (or tool 205-2 of Figure 2B) can be used in LWD applications to provide horizontal transmitter and receivers LWD measurements.

Using the measurements obtained to conform to the measurements equivalent to the physical structure shown in Figure 14, a full voltage matrix can also be solved. The voltage matrix can be used to process a triaxial LWD measurement and to perform one dimensional inversion to obtain R_h , R_v , and dip angle of a formation. The relative azimuthal angle relative to a borehole can also be computed by bin shifting from the set of measurements taken corresponding to mimicking the configuration shown in Figure 14. Operating a tool, such as tool 205-1 or 205-2 of Figures 2A and 2B, respectively, to effectively realize the tool of Figure 14 can provide measurement solutions in deep water exploration to obtain structure dip, azimuth, R_h , and R_v .

Figure 17 shows features of an example embodiment of a method 1700 of operating a tool downhole in a well. At 1710, a first transmitter in an arrangement of transmitters and receivers along a longitudinal axis of a tool is

selectively activated at different positions downhole. At 1720, a signal at a receiver in the arrangement of transmitters and receivers is selectively collected in response to activating the first transmitter. At 1730, a signal at a second transmitter in the arrangement of transmitters and receivers is selectively collected in response to activating the first transmitter, when the second transmitter is located at a position at which the receiver collected the signal in response to activating the transmitter. At 1740, the collected signals are processed such that the arrangement of transmitters and receivers provides measurements that mimic operation of a different arrangement of transmitters and receivers.

Method 1700 can be used with tools and processing units similar or identical to tools and processing units described herein. For example, the arrangement of transmitters and receivers along a longitudinal axis of a tool can be implemented using tool 205-1 of Figure 2A or tool 205-2 of Figure 2B. Depth shifting such tools to activate the transmitters at different positions downhole and collect signals at receivers and transmitters can be conducted such that a physical structure of an arrangement of transmitter antennas and receiver antennas different from the physical arrangement shown in Figures 2A and 2B can be mimicked by the physical arrangement shown in Figures 2A and 2B.

In various embodiments, a method can include, in addition to the processes discussed above with respect to method 1700, selectively activating, at different positions downhole, the second transmitter in the arrangement of transmitters and receivers; selectively collecting a signal at a receiver in the arrangement of transmitters and receivers in response to activating the second transmitter; selectively collecting a signal at the first transmitter in response to activating the second transmitter, when the first transmitter is located at a position at which the receiver collected a signal in response to activating the second transmitter; and processing the collected signals from activating the second transmitter with the collected signals from activating the first transmitter.

In various embodiments, a method can include, in addition to the processes discussed above with respect to method 1700, selectively activating, at different positions downhole, the second transmitter in the arrangement of transmitters and receivers; selectively collecting a signal at a receiver in the

arrangement of transmitters and receivers in response to activating the second transmitter; selectively collecting a signal at the first transmitter in response to activating the second transmitter, when the first transmitter is located at a position at which the receiver collected a signal in response to activating the second transmitter; and processing the collected signals from activating the second transmitter with the collected signals from activating the first transmitter such that the arrangement of transmitters and receivers provides measurements that mimic measurements from a desired triaxial tool.

Various methods associated with method 1700 can include operation of a tool similar to or identical to tool 205-1 of Figure 2A or tool 205-2 of Figure 2B in accordance with the various operations discussed herein with respect to tool 205-1. Such operations can include various activations of transmitters and collections of signals at receivers and transmitters at different positions of the tool downhole. Positioning at such positions can be realized by depth shifting the tool. The various methods may be performed in which the arrangement of transmitters and receivers is structured as an arrangement of transmitter antennas and receiver antennas including the first transmitter antenna and the second transmitter antenna separated by two receiver antennas and arranged along the longitudinal axis of a tool with the first transmitter antenna, the second transmitter antenna, and the two receiver antennas tilted with respect to the longitudinal axis of the tool, the first transmitter antenna and the second transmitter antenna being oriented such that they lie in directions perpendicular to each other. The first and second transmitter antennas can be arranged as an up transmitter antenna and a down transmitter antenna, where up and down are relative to the longitudinal axis of the tool, with the tool being downhole. The first transmitter antenna, the second transmitter antenna, and the two receiver antennas can be arranged symmetrically relative to a reference location between the two receiver antennas.

In various embodiments, a method can include shifting the tool relative to a reference location between the two receiver antennas such that the first transmitter antenna or the second transmitter antenna is shifted to a position of one of the two receiver antennas relative to the reference location before the shift. Various methods can include selectively activating the transmitter

antennas and selectively collecting signals at the receiver antennas and transmitter antennas at different angles of rotation of the tool, the different angles corresponding to partitioning a rotation of the tool into a number of different bins. From processing the collected signals, anisotropic formations can be identified. From the collected signals, computation of a voltage matrix can be conducted such that the tool operates as a triaxial tool. Using the computed voltage matrix, one or more of horizontal resistivity, vertical resistivity, or dip angle can be determined. In various methods similar to or identical to operations of tools and/or processing units described herein, the tool can be operated as a logging-while-drilling tool.

Various components of a tool, having an arrangement of transmitters and receivers, and a processing unit that selectively activates the transmitters and selectively collects signals received at the arrangement of transmitters and receivers at different locations downhole in a well such that the tool operates to mimic a tool structure having a different arrangement of transmitters and receivers, as described herein or in a similar manner, can be realized in hardware implementations, software implementations, and combinations of hardware and software implementations. These implementations may include a machine-readable storage medium having machine-executable instructions stored thereon, such as a computer-readable medium having computer-executable instructions, which instructions when executed by a processor, cause the machine to perform various operations. The operations can include selectively activating, at different positions downhole, a first transmitter in an arrangement of transmitters and receivers along a longitudinal axis of a tool; selectively collecting a signal at a receiver in the arrangement of transmitters and receivers in response to activating the first transmitter; selectively collecting a signal at a second transmitter in the arrangement of transmitters and receivers in response to activating the first transmitter, when the second transmitter is located at a position at which the receiver collected the signal in response to activating the transmitter; and processing the collected signals such that the arrangement of transmitters and receivers provides measurements that mimic operation of a different arrangement of transmitters and receivers. A machine-readable storage medium can be realized, where the machine-readable storage medium has

instructions stored thereon, which when performed by a machine, cause the machine to perform operations, the operations comprising one or more processes, similar or identical to one or more processes described herein. In various embodiments, machine-readable storage medium is used with a
5 processor to manage a tool and collect signals from the tool such that the tool mimics an arrangement of transmitters and receivers for a desired triaxial tool, which may not be physically implementable. The form of the machine-readable medium is not limited to any one type of machine-readable medium, but can be any machine-readable medium. For example, a machine-readable medium can
10 include a data storage medium that can be implemented in a housing disposed in a collar of a drill string or in a wireline configuration and/or in a system control center.

Figure 18 depicts a block diagram of features of an example system 1800 having a processing unit and a tool to operatively provide measurements to
15 mimic different arrangements of transmitters and receivers. System 1800 includes a sensor tool 1805 having an arrangement of transmitters and receivers in which measurement signals can be acquired in the arrangement of transmitters and receivers in response to selectively activating one or more transmitters in the arrangement, where processing the collected signals from the receivers and
20 transmitter provides measurements such that the tool mimics a different arrangement of transmitters and receivers. Operating sensor tool 1805, in accordance with procedures similar or identical to procedures discussed herein, can provide measurements corresponding to sensor tool 1805 mimicking a desired triaxial tool, which may not be implementable in a physical arrangement
25 of transmitters and receivers. An implementation of sensor tool 1805 can provide a triaxial LWD tool, which may not be physically implementable directly as a triaxial LWD tool. The arrangements of transmitters and receivers of sensor tool 1805 can be realized in similar or identical manner to arrangements discussed herein.

30 System 1800 can also include a controller 1862, a memory 1864, an electronic apparatus 1868, and a communications unit 1866. Controller 1862, memory 1864, and communications unit 1866 can be arranged to control operation of sensor tool 1805 in a manner similar or identical to a processing

unit discussed herein. Various components of system 1800 can operate together as a processing unit to provide control and processing for sensor tool 1805 to mimic different arrangements of transmitter and receivers, such as a triaxial tool. Controller 1862, memory 1864, and electronic apparatus 1868 can be realized to
5 control activation of transmitter antennas and selection of receiver antennas and transmitter antennas in sensor tool 1805 and to manage processing schemes in accordance with measurement procedures and signal processing as described herein. Communications unit 1866 can include downhole communications in a drilling operation. Such downhole communications can include a telemetry
10 system.

System 1800 can also include a bus 1863, where bus 1863 provides electrical conductivity among the components of system 1800. Bus 1863 can include an address bus, a data bus, and a control bus, each independently configured. Bus 1863 can also use common conductive lines for providing one
15 or more of address, data, or control, the use of which can be regulated by controller 1862. Bus 1863 can be configured such that the components of system 1800 are distributed. Such distribution can be arranged between downhole components such as transmitters and receivers of sensor tool 1805 and components that can be disposed on the surface. Alternatively, the components
20 can be co-located such as on one or more collars of a drill string or on a wireline structure.

In various embodiments, peripheral devices 1867 can include displays, additional storage memory, and/or other control devices that may operate in conjunction with controller 1862 and/or memory 1864. In an embodiment,
25 controller 1862 is a processor. Peripheral devices 1867 can be arranged with a display can be used with instructions stored in memory 1864 to implement a user interface to manage the operation of sensor tool 1805 and/or components distributed within system 1800. Such a user interface can be operated in conjunction with communications unit 1866 and bus 1863. Various components
30 of system 1800 can be integrated with sensor tool 1805 such that processing identical to or similar to the processing schemes discussed with respect to various embodiments herein can be performed downhole in the vicinity of the measurement.

Figure 19 depicts an embodiment of a system 1900 at a drilling site, where system 1900 includes a measurement tool 1905 having a processing unit and a sensor unit, where sensor unit includes an arrangement of transmitters and receivers in which measurement signals can be acquired in the arrangement of transmitters and receivers in response to selectively activating one or more transmitters in the arrangement, where processing the collected signals from the receivers and transmitter provides measurements such that the tool mimics a different arrangement of transmitters and receivers. Though shown as a single unit in Figure 19 the processing unit of measurement can be distributed among downhole apparatus and surface apparatus. Measurement tool 1905 can be structured and fabricated in accordance with various embodiments as taught herein with respect to a processing unit and a sensor tool having an arrangement of transmitters and receivers.

System 1900 can include a drilling rig 1902 located at a surface 1904 of a well 1906 and a string of drill pipes, that is, drill string 1908, connected together so as to form a drilling string that is lowered through a rotary table 1907 into a wellbore or borehole 1912. The drilling rig 1902 can provide support for drill string 1908. The drill string 1908 can operate to penetrate rotary table 1907 for drilling a borehole 1912 through subsurface formations 1914. The drill string 1908 can include drill pipe 1918 and a bottom hole assembly 1920 located at the lower portion of the drill pipe 1918.

The bottom hole assembly 1920 can include drill collar 1915, measurement tool 1905 attached to drill collar 1915, and a drill bit 1926. The drill bit 1926 can operate to create a borehole 1912 by penetrating the surface 1904 and subsurface formations 1914. Measurement tool 1905 can be structured for an implementation in the borehole of a well as a measurements-while-drilling (MWD) system such as a logging-while-drilling (LWD) system. The housing containing measurement tool 1905 can include electronics to activate transmitters of measurement tool 1905 and collect responses from receivers and transmitters of measurement tool 1905. Such electronics can include a processing unit to analyze signals sensed by measurement tool 1905 and provide measurement results to the surface over a standard communication mechanism for operating a well. Alternatively, electronics can include a communications

interface to provide signals sensed by measurement tool 1905 to the surface over a standard communication mechanism for operating a well, where these sensed signals can be analyzed at a processing unit at the surface.

5 In various embodiments, measurement tool 1905 may be included in a tool body 1970 coupled to a logging cable 1974 such as, for example, for wireline applications. Tool body 1970 containing measurement tool 1905 can include electronics to activate transmitters of measurement tool 1905 and collect responses from receivers and transmitters of measurement tool 1905. Such electronics can include a processing unit to analysis signals sensed by
10 measurement tool 1905 and provide measurement results, such as formation properties, to the surface over a standard communication mechanism for operating a well. Alternatively, electronics can include a communications interface to provide signals sensed by measurement tool 1905 to the surface over a standard communication mechanism for operating a well, where these
15 collected sensed signals are analyzed at a processing unit at the surface. Logging cable 1974 may be realized as a wireline (multiple power and communication lines), a mono-cable (a single conductor), and/or a slick-line (no conductors for power or communications), or other appropriate structure for use in bore hole 1912.

20 During drilling operations, the drill string 1908 can be rotated by the rotary table 1907. In addition to, or alternatively, the bottom hole assembly 1920 can also be rotated by a motor (e.g., a mud motor) that is located downhole. The drill collars 1915 can be used to add weight to the drill bit 1926. The drill collars 1915 also can stiffen the bottom hole assembly 1920 to allow the bottom
25 hole assembly 1920 to transfer the added weight to the drill bit 1926, and in turn, assist the drill bit 1926 in penetrating the surface 1904 and subsurface formations 1914.

During drilling operations, a mud pump 1932 can pump drilling fluid (sometimes known by those of skill in the art as "drilling mud") from a mud pit
30 1934 through a hose 1936 into the drill pipe 1918 and down to the drill bit 1926. The drilling fluid can flow out from the drill bit 1926 and be returned to the surface 1904 through an annular area 1940 between the drill pipe 1918 and the sides of the borehole 1912. The drilling fluid may then be returned to the mud

pit 1934, where such fluid is filtered. In some embodiments, the drilling fluid can be used to cool the drill bit 1926, as well as to provide lubrication for the drill bit 1926 during drilling operations. Additionally, the drilling fluid may be used to remove subsurface formation 1914 cuttings created by operating the drill
5 bit 1926.

Although specific embodiments have been illustrated and described herein, it will be appreciated by those of ordinary skill in the art that any arrangement that is calculated to achieve the same purpose may be substituted for the specific embodiments shown. Various embodiments use permutations
10 and/or combinations of embodiments described herein. It is to be understood that the above description is intended to be illustrative, and not restrictive, and that the phraseology or terminology employed herein is for the purpose of description. Combinations of the above embodiments and other embodiments will be apparent to those of skill in the art upon studying the above description.

15

CLAIMS

1. A method of measuring properties downhole, the method comprising:
 - activating (1710), at different positions downhole, a first transmitter (212-1) in an arrangement (105) of transmitters (212-1, 212-2) and receivers (214-1, 214-2) along a longitudinal axis (207-1);
 - collecting (1720) a signal at a receiver (214-2) in the arrangement of transmitters and receivers in response to activating the first transmitter;
 - collecting (1730) a signal at a second transmitter (212-2) in the arrangement of transmitters and receivers in response to activating the first transmitter, when the arrangement of transmitters and receivers has been moved to a different position at which the second transmitter is located at substantially the same position at which the receiver collects the signal in response to activating the first transmitter; and
 - processing together (1740) the signals that were collected at substantially the same position by both the receiver and the second transmitter, thereby to provide measurements that simulate operation of an arrangement of receivers co-located at a single downhole position.
2. The method of claim 1, wherein the method comprising:
 - activating, at different positions downhole, the second transmitter in the arrangement of transmitters and receivers;
 - collecting a signal at the or another receiver (214-1) in the arrangement of transmitters and receivers in response to activating the second transmitter;
 - collecting a signal at the first transmitter in response to activating the second transmitter, when the first transmitter is located at substantially the same position at which the or the other receiver collects the signal in response to activating the second transmitter; and
 - processing the collected signals from activating the second transmitter with the collected signals from activating the first transmitter to provide measurements that simulate operation of an arrangement of transmitters and receivers that differs from the actual arrangement of transmitters and receivers.

3. The method of claim 1 or 2, wherein the collected signals are processed to provide measurements that simulate measurements from a triaxial tool.
4. The method of claims 1, 2 or 3 wherein the arrangement of transmitters and receivers includes the first transmitter antenna and the second transmitter antenna separated by two receiver antennas and arranged along the longitudinal axis of a tool with the first transmitter antenna, the second transmitter antenna, and the two receiver antennas tilted with respect to the longitudinal axis of the tool, the first transmitter antenna and the second transmitter antenna being oriented such that they lie in directions perpendicular to each other.
5. The method of claim 4, wherein the first transmitter antenna and the second transmitter antenna are arranged equidistant on either side of a reference location (Z) which is at the midpoint between the two receiver antennas.
6. The method of claim 5, wherein the method includes shifting the tool relative to the reference location between the two receiver antennas such that the first transmitter antenna or the second transmitter antenna is shifted to a position of one of the two receiver antennas relative to the reference location before the shift.
7. The method of any preceding claim 1 or 2, wherein the method includes selectively activating the transmitter antennas and selectively collecting signals at the receiver antennas and at one or more of the transmitter antennas at different angles of rotation (θ) of the arrangement of transmitters and receivers about the longitudinal axis, the signals at different angles being collected in a number of different bins corresponding to partitions of a complete rotation about the axis.
8. The method of any preceding claim, wherein the method further includes identifying anisotropic downhole formations from the processed collected signals.

9. The method of any preceding claim, wherein the method includes computation of a voltage matrix from the collected signals such that the arrangement of transmitters and receivers operates as a triaxial tool.
10. The method of claim 9, wherein the method includes determining one or more of horizontal resistivity, vertical resistivity, or dip angle using the voltage matrix.
11. The method of any preceding claim, wherein the method is a logging-while-drilling method.
12. A machine-readable storage medium having instructions stored thereon, which, when performed by a machine, cause the machine to perform the method of any of claims 1 to 10.
13. An apparatus to measure properties downhole, the apparatus comprising:
 - a tool having an arrangement of transmitters and receivers along a longitudinal axis of the tool; and
 - a processing unit to control activation of the transmitters of the tool and to process signals received from receivers and transmitters in the tool in accordance with the method of any of claims 1 to 11.
14. The method of claim 1, wherein the second transmitter is a transceiver or a transmitter operated as a receiver.