

Description

The invention relates to a method of severing a plate of brittle material, in which a crack initiation is provided in a side of a plate of brittle material as initiation for a crack, after which a thermal load is provided along a heating track on at least one major surface of a plate to be severed, as a result of which stresses are produced in the plate, which, starting from the crack initiation, cause a crack transverse to the major surface along the desired cutting line.

A method of the kind to which the present invention relates is known from DE-C-28.13.302. In this known method, a crack initiation is provided in a side of a plate of flat glass and the plate is heated in one of two consecutively arranged regions symmetrical with respect to the desired cutting line and is cooled in the other of these regions, as a result of which, due to temperature gradients, thermal stresses are produced in the plate, which cause a crack, starting from the crack initiation. When the plate is severed symmetrically, the crack follows the desired cutting line. However, when the plate is severed asymmetrically, the crack deviates from the desired cutting line.

The invention has for its object to provide a method of the kind described above, by means of which a plate of brittle material is severed accurately and rapidly along a desired cutting line. According to the invention, this object is achieved in that the thermal load is provided asymmetrically with respect to the desired asymmetrical cutting line in such a manner that the mechanical stresses close to a crack tip, which are the resultant of the asymmetrical severing of the plate and the thermal load stresses, are symmetrical with respect to the desired asymmetrical cutting line when the crack tip is located on the desired cutting line.

By means of this method according to the invention, it is possible to cut along a straight line and along contours without deviations of the crack occurring with respect to the desired cutting line. When there is severed asymmetrically according to the known method from DE-C-28.13.302, two kinds of deviations occur: lateral deviations, i.e. deviations of the crack with respect to the desired cutting line in a major surface of the plate, and squareness deviations, i.e. deviations of the crack with respect to a surface, starting from the desired cutting line and transverse to a major surface of the plate. The said deviations are due to mechanical asymmetry. When a plate is severed asymmetrically, the plate is subdivided into two strips having different widths. During severing, the material along the crack has a higher temperature than the surrounding material and consequently the thermal expansion of the material along the crack is greater

than that of the surrounding material. As a result, the strips of material on either side of the crack warp: the strips bend away from the crack. However, the narrow strip bends more strongly than the wide strip due to the fact that the latter is connected to a larger quantity of cold material and is thus prevented from bending away from the crack. The stress in the material close to the crack tip in the direction of the crack is thus greater on the side of the wider strip; the condition of stress is asymmetrical. Ultimately, a shear load is formed on the material immediately in front of the crack tip. As a result, the crack will change in direction towards the narrow strip and will follow no longer the desired cutting line. According as the crack obtains a larger lateral deviation, the shear load becomes smaller until with a sufficient lateral deviation the shear load has become zero and the condition of stress around the crack tip is symmetrical.

The value of the lateral deviation is determined by a larger number of parameters, such as: thermal and mechanical properties of the material, power, shape and dimension of the heat source and geometrical parameters, such as dimensions of the plate and the position of the crack in the plate.

The squareness deviations occur, for example, when the thermal load is provided only on one major surface of the plate to be severed. The heated or cooled zone on the other major surface is larger due to diffusion. The lateral deviation is thus different on the two major surfaces. Both deviations are therefore due to the difference in width and hence in rigidity of the strips of material on either side of the crack, i.e. to mechanical asymmetry. These deviations occur both when cutting along a straight line and when cutting along contours.

By means of the method according to the invention, the thermal load is provided along a heating track which is such that the stresses in the material of the plate close to the crack tip are symmetrical when the crack tip is located on the desired cutting line. Thus, no lateral and squareness deviations occur with respect to the desired cutting line. The plate is severed asymmetrically along the desired cutting line. By this method, it is possible to cut along a straight line and along contours.

In a preferred embodiment of the method according to the invention, a spot-shaped heat source and the plate to be severed are moved with respect to each other, a deviation of the crack with respect to the desired cutting line being fed back and the relative movement being readjusted. The position of the crack tip is measured during severing. When the measured position does not lie on the desired cutting line, the spot-shaped heat

source is moved with respect to the plate to be severed in such a manner that the crack follows the desired cutting line. Deviations are immediately corrected.

The position of the crack tip could be measured, for example, mechanically, acoustically or optically. In the case of mechanical measurement, a scanner with a sharp point scanning the crack should follow the source. Apart from the usual disadvantages of mechanical contact, a great disadvantage is that there cannot be measured at the area of the crack tip because the point of the scanner always has a finite radius, whereas the crack opening at the area of the crack tip is nihil. The scanner will then have to move at a certain distance behind the crack tip. This gives rise to inaccuracies in the system so that this is at the expense of the accuracy with which there can be adjusted.

Acoustic measurement is an alternative. It is known that acoustic waves produced in the plate are reflected by a crack. The position of the crack and of the crack tip can be derived from the connection between emitted waves and reflected waves.

The most promising method consist in optically measuring the position of the crack tip. This can be effected in that the region around the crack tip is recorded by means of a video camera following the movement of the source. As a matter of course, the plate may also be moved with respect to the source and with respect to the camera. The illumination and the wavelength of the light to be used depend upon the material to be cut. For a material such as glass a visible-light camera may be used, while the illumination can take place through the glass plate so that the camera "sees" the reflections on the crack. On the contrary, silicon is not transparent to visible light, but is transparent to infrared light. Use could then be made of an infrared light source and camera. With a material which is not sufficiently transparent for any camera, the crack can be "seen" by reflection of incident light. In this case, however, it will be much more difficult to obtain a clear image of the crack. When once an image of the extending crack has been obtained, the position of the crack tip can be calculated by means of image processing techniques. This information is then fed back to control the relative movement. The spot of the spot-shaped heat source may be circular, oval or elongate. With an elongate spot, the longitudinal direction of the spot is chosen to be parallel to the desired cutting line. As a result, the material around the crack tip and in the direction of the desired cutting line is heated more satisfactorily.

In a further embodiment of the method according to the invention, both the relative speed of the

spot-shaped heat source with respect to the plate in the direction of the desired cutting line and the relative displacement of the spot-shaped heat source with respect to the plate at right angles to the direction of the desired cutting line are readjusted by feedback. By these measures, the relative movement of the spot-shaped heat source is readjusted. The two measures are not dependent upon one another. A change of the relative speed influences the position of the crack tip in and transverse to the desired direction of the cutting line. By increase of the relative speed, the lateral deviation is reduced, and conversely. Besides, due to the relative movement of the spot-shaped heat source with respect to the plate transverse to the direction of the desired cutting line, the position of the crack tip will also change in the direction of the desired cutting line. It is also possible to correct the position of the crack tip by adapting the thermal power of the spot-shaped heat source.

In another embodiment of the method according to the invention, the thermal load is provided on the plate along a predetermined heating track, which does not coincide with the desired cutting line. Apart from a small stochastic variation, the lateral deviation is a reproducing phenomenon, that is to say that upon repeated severing of identical plates the deviation is substantially the same. By adapting the heating track, the stress around the crack tip can thus be influenced and the lateral deviation can be reduced. From a viewpoint of adjustment technique, this can be designated as positive feedback. The exact shape of the heating track can be determined by experiments or by calculation. This method has great advantages when large numbers of identical plates are severed in the same manner.

In a still further embodiment of the method according to the invention, a stationary linear heat source is used, whose shape corresponds to that of the heating track. The exact shape of the line source is determined empirically or by calculation. The shape of the line source will have a curvature towards the wide strip so that the wide strip becomes warmer and bends away from the crack over the same distance as the narrow strip. The stress around the crack tip is then symmetrical. The severing of plates with a linear heat source is effected very rapidly.

In a further embodiment of the method according to the invention, a spot-shaped heat source is used, which is moved along the heating track by a relative movement of the heat source with respect to the plate. The heating track along which the spot-shaped heat source is moved is predetermined empirically or by calculation. This in contrast with the aforementioned embodiment, in which the heating track of the spot-shaped heat source is

determined by feedback. The heating track with the use of a spot-shaped heat source deviates from the heating track with the use of a linear heat source because the thermal load is different. The use of a spot-shaped heat source is particularly advantageous when cutting contours into the plate.

In a still further embodiment of the method according to the invention, several heat sources are used. By a suitable combination of several heat sources, the stress around the crack tip can be kept symmetrical. Several heat sources can be used when severing a plate with feedback and with positive feedback. Instead of several heat sources, also a combination of heat and cold sources may be used. A cold source is then considered as a negative heat source. When the heat sources do not influence each other thermally, the overall thermal load due to several heat sources is found by superimposition of the stress distributions due to the separate sources.

The invention will be described more fully with reference to a few embodiments and the Figures.

In the drawing:

Figure 1 shows diagrammatically an embodiment of a method according to the invention, in which the crack tip position is measured mechanically;

Figure 2 shows diagrammatically another embodiment of a method according to the invention, in which the crack tip position is measured optically;

Figure 3 shows the adaptation of the relative movement by feedback with a rectilinear severing;

Figure 4 shows the adaptation of the relative movement by feedback with a contour severing;

Figure 5 shows diagrammatically an embodiment of the pre-adaptation of the heating track with rectilinear severing;

Figure 6 shows diagrammatically an embodiment of the pre-adaptation of the heating track with contour severing;

Figure 7 shows the adaptation of the thermal load by addition of an additional heat source.

Figure 1 shows an embodiment of the method according to the invention, in which the position of the crack tip 1 is measured mechanically. The plate 3 and the spot-shaped heat source 5 are moved with respect to each other, the position of the crack tip 1 with respect to the desired cutting line 7 being measured by a scanner 9 with a sharp point 11 and deviations being fed back and the relative movement being readjusted.

Figure 2 shows an embodiment of the method according to the invention, in which the position of the crack tip 1 is measured optically. The parts corresponding to Figure 1 are provided with the same reference numerals. The spot-shaped heat

source 5 is moved over the plate 3. Instead of the scanner, in this embodiment use is made of a video camera 13, which follows the movement of the source and records the region 15 around the crack tip 1. When the image of the extending crack 17 has been obtained, the position of the crack tip 1 with respect to the desired cutting line 7 can be calculated by means of image processing techniques. This information is then fed back to control the position and the speed of the heat source 5 with respect to the plate 3.

Figure 3 shows diagrammatically the adaptation of the relative movement of the spot-shaped heat source with respect to the plate 3 with rectilinear severing. Figure 3 shows a circular spot 19 and the image field 21 of the camera. The desired cutting line 7 extends parallel to the X axis. The position of the image field 21 is adjusted so that the centre H coincides with the desired cutting line 7. The camera not shown and the spot 19 are fixed in the X direction at a relative distance C. The spot 19 can be moved freely in the Y direction, however. (With the use of a laser as heat source, this may be effected, for example, by means of a mirror or lens rotating about the X axis.) The plate 3 is moved in the negative X direction. The severing process and the camera are considered as a "black box" process with two parameters at the input: the y position y_b of the spot 18 and the speed V, and with two parameters at the output: the x and y positions x_s and y_s of the crack tip 1 with respect to the centre H of the camera image field 21. The y value y_s is equal to the deviation Δy of the crack 17 with respect to the desired cutting line 7; it is compared with the desired value of Δy , $\Delta y = 0$. The difference is fed back through a regulator to the y position y_b of the spot 19: if $\Delta y > 0$, the y position y_b is made smaller, and conversely. The x value x_s of the position of the crack tip 1 is used to adjust the speed V; in fact, it has to be avoided that the crack tip 1 moves out of the image field 21 of the camera. The desired value of x_s is set, for example, to zero so that the desired position of the crack tip 1 coincides with the centre H of the image field 21 of the camera. If x_s is positive, the speed V is increased: with a negative x_s , the speed V is reduced. This adjustment may be omitted if the position of the crack tip 1 with respect to the spot-shaped heat source 19 substantially does not vary along the whole cutting line 7. The speed V can then be kept constant along the whole crack.

The two adjustments are not independent of one another. A change of the speed V influences not only the x position x_s , but also the y position y_s of the crack tip 1. Upon increase of the speed V, the lateral deviation Δy will decrease. Besides, when the y position y_b of the spot 19 changes, not

only the y position y_s of the crack tip 1, but also the x position x_s will change. This cross connection should be taken into account when designing the regulators.

Figure 4 shows diagrammatically the adaptation of the relative movement by feedback with contour severing. In the case of contour severing, the crack tip 1 can in principle occupy all positions with respect to the hot spot 19. The method as described in Figure 3 cannot be used here. A solution to avoid that the crack tip 1 moves out of the image field 21 of the camera, is shown in Figure 4. The desired position of the crack tip 1 coincides with the centre H of the image field 21. The centre H of the image field 21 is moved along the desired cutting line 7. From the desired cutting line 7, also the orientation of a local coordinate system is determined having as origin the centre H of the image field 21 in such a manner that the X axis is tangent to the desired cutting line 7. The position of the crack tip 1 is determined with respect to this local coordinate system. The spot 19 now cannot perform a translatory movement with respect to the camera, as in Figure 3, but can perform a rotary movement about the centre H of the image field 21. The y position y_s of the crack tip 1 is now used to adjust the position of the spot 19 with respect to the centre H of the image field 21: if y_s is positive, the spot 19 is rotated clockwise, whereas with a negative y_s the spot 19 is rotated counterclockwise. The x position x_s is used to adjust the tangential speed.

Theoretically, it would be possible that in this manner the lateral deviation is not entirely adjusted to zero because the lateral deviation of the hot spot 19 obtains a maximum. In fact, the latter is equal to the distance C between the image centre H and the hot spot 19. It is achieved when an angle ϕ is equal to 90° . It can then be necessary to add an additional freedom of movement of the hot spot 19 with respect to the camera cage 21, for example a completely free movement of the hot spot 19 in the X and Y directions or a tangential translation superimposed on the rotary movement. In most cases, however, this will not be necessary. Perhaps other positionings and movements of the image field with respect to the hot spot are possible. They are all due to the same principle of track correction by means of feedback. As a matter of course, this principle for contour cutting may also be used for rectilinear cutting.

Figure 5 shows diagrammatically an embodiment of the pre-adaptation of the heating track 23 with rectilinear severing. A plate 3 is severed asymmetrically along a desired cutting line 7 by adaptation of the heating track 23. The heating track 23 is determined empirically or by calculations. The shape of the track 23 depends upon the

chosen heat source: a spot source or a line source.

Figure 6 shows diagrammatically an embodiment of the pre-adaptation of the heating track 23 with contour severing. Also in this case, the heating track 23 depends upon the heat source chosen. The heating track 23 does not coincide with the desired cutting line 7.

These two embodiments are based on the principle of track correction by means of positive feedback. Both with the principle of positive feedback and with the principle of feedback, the stress around the crack tip is made symmetrical so that the crack follows the desired cutting line 7.

Figure 7 shows the adaptation of the thermal load by addition of an additional heat source. A plate 3 is thermally severed asymmetrically along a straight line. In a usual manner, the desired cutting line 7 is heated by means of a linear heat source 25, but in this case further a non-uniform thermal load is provided on the narrow strip 31 by means of another linear source 27. The stress distribution 33 can now be found from the superimposition of the stress distributions 35, 37 due to both separate sources 25, 27. The additional source 27 ensures that the stress on the upper side of the crack 17 increases. With a suitable dimensioning, the stress distribution 33 will be accurately equal on either side of the crack 17 and a shear load will not be formed.

Various kinds of materials can be severed by means of the method described. The material should be brittle, however, such as, for example, glass or silicon. A great advantage is that upon severing no splinters and chips are formed, which can damage the surfaces of the narrow and wide strips. As crack initiation a provided scratch or an unevenness in the side wall of the material may be used. A major surface of the plate to be severed can be both planar and curved.

Claims

1. A method of severing a plate of brittle material (3) along a desired cutting line, in which a crack initiation is provided in a side of a plate of brittle material as initiation for a crack, after which a thermal load is provided along a heating track on at least one major surface of a plate to be severed, as a result of which stresses are produced in the plate, which, starting from the crack initiation, cause a crack transverse to the major surfaces along the desired cutting line (7), characterized in that the thermal load is provided asymmetrically with respect to the desired asymmetrical cutting line (7) in such a manner that the mechanical stresses close to a crack tip (1), which are the resultant of the asymmetrical severing of the

only the y position y_s of the crack tip 1, but also the x position x_s will change. This cross connection should be taken into account when designing the regulators.

Figure 4 shows diagrammatically the adaptation of the relative movement by feedback with contour severing. In the case of contour severing, the crack tip 1 can in principle occupy all positions with respect to the hot spot 19. The method as described in Figure 3 cannot be used here. A solution to avoid that the crack tip 1 moves out of the image field 21 of the camera, is shown in Figure 4. The desired position of the crack tip 1 coincides with the centre H of the image field 21. The centre H of the image field 21 is moved along the desired cutting line 7. From the desired cutting line 7, also the orientation of a local coordinate system is determined having as origin the centre H of the image field 21 in such a manner that the X axis is tangent to the desired cutting line 7. The position of the crack tip 1 is determined with respect to this local coordinate system. The spot 19 now cannot perform a translatory movement with respect to the camera, as in Figure 3, but can perform a rotary movement about the centre H of the image field 21. The y position y_s of the crack tip 1 is now used to adjust the position of the spot 19 with respect to the centre H of the image field 21: if y_s is positive, the spot 19 is rotated clockwise, whereas with a negative y_s the spot 19 is rotated counterclockwise. The x position x_s is used to adjust the tangential speed.

Theoretically, it would be possible that in this manner the lateral deviation is not entirely adjusted to zero because the lateral deviation of the hot spot 19 obtains a maximum. In fact, the latter is equal to the distance C between the image centre H and the hot spot 19. It is achieved when an angle ϕ is equal to 90° . It can then be necessary to add an additional freedom of movement of the hot spot 19 with respect to the camera cage 21, for example a completely free movement of the hot spot 19 in the X and Y directions or a tangential translation superimposed on the rotary movement. In most cases, however, this will not be necessary. Perhaps other positionings and movements of the image field with respect to the hot spot are possible. They are all due to the same principle of track correction by means of feedback. As a matter of course, this principle for contour cutting may also be used for rectilinear cutting.

Figure 5 shows diagrammatically an embodiment of the pre-adaptation of the heating track 23 with rectilinear severing. A plate 3 is severed asymmetrically along a desired cutting line 7 by adaptation of the heating track 23. The heating track 23 is determined empirically or by calculations. The shape of the track 23 depends upon the

chosen heat source: a spot source or a line source.

Figure 6 shows diagrammatically an embodiment of the pre-adaptation of the heating track 23 with contour severing. Also in this case, the heating track 23 depends upon the heat source chosen. The heating track 23 does not coincide with the desired cutting line 7.

These two embodiments are based on the principle of track correction by means of positive feedback. Both with the principle of positive feedback and with the principle of feedback, the stress around the crack tip is made symmetrical so that the crack follows the desired cutting line 7.

Figure 7 shows the adaptation of the thermal load by addition of an additional heat source. A plate 3 is thermally severed asymmetrically along a straight line. In a usual manner, the desired cutting line 7 is heated by means of a linear heat source 25, but in this case further a non-uniform thermal load is provided on the narrow strip 31 by means of another linear source 27. The stress distribution 33 can now be found from the superimposition of the stress distributions 35, 37 due to both separate sources 25, 27. The additional source 27 ensures that the stress on the upper side of the crack 17 increases. With a suitable dimensioning, the stress distribution 33 will be accurately equal on either side of the crack 17 and a shear load will not be formed.

Various kinds of materials can be severed by means of the method described. The material should be brittle, however, such as, for example, glass or silicon. A great advantage is that upon severing no splinters and chips are formed, which can damage the surfaces of the narrow and wide strips. As crack initiation a provided scratch or an unevenness in the side wall of the material may be used. A major surface of the plate to be severed can be both planar and curved.

Claims

1. A method of severing a plate of brittle material (3) along a desired cutting line, in which a crack initiation is provided in a side of a plate of brittle material as initiation for a crack, after which a thermal load is provided along a heating track on at least one major surface of a plate to be severed, as a result of which stresses are produced in the plate, which, starting from the crack initiation, cause a crack transverse to the major surfaces along the desired cutting line (7), characterized in that the thermal load is provided asymmetrically with respect to the desired asymmetrical cutting line (7) in such a manner that the mechanical stresses close to a crack tip (1), which are the resultant of the asymmetrical severing of the



plate and the thermal load stresses, are symmetrical with respect to the desired asymmetrical cutting line (7) when the crack tip is located on the desired cutting line.

2. A method as claimed in Claim 1, characterized in that said thermal load is provided by a spot-shaped heat source and in that the spot-shaped heat source and the plate to be severed are moved with respect to each other, a deviation of the crack with respect to the desired cutting line being fed back by measuring the position of the crack tip during severing to control the position and the speed of the heat source (5) with respect to the plate (3) and readjust the relative movement of the heat source and the plate.
3. A method as claimed in Claim 2, characterized in that both the relative speed of the spot-shaped heat source with respect to the plate in the direction of the desired cutting line and the relative displacement of the spot-shaped heat source with respect to the plate transverse to the direction of the desired cutting line are readjusted by feedback.
4. A method as claimed in Claim 1, characterized in that the thermal load is provided on the plate along a predetermined heating track, which does not coincide with the desired cutting line.
5. A method as claimed in Claim 4, characterized in that a stationary linear heat source is used, whose shape corresponds to that of the heating track.
6. A method as claimed in Claim 4, characterized in that a spot-shaped heat source is used, which is moved along the heating track by a relative movement of the heat source with respect to the plate.
7. A method as claimed in any one of the preceding Claims, characterized in that several heat sources are used.

Patentansprüche

1. Verfahren zum asymmetrischen Spalten einer Platte (3) aus sprödem Werkstoff längs einer gewünschten Schnitlinie, in der eine Rißeinleitung in einer Seite einer Platte aus sprödem Werkstoff als Rißansatz angebracht ist, wonach eine Wärmebelastung längs einer Wärmespur auf wenigstens einer Hauptfläche einer zu spaltenden Platte angebracht ist, wodurch

Spannungen in der Platte erzeugt werden, die von der Rißeinleitung ausgehend einen Riß quer zur Hauptfläche entlang der gewünschten Schnitlinie (7) bewirkt, dadurch gekennzeichnet, daß die Wärmebelastung in bezug auf die gewünschte asymmetrische Schnitlinie (7) derart asymmetrisch angebracht wird, daß die mechanischen Spannungen nahe bei einem Rißansatz (1), die das Ergebnis der asymmetrischen Spaltung der Platte und der Wärmebelastungsspannungen sind, in bezug auf die gewünschte asymmetrische Schnitlinie (7) symmetrisch sind, wenn der Rißansatz sich auf der gewünschten Schnitlinie befindet.

2. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß die thermische Belastung mit einer punktförmigen Wärmequelle angebracht wird, und daß die punktförmige Wärmequelle und die zu spaltende Platte gegeneinander verschoben werden, wobei eine Abweichung des Risses von der gewünschten Schnitlinie durch Messung der Position des Rißansatzes beim Spalten zum Steuern der Position und der Geschwindigkeit der Wärmequelle (5) in bezug auf die Platte (3) und zum Neueinstellen der relativen Bewegung der Wärmequelle und der Platte rückgekoppelt werden.
3. Verfahren nach Anspruch 2, dadurch gekennzeichnet, daß sowohl die relative Geschwindigkeit der punktförmigen Wärmequelle in bezug auf die Platte in der Richtung der gewünschten Schnitlinie und die relative Verschiebung der punktförmigen Wärmequelle in bezug auf die Platte quer zur Richtung der gewünschten Schnitlinie durch Rückkopplung neu eingestellt werden.
4. Verfahren nach Anspruch 1, dadurch gekennzeichnet, daß die Wärmebelastung auf der Platte längs einer vorgegebenen Wärmespur angebracht wird, die nicht mit der gewünschten Schnitlinie zusammenfällt.
5. Verfahren nach Anspruch 4, dadurch gekennzeichnet, daß eine statische lineare Wärmequelle verwendet wird, deren Form der der Wärmespur entspricht.
6. Verfahren nach Anspruch 4, dadurch gekennzeichnet, daß eine punktförmige Wärmequelle verwendet wird, die entlang der Wärmespur durch eine relative Bewegung der Wärmequelle in bezug auf die Platte verschoben wird.
7. Verfahren nach einem oder mehreren der vorangehenden Ansprüche, dadurch gekennzeichnet,



net, daß mehrere Wärmequellen verwendet werden.

Revendications

1. Procédé pour fendre de façon asymétrique une plaque de matériau fragile (3) le long d'une ligne de coupe désirée, selon lequel un début de fissure est pratiqué dans une face d'une plaque de matériau fragile comme début pour une fissure, après quoi une charge thermique est disposée le long d'un trajet de chauffage sur au moins une surface principale d'une plaque à fendre, de façon que des tensions se produisent dans la plaque qui, partant du début de fissure, provoquent une fissure transversale à la surface principale le long de la ligne de coupe désirée (7), caractérisé en ce que la charge thermique est disposée de façon asymétrique par rapport à la ligne de coupe asymétrique désirée (7), de façon que les tensions mécaniques se produisant à proximité d'une amorce de fissure (1) - qui sont le résultat du fendage asymétrique de la plaque et des tensions de charge thermiques - soient symétriques par rapport à la ligne de coupe asymétrique désirée (7), lorsque l'amorce de fissure se situe sur la ligne de coupe désirée.

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2. Procédé selon la revendication 1, caractérisé en ce que ladite charge thermique est fournie par une source de chaleur ponctuelle et en ce que la source de chaleur ponctuelle et la plaque à fendre sont déplacées l'une par rapport à l'autre, une déviation de la fissure par rapport à la ligne de coupe désirée étant rétrocouplée par mesure de la position de l'amorce de fissure pendant le fendage pour commander la position et la vitesse de la source de chaleur 5 par rapport à la plaque 3 et corriger le mouvement relatif de la source de chaleur et de la plaque.

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3. Procédé selon la revendication 2, caractérisé en ce que la vitesse relative de la source de chaleur ponctuelle par rapport à la plaque dans la direction de la ligne de coupe désirée et le déplacement relatif de la source de chaleur ponctuelle par rapport à la plaque transversale à la direction de la ligne de coupe désirée sont corrigés par rétrocouplage.

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4. Procédé selon la revendication 1, caractérisé en ce que la charge thermique est disposée sur la plaque le long d'un trajet de chauffage préalablement déterminé, qui ne coïncide pas avec la ligne de coupe désirée.

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5. Procédé selon la revendication 4, caractérisé par l'utilisation d'une source de chaleur linéaire stationnaire, dont la forme correspond à celle du trajet de chauffage.

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6. Procédé selon la revendication 4, caractérisé par l'utilisation d'une source de chaleur ponctuelle qui est déplacée le long du trajet de chauffage par un déplacement relatif de la source de chaleur par rapport à la plaque.

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7. Procédé selon l'une des revendications précédentes, caractérisé par l'utilisation de plusieurs sources de chaleur.

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