

PROCESS FOR TRANSPORTING THERMALLY UNSTABLE VISCOUS MASSES

The invention is concerned with a process for transporting thermally unstable viscous masses. In particular, the present invention is concerned with a process for transporting a dope containing cellulose and an aqueous tertiary amine-oxide.

For the purposes of the present specification and claims, the term dope is used for any viscous mass containing cellulose and an aqueous tertiary amine-oxide able to be processed to cellulose moulded bodies of any shape, particularly fibres and films.

Tertiary amine-oxides have been known as alternative solvents for cellulose. It is known for instance from US-PS 2,179,181 that tertiary amine-oxides are capable of dissolving cellulose without derivatisation and that from these solutions cellulose moulded bodies, such as fibres, may be produced by precipitation. From EP-A - 0 553 070 of the applicant, further tertiary amine-oxides are known. In the following, all tertiary amine-oxides capable of dissolving cellulose are meant when, for the sake of simplicity, only NMMO (= N-methylmorpholine-N-oxide) is cited.

As alternative solvents, tertiary amine-oxides are advantageous insofar as the cellulose is dissolved by the NMMO without derivatisation, contrary to the viscose process. Thus the cellulose does not have to be chemically regenerated, the NMMO remains chemically unchanged and passes during its precipitation into the precipitation bath and may be recovered from the latter and reused for the preparation of new solution. Therefore the NMMO process offers the possibility of a closed solvent cycle. Additionally, NMMO has an extremely low toxicity.

However, when cellulose is dissolved in NMMO, the polymerisation degree of the cellulose decreases. Moreover, particularly the presence of metal ions (such as Fe^{3+}) leads to radically initiated chain cleavages and thus to a

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significant degradation of the cellulose and the solvent (Buijtenhuijs et al. The Degradation and Stabilization of Cellulose Dissolved in N-Methylmorpholin-N-Oxide (NMM), in "Das Papier", Volume 40, number 12, pages 615-619, 1986).

On the other hand, amine-oxides generally have only a limited thermal stability which varies depending on their structure. Under normal conditions, the monohydrate of NMMO is present as a white crystalline solid, which melts at 72°C. Its anhydric compound however melts at no less than 172°C. When heating the monohydrate, strong discoloration will occur from 120/130°C up. From 175°C up, an exothermal reaction is initiated, the melted mass being completely dehydrated and great amounts of gas developing which eventually lead to an explosion, the temperatures rising to far over 250°C.

It is known that metallic iron and copper and particularly their salts significantly reduce the decomposition temperature of NMMO, while the decomposition rate is simultaneously increased.

Moreover, additionally to the problems mentioned above, there is another difficulty, i.e. the thermal instability of the NMMO/cellulose solutions themselves. This means that at the elevated processing temperatures (approximately 110-120°C), uncontrollable decomposition processes are initiated in the solutions which due to the development of gases may lead to strong deflagrations, fires and even explosions.

It is evident that the decomposition products of the cellulose and the amine-oxide have a negative effect on the mechanical properties of the cellulose moulded body. This applies particularly to the production of fibres and films. Thus efforts are made on the one hand to prevent the formation of decomposition products by adding stabilizers and on the other to keep the residence time of the cellulose solution to be processed as short as possible. These efforts however have a limit, since at an industrial scale usually

significantly more cellulose solution per time unit is produced than can be taken up by e.g. a spinneret. When several spinnerets are used, the problem of dividing the dope arises, a number of partial streams or flows being provided wherein different decomposition processes will occur, the products of which will influence the mechanical properties of each of the moulded bodies in a different way. This means again that the production of moulded bodies having uniform properties cannot be assured by the industrial process.

This is the starting point of the present invention: It is its object to provide a process for transporting thermally unstable viscous masses, particularly a process for transporting a dope containing cellulose and an aqueous tertiary amine-oxide, which do not exhibit the above problems.

The process according to the invention for transporting a thermally unstable viscous mass through pipes is characterized in that

- (a) during transportation, the mass is divided into X_1 partial flows T_1 , X_1 being calculated according to the relation

$$X_1 = Q(N-1), \quad (I)$$

wherein Q and N indicate positive integers independent from each other, and

- (b) the viscous mass in the partial flows is transported at the same rate.

It has been shown that when the mass is divided into partial flows it is of vital importance to transport the mass in the partial flows at the same rate through the pipes. Thus it is assured that the mass which finally arrives at the forming tool has the same thermal history, so that moulded bodies having uniform properties may be produced.

From WO 94/28208 it is known to transport a solution of cellulose in NMMO through a branching valve whereby the solution is optionally directed to one of two filters. Under normal operation, one filter is always in a "stand-by" position. To provide a continuous operation while the filter is changed, during the time one filter is being changed the other filter is operated. Moreover, it is mentioned that by adjusting the branching valve in an intermediate position, the solution may be divided into two flows and transported to two filters. To those skilled in the art however, it is not evident from WO 94/28208 that the cellulose solutions are to be transported at the same rate, thus allowing a uniform quality of the moulded bodies.

To promote the uniform thermal history of the mass, static mixers may be employed to level the temperature and viscosity differences possibly present in the mass.

When dividing the mass into partial flows, it is best assured by means of a reduction of the pipe diameters that the rate does not drop due to the reduction of its volume when the mass is divided. Thus a uniform rate profile is achieved which is particularly advantageous regarding an equal residence time.

A preferred embodiment of the process according to the invention consists in that the X_1 partial flows T_1 are further divided into X_2 partial flows T_2 , X_2 being calculated according to the relation

$$X_2 = X_1 \cdot Q^{(N-1)}, \quad (II)$$

wherein Q and N denote positive integers independent from each other.

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It is further preferred to divide the X_2 partial flows T_2 into X_3 partial flows T_3 , X_3 being calculated according to the relation

$$X_3 = X_2 \cdot Q^{(N-1)}, \quad (\text{III})$$

wherein Q and N denote positive integers independent from each other.

Each of the partial flows T_3 may be divided at least one more time.

Q denotes preferably the number 2.

It is further preferred that in the relations (I), (II) and (III), Q refers to different integers.

N denotes preferably an integer between 2 and 12, preferably between 5 and 10.

A preferred embodiment of the process according to the invention consists in transporting the same amount of viscous mass per time unit in each of the X_1 partial flows T_1 , in each of the X_2 partial flows T_2 and in each of the X_3 partial flows T_3 .

It has been shown that the process according to the invention is particularly appropriate to transport a solution of cellulose in an aqueous, tertiary amine-oxide, the cellulose solution being best divided into X_n partial flows and being transported to X forming tools, particularly spinnerets.

The dividing of the viscous mass is best carried out in a pipe component shown in the attached drawing.

In the drawing, a pipe element for dividing a mass flow is shown. The transport direction of the mass is indicated by arrows.

The pipe element consists of a crosspiece 1 whereby the mass flow is divided into two equal partial flows. The feeding of the mass and the branching of the partial flows is carried out conveniently by means of transportation elements such as pumps. When highly viscous masses are transported, as is the case in the NMMO system, transportation will be carried out by forced transportation elements such as gear pumps etc. Between the crosspieces, different elements such as mixers, heat exchangers and pumps may be incorporated.

Crosspiece 1 is attached to a feeding pipe 3 by means of a flange 2 in a conventional manner. Between feeding pipe 3 and crosspiece 1 a seal 4 is provided. Similarly, crosspiece 1 is attached at its branchings 5a and 5b to counterflanges 7a and 7b respectively of branchings 8a and 8b by means of flanges 6a and 6b. Between flanges 6a, 6b and 7a, 7b respectively, seals 9a and 9b respectively are provided.

In crosspiece 1, a jacket 10 for a heating medium or a cooling medium is provided, whereby the temperature of the flowing viscous mass may be adjusted and controlled. Such heating jackets are also provided in counterflanges 7a, 7b of branchings 5a and 5b respectively and in the flange of feeding pipe 3. As a heating medium, water, vapour or thermo oil may be employed. As a cooling medium, water or thermo oil may be employed.

By means of providing crosspieces as the one shown in the drawing subsequently to each other, the mass flow may be divided into additional partial flows. Thus, according to the invention, 4, 8, 16, 32 etc. partial flows may be provided, depending on the number of crosspieces used. In this case, the number Q in the above mathematical relation therefore is 2.

Although the embodiment described above is preferred, it is also possible to divide the mass flow into 3 partial flows,

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whereby 3, 9, 27 etc. partial flows are provided. Therefore, in this case Q is the number 3.

Furthermore it may be provided that Q denotes different numbers in the divisions, e.g. the number 2 for a part of the divisions and the number 3 for the rest of the divisions.



CLAIMS:

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1. A process for transporting a thermally unstable viscous mass through pipes, characterized in that

(a) during transportation, said mass is divided into X_1 partial flows T_1 , X_1 being calculated according to the relation

$$X_1 = Q(N-1),$$

(I)

$$Q = 1 \quad N = 2$$

2	3
3	4

wherein Q and N indicate positive integers independent from each other, and

- (b) the viscous mass in said partial flows is transported at the same rate.

$$X_1 = 1 \quad X_1 = 2 \quad X_1 = 3$$

2	4	9
3	8	27

2. A process according to Claim 1, characterized in that said X_1 partial flows T_1 are further divided into X_2 partial flows T_2 , X_2 being calculated according to the relation

$$X_2 = X_1 \cdot Q(N-1),$$

(II)

wherein Q and N denote positive integers independent from each other.

3. A process according to Claim 2, characterized in that said X_2 partial flows T_2 are further divided into X_3 partial flows T_3 , X_3 being calculated according to the relation

$$X_3 = X_2 \cdot Q(N-1),$$

(III)

wherein Q and N denote positive integers independent from each other.

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4. A process according to Claim 3, characterized in that each of said partial flows T_3 is divided at least one more time.
5. A process according to one of the Claims 1 to 4, characterized in that Q denotes the number 2.
6. A process according to one of the Claims 1 to 4, characterized in that in the relations (I), (II) and (III), Q denotes different integers.
7. A process according to one of the Claims 1 to 6, characterized in that N denotes an integer between 2 and 12, preferably between 5 and 10.
8. A process according to one of the Claims 1 to 7, characterized in that the same amount of viscous mass per time unit is transported in each of said X_1 partial flows T_1 , in each of said X_2 partial flows T_2 and in each of said X_3 partial flows T_3 .
9. A process according to one or more of the Claims 1 to 8, characterized in that as a thermally unstable, viscous mass, a solution of cellulose in an aqueous, tertiary amine is used.
10. A process according to one of the Claims 1 to 9, characterized in that said X_n partial flows of said cellulose solution are transported to X forming tools, particularly spinnerets.



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