

TV/FM receiver for multi-media applications. ✓

5 The invention relates to a receiver for receiving first type of reception signals, for example TV signals, and second type of reception signals, for example FM-radio signals. The invention also relates to a multi-media apparatus incorporating such a receiver. The receiver may enhance the functionality of the multi-media apparatus with TV and FM-radio reception, for example. The multi-media apparatus may be in the form of a personal computer (PC) having slots in which add-on cards are plugged in. The receiver may be implemented on one of these add-on cards. Accordingly, the PC can access information transmitted by FM-radio and TV stations.

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15 A receiver capable of receiving TV and FM-radio signals is described in US-A 5,148,420. In the prior art receiver, both TV and FM-radio signals are supplied to a single tuner via a common RF input. The single tuner converts a particular reception signal to a fixed intermediate frequency (IF) of approximately 40 MHz, which is common for TV reception. The IF signal produced by the tuner, is processed differently for TV or FM-radio reception. For TV reception, the IF signal is processed in a manner which is very similar to IF signal processing in most present-day receivers. For FM-radio reception, the IF signal is supplied to a single chip FM-radio integrated circuit (IC) via a filter unit. In the FM-radio IC, the IF signal is frequency converted to obtain a nominal 20 10,7 MHz FM IF signal, which is further processed in a common manner.

Although the prior art receiver is capable of retrieving information from both TV and FM-radio signals received at the common RF input, the flexibility of the prior art receiver is relatively low.

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An object of the invention is to provide a receiver which is more flexible in retrieving information, than the above described prior art receiver.

According to one aspect of the invention, there is provided a receiver as

defined in Claim 1.

According to another aspect of the invention, a multi-media apparatus comprises such a receiver.

Yet another aspect of the invention provides a tuner as defined in Claim 4.

5 The invention may be used in reception of both TV and FM-radio signals. In an example of such a use, a tuner for receiving both TV and FM-radio signals has an input section which comprises two inputs to which reception signals can be applied. One input may, for example, be coupled to a cable network via which reception signals are distributed. The other input may, for example, be used to plug-in a simple wire antenna. 10 Such a wire antenna will in many cases be sufficient to receive local stations with acceptable quality. The invention takes into consideration that local stations, or any other on-air reception signal, may not always be offered by the cable network.

The invention is particularly suited for multi-media applications. As indicated in the opening paragraph, a receiver in accordance with the invention, may be 15 implemented on an add-on card. The flexibility offered by the invention, may further enhance the functionality of the add-on card. This makes that the add-on card can be applied in a great variety of multi-media applications.

Advantageously, the input section comprises a switch for effectively decoupling at least one of the two inputs from the tuner. This embodiment of the 20 invention takes into consideration that user-made wire antennas have an undefined impedance. The undefined impedance at the wire antenna input, may affect reception of cable network signals received via the other input. The switch can electrically isolate the undefined impedance from the tuner.

Advantageously, a multi-band tuner is used for processing a reception 25 signal in one of a plurality of branches depending on the frequency of the reception signal, and the switch is coupled to an input of one branch. Accordingly, reception signals which are processed in the other branches effectively by-pass the switch. This embodiment of the invention takes into consideration that, in practice, most switches have to some extent non-linearities. Such non-linearities may impair the reception quality, for 30 example, by causing intermodulation.

The invention will hereinafter be described in greater detail with reference to examples shown in the drawings. Furthermore, advantageous implementation details



which are defined in the dependent Claims, will also be described with reference to the examples shown.

5 In the drawings:

Fig. 1 shows an example of a tuner in accordance with the invention in the form of a block diagram;

Fig. 2 shows, in a circuit diagram form, an example of a switchable input section for conveying signals to various branches in the Fig. 1 tuner;

10 Fig. 3 shows, in a circuit diagram form, an example of a preferred switchable input section for conveying signals to various branches in the Fig. 1 tuner; and

Fig. 4 shows, in an abstract diagram form, an example of a multi-media apparatus comprising the Fig. 1 tuner.

Like elements have like reference signs throughout the drawings.

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The invention will be exemplified by means of the Fig. 1 tuner, which tuner can receive both TV and FM-radio signals. To that respect, implementation aspects of the Fig. 1 tuner will also be discussed with reference to Figs. 2 and 3, and an example of a multi-media application of the Fig. 1 tuner will be discussed with reference to Fig. 20 4. Finally, some remarks are made so as to indicate that the scope of the invention claimed, is well beyond the examples shown in the Figures.

Referring to the Fig. 1 tuner, TV and FM-radio signals may be applied at inputs TVIN and FMIN, respectively. The Fig. 1 tuner receives tuning control data TCD 25 relating to a desired reception signal, for example the frequency and the type of signal: TV or FM. In response to the desired reception signal, the Fig. 1 tuner provides an intermediate frequency signal IFS at an output IFOUT.

The Fig. 1 tuner can operate in two modes: a TV-mode if the desired reception signal is a TV signal, or an FM-mode if the desired reception signal is an 30 FM-radio signal. In TV-mode, the intermediate frequency signal IFS is at an intermediate frequency of 38,9 MHz, hereinafter abbreviated to TV-IF. In FM-mode, the intermediate frequency signal IFS is at an intermediate frequency of 10,7 MHz, hereinafter abbreviated

to FM-IF.

The Fig. 1 tuner is based on a so-called three band concept. This means that the Fig. 1 tuner comprises three separate branches for processing the TV signals in three respective frequency bands: high-band, medium-band and low-band. Each branch comprises the following parts: an input filter RFI-H/-M/-L, an input amplifier RFA-H/-M/-L, a band-pass filter BPF-H/-M/-L, a mixer MIX-H/-M/-L, an oscillator circuit OSC-H/-M/-L and an oscillator resonance circuit ORC-H/-M/-L. The suffixes -H, -M and -L used in the reference signs for these parts, indicate whether a relevant part belongs to the high-, medium- or low-band branch. The Fig. 1 tuner may be implemented using a mixer-oscillator integrated circuit MOIC, for example of the type TDA 5736 manufactured by Philips Semiconductors, which comprises the parts present within the dotted rectangle designated MOIC in Fig. 1.

In the Fig. 1 tuner, FM-radio signals are processed in the low-band branch. A switch SWIN couples the low-band branch either to the input TVIN or to the input FMIN. In the first case, TV signals are supplied to the low-band branch, in the other case FM-radio signals are supplied to the low-band branch. The position of the switch SWIN may depend on the mode, TV or FM, in which the Fig. 1 tuner operates. However, in some applications it may be preferable to control the switch SWIN independently of the mode. For example, FM-radio signals may be present both at the input TVIN and at the input FMIN. In that case, it may be advantageous to select the position of the switch SWIN, in FM-mode, for best FM-radio reception. A kind of antenna diversity is provided. One antenna may be a wire antenna coupled to the input FMIN, for example, the other antenna may be a VHF/TV antenna, for example, via which FM-radio signals can also be received.

In each branch, the input filter RFI-H/-M/-L attenuates signals which are relatively frequency distant from the desired reception signal, to prevent overload of the input amplifier RFA-H/-M/-L. The amplifier RFA-H/-M/-L is controlled by a gain control voltage V_{agc}. The band-pass filter BPF-H/-M/-L provides a further attenuation of undesired signals. The mixer MIX-H/-M/-L effects a frequency shift of the desired reception signal, by multiplying the desired reception signal with an oscillator signal OSS-H/-M/-L. The oscillator signal OSS-H/-M/-L is generated by the oscillator circuit OSC-H/-M/-L and the oscillator resonance circuit ORC-H/-M/-L, which determines the

frequency of the oscillator signal OSS-H/-M/-L. The mixer provides, via an intermediate frequency amplifier IFAMP, the intermediate frequency signal IFS.

In each branch, a phase-lock circuit PLL controls the oscillator signal OSS-H/-M/-L of the relevant branch. The phase-lock circuit PLL derives, in a conventional manner, a tuning voltage V_{tun} from the tuner control data TCD and the oscillator signal OSS-H/-M/-L received via an oscillator signal amplifier OSSA. The tuning voltage V_{tun} is applied to the oscillator resonance circuit ORC-H/-M/-L. In TV-mode, the oscillator signal OSS-L in the low band-branch, is set to a frequency which is the sum of the desired reception signal and the TV-IF (38,9 MHz). In FM-mode, the oscillator signal OSS-L is set to a frequency which is the sum of the desired reception signal and the FM-IF (10,7 MHz).

In each branch, the tuning voltage V_{tun} is also used to vary the respective pass bands of the input filter RFI-H/-M/-L and the band-pass filter. Preferably, the pass bands should encompass the desired reception signal. If not, the desired reception signal is distorted and undesired signals may not be sufficiently attenuated. In TV-mode, the pass bands should encompass the difference of the oscillator signal frequency and the TV-IF. In FM-mode, the pass bands should be centred at the difference of the oscillator signal frequency and the FM-IF. The position of the pass bands with respect to the frequency of the oscillation signal, while tuning over the reception bands, is hereinafter referred to as tracking.

The phase-lock circuit PLL also provides a mode switch signal TV/FM. In the low-band branch, the mode switch signal TV/FM is used to switch the oscillator resonant circuit ORC-L. The oscillator signal OSS-L is switched to a higher frequency in TV mode than in FM-mode, for a given value of the tuning voltage V_{tun} . Respective pass-bands of the input filter RFI-L and the band-pass filter BPF-L, remain substantially constant for a given value of the tuning voltage V_{tun} . Thus, the frequency offset between the input filter RFI-L and the band-pass filter BPF-L, on the one hand, and the oscillator signal OSS-L, on the other hand, is switched. The frequency offset preferably switched to the TV-IF in TV-mode and to the FM-IF in FM-mode.

In addition, the mode control signal TV/FM preferably switches the pass-bandwidth of the band-pass filter BPF-L in the low-band branch. In TV-mode, the pass band of the band-pass filter BPF-L is preferably relatively wide, for example 10

MHz, whereas in FM-mode the pass band is preferably relatively narrow, for example 1 MHz.

Fig. 2 shows, in a circuit diagram form, an example of a switchable input section for conveying signals at the inputs TVIN and FMIN to the low-band, medium-band and high-band branches in the Fig. 1 tuner. It should be noted that the switch SWIN shown in Fig. 1 is rather a functional representation of the Fig. 2 input section, than an electrical equivalent. The Fig. 2 input section not only provides switching, but also includes circuitry for suitably routing high-band, mid-band and low-band TV signals from the input TVIN to the relevant branches.

The Fig. 2 input section is based on a prior art TV-RF input circuit which is described in US-A 4,851,796, incorporated by reference herein. Elements in Fig. 2 which correspond to the prior art TV-RF input circuit are the following: an image trap 10, inductances L1, L2 and L3, and a capacitor C. In Fig. 2, the reference signs of the aforementioned elements are identical to reference signs of corresponding elements in the Figure of US-A 4,851,796 which shows the prior art TV-RF input circuit.

In accordance with the present example of the invention, the Fig. 2 input section comprises four switching diodes D1, D2, D3 and D4, respectively. In FM-mode, switching diodes D2 and D4 are conducting, while switching diodes D1 and D3 are both non-conducting. In TV-mode, the switching diodes D1 and D3 are conducting, while the switching diodes D2 and D4 are non-conducting. The four switching diodes D1, D2, D3 and D4, may be controlled by the mode control signal TV/FM, present in the Fig. 1 tuner, in a common manner. However, in some applications it may be preferable to control the switch SWIN independently from the mode, TV or FM, in which the tuner operates. Accordingly, in those applications a separate control signal will be used for controlling the switch SWIN.

In the Fig. 2 input section, in TV-mode, the switching diode D1 effectively short-circuits the input FMIN to which FM-radio signals are applied. This promotes the reception quality of high-band TV signals in particular, which can be explained as follows.

The source connected to the input FMIN may not have a well-defined impedance. For example, it is very well possible that a user just connects a piece of wire, as this often will be sufficient to receive local FM-radio stations with sufficient quality. The impedance of such a wire-antenna is quite undefined and, moreover, the impedance

may vary considerably over the TV frequency range from 48 to 855 MHz approximately. If the input FMIN is not sufficiently isolated from the TV-RF input circuit, this may affect the power matching between the source connected to the input TVIN and the relevant input filter RFI-H/-M/-L.

5 In TV-mode, the switching diodes D2 and D4 provide isolation. However, in TV-mode the switching diodes D2 and D4 are reverse biased and have parasitic capacitances. As a result, the isolation becomes weaker and weaker with increasing frequency. Depending on, for example, the wire-antenna connected to the input FMIN, it may happen that an insufficient amount of TV signal power is transferred to the relevant
10 input filter. Especially the high-band TV signals may be affected in that sense. The above described problem is solved by effectively short-circuiting the input FMIN in TV-mode.

In the Fig. 2 input section, the isolation is provided, as already mentioned, by the switching diodes D2 and D4, which are in a back-to-back configuration. This additional feature also promotes the reception quality of high-band signals, which can be
15 explained as follows. In practice, the parasitic capacitance of the isolation of the input FMIN may form, in combination with a parasitic inductance of a connection for example, a parasitic resonant circuit which causes poor matching. By halving the parasitic capacitance, for example, the parasitic resonant circuit may be de-tuned sufficiently to obtain satisfactory power matching.

20 The Fig. 2 input section comprises a resistance R2 in series with the switching diode D3. Depending on the state of the switching diode D3, the resistance R2 does or does not affect the characteristics of the input filter RFI-L, which is shown in detail. The input filter RFI-L is basically a parallel resonance circuit, which includes an inductance L4. In FM-mode, the switching diode D3 is non-conducting, such that the
25 resistance R2 is effectively isolated from the parallel resonance circuit, which has a relatively high quality factor. In TV-mode, however, the switching diode D3 conducts and the resistance R2 effectively reduces the quality factor of the parallel resonance circuit in the input filter RFI-L. This produces the advantageous effect that, in FM-mode, the bandwidth of the input filter RFI-L is narrower than in TV-mode.

30 In the Fig. 2 input section, the input FMIN is coupled to switching diodes D1 and D4 via an FM input filter. The FM input filter is formed by two inductances L5 and L6 and a capacitance C1. Elements in Fig. 2 which have no reference signs, are used

for suitably coupling AC and/or DC signals, as a skilled worker will immediately recognize. Consequently, those elements need not to be further discussed in this specification.

Fig. 3 shows, in a circuit diagram form, a preferred input section for conveying signals at the inputs TVIN and FMIN to the low-band, medium-band and high-band branches in the Fig. 1 tuner. Like the Fig. 2 input section, the Fig. 3 input section is based on the prior art TV-RF input circuit described in US-A 4,851,796. However, in accordance with the present example of the invention, in the Fig. 3 input section, low-band TV signals at the input TVIN are routed to the low-band branch in a different manner than in the Fig. 2 input section. In the Fig. 3 input section, low-band TV signals are applied to the input filter RFI-L via the input filter RFI-H in the high-band branch.

In Fig. 3, the input filter RFI-H in the high-band branch, through which low-band TV signals are routed, is shown in detail. The input filter RFI-L comprises an inductance LH, a varicap diode CHvar and a capacitance CHpad, which constitute a parallel resonance circuit. A signal in the parallel resonance circuit is tapped off via a series arrangement of an inductance LHtap and a capacitance CHtap. The value of the inductance LH in the input filter RFI-H should be suitable for tuning the parallel resonance circuit in the high-band. Consequently, the impedance of the LH in the low-band is relatively small and may, by way of approximation, be seen as a short-circuit in the low-band.

The Fig. 3 input section comprises three switching diodes D1A, D2A and D3A, instead of four as in the Fig. 2 input section. When switching diode D1A is conducting, one end of the parallel resonance circuit in the input filter RFI-H is effectively coupled to ground. However, when the switching diode D1A is non-conducting, a low-band TV signal may be transferred via the input filter RFI-H to the input filter RFI-L. For such a transfer, switching diode D2A should be in a conductive state. Switching diode D3A provides, when switched to a non-conductive state, a satisfactory isolation of the input FMIN from the TV-RF circuit. A switching diode for effectively short-circuiting the input FMIN, like the switching diode D1 in Fig. 2, is not present in the Fig. 3 input section.

The Fig. 3 input section can be put in four switching states: TV-low, TV-mid, TV-high and FM. Table 1 below lists the relation between the switching state and the state of each of the three switching diodes individually. In the table 1, a 0 indicates that the relevant switching diode is in a non-conductive state, and a 1 indicates that it is in a conductive state.

	D1A	D2A	D3A
TV-low	0	1	0
TV-mid	0	0	0
TV-high	1	0	0
FM	1	0	1

Table 1.

In Fig. 3, each of the three switching diodes D1A, D2A and D3A receives an individual control signal S(D1A), S(D2A) and S(D3A), respectively. The control signals may be obtained, for example, from the phase-lock circuit PLL via a band-switching logic circuit, not shown.

In the TV high-band switching state, any undefined impedance at the input FMIN, is very well electrically isolated from the high-band branch. This is, because all the three switching diodes D1A, D2A and D3A effectively contribute to that isolation. In the TV high-band switching state, switching diodes D2A and D3A are non-conducting and the switching diode D1A is conducting. In the FM switching state, the switching diodes D3A is conducting for conveying an FM-radio signal at the input FMIN to the low-band branch. The switching diode D1A and the switching diode D2A is non-conducting to electrically isolate the input TVIN from the low-band branch.

In the Fig. 3 input section, an inductance L1A is coupled in series with the resistor R2, whose function was already explained with reference to Fig. 2. The inductance L1A tunes the input filter RFI-L differently in TV-mode and in FM-mode. Referring to the Fig. 1 tuner, the difference in tuning may advantageously be used to compensate for any de-tuning of the band-pass filter BPF-L, as a result of pass-band switching of this filter. With an appropriate value of the inductance L1A, the pass-bands of the input filter RFI-L and the band-pass filter BPF-L are substantially matched.

Elements in Fig. 3 which have no reference signs, are used for suitably coupling AC and/or DC signals, as a skilled worker will immediately recognize. Consequently, those elements need not to be further discussed in this specification.

Fig. 5 shows an example of a multi-media apparatus comprising the Fig. 1 tuner TUN. The Fig. 1 tuner TUN is implemented on an add-on card PCAO, which add-on card PCAO is plugged into an add-on card holder HOL of the multi-media apparatus. Apart from the Fig. 1 tuner TUN, the add-on card includes TV IF signal processing circuitry TVIFC and FM IF signal processing circuitry FMIFC. The latter circuitries receive the intermediate frequency signal IFS provided by the Fig. 1 tuner TUN via an IF splitting filter IFSF. The Fig. 1 tuner TUN, the IF splitting filter IFSF and the TV IF signal processing circuitry TVIFC are housed in a shielded metal box SMB. The shielded metal box SMB with the aforementioned parts may, as such, be manufactured and sold to add-on card manufacturers.

The Fig. 5 multi-media apparatus includes a user interface UIF, a control unit CCU, a picture display device PDD, a sound reproduction unit SRU. A user selects the desired reception signal via the user interface UIF. For example, he may enter a program number on a key-board which is part of the user-interface UIF. The control unit CCU effectively controls the add-on card PCAO, such that the Fig. 1 tuner TUN selects the desired reception signal. For example, the control unit CCU provides instructions which are stored in a memory, not shown, relating to the frequency of the desired reception signal and the type of signal: FM or TV. These instructions are supplied to the Fig. 1 tuner TUN in the form of the tuner control data TCD. The add-on card PCAO provides sound and/or video information, for example, obtained from the desired reception signal, which information may be further processed in the control unit CCU. The sound and/or video information is provided to the user via the sound reproduction unit SRU and the picture display device PDD, respectively.

Evidently, the invention may be implemented differently from the examples described above. To that respect, any reference signs in a claim cannot be construed as limiting the claim concerned. To indicate that the scope of the invention claimed is well beyond the examples described above, some final remarks are made.

It should be noted that the invention is not limited to combined TV and FM-radio reception.

It should be noted that the invention is not limited to two different types of reception signals.

It should be noted that the invention is not limited to two inputs, such as the inputs TVIN and FMIN. If so desired, more inputs can be used.

5 It should be noted that the invention is not limited to multi-media applications. The invention may be used in any apparatus comprising a receiver, such as TV receivers and video-tape recorders.

10 It should be noted that the invention is not limited to a 3 band tuner concept, as shown in Fig. 1. The invention may, in principle, be applied in any tuner concept, for example in a 2 band tuner concept.

 It should be noted that the invention is not limited to the use of an RF-TV input circuit as described in US-A 4,851,796.

15 It should be noted that more or less switching diodes can be used. For example, in the Fig. 2 input section, any one of the switching diodes D2 and D4 may be dispensed with. The switching diode D4 may be replaced by a capacitor, for example.



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Claims:



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1. A receiver for receiving first type of reception signals and second type of reception signals, the receiver comprising:

an input section (TVIN, FMIN, SWIN) for receiving a reception signal;

5 a tuner (TUN) for providing, in response to the reception signal, an intermediate frequency signal (IFS);

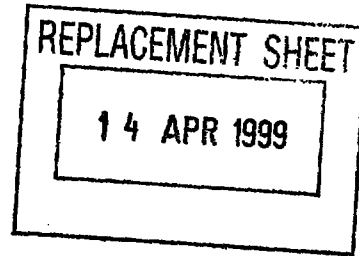
a first intermediate frequency signal processing arrangement (TVIFC) coupled to process said intermediate frequency signal (IFS) when receiving said first type of reception signals; and

10 a second intermediate frequency signal processing arrangement (FMIFC) coupled to process said intermediate frequency signal (IFS) when receiving said second type of reception signals, characterized in that said input section (TVIN, FMIN, SWIN) comprises a plurality of inputs (TVIN, FMIN) to which the reception signal may be applied.

15 2. A receiver as claimed in Claim 1, characterized in that said input section (TVIN, FMIN, SWIN) comprises a switch (SWIN) for effectively decoupling at least one of said plurality of inputs from the tuner (TUN).

20 3. A receiver as claimed in Claim 2, characterized in that said tuner (TUN) is of the multi-band type for processing the reception signal in one of a plurality of branches (RFI-L ..., RFI-M ..., RFI-H ...) depending on the frequency of the reception signal, and in that said switch (SWIN) is coupled to an input of one (RFI-L ...) of said plurality of branches.

25 4. A tuner for receiving first type of reception signals and second type of reception signals, the tuner comprising:
an input section (TVIN, FMIN, SWIN) for receiving a reception signal;



Claims:

1. A receiver for receiving reception signals of a first and a second type, the receiver comprising:
 - an input section (TVIN, FMIN, SWIN) for receiving reception signals;
 - a tuner (TUN) for providing, in response to the reception signals,
- 5 intermediate frequency signals (IFS);
 - a first intermediate frequency signal processing arrangement (TVIFC) coupled to process said intermediate frequency signals (IFS) when receiving said first-type reception signals; and
 - a second intermediate frequency signal processing arrangement (FMIFC)
- 10 coupled to process said intermediate frequency signals (IFS) when receiving said second-type reception signals,
 - characterized in that said input section (TVIN, FMIN, SWIN) comprises a plurality of inputs (TVIN, FMIN) to which the reception signals may be applied, and a switch (SWIN) for effectively decoupling at least one of said plurality of inputs from the tuner (TUN).
- 15
2. A receiver as claimed in Claim 1, characterized in that said tuner (TUN) is of the multi-band type for processing the reception signals in one of a plurality of branches (RFI-L .., RFI-M .., RFI-H ..) depending on the frequency of the reception signals, and in that said switch (SWIN) is coupled to an input of one (RFI-L ..) of said plurality of branches.
- 20
3. A tuner for receiving reception signals of a first and a second type, the tuner comprising:
 - an input section (TVIN, FMIN, SWIN) for receiving reception signals; and
 - a mixer-oscillator arrangement (MOIC) for providing, in response to the
- 25 reception signals, an intermediate frequency signal (IFS),
 - characterized in that said input section (TVIN, FMIN, SWIN) comprises a plurality of inputs (TVIN, FMIN) to which the reception signals may be applied, and a switch (SWIN) for effectively decoupling at least one of said plurality of inputs from the tuner (TUN).



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and

a mixer-oscillator arrangement (MOIC) for providing, in response to the reception signal, an intermediate frequency signal (IFS), characterized in that said input section (TVIN, FMIN, SWIN) comprises a plurality of inputs (TVIN, FMIN) to which the reception signal may be applied.

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5. A multi-media apparatus comprising:
a receiver as claimed in Claim 1; and
a control unit (CCU) for controlling said receiver and for processing data
10 signals.

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