

Improvement In Rotary Displacement Machines having Rotors of Asymmetrical Profile

The invention relates to an improvement in rotary displacement machines.

5 The invention concerns rotary displacement machines intended to receive compressible fluids and able to be used as pumping machines, even as engines.

 The invention concerns more particularly, but not in a limiting way, the machines which comprise a housing and at least two twinned rotors, i.e. a
10 first rotor and a second rotor, said rotors being mounted rotating in said housing and driven in directions which are opposed, one with respect to the other.

 The rotors are conventionally composed of pieces of screw shape, i.e. pieces comprising a core bearing one or more threads of which the pitch can be constant or variable along the longitudinal dimension of said rotor.

15 In the housing, the screws form a series of "chambers without connections" for which the leaks due to operational play as well as to the architecture and the geometry of the machine influence the volumetric efficiency, the energy efficiency as well as the final pressure obtained.

 Owing to the fact that the rotors mesh in the manner of toothed
20 wheels, one looks upon the thread or threads as each constituting a tooth situated projecting on the central core.

 The rotors can be represented in section according to a transverse plane approximately orthogonal to the longitudinal axes of their core.

 On the sections, one can observe the shape of each tooth, and, to be
25 precise, note that the outer contour of this tooth is defined by two opposite flanks, i.e. a first flank and a second flank which each extend between

- the core of the rotor being considered, and
- a portion of the tooth which is situated at a predetermined distance from the core and at the level of which said first flank and second flank are connected.

5 One distinguishes in general between three categories of rotors according to the cross section of the tooth or teeth of these rotors, and, to be precise, rotors with cross sections referred to as mating, rotors with profiles referred to as symmetrical, and rotors with profiles referred to as asymmetrical.

10 As concerns the expression "rotors with mating profiles", it characterizes the use of rotors the profiles of the teeth of which are different and, particularly, on the one hand, a first rotor equipped with at least one tooth having a first convex flank and a second convex flank, and, on the other hand, a second rotor equipped with at least one tooth which can have

- a first concave flank and a second concave flank, or

15 - a first flank on which one can distinguish two consecutive portions, which are a first concave portion and a second convex portion, and a second flank on which one can also distinguish two consecutive portions, which are a third convex portion and a fourth concave portion.

20 The manufacture by machining of this type of rotors with mating profiles is relatively easy, and the essential difficulty resides in the calculation of the profiles.

25 As concerns the expression "rotors with sections called symmetrical", it characterizes the use of rotors, on the one hand, of which the first flank and the second flank of each tooth are symmetrical with respect to a radial axis passing through the centre of the tooth, and, on the other hand, of which the geometry of the section is symmetrical and similar for the two rotors.

The calculation of the profiles and the manufacture by machining of this type of rotors with symmetrical profiles are easy, but the tightness derived from the co-operation of the rotors in the zones of the tooth crests (upper zones of the teeth) of the rotors is imperfect which can negatively affect the volumetric efficiency of the machines which contain them.

Concerning the expression "rotors having asymmetrical profiles," it characterizes the use of a first rotor and of a second rotor which have similar profiles and of which at least one tooth has a first convex flank and a second concave flank (DE-A-686298, GB-A-112104), the concavity and the convexity being accentuated to the point that the tooth assumes a curved shape.

The machines comprising rotors of this type are characterized by their excellent performance in terms of volumetric efficiency and final pressure obtained.

A drawback of this type of rotor is that their manufacture by machining is rendered delicate owing to the presence of a peculiarity in the form of an acute angle which is situated at tooth crest of the concave flank.

The performance of machines implementing rotors with asymmetrical profiles is strongly linked, on the one hand, to the fineness with which the aforementioned geometric peculiarity is machined, and, on the other hand, to the manner in which the rotors are assembled and adjusted with a view to obtaining a predetermined operational play.

Machines implementing rotors with asymmetrical profiles and variable pitch (WO-A-02/08609) make it possible moreover to obtain very good performance, but the tolerances with respect to manufacture and assembly are very constraining.

One will easily see that it is not possible to guarantee that the sharp edge situated at the crest of the concave flank is uniformly machined along the edge, so much so that in practice a sharp edge situated at the crest of the concave flank thus exhibits deficiencies in regularity.

These deficiencies in machining translate into irregularities in the operational play present between two concave flanks when they co-operate along the screw, and leaks will impair the performance of the machine.

In addition, the edge at the crest of the concave flank is very
5 susceptible to abrasion and the fluid which transits through the machine can lead to a wear and tear through abrasion which quickly worsens the performance of the machine.

Precisely, the invention concerns the rotary displacement machines the rotors of which are referred to as being of asymmetrical profile, and one
10 result which the invention aims to obtain is a machine that, while being of less constrained manufacture, does not have as much reduced performance.

Another result which the invention aims to obtain is a machine the performance of which is maintained over time.

To this end, the invention has as its subject matter a machine of the
15 aforementioned type in accordance with claim 1.

The invention will be better understood from reading the following description, given by way of non-limiting example, with reference to the attached drawing representing schematically:

- Figure 1 : in a top view, two twinned rotors, each with a thread of
20 constant pitch,

- Figure 2 : a sectional view of the set of twinned rotors of Figure 1, along a radial plane relative to the two rotors,

- Figure 3 : on an enlarged scale, any one of the twinned rotors of Figure 1, seen in section along a radial plane,

25 - Figure 4 : on an enlarged scale, a detail from Figure 3,

- Figure 5 : a section of the meshing of the rotors of Figure 1 in the plane V-V indicated in said Figure 1,

- Figure 6 : a section of the meshing of the rotors of Figure 1 in the plane VI-VI indicated in said Figure 1,

5 - Figure 7 : a section of the meshing of the rotors of Figure 1 in the plane VII-VII indicated in said Figure 1,

- Figure 8 : a section of the meshing of the rotors of Figure 1 in the plane slightly offset with respect to the plane V-V indicated in said Figure 1,

10 - Figure 9 : on a large scale, a detail of one of the rotors of Figure 1 in the plane IX-IX indicated in said Figure 1,

- Figure 10 : in a top view, two twinned rotors, each with a variable pitch,

- Figure 11 : a sectional view of the set of twinned rotors of Figure 10, along a radial plane relative to the two rotors,

15 - Figure 12 : in a sectional view, two twinned rotors, each with two threads of variable pitch,

- Figure 13 : a sectional view of the set of twinned rotors of Figure 12, along a radial plane relative to the two rotors.

20 Referring to the drawing, one sees a rotary displacement machine 1 comprising a housing 2 and at least two twinned rotors 3, 4 referred to as of asymmetrical profile, a first rotor 3 and a second rotor 4, said twinned rotors 3, 4, of which being mounted rotating in the housing 2 and driven in rotation about their longitudinal axis 6.

25 In a preferred, but non-limiting, way, the longitudinal axes 6 of the twinned rotors 3, 4 are parallel.

The twinned rotors 3, 4 are each made up of a core 5 on which projects at least one helicoidal thread 7 which, seen in a cross-sectional view of that of the twinned rotors under consideration 3, 4, extends above said core 5 in the manner of a tooth 8, which tooth 8

- 5 • has a first predetermined dimension "h" in a direction radial to the longitudinal axis 6 of that of the twinned rotors 3, 4 under consideration and above the surface 51 of this rotor,
- comprises a first flank 9 of concave shape and a second flank 10 of convex shape which connect at the level of an upper portion 11 of the tooth 8, said first flank 9 having the shape of an epicycloidal arc.

The twinned rotors 3, 4 can be of constant pitch type or of variable pitch type.

In a noteworthy way, instead of comprising a first flank 9 and a
15 second flank 10 the conventional shapes 91 and 101 of which connect at a first point "W" in such a way as to form a sharp edge along the helicoidal thread 7:

- on the one hand, said first flank 9 has a modified shape 92, of which the position and the length of the arc are predetermined in such a way that said modified shape 92 of this first flank 9 and the conventional shape 101
20 of the second flank 10 each connect to one of the opposite ends "B" and "C" of a short segment, referred to as connecting segment 12, which, by its presence along the entire helicoidal thread constitutes a helicoidal surface 13, referred to as flattened, eliminating the presence of a sharp edge,

- on the other hand, said connecting segment 12 has, in a direction
25 radial to the longitudinal axis 6 of that of the twinned rotors 3, 4 under consideration, a second predetermined dimension "L", such that the ratio of the second dimension "L" over the first dimension "h" ranges between 0.005 and 0.1 (five thousandths and one tenth).

When each tooth of the twinned rotors 3, 4 is defined by a first flank 9 and a second flank 10 which are connected to an outer surface 14 of substantially cylindrical profile of outer radius "Ra", instead of this outer surface 14 being connected to the shape of the first flank 9 at a first point "W" in such a way as to form a sharp edge along the helicoidal thread 7, the outer surface 14 is connected to the shape of said first flank 9 by the connecting segment 12.

Preferably, the ratio of the second dimension "L" over the first dimension "h" ranges between 0.005 and 0.1 (five thousandths and one tenth), when the twinned rotors 3, 4 have a diameter ranging between fifty millimeters (50 mm) and three hundred fifty millimeters (350 mm).

In a likewise noteworthy way:

- the conventional shape 91 of the first flank 9 and the circle, referred to as addendum circle "F" which circumscribes that of the twinned rotors 3, 4 being considered, have a point of intersection "W", referred to as first point "W", situated on a straight line "D1" which passes through a second point "O" situated on the longitudinal axis 6 of that of the twinned rotors 3, 4 being considered,

- the modified shape 92 of the first flank 9 and the circle "F" have a point of intersection "Z", referred to as third point "Z", situated on a second straight line "D2" which passes through the second point "O" and forms with the first straight line "D1" a first angle alpha, the value of which is able to be approximated by calculation according to the first equation

$$\text{ArcCos} \left[\frac{-L^2(L-2Ra)^2 + H^2(L^2 - 2LRa + 2Ra^2)}{2H^2 Ra (-L + Ra)} \right]$$

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with the values of the parameters

- "Ra" which represents the outer radius of that of the twinned rotors 3, 4 being considered,
- 5 • "L" which represents the relative value of the connecting segment 12 in one direction radial to that of the twinned rotors being considered, the magnitude of the relative value corresponding to the difference between the outer radius "Ra" and the value of a radius "Rp" which separates the longitudinal axis 6 of the core 5 from a point of the connecting segment 12 which is closest to this longitudinal axis 6,
- 10 • "H" which represents the center distance of axes between the twinned rotors 3, 4.

The modified shape 92 of the first flank 9 and the outer surface 51 of the core 5 connect at a point "A".

15 In a manner also noteworthy, the connecting segment 12 is inclined with respect to the first straight line "D1" of a second angle beta whose value is able to be approximated by calculation according to the second equation

$$\text{Arc Cosine } (H / (2 Ra))$$

with:

- "H" which represents the center distance of axes between the
20 twinned rotors 3, 4, and
- "Ra" which represents the outer radius of that of the twinned rotors 3, 4 being considered.

In practice, the position of the modified shape 92 of the first flank 9 can be adjusted by bringing about an oscillation of the support of the
25 conventional shape 91 of said first flank 9, of a first angle Alfa about the point O.

The connecting segment 12 is inclined with respect to the first straight line "D1" of a second angle β , this second angle being adjusted such that along the entire helicoidal threads 7 of the twinned rotors 3, 4, each helicoidal surface 13 which connects to a first flank 9 of one of the twinned
5 rotors 3, 4 is able to extend substantially parallel at least to a zone of the first flank 9 of the other of the twinned rotors 3, 4 which is contiguous to the connecting segment 12 of this other rotor.

A machine conforming to the present invention has instead and in place of the conventional sharp edge a helicoidal surface 13 made up of a
10 flattened region.

Such a flattened region can be machined easily and precisely, in particular by means of conventional tools, ensuring fewer leaks than with a sharp edge.

The variability of performance with respect to tolerances of
15 machining and assembly will thus be clearly less, while providing a simplification of the machining of the twinned rotors and the possibility of increasing the operational play of the machine without reducing performance.

Advantageously, the helicoidal surface 13 obtained thanks to the presence of the flattened region remains a controlled surface, and this
20 regardless of whether the pitch of the rotors is constant or variable.

As concerns the flattened region, it is also desirable for its length to remain small in relation to the tooth elevation in order to avoid the occurrence of a localized leak (expression better known by the German term "Blasloch" "blow hole") which is of a nature to reduce the performance of the system (Figures 7
25 and 8).

By way of illustrative example, for :

- a radius "Ra" of 65 mm (sixty-five millimeters) and a tooth elevation "h" of 30 mm (thirty millimeters), one has a width "L" of flattened region 12 of 1 mm (one millimeter),

5 - a radius "Ra" of 105 mm (one hundred and five millimeters) and a tooth elevation "h" of 60 mm (sixty millimeters), one has a width "L" of flattened region 12 of 1.5 mm (one point five millimeter),

- a radius "Ra" of 130 mm (one hundred thirty millimeters) and a tooth elevation "h" of 75 mm (seventy-five millimeters), one has a width "L" of flattened region 12 of 2 mm (two millimeters).

10 In the drawings, the localized leak has been symbolized by a simple arrow, not marked, in Figures 7 and 8.

It must be noted that the above-mentioned dimensions, angles and profiles are defined to within the operational play.

15 It must likewise be noted that the mentioned characteristics are applicable to machines comprising more than two rotors.

The rotors being of the same diameter, of different diameter, even each having different diameters along their longitudinal dimension, remains compatible with the present invention.

Claims

1. Rotary displacement machine (1) comprising a housing (2) and at least two twinned rotors (3, 4) referred to as being of asymmetrical profile, of which a first rotor (3) and a second rotor (4), said twinned rotors (3, 4), being
 5 mounted rotating in the housing (2) and driven in rotation about their longitudinal axis (6)

- 10 • these twinned rotors (3, 4) each being made up of a core (5) on which projects at least one helicoidal thread (7) which, seen in a cross-sectional view of that of the twinned rotors (3, 4) being considered, extends above said core (5) in the manner of a tooth (8), which tooth (8)
- has a first predetermined dimension ("h") in a direction radial to the longitudinal axis (6) of that of the twinned rotors (3, 4) being considered and above the surface (51) of this rotor,
- 15 • comprises a first flank (9) of concave shape and a second flank (10) of convex shape which connect at the level of an upper portion (11) of the tooth (8), said first flank (9) having the shape of an epicycloidal arc,

this machine being characterized in that instead of comprising a first
 20 flank (9) and a second flank (10) whose conventional shapes (91) and (101) connect at a first point ("W") in such a way as to form a sharp edge along the helicoidal thread (7):

- 25 - on the one hand, said first flank (9) has a shape (92), referred to as modified shape (92), whose position and length of arc are predetermined such that said modified shape (92) of this first flank (9) and the conventional shape (101) of the second flank (10) each connect to one of the opposite ends ("B") and ("C") of a short segment, referred to as connecting segment (12), which by its presence along the entire helicoidal thread (7) constitutes a helicoidal surface (13), referred to as flattened, eliminating the presence of a sharp edge,

- on the other hand, said connecting segment (12) has, in a direction radial to the longitudinal axis (6) of that of the twinned rotors (3, 4) being considered, a second predetermined dimension ("L") such that the ratio of the second dimension ("L") over the first dimension ("h") ranges between 0.005 and 0.1 (five thousandths and one tenth).

2. Machine according to claim 1 characterized in that when each tooth (8) of the twinned rotors (3, 4) is defined by a first flank (9) and a second flank (10) which are connected to an outer surface (14) of substantially cylindrical profile of outer radius ("Ra"), instead of this outer surface (14) being connected to the shape of the first flank (9) at a first point ("W") in such a way as to form a sharp edge along the helicoidal thread (7), the outer surface (14) is connected to the shape of said first flank (9) by the connecting segment (12).

3. Machine according to claim 1 or 2, characterized in that the ratio of the second dimension ("L") over the first dimension ("h") ranges between 0.005 and 0.1 (five thousandths and one tenth), when the twinned rotors (3, 4) have a diameter ranging between fifty millimeters (50 mm) and three hundred fifty millimeters (350 mm).

4. Machine according to one of the claims 1 to 3, characterized in that the connecting segment (12) is inclined with respect to the first straight line ("D1") of a second angle beta, this second angle being adjusted such that along the entire helicoidal threads (7) of the twinned rotors (3, 4), each helicoidal surface (13) which connects to a first flank (9) of one of the twinned rotors (3, 4) is able to extend substantially parallel at least to a zone of the first flank (9) of the other of the twinned rotors (3, 4) which is contiguous to the connecting segment (12) of this other rotor.

5. Machine according to one of the claims 1 to 4 characterized in that the connecting segment (12) is inclined with respect to the first straight line ("D1") of a second angle beta the value of which is able to be approximated by calculation according to the second equation

$$\text{Arc Cosine } (H / (2 Ra))$$

with :

- ("H") which represents the center distance of axes between the twinned rotors (3, 4), and

- ("Ra") which represents the outer radius of that of the twinned
5 rotors (3, 4) being considered.

6. Machine according to any one of the claims 1 to 5, characterized in that :

- the conventional shape (91) of the first flank (9) and the circle, referred to as addendum circle ("F") which circumscribes the one of the twinned
10 rotors (3, 4) under consideration, have a point of intersection ("W"), referred to as first point ("W"), situated on a straight line ("D1") which passes through a second point ("O") situated on the longitudinal axis (6) of that of the twinned rotors (3, 4) under consideration,

- the modified shape (92) of the first flank (9) and the circle ("F") have
15 a point of intersection ("Z"), referred to as third point ("Z"), situated on a second straight line ("D2") which passes through the second point ("O") and forms with the first straight line ("D1") a first angle alpha, the value of which is able to be approximated by calculation according to the first equation

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$$\text{ArcCos} \left[\frac{-L^2(L-2Ra)^2 + H^2(L^2 - 2LRa + 2Ra^2)}{2H^2 Ra (-L + Ra)} \right]$$

with the values of the parameters

• ("Ra") which represents the outer radius of that of the twinned
25 rotors (3, 4) being considered,

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- ("L") which represents the relative value of the connecting segment (12) in one direction radial to that of the twinned rotors being considered, the magnitude of the relative value corresponding to the difference between the outer radius ("Ra") and the value of a radius ("Rp") which separates the longitudinal axis (6) of the core (5) from a point of the connecting segment (12) which is closest to this longitudinal axis (6),

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- ("H") which represents the center distance of axes between the twinned rotors (3, 4).