

METHOD AND APPARATUS FOR THE DETERMINATION OF ANALYTES

The present invention relates to a test device and method for the colorimetric determination of chemical and biochemical components (analytes) in aqueous fluids, particularly whole blood. In one preferred embodiment it concerns a test device and method for colorimetrically measuring the concentration of glucose in whole blood.

5 The quantification of chemical and biochemical components in colored aqueous fluids, in particular colored biological fluids such as whole blood and urine and biological fluid derivatives such as blood serum and blood plasma, is of ever-increasing importance. Important applications exist in medical diagnosis and treatment and in the quantification of exposure to therapeutic drugs, intoxicants, hazardous chemicals and the like. In some instances, the amounts of materials being determined are either so miniscule--in the range
10 of a microgram or less per deciliter--or so difficult to precisely determine that the apparatus employed is complicated and useful only to skilled laboratory personnel. In this case the results are generally not available for some hours or days after sampling. In other instances, there is often an emphasis on the ability of lay operators to perform the test routinely, quickly and reproducibly outside a laboratory setting with rapid or immediate information display.

15 One common medical test is the measurement of blood glucose levels by diabetics. Current teaching counsels diabetic patients to measure their blood glucose level from two to seven times a day depending on the nature and severity of their individual cases. Based on the observed pattern in the measured glucose levels the patient and physician together make adjustments in diet, exercise and insulin intake to better manage the disease. Clearly, this information should be available to the patient immediately.

20 Currently a method widely used in the United States employs a test article of the type described in U.S. Patent 3,298,789 issued January 17, 1967 to Mast. In this method a sample of fresh, whole blood (typically 20-40 μ l) is placed on an ethylcellulose-coated reagent pad containing an enzyme system having glucose oxidase and peroxidase activity. The enzyme system reacts with glucose and releases hydrogen peroxide. The pad also contains an indicator which reacts with the hydrogen peroxide in the presence of peroxidase
25 to give a color proportional in intensity to the sample's glucose level.

Another popular blood glucose test method employs similar chemistry but in place of the ethylcellulose-coated pad employs a water-resistant film through which the enzymes and indicator are dispersed. This type of system is disclosed in United States Patent 3,630,957 issued December 28, 1971 to Rey et al.

30 In both cases the sample is allowed to remain in contact with the reagent pad for a specified time (typically one minute). Then in the first case the blood sample is washed off with a stream of water while in the second case it is wiped off the film. The reagent pad or film is then blotted dry and evaluated. The evaluation is made either by comparing color generated with a color chart or by placing the pad or film in a diffuse reflectance instrument to read a color intensity value.

35 While the above methods have been used in glucose monitoring for years, they do have certain limitations. The sample size required is rather large for a finger stick test and is difficult to achieve for some people whose capillary blood does not express readily.

In addition, these methods share a limitation with other simple lay-operator colorimetric determinations in that their result is based on an absolute color reading which is in turn related to the absolute extent of reaction between the sample and the test reagents. The fact that the sample must be washed or wiped off
40 the reagent pad after the timed reaction interval requires that the user be ready at the end of the timed interval and wipe or apply a wash stream at the required time. The fact that the reaction is stopped by removing the sample leads to some uncertainty in the result, especially in the hands of the home user. Overwashing can give low results and under-washing can give high results.

45 Another problem that often exists in simple lay-operator colorimetric determinations is the necessity for initiating a timing sequence when blood is applied to a reagent pad. A user will typically have conducted a finger stick to a obtain a blood sample and will then be required to simultaneously apply the blood from the finger to a reagent pad while initiating a timing circuit with his or her other hand, thereby requiring the use of both hands simultaneously. This is particularly difficult since it is often necessary to insure that the timing circuit is started only when blood is applied to the reagent pad. All of the prior art methods require
50 additional manipulations or additional circuitry to achieve this result. Accordingly, simplification of this aspect of reflectance reading instruments is desirable.

The presence of red blood cells or other colored components often interferes with the measurements of these absolute values thereby calling for exclusion of red blood cells in these two prior methods as they are most widely practiced. In the device of patent 3,298,789 an ethyl cellulose membrane prevents red blood
55 cells from entering the reagent pad. Similarly, the water-resistant film of patent 3,630,957 prevents red blood cells from entering. In both cases the rinse or wipe also acts to remove these potentially interfering red blood cells prior to measurement.

Accordingly, there remains a need for a system of detecting analytes in colored liquids, such as blood,

that does not require removal of excess liquid from a reflectance strip from which a reflectance reading is being obtained.

Summary of the Invention

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Novel methods and apparatus are provided for diagnostic assays comprising a reflectance measuring apparatus and method which uses light of two wavelengths for examining the sample. It may be activated upon a change in reflectance of the matrix when fluid penetrates the matrix. The method comprises adding the sample, typically whole blood, to the matrix which filters out large particles, such as red blood cells, typically with the matrix present in the apparatus. The signal-producing system produces a product which further changes the reflectance of the matrix, which change can be related to the presence of an analyte in a sample.

Exemplary of the diagnostic assay system is the determination of glucose in the whole blood, where the determination is made without interference from the blood and without a complicated protocol subject to use error.

The present invention can be more readily understood by reference to the following detailed description when read in conjunction with the attached drawings, wherein:

Figure 1 is a perspective view of one embodiment of a test device containing the reaction pad to which the fluid being analyzed is applied.

Figure 2 is a block diagram schematic of an apparatus that can be employed in the practice of the invention.

Figure 3 is a block diagram schematic of an alternate apparatus that can be employed in the practice of the invention.

Detailed Description

The Reagent Element

The element, its various chemical systems and its manner of use are described in EP-A-256806, from which the present application is divided. However a very brief description follows with reference to the Figures.

As can be seen from Figure 1, a support holds reagent pad 11 so that a sample can be applied to one side of the reagent pad while light reflectance is measured from the side of the reagent pad opposite the location where sample is applied.

Figure 2 shows a system in which the reagent is applied to the side with the hole in the support handle while light is reflected and measured on the other side of the reagent pad. Other structures than the one depicted may be employed. The pad may take various shapes and forms, subject to the limitations provided herein. The pad will be accessible on at least one surface and usually two surfaces.

The hydrophilic layer (reagent element) may be attached to the support by any convenient means, e.g., a holder, clamp or adhesives; however, in the preferred method it is bonded to the support. The bonding can be done with any non-reactive adhesive, by a thermal method in which the support surface is melted enough to entrap some of the material used for the hydrophilic layer, or by microwave or ultrasonic bonding methods which likewise fuse the hydrophilic sample pads to the support. It is important that the bonding be such as to not itself interfere substantially with the diffuse reflectance measurements or the reaction being measured, although this is unlikely to occur as no adhesive need be present at the location where the reading is taken. For example, an adhesive 13 can be applied to the support strip 12 followed first by punching hole 14 into the combined strip and adhesive and then applying reagent pad 11 to the adhesive in the vicinity of hole 14 so that the peripheral portion of the reagent pad attaches to the support strip.

When used with whole blood, the porous matrix preferably has pores with an average diameter in the range of from about 0.1 to 2.0 μm , preferably about 0.2 to 1.0 and more preferably from about 0.6 to 1.0 μm .

A preferred manner of preparing the porous material is to cast the hydrophilic polymer such as polyamide onto a core of non-woven fibers. The core fibers can be any fibrous material that produce the described integrity and strength, such as polyesters and polyamides. The reagent that will form the light-absorbing reaction product, which is discussed later in detail, is present within the pores of the matrix but does not block the matrix so that the liquid portion of the assay medium, e.g. blood, being analyzed can flow through the pores of the matrix, while particles, such as erythrocytes, are held at the surface.

Any signal producing system may be employed that is capable of reacting with the analyte in the



sample to produce (either directly or indirectly) a compound that is characteristically absorptive at a wavelength other than a wavelength at which the assay medium substantially absorbs, but a reagent producing a light-absorbing reaction product upon reacting with glucose will be especially useful.

5 The Analysis Method

10 The analysis method of this invention relies on a change in absorbance, as measured by diffuse reflectance, which is dependent upon the amount of analyte present in a sample being tested. This change may be determined by measuring the change in the absorbance of the test sample between two or more points in time.

15 The first step of the assay to be considered will be application of the sample to the matrix. In practice, an analysis could be carried out as follows: First a sample of aqueous fluid containing an analyte is obtained. Blood may be obtained by a finger stick, for example. An excess over matrix saturation in the area where reflectance will be measured (i.e., about 5-10 microliters) of this fluid is applied to the reagent
20 element or elements of the test device. Simultaneous starting of a timer is not required (as is commonly required in the prior art), as will become clear below. Excess fluid can be removed, such as by light blotting, but such removal is also not required. The test device is typically mounted in an instrument for reading light absorbance; e.g., color intensity, by reflectance, prior to application of the sample. Absorbance is measured at certain points in time after application of the sample. Absorbance refers in this application
25 not only to light within the visual wavelength range but also outside the visual wavelength range, such as infrared and ultraviolet radiation. From these measurements of absorbance a rate of color development can be calibrated in terms of analyte level.

30 The Measuring Instrument

35 A suitable instrument, such as a diffuse reflectance spectrophotometer with appropriate software, can be made to automatically read reflectance at certain points in time, calculate rate of reflectance change, and, using calibration factors, output the level of analyte in the aqueous fluid. Such a device is schematically shown in Figure 2 wherein a test device of the invention comprising backing 12 to which reagent pad
40 11 is affixed is shown. Light source 5, for example a high intensity light emitting diode (LED) projects a beam of light onto the reagent pad. A substantial portion (at least 25%, preferably at least 35%, and more preferably at least 50%, in the absence of reaction product) of this light is diffusively reflected from the reagent pad and is detected by light detector 6, for example a phototransistor that produces an output current proportional to the light it receives. Light source 5 and/or detector 6 can be adapted to generate or
45 respond to a particular wavelength light, if desired. The output of detector 6 is passed to amplifier 7, for example, a linear integrated circuit which converts the phototransistor current to a voltage. The output of amplifier 7 can be fed to track and hold circuit 8. This is a combination linear/digital integrated circuit which tracks or follows the analog voltage from amplifier 7 and, upon command from microprocessor 20, locks or holds the voltage at its level at that time. Analog-to-digital converter 19 takes the analog voltage from track
50 and hold circuit 8 and converts it to, for example, a twelve-bit binary digital number upon command of microprocessor 20. Microprocessor 20 can be a digital integrated circuit. It serves the following control functions: 1) timing for the entire system; 2) reading of the output of analog/digital converter 19; 3) together with program and data memory 21, storing data corresponding to the reflectance measured at specified time intervals; 4) calculating analyte levels from the stored reflectances; and 5) outputting analyte concentration data to display 22. Memory 21 can be a digital integrated circuit which stores data and the microprocessor operating program. Reporting device 22 can take various hard copy and soft copy forms. Usually it is a visual display, such as a liquid crystal or LED display, but it can also be a tape printer, audible signal, or the like. The instrument also can include a start-stop switch and can provide an audible or visible time output to indicate times for applying samples, taking readings, etc., if desired.

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55 Reflectance Switching

60 In the present invention, the reflectance circuit itself can be used to initiate timing by measuring a drop in reflectance that occurs when the aqueous portion of the suspension solution applied to the reagent pad (e.g., blood) migrates to the surface at which reflectance is being measured. Typically, the measuring device is turned on in a "ready" mode in which reflectance readings are automatically made at closely spaced intervals (typically about 0.2 seconds) from the typically off-white, substantially dry, unreacted reagent strip. The initial measurement is typically made prior to penetration of the matrix by fluid being





analyzed but can be made after the fluid has been applied to a location on the reagent element other than where reflectance is being measured. The reflectance value is evaluated by the microprocessor, typically by storing successive values in memory and then comparing each value with the initial unreacted value. When the aqueous solution penetrates the reagent matrix, the drop in reflectance signals the start of the measuring time interval. Drops in reflectance of 5-50% can be used to initiate timing, typically a drop of about 10%. In this simple way there is exact synchronization of assay medium reaching the surface from which measurements are taken and initiation of the sequence of readings, with no requirement of activity by the user.

Although the total systems described in this application are particularly directed to the use of polyamide matrices and particularly to the use of such matrices in determining the concentration of various sugars, such as glucose, and other materials of biological origin, there is no need to limit the reflectance switching aspect of the invention to such matrices. For example, the matrix used with reflectance switching may be formed from any water-insoluble hydrophilic material and any other type of reflectance assay.

15 Particular Application to Glucose Assay

A particular example with regard to detecting glucose in the presence of red blood cells will now be given in order that greater detail and particular advantage can be pointed out. Although this represents a preferred embodiment of the present invention, the invention is not limited to the detection of glucose in blood.

The use of polyamide surfaces to form the reagent element provides a number of desirable characteristics in the present invention. These are that the reagent element is hydrophilic (i.e., takes up reagent and sample readily), does not deform on wetting (so as to provide a flat surface for reflectance reading), is compatible with enzymes (in order to impart good shelf stability), takes up a limited sample volume per unit volume of membrane (necessary in order to demonstrate an extended dynamic range of measurements), and shows sufficient wet strength to allow for routine manufacture.

In a typical configuration, the method is carried out using an apparatus consisting of a plastic holder and the reagent element (the matrix having the signal producing system impregnated therein), as described in EP-A-256806.

The electronic apparatus used to make the reflectance readings minimally contains a light source, a reflected light detector, an amplifier, an analog to digital converter, a microprocessor with memory and program, and a display device.

The light source typically consists of a light emitting diode (LED). Although it is possible to use a polychromatic light source and a light detector capable of measuring at two different wavelengths, a preferred apparatus would contain two LED sources or a single diode capable of emitting two distinct wavelengths of light. Commercially available LEDs producing the wavelengths of light described as being preferred in the present specification include a Hewlett Packard HLMP-1340 with an emission maximum at 635nm and a Hewlett Packard QEMT-1045 with a narrow-band emission maximum at 700nm. Suitable commercially available light detectors include a Hamamatsu 5874-18K and a Litronix BPX-65.

Although other methods of taking measurements are feasible, the following method has provided the desired results. Readings are taken by the photo-detector at specified intervals after timing is initiated. The 635nm LED is powered only during a brief measuring time span that begins approximately 20 seconds after the start time as indicated by reflectance switching. If this reading indicates that a high level of glucose is present in the sample, a 30-second reading is taken and used in the final calculation in order to improve accuracy. Typically, high levels are considered to begin at about 250 mg/dl. The background is corrected with a 700nm reading taken about 15 seconds after the start of the measurement period. The reading from the photodetector is integrated over the interval while the appropriate LED is activated, which is typically less than one second. The raw reflectance readings are then used for calculations performed by the microprocessor after the signal has been amplified and converted to a digital signal. Numerous microprocessors can be used to carry out the calculation. An AIM65 single-board microcomputer manufactured by Rockwell International has proven to be satisfactory.

The present methods and apparatuses allow a very simple procedure with minimum operational steps on the part of the user. In use, the reagent strip is placed in the detector so that the hole in the strip registers with the optics of the detecting system. A removable cap or other cover is placed over the optics and strip to shield the assembly from ambient light. The measurement sequence is then initiated by pressing a button on the measuring apparatus that activates the microcomputer to take a measurement of reflected light from the unreacted reagent pad, called an R_{dry} reading. The cap is then removed and a drop of blood is applied to the reagent pad, typically while the reagent pad is registered with the optics and the

reading device. It is preferred that the reagent strip be left in register with the optics in order to minimize handling. The instrument is capable of sensing the application of blood or other sample by a decrease in the reflectance when the sample passes through the matrix and reflected light is measured on the opposite side. The decrease in reflectance initiates a timing sequence which is described in detail at other locations in this specification. The cover should be replaced within 15 seconds of sample application, although this time may vary depending on the type of sample being measured. Results are typically displayed at approximately 30 seconds after blood application when a blood glucose sample is being measured, although a 20 second reaction is permissible for glucose samples having a concentration of glucose of less than 250mg/dl. If other samples are being measured, suitable times for displaying the result may differ and can be readily determined from the characteristics of the reagent/sample selected.

A particularly accurate evaluation of glucose level (or any other analyte being measured) can be made using the background current, i.e., the current from the photodetector with power on but with no light reflected from the reagent pad, in order to make a background correction. It has been demonstrated that over a 2-3 month period that this value does not change for a particular instrument prepared according to the preferred embodiments of this specification, and it is possible to program this background reading into the computer memory as a constant. With a slight modification of the procedure, however, this value can be measured with each analysis for more accurate results. In the modified procedure the meter would be turned on with the lid closed before the reagent strip is in place, and the background current would be measured. The test strip would then be inserted into the meter with the cover closed, an R_{dry} measurement taken, and the procedure continued as described above. With this modified procedure the background current does not need to be stable throughout the life of the meter, thereby providing more accurate results.

The raw data necessary for calculating a result in a glucose assay are a background current reported as background reflectance, R_b , as described above; a reading of the unreacted test strip, R_{dry} , also described above; and an endpoint measurement. Using the preferred embodiments described herein, the endpoint is not particularly stable and must be precisely timed from the initial application of blood. However, the meter as described herein performs this timing automatically. For glucose concentrations below 250mg/dl, a suitably stable endpoint is reached in 20 seconds, and a final reflectance, R_{20} , is taken. For glucose concentrations up to 450mg/dl, a 30-second reflectance reading, R_{30} , is adequate. Although the system described herein displays good differentiation up to 800mg/dl of glucose, the measurement is somewhat noisy and inaccurate above 450mg/dl, although not so great as to cause a significant problem. Longer reaction times should provide more suitable readings for the higher levels of glucose concentration.

The 700nm reflectance reading for the dual wavelength measurement is typically taken at 15 seconds (R_{15}). By this time blood will have completely saturated the reagent pad. Beyond 15 seconds the dye reaction continues to take place and is sensed, to a small part, by a 700nm reading. Accordingly, since dye absorption by the 700nm signal is a disadvantage, readings beyond 15 seconds are ignored in the calculations.

The raw data described above are used to calculate parameters proportional to glucose concentration which can be more easily visualized than reflectance measurements. A logarithmic transformation of reflectance analogous to the relationship between absorptivity and analyte concentration observed in transmission spectroscopy (Beer's Law) can be used if desired. A simplification of the Kubelka-Munk equations, derived specifically for reflectance spectroscopy, have proven particularly useful. In this derivation K/S is related to analyte concentration with K/S defined by Equation 1.

$$K/S-t = (1 - R^*t)^2 / (2 \times R^*t) \quad (1)$$

R^*t is the reflectivity taken at a particular endpoint time, t , and is the absorbed fraction of the incident light beam described by Equation 2, where R_t is the endpoint reflectance, R_{20} or R_{30} .

$$R^*t = (R_t - R_b) / (R_{dry} - R_b) \quad (2)$$

R^*t varies from 0 for no reflected light (R_b) to 1 for total reflected light (R_{dry}). The use of reflectivity in the calculations greatly simplifies meter design as a highly stable source and a detection circuit become unnecessary since these components are monitored with each R_{dry} and R_b measurement.

For a single wavelength reading K/S can be calculated at 20 seconds ($K/S-20$) or 30 seconds ($K/S-30$). The calibration curves relating these parameters to YSI (Yellow Springs Instruments) glucose measurements can be precisely described by the third order polynomial equation outlined in Equation 3.

$$YSI = a_0 + a_1(K/S) + a_2(K/S)^2 + a_3(K/S)^3 \quad (3)$$

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The coefficients for these polynomials are listed in Table 1

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TABLE 1

Coefficients for Third Order Polynomial Fit of Single Wavelength Calibration Curves		
	K/S-20	K/S-30
a_0	-55.75	-55.25
a_1	0.1632	0.1334
a_2	-5.765×10^{-5}	-2.241×10^{-5}
a_3	2.58×10^{-8}	1.20×10^{-8}

The single chemical species being measured in the preferred embodiments is the MBTH-DMAB indamine dye and the complex matrix being analyzed is whole blood distributed on a 0.8 μ Posidyne membrane. A review entitled "Application of Near Infra Red Spectrophotometry to the Nondestructive Analysis of Foods: A Review of Experimental Results", CRC Critical Reviews in Food Science and Nutrition, 18(3) 203-30 (1983), describes the use of instruments based on the measurement of an optical density difference $\Delta OD (\lambda_a - \lambda_b)$ where OD_{λ_a} is the optical density of the wavelength corresponding to the absorption maximum of a component to be determined and OD_{λ_b} is the optical density at a wavelength where the same component does not absorb significantly.

The algorithm for dual wavelength measurement is by necessity more complex than for single wavelength measurement but is much more powerful. The first order correction applied by the 700nm reading is a simple subtraction of background color due to blood. In order to make this correction, a relationship between absorbance at 635nm and 700nm due to blood color can be and was determined by measuring blood samples with 0 mg/dl glucose over a wide range of blood color. The color range was constructed by varying hematocrit, and fairly linear relationships were observed. From these lines the K/S-15 at 700nm was normalized to give equivalence to the K/S-30 at 635nm. This relationship is reported in Equation 4, where K/S-15n is the normalized K/S-15 at 700nm.

$$K/S-15n = (K/S-15 \times 1.54) - 0.133 \quad (4)$$

Note that the equivalence of the normalized 700nm signal and the 635nm signal is only true at zero glucose. The expressions from which the calibration curves were derived are defined by Equations 5 and 6.

$$K/S-20/15 = (K/S-20) - (K/S-15n) \quad (5)$$

$$K/S-30/15 = (K/S-30) - (K/S-15n) \quad (6)$$

These curves are best fit by fourth-order polynomial equations similar to Equation 3 to which a fourth-order term in K/S is added. The computer-fit coefficients for these equations are listed in Table 2.

TABLE 2

Coefficients for Fourth-Order Polynomial Fit of Dual Wavelength Calibration Curves		
	K/S-20/15	K/S-30/15
a_0	-0.1388	1.099
a_1	0.1064	0.05235
a_2	6.259×10^{-5}	1.229×10^{-4}
a_3	-6.12×10^{-8}	-5.83×10^{-8}
a_4	3.21×10^{-11}	1.30×10^{-11}

A second order correction to eliminate errors due to chromatography effects has also been developed. Low hematocrit samples have characteristically low 700nm readings compared to higher hematocrit samples with the same 635nm reading. When the ratio of $(K/S-30)/(K/S-15)$ is plotted versus K/S-30 over a

wide range of hematocrits and glucose concentrations, the resulting line on the graph indicates the border between samples which display chromatography effects (above the curve) and those that do not (below the curve). The K/S-30 for the samples above the curve are corrected by elevating the reading to correspond to a point on the curve with the same (K/S-30)/(K/S-15).

5 The correction factors reported above were tailor made to fit a single instrument and a limited number of reagent preparations. The algorithm can be optimized for an individual instrument and reagent in the same manner that is described above.

10 In summary, the system of the present invention minimizes operator actions and provides numerous advantages over prior art reflectance-reading methods. When compared to prior methods for determining glucose in blood, for example, there are several apparent advantages. First, the amount of sample required to saturate the thin reagent pad is small (typically 5-10 microliters). Second, operator time required is only that necessary to apply the sample to the thin hydrophilic layer and close the cover (typically 4-7 seconds). Third, no simultaneous timing start is required. Fourth, whole blood can be used. The method does not require any separation or utilization of red-cell-free samples and likewise can be used with other deeply colored samples.

15 The invention now being generally described, the same will be better understood by reference to the following specific examples which are presented for purposes of illustration only and are not to be considered limiting of the invention unless so specified.

20 Example I

Reproducibility:

25 One male blood sample (JG, hematocrit = 45) was used to collect the reproducibility data set forth in Tables 3-5.

TABLE 3

Reproducibility of a Single Wavelength MPX System						
YSI (mg/dl)	Average (mg/dl)		S.D. (mg/dl)		%C.V.	
	20 sec.	30 sec.	20 sec.	30 sec.	20 sec.	30 sec.
25	23.1	23.0	2.1	2.04	9.1	9.0
35 55	53.3	53.2	3.19	3.32	6.0	6.3
101	101	101	3.0	3.3	3.0	3.3
326	326.6	327	13.3	9.8	4.1	3.0
501		503		17.1		3.4
690		675		28		4.15
40 810		813		37		4.5

TABLE 4

Reproducibility of a Dual Wavelength MPX System						
YSI (mg/dl)	Average (mg/dl)		S.D. (mg/dl)		%C.V.	
	20 sec.	30 sec.	20 sec.	30 sec.	20 sec.	30 sec.
25	25	27	1.34	1.55	5.4	5.7
55	55	57.4	2.58	2.62	4.7	4.6
101	101	101.5	2.55	2.18	2.5	2.1
326	332	330	15.0	7.1	4.5	2.1
501		505		21.3		4.2
55 690		687		22.8		3.3
810		817		30.4		3.7

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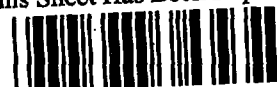


TABLE 5

Reproducibility of a 3.0mm Diameter Aperture		
YSI (mg/dl)	% C.V.	
	4.7mm	3.0mm
55-100	4.8	4.9
300	3.0	5.0
600	3.8	5.5
avg.	3.9	5.1

The blood was divided into aliquots and spiked with glucose across a range of 25-800mg/dl. Twenty determinations were made at each glucose test level from strips taken at random from a 500 strip sample (Lot FJ4-49B). The results of this study lead to the following conclusions:

1. Single vs. Dual Wavelength: The average C.V. for the 30-second dual result was 3.7% vs. 4.8% for the 30-second single wavelength result, an improvement of 23% across a glucose range of 25-810mg/dl. There was a 33% improvement in C.V. in the 25-326mg/dl glucose range. Here the C.V. decreased from 5.4% to 3.6%, a significant improvement in the most used range. The 20-second dual wavelength measurement gave similar improvements in C.V. compared to the single wavelength measurement in the 25-325mg/dl range (Tables 3 and 4).

2. Dual Wavelength, 20 vs. 30-second Result: The average C.V. for a 20-second result in the 25-100 mg/dl range is nearly identical to the 30-second reading, 4.2% vs. 4.1%. However, at 326 mg/dl the 30-second reading has a C.V. of 2.1% and the 20-second result a C.V. of 4.5%. As was seen in the K/S-20 response curve, the slope begins to decrease sharply above 250 mg/dl. This lead to poor reproducibility at glucose levels greater than 300 for the 20-second result. From this reproducibility data the cutoff for the 20-second result is somewhere between 100 and 326 mg/dl. A cutoff of 250 mg/dl was later determined from the results of the recovery study set forth in Example II.

3. Aperture Size: A smaller optics aperture size, 3.0mm vs. 5-0 mm., was investigated. Initial experimentation using a 10- replicate, hand-dipped disk sample did show improved C.V.s with the 3.0mm aperture, apparently because of easier registration with the system optics. However, when machine-made roll membrane was used, the average C.V. (Table 5) of the larger aperture, 4.7mm, was 3.9% vs. an average C.V. for the 3.0mm aperture of 5.1%. This 30% increase in C.V. was probably due to the uneven surface of the roll membrane lot as discussed below.

Example II

Recovery:

For comparison of the present method (MPX) against a typical prior art method using a Yellow Springs Instrument Model 23A glucose analyser manufactured by Yellow Springs Instrument Co., Yellow Springs, Ohio (YSI), blood from 36 donors was tested. The donors were divided equally between males and females and ranged in hematocrit from 35 to 55%. The blood samples were used within 30 hours of collection, with lithium heparin as the anti-coagulant. Each blood sample was divided into aliquots and spiked with glucose to give 152 samples in the range of 0-700 mg/dl glucose. Each sample was tested in duplicate for a total of 304 data points.

Response curves were constructed from these data and glucose values then calculated from the appropriate equation (Tables 1 and 2). These MPX glucose values were then plotted vs. the YSI values to give scattergrams.

Comparison of MPX Systems: For both the 20-second and 30-second measurement times there is visually more scatter in the single-wavelength scattergrams than the dual-wavelength scattergrams. The 20-second reading becomes very scattered above 250 mg/dl but the 30-second measurement does not have wide scatter until the glucose level is ≥ 500 mg/dl.

These scattergrams were quantitated by determining the deviations from YSI at various glucose ranges. The following results were obtained.

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TABLE 6.

Accuracy of MPX from Recovery Data

MPX Wavelength	Measurement Time (sec.)	S.D. (mg/dl) 0-50	C.V. for Range*		
			50-250	250-450	450-7
Single	20	±5.6	7.2	14.5	-
Single	30	±6.9	7.1	8.8	10.2
Dual	20	±2.3	5.3	12.8	-
Dual	30	±2.19	5.5	5.8	8.4

Note: These are inter method C.V.s.

- a. The dual wavelength system gave C.V.s that ranged 30% lower than the single wavelength system.
- b. The single wavelength system, from 0-50 mg/dl, showed a S.D. of ±6-7 mg/dl whereas the S.D. for a dual wavelength measurement was only ±2.2 mg/dl.
- c. The cutoff for a 30-second MPX measurement is 250 mg/dl. For the 50-250 mg/dl range both the 20- and 30-second measurements gave similar inter-method C.V.s (approximately 7% for single wavelength, 5.5% for dual wavelength). However, in the 250-450 mg/dl range inter-method C.V.s more than double for the 20-second reading to 14.5% for the single and 12.8% for the dual wavelength.
- d. The 30-second reading was unusable above 450 mg/dl for both the single and dual wavelength measurement (C.V.s of 10.2 and 8.4%).

In conclusion, two MPX systems gave optimum quantitation in the 0-450 mg/dl range.

1. MPX 30 Dual: This dual wavelength system gave a 30-second measurement time with a 95% confidence limit (defined as the probability of a measurement being within 2 S.D. of the YSI) of 11.3% (C.V.) for the range from 50-450 mg/dl (Table 7) and ±4.4 mg/dl (S.D.) for 0-50 mg/dl.
2. MPX 30/20 Dual: This dual wavelength system gave a 20-second measurement time in the 0-250



mg/dl range and a 30-second time for the 250-450 range. The 95% confidence limits are nearly identical to the MPX 30 Dual System (Table 7), 11.1% (C.V.) for 50-450 mg/dl and ± 4.6 mg/dl (S.D. for 0-50 mg/dl).

TABLE 7.

Comparison of 95% Confidence Limits for MPX,
GlucoScan Plus and Accu-Chek bG* Reagent Strips

Measuring Range mg/dl	MPX Single Wavelength		MPX Dual Wavelength	
	20 sec.	30 sec.	20 sec.	30 sec.
0-50	11.2 mg/dl	13.8 mg/dl	4.6 mg/dl	4.4 mg/dl
50-250	14.4%	14.2%	10.6%	11.0%
250-450	-	17.6%	-	11.6%
77-405	GlucoScan Plus (Drexler Clinical)		15.9%	
77-405	Accu-Chek bG (Drexler Clinical)		10.7%	
50-450	MPX 20/30 Dual Hybrid		11.1%	
50-450	MPX 30 Dual		11.3	

* Confidence limits for MPX were from the YSI. The confidence limits for GlucoScan Plus and Accu-Chek bG were from the regression equation vs. YSI which eliminates bias due to small differences in calibration.

Example III

Stability:

Most of the bench-scale work carried out in optimizing stability was completed using hand-dipped 0.8 μ Posidyne membrane disks. The specific dye/enzyme formulation was set forth previously.

1. Room Temperature Stability: This study attempted to chart any change in response of the 0.8 μ Posidyne membrane reagent stored at 18-20°C over silica gel desiccant. After 2.5 months there was no noticeable change as measured by the response of a room temperature sample vs. the response of a sample stored at 5°C. Each scattergram represented a glucose range of 0-450 mg/dl.

2. Stability at 37°C: A 37°C stability study using the same reagent as the RT study was carried out. The differences in glucose values of reagent stressed at 37°C vs. RT reagent, for strips stressed with and without adhesive, was plotted over time. Although the data was noisy, due to the poor reproducibility of handmade strips, the stability was excellent for strips whether they were stressed with or without adhesive.

3. Stability at 56°C: Eight 5- to 6-day stability studies were carried out using different preparations of a similar formulation on disk membrane (Table 8). For the low glucose test level (80-100 mg/dl) the average glucose value dropped upon stressing by 3.4%, with the highest drop being 9.55%. At the high test level (280-320 mg/dl) the glucose reading declined by an average of 3.4%, the largest decline being 10.0%.

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TABLE 8.

Stability of pH = 4.0, .8 Posidyne Disk Reagent
Formulation Stressed for 5 to 6 Days at 56°C

Sample No.	% Difference (56°C vs. RT Sample)	
	YSI (80-100 mg/dl)	YSI (280-320 mg/dl)
FJ22B	-6.25	+5.4
FJ27A	-4.0	-5.14
FJ28B	-2.4	-5.3
FJ30H	-9.55	-10.0
FJ31C	+4.43	-1.24
FJ36	-3.2	-8.5
FJ48B*	-3.0	0.0
GM48A*	-3.0	-2.5
Average of 8	-3.4	-3.4

* These two samples contained twice the normal concentration of enzyme and dye.

A study of the 56°C stressing of this membrane over a 19-day period showed no major difference for strips stressed with or without adhesive. In both cases the 19-day decline in glucose value was <15% at low test levels (80-100) and 300 mg/dl. Another 56°C study using hand-dipped 0.8μ Posidyne membrane with twice the normal concentration of enzyme and dye was completed. Two separate preparations of the same formulation were made up and the stability measured over a 14-day period. The average results of the two studies were plotted. Changes were within ±10% over the 14-day period at both the high and low glucose test level. These data show this formulation to be particularly stable.

Example IV

Sample Size:

The sample size requirements for MPX are demonstrated in Table 9.

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TABLE 9.

Effect of Sample Size on MPX Measurements

Sample Size (ul)	Dual Wavelength					Single Wavelength				
	Average					Average				
	Low Glucose YSI = 56									
3	41	50	39	31	40	31	42	30	19	30
4	44	49	49	49	48	41	45	44	45	44
5	54	48	49	51	50	50	49	48	49	49
10	48	48	50	47	48	54	53	56	55	54
20	49	49	49	50	49	55	57	58	60	58
High Glucose YSI = 360										
3	301	260	276	286	280	274	232	244	260	252
4	383	378	367	341	367	361	356	342	318	344
5	398	402	382	370	388	378	387	366	351	370
10	364	362	378	368	368	356	358	379	369	366
20	375	370	380	378	376	380	382	389	385	384

The volumes reported in the table were transferred to the reagent pad shown in Figure 1 using a micro pipet. When blood from a finger stick is applied to a strip the total sample cannot be transferred, therefore the volumes reported here do not represent the total sample size needed to be squeezed from the finger for the analysis. A 3- μ l sample is the minimum necessary to completely cover the reagent pad circle. This does not provide enough sample to completely saturate the reagent pad and MPX gives low results. A 4- μ l sample barely saturates the reagent pad, while a 5- μ l sample is clearly adequate. A 10- μ l sample is a large shiny drop and a 20- μ l sample is a very large drop and is only likely to be used when blood from a pipet is used for sampling.

At low glucose concentration the single wavelength result has some dependence on sample size which is completely eliminated using the dual wavelength measurement. Although this dependence with the single wavelength might be considered acceptable, it is clearly undesirable.

Example V

15 Reproducibility:

Experimental measurements described above were always run in replicate, usually 2, 3 or 4 determinations per data point. These sets have always shown close agreement even for samples with extreme hematocrits or extreme oxygen levels. C.V.s were well below 5%. It appears, therefore, that reproducibility is very good to excellent.

The subject invention provides for many advantages over systems which are presently available commercially or have been described in the literature. The protocols are simple and require little technical skill and are relatively free of operator error. The assays can be carried out rapidly and use inexpensive and relatively harmless reagents, important considerations for materials employed in the home. The user obtains results which can be understood and used in conjunction with maintenance therapy. In addition, the reagents have long shelf lives, so that the results obtained will be reliable for long periods of time. The equipment is simple and reliable and substantially automatic.

All patents and other publications specifically identified in this specification are indicative of the level of skill of those of ordinary skill in the art to which this invention pertains and are herein individually incorporated by reference to the same extent as would occur if each reference were specifically and individually incorporated by reference.

The invention now being fully described, it will be apparent to one of ordinary skill in the art that many modifications and changes can be made thereto.

35 Claims

1. A measuring apparatus for the determination of an analyte in a fluid, which comprises:
 - a container having a light-tight closure adapted to removably contain a porous matrix capable of containing an absorbed fluid to be analyzed;
 - means for illuminating a surface of said matrix;
 - means for detecting light of two different wavelengths reflected from said matrix;
 - control means for collecting readings of reflected light and calculating a value for the amount of analyte in said fluid based on readings of analyte or reaction product absorbance from the first wavelength of reflected light and of background absorbance from the second wavelength of reflected light; and
 - means for reporting said value.
2. An apparatus according to claim 1, wherein said apparatus further comprises a self-contained electronic power supply operationally connected to said means for illuminating, means for detecting, control means, and reporting means.
3. An apparatus according to claim 1 or claim 2, wherein said means for illuminating and means for detecting light of two different wavelengths together comprise: (1) two light sources of different wavelengths and a single light detector; or (2) a polychromatic light source and two detectors restricted to detecting different wavelengths of light.
4. An apparatus according to claim 1, claim 2 or claim 3, wherein the first wavelength of light is from 690 to 710nm and the second wavelength of light is from 625 to 645nm.

- 5
6. An apparatus according to any one of the preceding claims, wherein said control means causes a timing circuit to be initiated based on initial decrease in reflectance of either wavelength of light, said decrease occurring when said fluid penetrates said matrix after being applied to said matrix on a surface other than the surface illuminated by said illuminating means.
- 10
7. An apparatus according to claim 6, wherein said control means is capable of collecting and storing a reading of reflectance from said reagent pad prior to application of fluid to said reagent pad.
- 15
8. An apparatus according to claim 7, wherein said control means is further capable of collecting and storing a background detector current reading in the absence of light reflected from said reagent pad.
- 20
9. An apparatus according to claim 7 or claim 8, wherein when power is supplied to said control means in an analyte detection mode, said control means automatically collects and compares sequential reflectance readings from said detector, initiates a timing circuit upon detection of a drop in reflectance, collects reaction reflectance readings at predetermined intervals after said drop in reflectance, calculates a value for the concentration of analyte in said fluid being analyzed from said reaction reflectance readings, and transfers said value to said reporting means.
- 25
10. An apparatus according to claim 7 or claim 8, wherein when power is supplied to said control means in a base reflectance mode prior to said analyte detection mode, said control means collects and stores a base reflectance reading from said matrix prior to application of fluid to said matrix and wherein when power is next supplied to said control means in the analyte detection mode, said base reflectance reading is subtracted from said reaction reflectance readings by said control means prior to calculation by said control means of said value.
- 30
11. A method of determining analyte concentration in a liquid, which comprises:
quantitatively measuring base reflectance from a first surface of a reagent element comprising an inert porous matrix and a reagent system capable of interacting with said analyte to produce a light-absorbing reaction product, said reagent system being impregnated in the pores of said matrix, prior to application of said liquid to said reagent element;
35 quantitatively measuring reaction reflectance from said reagent element after application of said liquid to a second surface of said reagent element other than the first surface from which said reaction reflectance is measured and after said liquid has migrated through said reagent element from said second surface to said first surface;
quantitatively measuring interference reflectance from said first surface of said reagent element after said application of liquid using a wavelength of light different from the wavelength of light used to measure said reaction reflectance; and
40 calculating a value expressing said concentration from said reflectance measurements.
- 45
12. A method according to claim 11, wherein said matrix has surfaces formed from a polyamide.
- 50
13. A method according to claim 11 or claim 12, wherein the average diameter of the pores in said matrix is from 0.2 to 1.0 μm and said liquid is whole blood.
- 55
14. A method according to claim 13, wherein said reagent produces a light-absorbing reaction product upon reacting with glucose.

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