

-1-

SYSTEM FOR OPERATING A SUCKER ROD STRING CONNECTED WITH
A WELL PUMP

This invention relates to a system for operating a sucker rod string connected with a well pump.

Often it is necessary to produce wells such as oil wells by pumping. One of the most commonly used well pumping systems includes a downhole reciprocating pump having a plunger which is raised and lowered by a sucker rod string connected at the surface end of the well with a walking beam. The walking beam is generally driven by pitman arms connected with crank arms rotated by a shaft which is driven by an electric motor or an internal combustion engine of the gasoline or diesel type. The motor or engine is coupled with the shaft through belts, chains, and some form of transmission. Counterweights are generally mounted on the crank arms. The centre of the walking beam is pivoted on a samson post at a sufficient height to permit the beam to be rocked by the pitman arms for raising and lowering the sucker rod string in the well. The conventional walking beam type pumping jack or unit is an inefficient system having many bearings and other parts which are subject to wear and often is quite large and expensive where used on deep wells. For example, such a pump having a stroke of twenty feet may be forty feet high. Obviously such a pump will have a large, long walking beam and quite heavy counterweights. Some deep wells have even been known to use pumps having an eighty foot stroke. The massive components of such a pumping system which must be moved during the operation of the pump causes substantial wear in the many bearings, gears, and other elements in the drive system requiring time consuming and expensive maintenance. Additionally such forces as those caused particularly by "rod pound" which is the reaction of the pump piston to hitting liquid in the well bore transmits shock forces to the walking beam, pitman arms, and cranks

-2-

as well as the gears and other parts of the system contributing to additional wear. Further disadvantages of the walking beam type well pump include limitations on the length of stroke of the pump and thus the length of the reciprocating movement of the sucker rod. Still further disadvantages of the walking beam type pump include the difficulty of satisfactorily hiding or enclosing the pump and noise produced by the pumping apparatus making it difficult to place such pumps in populated areas.

According to the present invention there is provided a system for operating a sucker rod string connected with a well pump comprising:

a double-acting fluid cylinder having opposing power ends;

means for connecting said cylinder with said sucker rod string for raising and lowering said string to operate said pump;

means for supplying pressurized fluid alternately to the cylinder ends including a direction control valve means movable between extend and retract conditions to extend and retract said cylinder;

drive means for shifting said direction control;

control means for operating said drive means responsive to the extend and retract movements of said cylinder; including limit valves positioned to simulate the hydraulic cylinder extend and retract stroke end locations, said limit valves being movably mounted for changing the location of each limit valve and the distance between said limit valves for selectively adjusting the length of the strokes of said hydraulic cylinder and the end limit of the extend and retract strokes of said cylinder, cam operator means for opening

and closing each of said limit valves at said end
locations and connection means connecting said cam
operator means with said hydraulic cylinder whereby said
cam operator means simulates the extend and retract
5 strokes of said hydraulic cylinder, said connection means
including a flexible cable secured at a first end with
said hydraulic cylinder and connected with said cam
operator means to move said cam operator means; movable
sheave means arranged to move the cam operator means and
10 fixed sheave means spaced from said movable sheave means,
means biasing said movable sheave means away from said
fixed sheave means, said cable being reeved over said
movable and fixed sheave means and secured along the
second end thereof at a fixed location so that movement
15 of said cylinder causes the movable sheave means to move
relative to the fixed sheave means; and means for
applying a fluid counterbalancing force into said
cylinder for offsetting the combined weights of said
sucker rod string, a production fluid column in a well
20 bore above said pump, and movable surface equipment
supported on said cylinder.

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The details of specific embodiments of the invention and the foregoing objects and advantages will be better understood from the following description taken in conjunction with the accompanying drawings wherein:

5 Figure 1 is a schematic view in section and elevation of a hydraulic well pump incorporating the features of the invention;

10 Figures 2A and 2B taken together form a schematic diagram of a hydraulic power and control system for operating the hydraulic well pump of Figure 1;

 Figure 3 is a side view in section and elevation of a specific embodiment of the hydraulic well pump of Figure 1;

15 Figure 4 is a broken back view in elevation of the hydraulic well pump of Figure 3;

 Figure 5 is a view in perspective of the hydraulic well pump of Figures 3 and 4;

 Figure 6 is a schematic side view in section and elevation of another form of hydraulic well pump;

20 Figure 7 is a schematic diagram of components of a hydraulic power system which in combination with the components of the fluid system of Figure 2B may be used to operate the hydraulic pump of Figure 6;

25 Figure 8 is another form of hydraulic fluid and power system which may be used to operate the hydraulic pump of Figure 6;

30 Figure 9 is a schematic view of a hydraulic well pump in accordance with the invention including devices for sensing and controlling the pump stroke length and device for controlling the linear motion of the hydraulic cylinder;

 Figures 10A and 10B taken together form a view in section and elevation of the hydraulic cylinder stroke length sensor;

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Figure 11 is a fragmentary top view showing one of the cylinder limit valves of the sensor of Figures 10 and 10B;

5 Figure 12 is a right end view in section and elevation of the sensor illustrated in Figures 10A and 10B;

Figure 13 is a schematic view of the cable and sheave system of the sensor;

10 Figure 14 is a top broken plan view of the sensor body;

Figure 15 is a side view in elevation of the stationary sheave block of the sensor;

Figure 16 is a left end view in elevation of the stationary block of Figure 15;

15 Figure 17 is a top view in elevation and section of the stationary block;

Figure 18 is a side view in elevation of the travelling sheave block of the sensor;

20 Figure 19 is a right end view in elevation of the travelling block of Figure 18;

Figure 20 is a left end view in elevation of the travelling block of Figure 18;

Figure 21 is a top plan view of the travelling block of Figure 18;

25 Figure 22 is a view in section of the travelling block along the line 22-22 of Figure 18;

Figure 23 is a view in section and elevation of the hydraulic cylinder linear motion control device;

30 Figure 24 is a right end view in section and elevation of the device of Figure 23;

Figure 25 is a view in section and elevation of the valve body of the device of Figure 23;

Figure 26 is a fragmentary top plan view of the central portion of the valve body of Figure 25;

35 Figure 27 is a bottom fragmentary view of the valve

body of Figure 25;

Figure 28 is a front view in elevation of the cross head of the motion control device of Figure 23;

5 Figure 29 is a top plan view of the cross head of Figure 28;

Figure 30 is a front view in elevation of the cam crank of the motion control device of Figure 23;

Figure 31 is a side view in section of the cam crank along the line 31-31 of Figure 30;

10 Figure 32 is a side view in section and elevation of one of the valve seats of the motion control device of Figure 23;

Figure 33 is a side view in section and elevation of one of the valves of the motion control device of Figure 23;

15 Figure 34 is a longitudinal side view in section of one of the valve spools of the motion control device of Figure 23; and

20 Figure 35 is a view in section of the valve spool along the line 35-35 of Figure 34.

Referring to Figure 1, a hydraulic well pump A includes an air counterbalanced hydraulic cylinder assembly which operates a flexible tension member connected with a pump sucker rod raising and lowering the rod twice the distance of the lift of the hydraulic cylinder. The hydraulic cylinder assembly includes a stationary hydraulic piston 1 on the upper end of a hollow piston rod 2 mounted in coaxial spaced relation around a flow conductor 3. The piston rod has ports 4 below the piston 1 opening into the annular space between the piston rod 2 and the flow conductor 3. A counterbalance annular piston 5 is movable in sealed relationship along the piston rod 2 within a stationary cylinder 6 at the lower end of a hydraulic cylinder 7 which moves in sealed

relationship along the stationary hydraulic piston 1. An idler sheave platform 8 is secured on the upper end of the movable cylinder 7. Idler sheaves 9 and 10 are mounted in horizontal spaced relation on the platform 8.

5 A flexible tension member 11 is secured at one end 12 to the base or foundation for the hydraulic pump, extends over the sheaves 9 and 10 and downwardly connected at the other end with a well pump sucker rod string 13. A counterbalance air receiver 14 supplied with air from a
10 compressor 15 communicates through a conduit with the stationary cylinder 6 below the piston 5 for applying a pneumatic force upwardly on the piston 5 substantially equal to the downward force produced by the combined weights of the movable components of the well pump
15 including the polish rod string and the fluid column in the well above the pump plunger.

The hydraulic well pump A is operated by pumping hydraulic fluid through the conduit 3 into the movable hydraulic cylinder 7 above the piston 1 raising the
20 platform 8 with the sheaves 9 and 10. Because the first end of the tension member 11 is secured at 12 the second end of the tension member connected with the sucker rod 13 is lifted twice the distance that the sheaves are raised. The free running end of the tension member moves
25 at twice the rate of extension of the cylinder 7 with the platform 8 and the sheaves 9 and 10. The weight supported by the hydraulic cylinder assembly is equal to twice the weight supported by the sucker rod 13. That weight is also equal to the sum of the vertical force
30 provided by the piston 5 and the vertical force provided by the upper or cap end of the cylinder 7. When the hydraulic cylinder is extended to the upper end of the stroke, the well pump is reversed by pumping hydraulic fluid into the movable cylinder 7 below the piston 1
35 through the annulus between the conduit 3 and the piston rod 2 and outwardly through the ports 4 below the piston 1. Thus the hydraulic well pump is reciprocated by

alternately pumping the hydraulic cylinder assembly upwardly and downwardly. The pneumatic counterbalancing of the hydraulic well pump reduces the force required to reciprocate the pump to the sum of the force necessary to
5 overcome mechanical and fluid friction in the pumping system and column of fluid being lifted and accelerate the mass of the fluid column and the components of the pump and sucker rod being moved. Of course as the pump moves downwardly, the total forces are reduced by the
10 value attributable to the column of fluid above the plunger pump which of course is not lowered during the downward stroke.

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The counterbalancing substantially reduces the forces required to operate the hydraulic well pump and the employment of the particular arrangement of the idler sheaves and flexible tension member provides a pump plunger and sucker rod stroke twice the length of the travel of the hydraulic piston assembly thereby cutting the height of the required structure to half of the conventional walking beam type pumping jack.

A hydraulic fluid power system which may be used to operate the well pump A of Figure 1 is illustrated in Figures 2A and 2B. Referring to Figures 2A and 2B, only the hydraulic power and control circuitry is illustrated, it being understood that the reciprocating cylinder 7 which moves relative to the stationary piston 1 is connected at a lower end with the piston 5 operating in the outer cylinder 6 in response to the air counterbalance system schematically represented in Figure 1. The same reference numerals are used in Figure 2A to designate the corresponding parts of the hydraulic cylinder system as are used with such parts in Figure 1, such for example, as the numeral 2 designates the hollow piston rod 2 with the flow conductor connected with the piston rod for supplying the hydraulic fluid which drives the movable cylinder 7 and thus the pump A downwardly.

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The power circuit for delivering hydraulic fluid to the hydraulic cylinder assembly includes two fixed volume pumps 20a and 20b each capable of delivering a desired volume and pressure for the particular function of the well pump. The pump 20a is associated with the cap end of the cylinder 7 while the pump 20b is associated with the piston rod end of the cylinder. Thus the pump 20a drives the well pump during the lift cycle and the pump 20b drives the well pump during the retract or lowering cycle. The two pumps 20a and 20b are coupled to and driven by a common drive shaft 21 and a single power source, not shown, which may be an electric motor or internal combustion engine. A hydraulic fluid reservoir 22 indicated schematically with respect to several returns in the system provides the source of hydraulic fluid for both of the pumps. The outlet of the pump 20a is connected to the cap end of the cylinder 7 by a line 23a including a check valve 24a permitting flow only in the direction into the cap end of the cylinder. A pressure relief valve 25a is connected in a line 26a leading from the line 23a and dumping into the tank 22. The relief valve 25a responds to pressure in the line 23a and opens to dump fluid to the tank when the maximum selected pressure of that line is reached. The valve 25a thus limits the maximum fluid pressure available to the cap end of the cylinder 7. The outlet of the pump 20b is connected with the rod end of the cylinder by the line 23b including the check valve 24b and the line and piston rod 2 defining the flow path into the rod end of the cylinder. Because the effective area of the piston rod in the cylinder is less than that of the cap end, the pump 20b may have different operating parameters from those of pump 20a. A pressure relief valve 25b is connected by the line 26b into the line 23b and to the tank 22 for dumping fluid back to the tank when a

selected maximum pressure in the line 23b is reached.

As seen in Figure 2A, the control system for the delivery of hydraulic power fluid to the pump cylinder includes sequence valves 31a and 31b associated respectively with the cap and rod ends of the cylinder 7. The sequence valves are connected as cross-piloted valves to prevent the overrun of the reciprocating cylinder in the event resistance to movement should reverse for some reason. The sequence valve 31a is connected between the line 23a and the tank 22 by a line 32a. The valve 31b is connected between the line 23b and the tank 22 by a line 32b. The valve 31a is connected to the line 23b by a pilot line 33a so that the valve 31a is opened in response to pressure in the rod end of the cylinder. The valve 31b is connected to the line 23a by a pilot line 33b so that the valve 31b operates in response to pressure in the cap end of the cylinder 7. It will be apparent that as the cylinder 7 reciprocates in each direction, the pressure within the cylinder on the opposite end must be relieved for the cylinder to move. Thus, the sequence valve 31a relieves the pressure in the cap end of the cylinder 7 as the cylinder retracts or moves down downwardly; the sequence valve 31b relieves the pressure in the rod end of the cylinder as the cylinder extends or moves upwardly.

Direction control of the cylinder 7 is effected by control valve 40 connected between the outlets of the pumps 20a and 20b and the tank 22. The valve 40 may be any one of several types of valves including spool, plug, shear sal, double poppet, or rotary. The valve 40 is a three-position valve having an intermediate dump position in which the outlets of both of the pumps are communicated with the tank 22 effectively unloading both pumps. The valve 40 has extend and retract positions for fluid flow from each of the pumps to its respective end

of the cylinder 7. For controlling flow to the cap end of the cylinder 7, the outlet of the pump 20a is connected through the line 41a to the valve 40. When the valve 40 is in the dump position for the cap end of the cylinder, the outlet of the pump 20a is dumped to the tank 22. The outlet of the pump 20b is connected with the valve 40 through the line 41b. When the valve 40 is in the dump position for the rod end of the cylinder 7, the outlet of the pump 20b is dumped through the valve 40 to the tank 22. To extend the cylinder 7 to the right as seen in Figure 2A, lift the cylinder as viewed in Figure 1, the valve 40 is shifted to the left as seen in Figure 2A blocking the line 41a at the valve 40 while the line 41b remains open to dump fluid from the piston end of the cylinder back to the tank 22. The output from the pump 20a necessarily flows through the line 23a, the check valve 24a, and the line 3 into the cap end of the cylinder 7 thereby moving the cylinder 7 relative to the fixed piston 1. Similarly, to retract the cylinder 7 downwardly, to the left in Figure 2A, the valve 40 is shifted to the right to block the line 41b while the line 41a is opened to the tank 22. Fluid from the pump 20b flows to the rod end of the cylinder 7 through the line 23b, the check valve 24b, and the flow passage 2 extending into and through the piston rod 2. The pressure in the line 23b acts through the pilot line 33a to the valve 31a opening the valve permitting flow from the cap end of the cylinder 7 through the line 32a and the valve 31a back to the tank 22. The acceleration or deceleration of the reciprocating cylinder 7 will be directly related to the manner in which the direction control valve 40 is shifted. With appropriate manipulation of the direction control valve, it is possible to cause the cylinder to emulate simple harmonic motion in the pattern of acceleration and deceleration. For both directions of the cylinder

movement, the speed of movement will be proportional to the discharge rate of the particular pump driving the piston and the maximum force applied to the piston will be limited by the setting of the respective pressure relief valves.

5 The hydraulic system of Figures 2A and 2B includes mechanism provided to reciprocate the direction control valve 40 including a small rotary hydraulic motor 43 having an output shaft 44 driving a crank arm 45
10 non-rotatably fixed to the output shaft, Figure 2B. A pitman arm or link 46 is connected between the crank arm and the reciprocating valve member of the valve 40 to shift the direction control valve. A rotary cam 48 having diametrically opposed external lobes 49 is also
15 non-rotatably fixed to the motor shaft 44. A low pressure hydraulic pump 50 with an associated relief valve 51 provides pressurized fluid for driving the motor 43 and provides pilot fluid for operating certain pilot operated valves included in the hydraulic logic circuit
20 and system of Figures 2A and 2B. The pump 50 may be driven by the drive shaft 21 also driving the pumps 20a and 20b. The pump 50 discharges to the motor 43 through a fluid line 52 which includes branches 52a and 52b including pilot operated, two-way stop and start valves
25 53 and 54. The valves 53 and 54 control intermittent flow of fluid from the pump 50 to the motor 43. The stop and start valves 53 and 54 are controlled by limit valves 55 and 56 and a cam operated stop pilot valve 57 operated by the rotary stop cam 48. A variable orifice 60 is
30 provided in the line 52 between the stop and start valves to function as a speed control for the hydraulic motor 43. The limit valves 55 and 56 are actuated by a cam C movable with the cylinder 7. The limit valve 55 is operated by the cam when the cylinder 7 reaches the limit
35 of its retract stroke; the limit valve 56 is

operated by the cam C when the cylinder 7 approaches the limit of its extend stroke. The stop pilot valve 57 is actuated by the lobes 49 on the stop cam 48 for blocking the fluid line 52 to stop the motor 43. Fluid under pressure is supplied to the limit valves 55 and 56 from the pump 50 through the line 58 and the branch lines 58a and 58b. Pressurized fluid is also supplied to the pilot valve 57 from the pump 50 through the lines 52 and 59. Pilot fluid is conducted from the limit valves 55 and 56 to the start valve 54 through the pilot lines 61a, 61b, the shuttle valve 62, and the pilot line 61c. Pilot fluid is conducted from the stop pilot valve 57 to the stop valve 53 through a pilot line 65. The stop valve 53 is normally opened passing fluid to the pump 43 and is closed by pilot fluid from the pilot valve 57 when actuated by one of the lobes 49 on the stop cam 48. The pilot valve 57 is normally closed communicating the pilot line 65 with the tank 22 allowing the stop valve 53 to shift to the normal open position. When the pilot valve 57 is engaged by one of the cam lobes 49 on the cam 48, the valve 57 is opened passing pilot fluid from the line 59 to the stop valve 53 closing the stop valve.

The pilot operated start valve 54 connected in the branch line 52b is normally closed and is opened by pilot fluid from either one of the limit valves 55 and 56 conducted through the pilot line 61c leading from the shuttle valve 62. The limit valves 55 and 56 are identical in structure and function. Fluid is supplied to the limit valves 55 and 56 from the pump 50 through the lines 52 and 58 and through the dump valves 81 and 82 associated, respectively, with limit valves 55 and 56. The dump valve 81 supplies fluid to the limit valve 55 through the line 58a; the dump valve 82 supplies fluid to the limit valve 56 through the line 58b. The dump valves are bi-staple pilot operated valves opened and closed by

pilot fluid. When open the dump valves pass fluid from the line 58 to the lines 58a and 58b associated with the limit valves 55 and 56, respectively. When closed, the dump valves communicate the lines 58a and 58b with the tank 22 allowing the dumping of fluid from the lines 58a and 58b. Each of the dump valves 81 and 82 is opened to enable the limit valve associated with the dump valve to pass fluid when the limit valve is opened by the cam C. Referring to Figure 2A, when the cam C is moving to the left, the dump valve 81 has been previously opened when the cam C engage the limit valve 56 allowing flow of fluid through the line 61b to the shuttle valve 62. At this time pilot fluid is passed through the line 61e to open the dump valve 81 so that the valve 81 is preconditioned to allow fluids to pass through the limit valve 55 when that valve is engaged by the cam C at the retract stroke limit. Similarly, at that point, the dump valve 82 is preconditioned by fluid passing through the lines 61d to allow fluid to pass through the limit valve 56 at the extend stroke limit.

As illustrated in Figure 2B, the system and logic circuitry for closing the dump valves includes a rotary release cam 83 and cam operated release valves 84 and 85. The cam 83 is mounted on and rotated by the shaft 44 of the motor 43 and driven in timed relation with the crank 45 and the stop cam 48. The valves 84 and 85 are spring biased two-way normally closed valves opened by the operator lobe on the cam 83. Pilot fluid is supplied to the valves 84 and 85 through the lines 52, 59, and 59a. The valve 84 is associated with the dump valve 81 through pilot fluid line 86. Similarly, the valve 85 is associated with the dump valve 82 through pilot fluid line 87.

Referring to Figure 2B, the stop cam 48 and release cam 83 are timed so that when the motor 43 is started by

the engagement of the cam C with the limit valve 55, the stop valve 53 is opened by disengagement of the cam lobe 49 from the stop pilot valve 57. The release valve 84 is opened by the cam 83 passing pilot fluid to the dump valve 81 which occurs before the opposite lobe 49 of the cam 48 re-engages the stop pilot valve 57. The passing of the pilot fluid in the line 86 to the valve 81 closes the valve 81 allowing the dumping of fluid from the line 58a to tank 22 permitting the start valve 54 to close.

5 The start valve 54 is closed even though the limit valve 55 is still engaged by the cam C so that the motor 43 is stopped when the opposite lobe 49 of the stop cam 48 re-engages the stop pilot valve 57. The dump valve 81 will remain closed in the dump condition until

10 pre-conditioned by the limit valve 56 at the extend stroke limit. With the operation of the motor 43 initiated by the limit valve 56 at the extend stroke limit, a similar operating cycle occurs with the lobe of release cam 83 operating the release valve 85 to deliver

15 pilot fluid through the line 87 to the dump valve 82.

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Briefly, the operation of the hydraulic systems of Figures 2A and 2B is as follows. With the cylinder 7 moving to the left extending the cam C toward the limit valve 55, the dump valve 81 has been previously opened to

25 supply fluid to the limit valve 55. When the cam C approaches the limit of the stroke engaging the limit valve 55, pilot fluid is passed to the start valve 54 opening that valve and starting the motor 43. Simultaneously, pilot fluid is passed to the dump valve

30 82 through the line 61d opening that valve for a subsequent operation. The motor 43 first dis-engages the stop cam lobe 49 from the stop pilot valve 57 closing the stop pilot valve 57 removing pilot pressure from the stop valve 53 which is then opened by the stop valve spring.

35 Shortly thereafter the lobe of the release cam 83 engages

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the release valve 84 closing the dump valve 81. Fluid is dumped from the line 58a and the connecting lines allowing the start valve 54 to close. The motor 43 continues to operate until the opposite stop cam lobe 49 engages the stop pilot valve 57 opening the valve 57 thereby closing the valve 53 stopping the motor 43. At the end of the stroke to the right in Figure 2A the cam C engages the limit valve 56. First, the start valve 54 is opened to start the motor 43 and simultaneously the dump valve 81 is opened for a succeeding operation. Again, the motor 43 first disengages a stop cam lobe from the stop pilot valve 57 followed by the engagement of the release valve 85 by the lobe of release cam 83. This closes the dump valve 82 to close the start valve 54 even though the limit valve 56 is held open by the cam 16. When the cams 48 and 83 again reach the condition illustrated in Figure 2B, the stop valve 53 is closed to stop the motor 43.

It will be recognized that the hydraulic power and logic system of Figures 2A and 2B as used to operate the well pump A of Figure 1 functions independently of the counterbalance system including the air receiver 14 and the compressor 15 which supply air into the outer cylinder 6 below the base piston 6. As the well pump reciprocates to raise and lower the sucker rod string 13, the weight of the rod string and the reciprocating parts of the well pump is supported by the air supplied into the system beneath the piston 5. Thus, the hydraulic power system is relieved of this weight of such movable components, the sucker or polish rod string, and the fluid column in the well above the pump plunger during the upstroke. Thus the hydraulic system is primarily concerned with overcoming friction and accelerating and decelerating the movable masses involved in operating the pump A.

Figures 3, 4 and 5 show a specific preferred structural embodiment of the hydraulic well pump A shown in Figure 1. Corresponding parts of the pump as shown in Figures 3 - 5 will be identified by the same reference numerals used in Figures 1 and 2. Referring to the drawings, the stationary cylinder 6 is mounted on a base 100 provided with a flow coupling fitting 101 which admits counterbalanced air from the receiver 14 and the compressor 15 into the cylinder 6 below the piston 5. The annular counterbalance piston 5 is secured on the lower end of the vertically movable inner cylinder 7 which connects in sealed relationship at the upper end thereof into a cylinder cap 102 connected on the bottom of the sheave platform 8. The inner movable cylinder 7 is mounted in concentric spaced relation over the fixed piston rod 2' which connects at the lower end thereof into the base 100. The counterbalance piston 5 slides in sealed relationship along the outer surface of the piston rod 2'. The upper end of the fixed piston 2' connects into the fixed piston 1. The inner surface of the movable cylinder 7 slides in sealed relationship along the outer surface of the piston 1. The upper end portion of the fixed piston rod 2' is provided with circumferentially spaced ports 4 below the piston 1 to admit hydraulic fluid into the annular space 103 between the piston rod 2' and the cylinder 7 for operating the well pump through its downward stroke. The flow conductor 3 connects through the base 100 extending in concentric spaced relation within the fixed piston rod 2' connecting at the upper end into the piston 1 for supplying hydraulic fluid into the chamber 104 above the piston 1 within the cylinder 7 for operating the well pump through the upward or extend stroke. The flow conductor 3 is spaced within the fixed piston rod 2' defining with the piston rod an annular flow channel 104

for fluid communication between the ports 4 and flow passage means 105 in the base 100 communicating with the flow passage 2 for the hydraulic fluid which operates the pump through the downward stroke. A stop tube 110 is mounted within the annular space 103 on the piston 5 limiting the upward movement of the movable cylinder 7 at the upper end of the upward stroke. The upper end edge of the stop tube 110 engages the lower end edge of the fixed piston 1. The sheaves 9 and 10 are mounted in rotatable spaced relation on the platform 8 within a removable protective cover 111. The flexible tension members 11 extend from fixed ends connected with the anchor 12 to the sucker rod coupling 112 on the movable end of the tension members. The anchor 12 is mounted on the upper end of an anchor post or standard 113 secured on a base 114. A telescoping cable cover formed by an inner sleeve 116 and an outer sleeve 115 is connected between the bottom face of the sheave platform 8 and the platform 114. The upper end of the outer tube is connected with the bottom the platform 8 while the lower end of the inner tube is connected with the platform 114 so that the outer tube telescopes on the inner tube as the platform is raised and lowered during the strokes of the well pump. A cable 120 extends upwardly through the platform 114 through the inner and outer tubes connected at an upper end with the platform 8. As discussed in more detail hereinafter, the free end of the cable, not shown, extends to the hydraulic cylinder stroke length sensor shown in Figures 10A and 10B. The telescoping tube assembly protects that portion of the sensor cable 120 which runs between the platform 114 and the platform 8 during reciprocation of the well pump.

In accordance with the invention the flexible tension members 11 shown in Figures 3-5 are each a special multi-layer band or ribbon assembly each of which

is composed of a number of very thin steel strips bonded together along each end portion of the assembly of the strips adjacent to the anchor 12 and the coupling 112. For example, one set of tension members 11 operated on a

5 prototype of the hydraulic well pump A was formed by eight layers of steel strips each 10/1000 inch (0.025 cm) thick utilizing an epoxy bonding between the layers along the last several inches of each end portion of each strip. A very thin film lubricant was placed between the

10 strips to provide lubrication enhancing the slip between the strips as the strip assembly moves over the sheaves. The layers forming the strip assemblies are held together in a 180° bend around a radius of the same dimension as the sheave radius of the well pump while the bonding

15 procedure is performed. This assures that each of the layers of each strip assembly experiences the same stress when the layered tension member is subjected to normal operating tension over the idler sheaves 9 and 10. It will be apparent that as each layered tension member

20 moves over the sheaves there is a difference in the distance travelled between the inner and outer members and thus slippage occurs between the layers. The film lubricant between the layers provides lubrication for the slippage between the layers. The use of the multiple

25 layered tension members keeps the bending stresses low in each of the metal strips forming the members. It will be recognized that other tension members such as roller chains, single cables, and cables made up of multiple small cables may be used as tension members though the

30 preferred form of multi-layered tension members made up of the metal ribbons or strips provides superior performance. Cables tend to rapidly wear. A single cable requires much larger sheaves to minimize wear.

Referring to Figure 6, the hydraulic well pump B

35 illustrated schematically is a variation of the pump A

shown in Figure 1 wherein the only force supporting the pump load is contributed by the hydraulic cylinder. Counterbalancing is achieved by hydraulically supercharging the hydraulic pump supplying the pressure for lifting the sucker rod string. In Figure 6 those parts corresponding with similar parts of the pump A in Figure 1 will be referred to by the same reference numerals as used in Figure 1. The well pump B primarily differs from the well pump A by the elimination of the counterbalance piston 5 because the counterbalancing is obtained by supercharging the pump supplying the hydraulic pressure for the lift stroke. The lower end of the movable cylinder 7 is closed in sliding sealed relationship with the fixed piston 2 by the annular closure cap 7a. In the well pump B the hydraulic pump 20a is supercharged by a gas charged hydraulic accumulator N2 or a dead weight activated hydraulic accumulator W either of which is connected with the intake side of the pump 20a as shown in Figure 6. The hydraulic power and logic circuitry of Figures 7 and 2B taken together may be used to operate the well pump B. The portion of the system shown in Figure 2B is exactly the same as that portion of the system described in connection with the operation of the well pump A. The portion of the circuitry shown in Figure 7 differs only in the inclusion of the hydraulic accumulators. Referring back to Figures 6 and 7, the notations V1 and V2 as used in Figure 6 designate the right and left sides, respectively of the reversing valve 40 shown in Figure 7. Referring to Figure 6, during the lift stroke of the well pump B, hydraulic fluid pressure is supplied by the pump 20a through the line 23a into the conduit 3 raising the pressure in the chamber 104 above the piston 1 lifting the movable cylinder 7. The reversing valve side V1 is closed forcing the pressure in the accumulator

W or N2, which ever is being used, to supply supercharging pressure into the intake of the pump 20a thereby enhancing the lift of the pump. Hydraulic fluid below the piston 1 returns as the cylinder 7 is raised through the flow channel 2 along the line 23b and through the open reversing cylinder side V2 back to the tank 22. During the downstroke of the well pump B the reversing valve side V2 is closed whereby the output pressure from the pump 20b must flow through the line 23b into the flow passages 2 and outwardly through the ports 4 into the cylinder 7 below the piston 1 forcing the movable cylinder 7 downwardly. During the downward stroke the reversing valve side V1 is open permitting counterbalancing hydraulic fluid pressure to be effective from either the accumulator W or in the accumulator N2 along the line 41c, the line 23a, and the flow conductor 3 into the cylinder chamber 104 above the piston 1 which opposes the downward movement of the cylinder 7. The hydraulic power fluid and logic circuitry of Figures 7 and 2A taken together operate the hydraulic well pump B in exactly the same manner as previously described with respect to the system of Figures 2A and 2B in operating the well pump A. Looking at Figure 7, when the reversing valve 40 is shifted to the left communication between lines 41a and 41c is closed while the line 41b is opened to the tank 22. In this mode of operation the flow from the accumulators W or N2 can only pass to the intake of the pump 20a which discharges into the line 23a flowing to the cap end of the cylinder 7 for operating the pump in the upstroke. The pump 20a is thus supercharged from one of the hydraulic accumulators. During the downstroke the valve 40 is shifted to the right closing off flow in the line 41b to the tank. The pump 20b discharges into the line 23b pumping the cylinder 7 downwardly while the hydraulic accumulator W or N2 is communicated to the

line 41a applying the pressure from the accumulator from the line 23a into the cap end of the cylinder 7. With the exception of the hydraulic accumulators, the remainder of the power and logic circuitry for the hydraulic well pump B as illustrated in Figures 7 and 2B taken together operates exactly as previously described in connection with the well pump A.

A still further form of hydraulic power and logic circuitry employing hydraulic counterbalance is schematically illustrated in Figure 8. Those components of the system of Figure 8 which are similar in structure and function to the components of the previously described system are identified by the same reference numerals as previously used. Referring to Figure 8, the hydraulic cylinder system includes a cylinder 120, piston 121, and a piston rod 122. A weight W supported on the piston rod may be a well pump sucker rod string. A cam 123 movable with the piston rod is engageable with the limit valves 55 and 56 within the logic circuitry of the system. The system is powered by two variable volume hydraulic pumps 124 and 125 which discharge to the head and piston rod end of the cylinder respectively. The pumps are controlled by cams 130 and 131 which are driven on a common shaft with the cam 48 driven by the hydraulic motor 43. The cams are connected with the pumps through suitable links 133 and 134 respectively which operate through suitable bearings 135. A hydraulic counterbalancing accumulator 140 is connected into the suction side of pump 125. A makeup pump 141 also is connected into the suction side of the pump 125. The makeup pump 141 discharges into the suction line of pump 125 through a check valve 142. A line 143 including a pilot operated valve 144 also leads from the discharge of the pump 141 to the tank 22 and to the sequence valve 31a. A line 145 leads from the line 143 downstream from

the valve 144 into the line 23b including a valve 150 pilot operated by the pressure in the line 23b. The cams 130 and 131 are configured to allow only one of the pumps 124 or 125 to deliver fluid to the cylinder 120 at any one time. The accumulator 140 supercharges the suction of the pump 125 to serve as a counterbalance against the weight W so that the only work required of the pump is to overcome friction and that portion of the cylinder stroke which might be under counterbalanced. When pumping down the return fluid below the piston 121 passes through the valve 31b and line 88 to the accumulator providing counterbalancing.

Figure 9 illustrates schematically the hydraulic well pump A coupled with a pump stroke length sensor and controller 150 and a logic device 151 for controlling the linear motion of the hydraulic cylinder of the pump. The device 150 is illustrated in detail in Figures 10A, 10B and 11-22 inclusive. The device 151 is illustrated in Figures 23-35. It is to be understood that the devices 150 and 151 are illustrative of systems which may be employed to control the length of the stroke of the hydraulic pumps previously described and the character of motion during each stroke.

Referring to Figures 10A, 10B, and 11-13, the device 150 includes structure for mounting the limit valves 55 and 56 and the operating cam C (or cam 123 previously referred to) for the valves in a protected remote location from the hydraulic cylinder structure of the well pump. The only physical connection required between the device 150 and the hydraulic cylinder assembly is the operating cable 120 which extends between the hydraulic cylinder assembly and the sensor device 150. The device 150 simulates the cylinder movement shifting the cam C between the limit valves 55

and 56.

The sensor device 150 includes a travelling sheave block supporting the cam C and moving in a housing 153 between the valves 55 and 56. The cable 120 is reeved over a pair of sheaves 154 and 155 carried by the travelling block and fixed sheaves 160 and 161 in the housing as shown in Figure 13. As evident from Figures 10A, 10B, 12 and 14, the housing 153 is a hollow square elongate member having an elongated top slot 162 along which the cam C is moved between the valves 55 and 56. A rectangular elongated spacer bar 164 is secured on the back face of the housing as seen in Figure 14. The sheaves 154 and 155 are rotatably mounted in the travelling block 152 shown in detail in Figures 18-22. The sheaves are mounted in two slots which open through the opposite ends of the travelling block aligned at 90° angles with respect to each other. The sheave 154 is mounted in a slot 165, Figure 20, opening upwardly and downwardly into the left end of the block 152 as viewed in Figures 10A and 18. The sheave 154 is supported on a shaft, not shown, extending through a hole 170, Figure 22, intersecting the slot 165 at a 90° angle. Similarly the sheave 155 is mounted in a slot 170 opening through the top and bottom and opposite end of the travelling block as shown in Figures 18 and 19. The octagon shape of the travelling block permits the block to slide within the housing and sufficient portions of the sheaves to project beyond the block to carry the cable on the sheaves within the housing. The sheaves 160 and 161 are mounted on a stationary block 171 secured in the right end of the housing 153 as seen in Figures 10B and 12. The stationary block is shown in detail in Figures 15-17. The sheaves 160 and 161 are rotatably mounted in vertical

slots 172 and 173 along opposite sides of the stationary block. The stationary block has an internally threaded horizontal bore 174 opening at opposite ends to the slots 171 and 172 for the mounting shafts, not shown, on which the sheaves 160 and 161 are rotatably supported. The stationary block also has a horizontal internally threaded bore 175 for a bolt and nut assembly 180, Figures 10B and 12, securing the stationary block in the right end of the housing as seen in Figure 10B. A locking recess 181 is provided in the stationary block comprising a cylindrical recess portion which opens to a longitudinal recess opening through the top end of the stationary block opposite where the sheaves 160 and 161 are mounted. The recess 181 receives an anchor ball 119 secured on the fixed end of the cable 120 for anchoring the cable end with the stationary block. The cable is reeved over the sheaves as shown in Figure 13 with the cable passing off of the sheave 160 to the movable end of the cable connected with the platform 8 of the hydraulic well pump. A coil spring 182 is compressed in the housing between the stationary block 171 and the travelling block 152 for urging the travelling block away from the stationary block. Since the fixed end of the cable is anchored to the stationary block, when the cable is pulled by upward movement of the well pump platform 8, the travelling block is pulled toward the stationary block against the spring. When the well pump platform moves downwardly the cable is moved toward the sensor allowing the spring 182 to expand forcing the travelling block along the housing away from the stationary block moving the cam C toward the valve 55. In the particular embodiment of the sensor illustrated the cam C comprises two cam members C1 and C2 independently mounted in side-by-side relationship on the top of the travelling block so that the cams extend through and are movable

along the slot 162 in the top of the housing 153. One of the cam members operates one of the valves 55 and 56 while the other cam member operates the other limit valve.

5 As evident in Figures 10A, 10B, 11 and 12, the limit valves 55 and 56 are supported from a vertical mounting plate 183 secured to the bar 164 along the back of the housing 153. The limit valves are movably mounted over
10 the line of travel of the cam members C1 and C2 with one of the valves being aligned with one of the cam members and the other valve aligned with the other of the cam members. Each of the limit valves is secured with a valve manifold 184 which provides fluid communication to
15 the valve and a mounting for the valve. The valve manifolds 184 are slidable horizontally along a slot 185 in the mounting plate. Identical threaded adjusting bars 190 extend along the slot 185 through an internal threaded bore of the valve manifold so that when the
20 adjusting bar 190 is turned the limit valve associated with the adjusting bar is moved horizontally. The inward ends of the adjusting bars 190 have bearing portions mounted in a central retainer 191. The outward
25 end portions of the adjusting bars 190 have flat surfaces 192 for engagement of a wrench to rotate the bar for adjusting the longitudinal position of the limit valve associated with the bar. As seen in Figure 11 the limit valve 55 is secured with a spacer plate 193 which aligns the valve 55 slightly forward of the valve 56 so that the valve 55 is in alignment with the front cam member C1
30 while the valve 56 is aligned with the rear cam member C2. The valves 55 and 56 are independently movable longitudinally so that both the length of the hydraulic pump stroke and the upper and lower limit of the stroke are adjustable. The movement of the cam members exactly
35 simulates the movement of the well pump platform 8 which

is one-half of the full stroke of the pump. Since the only physical connection between the hydraulic cylinder assembly of the well pump and the sensor device 150 is through the cable 120, the sensor device may be housed separately at a location remote from the hydraulic cylinder assembly which is of course at the wellhead for raising and lowering the pump sucker rod string.

The control valve device or mechanism 151 illustrated in Figures 23-35 provides the operation requirements of the following components of the hydraulic power and logic system shown in Figures 2A and 2B: valve 40; coupling 46; crank arm 45; valve 85; cam 83; valve 84; valve 57; cam 48 with the cam lobes 49; and the logic drive motor 43. Utilizing the control valve mechanism 151, it is to be understood that the other components of the system of Figures 2A and 2B are connected with the control valve mechanism.

Referring to Figures 23 and 24, the valve control mechanism 151 includes a body 200 mounted on a bracket 201. The hydraulic drive motor 43 is secured to the back of the body. The valves 57 and 84 are mounted on top of the body. The valve 85 is supported from the bottom of the body. Identical poppet valve assemblies 202 are mounted on opposite sides of the body providing valve functions corresponding with the opposite side or end sections of the valve 40 for controlling the extend and retract functions of the hydraulic cylinder assembly. The details of the body 200 are shown in Figures 25-27. The body has a central rectangular portion 203 provided with an internal rectangular cavity 204. Cylindrical valve body portions 205 extend from the opposite sides of the body for housing the poppet valve assemblies 202. The valve bores of the body portions 205 communicate through cylindrical bores 210 to the central cavity 204 of the body. As seen in Figure 26, the top of the body

is provided with a forward opening 211 for the valve 57 and a rearward opening 212 for the valve 84. Similarly the bottom of the body, Figure 27, is provided with an opening 213 for the valve 85. The poppet valve body portions 205 each has a poppet valve inlet 214 and a poppet valve outlet 215. The valves 57, 84, 85, and the poppet valves 202 are operated by the hydraulic motor 43 through cam and cross head structure mounted on the motor shaft. Referring to Figures 23 and 24, a cam crank 220 is held on the motor shaft 221 of the motor 43 by a retainer 222 secured by a bolt 223. A key 224 is positioned in aligned slots of the shaft and crank for driving the crank as the shaft rotates. As shown in Figures 30 and 31, the cam crank 220 has an integral cam 225 for operating the valves 84 and 85 as the cam crank is turned by the motor. The cam also has an integral cross head shaft 230 for driving the cross head of the valve control mechanism. A cross head 231, Figures 28 and 29, is coupled with the cross head shaft 230. The cross head has a vertical slot 232 through which the cross head shaft extends. A bushing 233 is fitted on the cross head shaft within the slot 232. The cross head and bushing are held on the cross head shaft by a thrust washer secured on the cross head shaft by a lock ring 235. The cross head shaft has horizontally spaced sidewardly opening slots 240 for coupling the poppet valve assemblies 202 with the cross head. The cams 49 are secured in horizontal spaced relation in the top portion of the cross head in an upwardly opening recess 241 by cap screws 242. As the cross head reciprocates horizontally the cams 49 operate the valve 57.

The poppet valves assemblies 202 of the valve control mechanism 151, Figures 2-3 and 32-35, each includes a valve seat 250, a valve 251, and a valve operator spool 252. As shown in Figure 32, the valve

seat has a cylindrical externally threaded outer portion 253 which secures the valve seat in the body portion 205. The valve seat also has a tubular inner portion 254 provided with circumferentially spaced elongated flow ports 255. The valve seat portion 254 has a seat surface 260. The bore of the body portion 205 is enlarged along the valve seat providing an annular poppet valve discharge chamber 261 which communicates with the discharge opening 215 in the body portion 205. A ring seal 212 around the valve seat portion 254 seals between the valve seat and the poppet valve body portion 205 inward from the discharge chamber 261. Referring to Figure 33, the valve 251 has a tubular portion 270 which telescopes into the valve seat tubular portion 254. The tubular portion 270 of the valve is provided with four circumferentially spaced elongated discharge ports 271 which are circumferentially aligned with the discharge port 255 of the valve C so that fluid within the valve portion 270 flows outwardly through the ports 271 of the valve and through the ports 255 of the valve seat into the discharge chamber 261. The valve has an enlarged body portion 272 and an external annular tapered valve seat 273 between the tubular portion 270 and the body portion. The valve seat 273 on the valve is engageable with the valve seat 260 on the valve seat. The tubular portion 270 of the valve fits in close sliding relationship within the tubular portion 254 of the valve seat so that as the valve is moved relative to the valve seat in an axial direction, a linear relationship exists between the valve discharge ports 271 and the valve seat so that the flow rate through the valve is directly proportional to the distance travelled by the valve. For example if the valve is moved 25% of its total travel, the flow rate therethrough is changed 25 percent. The body portion of the valve is secured with the valve spool

252 by a retainer screw 274. As seen in Figure 34 the valve spool 252 has an endwardly opening internally threaded blind bore 275 for engagement of the retainer screws 274 in the spool. The bore of the body portion 205 along the valve and spool is enlarged to provide an annular inlet chamber 280 which communicates with the poppet valve inlet port 214. To provide for a tight shut-off between the valve seat and the poppet valve, an area differential between the poppet seal area and the area of the spool is provided so that the shut in pressure within the chamber 280 biases the poppet valve toward the seat. The inward end of the valve spool has upwardly and downwardly opening recesses 281 and flange portions 282 for coupling the valve spools with the cross head in the slots 240 of the cross head. The front of the body 203 of the valve control mechanism is closed by the plate 283 so that the chamber 204 in which the cams and cross head operate is sealed. Such chamber is communicated with the fluid reservoir of the system when the valve control mechanism is connected into the power and logic system such as shown in Figures 2A and 2B. The spool 252, and the retainer screws 274 have a longitudinal axial bore 284 which communicates the chamber 204 with the chamber 261 both of which are at reservoir pressure so that there is no pressure differential across the spool.

When the valve control device 151 is connected in a hydraulic power and logic system such as that shown in Figures 2A and 2B, the driving of the hydraulic motor 43 turns the cam crank 220 rotating the cam lobe 225 and the cross head shaft 230 which causes the cross head 231 to reciprocate horizontally. As the cam lobe 225 rotates the valves 84 and 85 are operated. As the cross head reciprocates the cam lobes 49 connected with the cross head operate the valve 57. Since the cross head is

coupled with the poppet valve spools 284 reciprocation of the spools opens and closes the poppet valves performing the valving function of both sides of the valve 40. At midposition of the cross head both of the poppet valves are open and thus the chambers 202 of both poppet valves communicate with the chambers 261 of the poppet valves so that the pumps 20a and 20b both communicate with the reservoir and thus are not operating the hydraulic well pump cylinder 7. At each extreme side position of the cross head, the poppet valve on the side to which the cross head is nearest is closed while the opposite poppet valve is fully open. The relationship between the ports in the valve and the ports in the valve seat of the poppet valve provides linear opening of each of the poppet valves so that the valves flow in direct proportion to the extent to which the valve is open. This arrangement provides for direct control of the acceleration and deceleration of the hydraulic well pump which is dependent upon the rates of opening and closing the poppet valves. In other words, the rate at which the hydraulic well pump accelerates or decelerates is directly proportional to the rate at which the poppet valves are opened and closed. That rate is controllable by the rate at which the motor 43 is operated which in turn may be controlled by a manual control of the metering valve 60 in the line 52 supplying hydraulic drive fluid to the motor 43. One of the poppet valves controls the cylinder extension in the hydraulic well pump while the other of the valves controls the cylinder retraction. The hydraulic motor driven cross head or "scotch yoke" mechanism when operating uniformly causes the two poppet valves to alternately open and close in a velocity pattern of harmonic motion. The cam lobes 49 on the cross head operate the limit valve 57 at the extreme right and left positions of the cross head.

Reference is hereby made to our U.K. Patent Application 8604537 which has been divided out of the present application.



-33-

CLAIMS

1. A system for operating a sucker rod string connected with a well pump comprising:

a double-acting fluid cylinder having opposing power ends;

5 means for connecting said cylinder with said sucker rod string for raising and lowering said string to operate said pump;

means for supplying pressurized fluid alternately to the cylinder ends including a direction control valve

10 means movable between extend and retract conditions to extend and retract said cylinder;

drive means for shifting said direction control;

control means for operating said drive means responsive to the extend and retract movements of said cylinder; including limit valves positioned to simulate the hydraulic cylinder extend and retract stroke end locations, said limit valves being movably mounted for changing the location of each limit valve and the distance between said limit valves for selectively

20 adjusting the length of the strokes of said hydraulic cylinder and the end limit of the extend and retract strokes of said cylinder, cam operator means for opening and closing each of said limit valves at said end locations and connection means connecting said cam

25 operator means with said hydraulic cylinder whereby said cam operator means simulates the extend and retract strokes of said hydraulic cylinder, said connection means including a flexible cable secured at a first end with said hydraulic cylinder and connected with said cam

30 operator means to move said cam operator means; movable sheave means arranged to move the cam operator means and fixed sheave means spaced from said movable sheave means, means biasing said movable sheave means away from said fixed sheave means, said cable being reeved over said



62

-34-

- movable and fixed sheave means and secured along the second end thereof at a fixed location so that movement of said cylinder causes the movable sheave means to move relative to the fixed sheave means; and means for applying
- 5 a fluid counterbalancing force into said cylinder for offsetting the combined weights of said sucker rod string, a production fluid column in a well bore above said pump, and movable surface equipment supported on said cylinder.
2. The system according to claim 1 further comprising a
- 10 longitudinally movable block secured with said movable sheave means and said cam operator means, a stationary block secured with said fixed sheave means and said second end of said cable, and said means biasing said movable sheave means away from said fixed sheave means comprises a
- 15 spring between said movable and said fixed blocks.
3. The system according to claim 2 further comprising an elongated housing, said stationary block being secured along one end of said housing, said movable block being slidable in said housing, said housing being provided with
- 20 a longitudinal top slot for said cam operator means, a limit valve mounting plate on said housing, and an adjusting screw securing each said limit valve with said plate, each said limit valve being movably supported on a separate one of said screws above said housing slot for
- 25 engagement by said cam operator means.
4. The system according to any of claims 1-3 wherein said counterbalance force means includes a counterbalance piston on said fluid chamber, a counterbalance cylinder around said fluid cylinder in sealed relationship with
- 30 said counterbalance piston and defining a counterbalance chamber below said counterbalance piston; and means for supplying a counterbalance fluid into said counterbalance chamber.
5. The system according to any of claims 1-4 wherein
- 35 said counterbalance fluid is a gas.
6. The system according to claim 5 wherein said counterbalance fluid is air.



- 5 7. The system according to any preceding claim wherein said direction control valve means is operable to direct said pressurized fluid into one of said power ends of said cylinder while returning pressurized fluid from the other of said power ends to extend and retract said cylinder; said direction control valve means including spaced fluid control valves having fluid connection, respectively, with the said power ends of said hydraulic cylinder, said drive means including a rotary fluid motor and a scotch-yoke having a crosshead coupling said motor with said direction control valve means, the control means being operative to control said motor responsive to the extend and retract movements of said cylinder.
- 10 8. The system according to claim 7 in which said control valves are positioned on opposite sides of and connected with the crosshead of said scotch-yoke.
- 15 9. The system according to claim 8 in which said fluid control valves are poppet valves having a valve member connected with said scotch-yoke crosshead.
- 20 10. The system according to claim 9 in which said poppet valves each include port means providing linear opening of said valves.
- 25 11. The system according to claim 10 in which said control means for operating said drive means includes a pilot valve for controlling fluid to said motor and cam means on said crosshead for operating said pilot valve.
- 30 12. The system according to claim 11 further comprising release valves associated with said control means and rotating cam means connected with said motor for operating said release valves.
13. The system according to any preceding claim including an idler sheave platform mounted on said cylinder, idler sheave means mounted on said platform and flexible tension member means secured at a first fixed



35

-36-

end with said hydraulic cylinder base, extending over said sheave means and downwardly therefrom to a movable second end having means for connecting said tension member means to the sucker rod string.

- 5 14. The system for operating a sucker rod string connected with a well pump comprising: a double-acting hydraulic cylinder assembly including a base, a stationary piston rod secured to its lower end to said base and extending upwardly therefrom, an annular stationary piston
- 10 secured along an upper end portion of said piston rod, a cylinder movable positioned around said annular piston, a cylinder cap secured on the upper end of said cylinder defining with said cylinder and said annular piston a hydraulic fluid extend chamber within said cylinder above
- 15 said annular piston, an annular closure between the lower end of said cylinder and said piston rod below said annular piston defining with said annular piston, said cylinder, and said piston rod an annular hydraulic fluid retract chamber below said annular piston, said piston rod
- 20 having ports along an upper portion thereof below said annular piston for admitting hydraulic fluid to said retract chamber, a flow conductor disposed in spaced concentric relation within said piston rod connecting through said annular piston at an upper end thereof into
- 25 said extend chamber and connecting through said base for admitting hydraulic fluid into said cylinder assembly to said extend chamber, the outer surface of said flow conductor and the inner surface of said piston rod defining an annular hydraulic fluid flow passage within
- 30 said piston rod around said flow conductor for hydraulic fluid flow to said annular retract chamber, and flow passage means including a flow coupling in said base communicating with said annular hydraulic fluid flow passage; an idler sheave platform mounted on the upper end
- 35 of said cylinder of said hydraulic cylinder assembly; idler sheave means mounted on said sheave platform;

(6)



-37-

flexible tension member means secured at a first fixed end with said hydraulic cylinder assembly base, extending over said sheave means and downwardly therefrom to a movable second end; means on said second end of said

5 tension member for securing said tension member with a well pump sucker rod string; hydraulic fluid power and logic circuitry connected with said hydraulic cylinder assembly for extending and retracting said movable cylinder to raise and lower said second movable end of

10 said tension member including movably positioned limit valves for sensing the end position of each said extend and retract stroke, said valves being adapted to be selectively positioned for varying said end of each of said strokes and varying the length of said strokes, cam

15 means secured in movable relation with said limit valves for engaging and operating said limit valves, a flexible member having a first end connected with said hydraulic cylinder and a second portion spaced from said first end coupled with said cam means to simulate the movement of

20 said hydraulic cylinder; a hydraulic fluid reversing valve for directing flow to the opposite ends of said hydraulic cylinder assembly; means for operating said reversing valve including a hydraulic drive motor actuated responsive to said limit valves and a

25 scotch-yoke coupled between said drive motor and said reversing valve for operating said reversing valve; and a hydraulic counterbalance system including an annular counterbalance piston and cylinder mounted around said hydraulic cylinder for offsetting the combined weights of

30 said sucker rod string, a column of well fluid in a well bore above a well pump operated by said sucker rod string, and the movable components of said sucker rod string supported by said movable hydraulic cylinder.

15. A system for operating a sucker rod string connected

35 with a well pump substantially as described with reference to and as illustrated in any of the accompanying drawings.
