

[DESCRIPTION]

[Title of Invention] METHOD OF BONDING METAL MEMBERS AND METAL MEMBER JOINT BODY

[Technical Field]

[0001]

The present disclosure relates to a method of bonding metal members and a metal member joint body.

[Background Art]

[0002]

Heat-resistant alloys such as Ni alloys and Fe alloys are used for metal members used in gas turbines and chemical plants that operate at high temperatures. Diffusion bonding, which can ensure high joint strength and sealing properties, may be applied to structural members with joints (see PTL 1).

[Citation List]

[Patent Literature]

[0003]

[PTL 1] Japanese Patent Application Publication No. 2014-161885

[Summary of Invention]

[Technical Problem]

[0004]

It is to be noted that, as the heat-resistant alloy as described above, a carbide-containing Ni alloy or carbide-containing Fe alloy containing a carbide is used in order to improve the mechanical strength and the like. Meanwhile, solid phase diffusion bonding may be applied to diffusion bonding of metal members formed of a carbide-containing Ni alloy or carbide-containing Fe alloy.

[0005]

However, in the case of solid phase diffusion bonding in

which the bonding surfaces of the metal members formed of a carbide-containing Ni alloy or carbide-containing Fe alloy are directly abutted with each other, the presence of carbides along the bonding interface can result in a situation where the bonding interface serves as a crack propagation path. As a result, the mechanical strength of the metal member joint body may decrease.

[0006]

Therefore, an object of the present disclosure is to provide a method of bonding metal members and a metal member joint body capable of further improving the mechanical strength.

[Solution to Problem]

[0007]

A method of bonding metal members according to the present disclosure includes a stacked body forming step of forming a stacked body by putting an insert material between a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys, and a solid phase diffusion bonding step of forming a metal member joint body by heating and pressurizing the stacked body to perform solid phase diffusion bonding, wherein the insert material contains Ni having a content higher than an Ni content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Ni alloys, and contains Fe or Ni having a content higher than an Fe content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Fe alloys.

[0008]

In the method of bonding metal members according to the present disclosure, the first metal member and the second metal member may be formed of the carbide-containing Ni alloys, and the insert material may contain Ni having a content higher than the Ni content of the first metal member and the second metal member.

[0009]

In the method of bonding metal members according to the present disclosure, the insert material may be formed of pure Ni.

[0010]

In the method of bonding metal members according to the present disclosure, it may include a heat treatment step in which the metal member joint body is heat-treated to grow crystal grains of a bonding portion between the first metal member and the second metal member across a bonding interface of the bonding portion.

[0011]

A metal member joint body according to the present disclosure includes a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys, and a bonding portion provided between the first metal member and the second metal member and formed of a diffusion layer, wherein the bonding interface of the bonding portion has no carbides precipitated therein.

[0012]

In the metal member joint body according to the present disclosure, the first metal member and the second metal member may be formed of the carbide-containing Ni alloys.

[0013]

In the metal member joint body according to the present disclosure, the crystal grains of the bonding portion may be across the bonding interface.

[0014]

The above configuration makes it possible to suppress carbides at the bonding interface between the first metal member and the second metal member, improving the mechanical strength of the metal member joint body.

[Brief Description of Drawings]

[0015]

[Fig. 1] Fig. 1 is a flowchart showing a configuration of a method of bonding metal members in an embodiment of the present disclosure.

[Fig. 2] Fig. 2 is a diagram showing a configuration of a stacked body in the embodiment of the present disclosure.

[Fig. 3] Fig. 3 is a diagram showing a configuration of a metal member joint body in the embodiment of the present disclosure.

[Fig. 4] Fig. 4 is a graph showing the results of tensile tests of each specimen in the embodiment of the present disclosure.

[Fig. 5] Fig. 5 is a graph showing the creep test results of each specimen in the embodiment of the present disclosure.

[Fig. 6] Fig. 6 is a photograph showing the metal structure observation results of the specimen of Comparative Example 1 in the embodiment of the present disclosure.

[Fig. 7] Fig. 7 is a photograph showing the metal structure observation results of the specimen of Example 1 in the embodiment of the present disclosure.

[Fig. 8] Fig. 8 is a photograph showing the metal structure observation results of the specimen of Example 2 in the embodiment of the present disclosure.

[Fig.9] Fig. 9 is a photograph showing the metal structure observation results of the specimen of Comparative Example 2 in the embodiment of the present disclosure.

[Description of Embodiments]

[0016]

Hereinafter, embodiments of the present disclosure are described in detail with reference to the drawings. Fig. 1 is a flowchart showing a configuration of a method of bonding metal members. The method of bonding metal members includes a stacked body forming step (S10) and a solid phase diffusion bonding step (S12).

[0017]

The stacked body forming step (S10) is a step of forming a stacked body by putting an insert material between a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys. Fig. 2 is a diagram showing a configuration of the stacked body 10. The stacked body 10 is configured by putting the insert material 16 between the first metal member 12 and the second metal member 14. The first metal member 12 and the second metal member 14 are formed of carbide-containing Ni alloys or carbide-containing Fe alloys. The first metal member 12 and the second metal member 14 may be formed of carbide-containing Ni alloys, or the first metal member 12 and the second metal member 14 may be formed of carbide-containing Fe alloys.

[0018]

The carbide-containing Ni alloy is an Ni alloy containing carbides, with the main component of the alloy being composed of Ni. The main component of an alloy is the alloying element having the highest content among the alloy components (the same

applies hereinafter). The carbide-containing Ni alloy contains C as an alloy component. The content of C can be, for example, 0.01% by mass to 1% by mass. As the carbide-containing Ni alloy, it is possible to use a solid solution strengthened Ni alloy obtained by solid-soloving Mo, W, or the like, a precipitation strengthened Ni alloy obtained by precipitating the γ' -phase, or the like.

[0019]

As the carbide-containing Ni alloy, for example, Haynes 230 alloy can be used. The Haynes 230 alloy is a solid solution strengthened Ni alloy containing carbides. The alloy composition of the Haynes 230 alloy includes, for example, 22% by mass of Cr (chromium), 14% by mass of W (tungsten), 2% by mass of Mo (molybdenum), 3% by mass or less of Fe (iron), 5% by mass or less of Co (cobalt), 0.5% by mass of Mn (manganese), 0.4% by mass of Si (silicon), 0.5% by mass or less of Nb (niobium), 0.3% by mass of Al (aluminum), 0.1% by mass or less of Ti (titanium), 0.1% by mass of C (carbon), 0.02% by mass of La (lanthanum), and 0.015% by mass or less of B (boron), in which the balance is composed of Ni (nickel) and incidental impurities. The carbides contained in the Haynes 230 alloy are Cr carbides, W carbides, and the like. Carbides are precipitated in crystal grains, crystal grain boundaries, and the like.

[0020]

The carbide-containing Fe alloy is an Fe alloy containing carbides, with the main component of the alloy being composed of Fe. The carbide-containing Fe alloy contains C as an alloy component. The content of C can be, for example, 0.01% by mass to 1.2% by mass.

[0021]

As the carbide-containing Fe alloy, stainless steel can be used. As the stainless steel, it is possible to use austenitic stainless steel, ferritic stainless steel, austenitic-ferritic stainless steel, martensitic stainless steel, precipitation hardened stainless steel, and the like.
[0022]

When the first metal member 12 and the second metal member 14 are formed of carbide-containing Ni alloys, the first metal member 12 and the second metal member 14 may be formed of the same carbide-containing Ni alloy, or the first metal member 12 and the second metal member 14 may be formed of different carbide-containing Ni alloys. For example, when the first metal member 12 is formed of a Haynes 230 alloy, the second metal member 14 may be formed of a Haynes 230 alloy, or the second metal member 14 may be formed of a carbide-containing Ni alloy different from the Haynes 230 alloy.
[0023]

When the first metal member 12 and the second metal member 14 are formed of carbide-containing Fe alloys, the first metal member 12 and the second metal member 14 may be formed of the same carbide-containing Fe alloy, or the first metal member 12 and the second metal member 14 may be formed of different carbide-containing Fe alloys.
[0024]

The insert material 16 is provided so as to be put between the first metal member 12 and the second metal member 14. More specifically, the insert material 16 is inserted between the bonding surface of the first metal member 12 and the bonding surface of the second metal member 14.
[0025]

The insert material 16 contains Ni having a content higher than an Ni content of the first metal member 12 and the second metal member 14 when the first metal member 12 and the second metal member 14 are formed of the carbide-containing Ni alloys, and contains Fe or Ni having a content higher than an Fe content of the first metal member 12 and the second metal member 14 when the first metal member 12 and the second metal member 14 are formed of the carbide-containing Fe alloys.

[0026]

Since the insert material 16 contains Ni or Fe having a content higher than the content of Ni or Fe in the first metal member 12 and the second metal member 14, carbides at the bonding interface of the first metal member 12 and the second metal member 14 and in the vicinity thereof can be solid-solved in the insert material 16 during solid phase diffusion bonding. This makes it possible to suppress the presence of carbides along the bonding interface between the first metal member 12 and the second metal member 14. As described above, the insert material 16 is formed so that carbides at the bonding interface and in the vicinity thereof can be dissolved during solid phase diffusion bonding.

[0027]

More specifically, the presence of carbides along the bonding interface of the first metal member 12 and the second metal member 14 can result in a situation where there will be cracks or a propagation path of the cracks. In addition, the presence of carbides along the bonding interface can result in a situation where the carbides act as a diffusion barrier and inhibit mutual solid phase diffusion, which may reduce the bonding strength. According to the insert material 16, by

solid-soluble carbides during solid phase diffusion bonding, it is possible to suppress the presence of carbides along the bonding interface of the first metal member 12 and the second metal member 14. This makes it possible to promote solid phase diffusion and suppress the occurrence of cracks.

[0028]

When the first metal member 12 and the second metal member 14 are formed of carbide-containing Ni alloys, the insert material 16 may be formed of an Ni alloy containing Ni having a content higher than the Ni content of the first metal member 12 and the second metal member 14, or the insert material 16 may be formed of pure Ni. Pure Ni having a purity of 99% or more may be used.

[0029]

When the first metal member 12 and the second metal member 14 are formed of carbide-containing Fe alloys, the insert material 16 may be formed of an Fe alloy containing Fe having a content higher than the Fe content of the first metal member 12 and the second metal member 14, or the insert material 16 may be formed of pure Fe. Pure Fe having a purity of 99% or more may be used. In addition, when the first metal member 12 and the second metal member 14 are formed of carbide-containing Fe alloys, the insert material 16 may be formed of an Ni alloy containing Ni having a content higher than the Fe content of the first metal member 12 and the second metal member 14, or the insert material 16 may be formed of pure Ni. Pure Ni having a purity of 99% or more may be used.

[0030]

When the insert material 16 is formed of pure Ni or pure Fe, the insert material 16 becomes softer and more easily

plastically deformed than when the insert material 16 is formed of an Ni alloy or an Fe alloy. For this reason, the insert material 16 can be brought into close contact with the bonding surfaces of the first metal member 12 and the second metal member 14 during solid phase diffusion bonding.

[0031]

The insert material 16 can be formed of a sheet, foil, or the like. The insert material 16 may be formed of, for example, a pure Ni foil or a pure Fe foil. The thickness of the insert material 16 can be 20 μm or less. This is because if the thickness of the insert material 16 is larger than 20 μm , it may take a long time for solid phase diffusion. The thickness of the insert material 16 may be 5 μm or more and 10 μm or less.

[0032]

For the first metal member 12, the second metal member 14, and the insert material 16, the surface roughness may be adjusted, and pretreatment such as degreasing cleaning may be performed before stacking.

[0033]

The solid phase diffusion bonding step (S12) is a step of forming a metal member joint body by heating and pressurizing a stacked body 10 to perform solid phase diffusion bonding. Fig. 3 is a diagram showing the configuration of the metal member joint body 20. By heating and pressurizing the stacked body 10 to perform solid phase diffusion bonding, a bonding portion 22 being a diffusion layer is formed between the first metal member 12 and the second metal member 14. The thickness of the bonding portion 22 can be, for example, 10 μm to 100 μm .

[0034]

More specifically, by heating and pressurizing the stacked body 10, metal elements are mutually solid phase diffused between the first metal member 12, the second metal member 14, and the insert material 16, and thereby a bonding portion 22 being a diffusion layer is formed. The bonding portion 22 may be formed to contain Ni or Fe having a content higher than the content of Ni or Fe of the first metal member 12 and the second metal member 14. For example, when the first metal member 12 and the second metal member 14 are formed of carbide-containing Ni alloys, the bonding portion 22 may be formed to contain Ni having a content higher than the content of Ni in the first metal member 12 and the second metal member 14.

[0035]

During solid phase diffusion bonding, since the carbides at the bonding interface 24 of the first metal member 12 and the second metal member 14 and in the vicinity thereof are solid-solved in the insert material 16, the bonding interface 24 of the first metal member 12 and the second metal member 14 has no carbides precipitated therein. This suppresses the presence of carbides along the bonding interface 24 of the first metal member 12 and the second metal member 14, making it possible to prevent a situation where the bonding interface 24 serves as a crack propagation path. As a result, it is possible to improve the bonding strength of the bonding portion 22.

[0036]

The bonding conditions (bonding temperature, bonding pressure, bonding time, and bonding atmosphere) when the first metal member 12 and the second metal member 14 are carbide-containing Ni alloys will be described. The bonding

temperature can be 1050°C or higher and 1200°C or lower. This is because if the bonding temperature is lower than 1050°C, it may be impossible to sufficiently solid-solve the carbides in the bonding interface 24 of the first metal member 12 and the second metal member 14 and in the vicinity thereof, which may result in insufficient solid phase diffusion and a decrease in bonding strength. This is also because if the bonding temperature is higher than 1200°C, the growth of crystal grains becomes rapid, which may decrease the mechanical strength. The bonding temperature may be 1050°C or higher and 1150°C or lower. [0037]

The bonding pressure can be 5 MPa or more and 20 MPa or less. This is because if the bonding pressure is less than 5 MPa, the adhesion between the first metal member 12, the second metal member 14, and the insert material 16 may decrease, which may result in insufficient solid phase diffusion. This is also because if the bonding pressure is more than 20 MPa, the first metal member 12 and the second metal member 14 may be deformed or the like. The bonding pressure may be 5 MPa or more and 10 MPa or less. [0038]

The bonding time can be 4 hours or longer and 10 hours or shorter. This is because if the bonding time is shorter than 4 hours, the solid phase diffusion at the bonding interface 24 of the first metal member 12 and the second metal member 14 and in the vicinity thereof may be insufficient, which may result in a decrease in bonding strength. The reason why the bonding time is 10 hours or shorter is that if the bonding time is 10 hours, the carbides at the bonding interface 24 and in the vicinity thereof can be sufficiently dissolved to enable solid

phase diffusion bonding. In addition, if the bonding time is longer than 10 hours, the productivity decreases.

[0039]

The bonding atmosphere may be non-oxidizing atmosphere such as a vacuum atmosphere or an inert gas atmosphere by argon gas or the like. This suppresses oxidation of the bonding surfaces of the first metal member 12, the second metal member 14, and the insert material 16, making it possible to promote solid phase diffusion. In the case of a vacuum atmosphere, it may be 1.3×10^{-2} Pa or less.

[0040]

The solid phase diffusion bonding step (S12) may be followed by a heat treatment step in which the metal member joint body 20 is heat-treated to grow crystal grains of a bonding portion 22 between the first metal member 12 and the second metal member 14 across a bonding interface 24 of the bonding portion 22. The creep characteristics of the metal member joint body 20 can be improved by growing the crystal grains of the bonding portion 22 across the bonding interface 24. In addition, by heat-treating the metal member joint body 20, the composition of the bonding portion 22 can be made more uniform.

[0041]

The heat treatment conditions (heat treatment temperature, heat treatment time, and heat treatment atmosphere) when the first metal member 12 and the second metal member 14 are carbide-containing Ni alloys will be described. The heat treatment temperature can be 1050°C or higher and 1200°C or lower. This is because when the heat treatment temperature is lower than 1050°C, the crystal grains of the bonding portion 22 may hardly grow. This is also because if

the heat treatment temperature is higher than 1200°C, the growth of crystal grains of the first metal member 12 and the second metal member 14 becomes rapid, which may decrease the mechanical strength. The heat treatment temperature may be 1050°C or higher and 1150°C or lower.

[0042]

The heat treatment time can be 5 hours or longer and 75 hours or shorter. This is because if the heat treatment time is shorter than 5 hours, the growth of crystal grains of the bonding portion 22 may be insufficient. The reason why the heat treatment time is 75 hours or shorter is that if the heat treatment time is 75 hours, it is a sufficient time for the crystal grains of the bonding portion 22 to grow across the bonding interface 24. The heat treatment time may be 50 hours or longer and 75 hours or shorter.

[0043]

The heat treatment atmosphere may be a non-oxidizing atmosphere such as a vacuum atmosphere or an inert gas atmosphere by argon gas or the like. This suppresses oxidation of the metal member joint body 20 during the heat treatment. The heat treatment atmosphere may be the same as the bonding atmosphere.

[0044]

For the solid phase diffusion bonding of the stacked body 10, a general diffusion bonding equipment can be used, such as a vacuum diffusion bonding equipment, a vacuum hot press equipment, or a hot isotropic pressing (HIP) equipment. In addition, for the heat treatment of the metal member joint body 20, it is possible to use a general heat treatment equipment for a metal material.

[0045]

Next, the configuration of the metal member joint body 20 bonded by the above metal member bonding method will be described. A metal member joint body 20 includes a first metal member 12 and a second metal member 14 formed of carbide-containing Ni alloys or carbide-containing Fe alloys, and a bonding portion 22 provided between the first metal member 12 and the second metal member 14 and formed of a diffusion layer. Additionally, the bonding interface 24 of the bonding portion 22 has no carbides precipitated therein.

[0046]

More specifically, the bonding portion 22 is formed of a diffusion layer in which the metal elements of the first metal member 12, the second metal member 14, and the insert material 16 are mutually solid phase diffused. Carbides are dissolved at the bonding interface 24 of the bonding portion 22 and in the vicinity thereof. For this reason, the bonding interface 24 of the bonding portion 22 has no carbides precipitated therein. This suppresses the formation of a diffusion barrier due to the presence of carbides along the bonding interface 24, making it possible to promote solid phase diffusion and increase the bonding strength of the bonding portion 22. In addition, since carbides are solid-solved at the bonding interface 24 of the bonding portion 22 and in the vicinity thereof, the formation of a crack propagation path due to the presence of carbides along the bonding interface 24 is suppressed. This makes it possible to suppress the formation and propagation of cracks at the bonding portion 22. As a result, the tensile characteristics and the like of the metal member joint body 20 can be improved.

[0047]

In addition, in the metal member joint body 20 heat-treated after solid phase diffusion bonding, the crystal grains of the bonding portion 22 are across the bonding interface 24 of the bonding portion 22. More specifically, by heat-treating the metal member joint body 20 after solid phase diffusion bonding, the crystal grains of the bonding portion 22 grow across the bonding interface 24. At the bonding interface 24, creep deformation due to slip or the like is likely to occur as in the case of crystal grain boundaries. However, since the crystal grains of the bonding portion 22 grow across the bonding interface 24, creep deformation can be suppressed. This makes it possible to improve the creep characteristics and the like of the metal member joint body 20.

[0048]

As described above, the metal member joint body 20 is excellent in mechanical strength such as tensile characteristics and creep characteristics. Therefore, it can be applied to turbine blades of aircraft and industrial gas turbines and the like. In addition, since the metal member joint body 20 is excellent in sealing properties for reaction gas and the like as well as in mechanical strength, it can be applied to heat exchangers, reactors, and the like in chemical plants.

[0049]

As mentioned above, the above configuration includes a stacked body forming step of forming a stacked body by putting an insert material between a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys, and a solid phase diffusion

bonding step of forming a metal member joint body by heating and pressurizing the stacked body to perform solid phase diffusion bonding, wherein the insert material contains Ni having a content higher than an Ni content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Ni alloys, and contains Fe or Ni having a content higher than an Fe content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Fe alloys. This suppresses the presence of carbides along the bonding interface of the bonding portion between the first metal member and the second metal member, making it possible to suppress the formation of a crack propagation path and promote solid phase diffusion. As a result, it is possible to improve mechanical strength such as tensile characteristics in the metal member joint body.

[0050]

The above configuration further includes a heat treatment step in which the metal member joint body is heat-treated to grow crystal grains of a bonding portion between the first metal member and the second metal member across a bonding interface of the bonding portion. This allows the crystal grains of the bonding portion to be across the bonding interface of the bonding portion, making it possible to improve mechanical strength such as creep characteristics.

Examples

[0051]

The mechanical strength characteristics of the Ni alloy member were evaluated by performing solid phase diffusion

bonding.

[0052]

(Preparation of Specimen)

First, the specimen of Example 1 is described. As the Ni alloy member, Haynes 230 alloy was used, which is a solid solution strengthened heat-resistant Ni-based alloy. The Haynes 230 alloy is a carbide-containing Ni alloy containing carbides such as Cr carbides and W carbides. As the Haynes 230 alloy, the one having the above-mentioned alloy composition was used. The shape of the Ni alloy member was a block shape. Pure Ni foil was used as the insert material. As the pure Ni foil, a foil having a purity of 99% or more was used. The thickness of the insert material was 5 μm to 10 μm . A stacked body was formed by putting an insert material between an Ni alloy member and an Ni alloy member formed of Haynes 230 alloys.

[0053]

Next, the stacked body was heated and pressurized in a vacuum atmosphere to perform solid phase diffusion bonding. A vacuum diffusion bonding equipment was used for solid phase diffusion bonding. The bonding temperature was 1050°C to 1150°C. The bonding pressure was 5 MPa to 10 MPa. The bonding time was 4 to 10 hours. The degree of vacuum was 1.3×10^{-2} Pa or less.

[0054]

The specimen of Example 2 is described. The specimen of Example 2 is different from the specimen of Example 1 in that heat treatment is performed after solid phase diffusion bonding. More specifically, in the specimen of Example 2, first, a stacked body was formed and solid phase diffusion bonding was performed in the same manner as in the specimen of Example 1.

Then, in the specimen of Example 2, the metal member joint body subjected to solid phase diffusion bonding was heat-treated. A heat treatment furnace was used for the heat treatment of the metal member joint body. The heat treatment was performed by heating from 1050°C to 1150°C in a vacuum atmosphere. The heat treatment time was 50 hours. The degree of vacuum was 1.3×10^{-2} Pa or less.

[0055]

The specimen of Example 3 is described. The specimen of Example 3 is different from the specimen of Example 1 in that heat treatment is performed after solid phase diffusion bonding. In addition, the specimen of Example 3 is different from the specimen of Example 2 in that the heat treatment time is longer. More specifically, in the specimen of Example 3, a stacked body was formed and solid phase diffusion bonding was performed in the same manner as in the specimen of Examples 1 and 2. Then, in the specimen of Example 3, the metal member joint body subjected to solid phase diffusion bonding was heat-treated. The heat treatment was performed by heating from 1050°C to 1150°C in a vacuum atmosphere. The heat treatment time was 72 hours. The degree of vacuum was 1.3×10^{-2} Pa or less.

[0056]

The specimen of Comparative Example 1 is described. The specimen of Comparative Example 1 is different from the specimen of Example 1 in that solid phase diffusion bonding was performed without using an insert material. More specifically, in the specimen of Comparative Example 1, the bonding surfaces of the Ni alloy members were directly abutted with each other, followed by solid phase diffusion bonding. The bonding conditions (such as bonding temperature, bonding pressure, bonding time, and

bonding atmosphere) of the specimen of Comparative Example 1 were the same as those of the specimen of Example 1.

[0057]

The specimen of Comparative Example 2 is described. The specimen of Comparative Example 2 is different from the specimen of Comparative Example 1 in that heat treatment is performed after solid phase diffusion bonding. More specifically, the specimen of Comparative Example 2 was formed by performing solid phase diffusion bonding without using an insert material as in the specimen of Comparative Example 1, and then heat-treating. The heat treatment conditions of the specimen of Comparative Example 2 were the same as the heat treatment conditions of the specimen of Example 2 (such as heat treatment temperature, heat treatment time, and heat treatment atmosphere).

[0058]

(Tensile Test)

The specimens of Example 1 and Comparative Example 1 were subjected to a tensile test at room temperature. The tensile test was performed in accordance with ASTM E8/E8M. The tensile test piece was prepared by cutting out from each specimen. The number of test pieces was 3 for each specimen. Fig. 4 is a graph showing the results of tensile tests on the specimens. In the graph of Fig. 4, the horizontal axis represents each specimen, the vertical axis represents the joint efficiency, and the joint efficiency of each specimen is represented by a bar graph. Note that the joint efficiency is a value when the standard value (760 MPa) of the room temperature tensile strength of the Haynes 230 alloy as the base material is set to 1.

[0059]

In the specimen of Comparative Example 1, the joint

efficiency was smaller than 1, and the tensile strength lower than the base material strength was obtained. In the specimen of Comparative Example 1, all of the test pieces were broken at the bonding portion. On the other hand, in the specimen of Example 1, the joint efficiency was higher than 1, and the tensile strength equivalent to the base material strength was obtained. In the specimen of Example 1, all of the test pieces were broken not at the bonding portion but at the base material. From these results, it has been found that the tensile characteristics are improved by solid phase diffusion bonding using pure Ni foil as an insert material.

[0060]

(Creep Test)

Creep tests were performed on the specimens of Examples 1 to 3. The creep tests were performed in accordance with JIS Z 2271. Creep test pieces were prepared by cutting out from each specimen. The number of test pieces was 3 for each specimen. Fig. 5 is a graph showing the results of creep tests on the specimens. In the graph of Fig. 5, the horizontal axis is the Larson-Miller parameter P , the vertical axis is the stress, the specimen of Example 1 is indicated as a rhombus, the specimen of Example 2 as a square, the specimen of Example 3 as a triangle, and the base material as a circle. The Larson mirror parameter P is a parameter represented by $P = T(C + \log t_r)$. T is the absolute temperature (K), t_r is the stress rupture time (h), and C is the material constant. Note that the material constant C was set to 20.

[0061]

The specimens of Examples 2 and 3 were improved in creep characteristics as compared with the specimen of Example 1.

From these results, it has been found that the creep characteristics are improved by performing the heat treatment after the solid phase diffusion bonding. In addition, the specimen of Example 3 was improved in creep characteristics as compared with the specimen of Example 2. From these results, it has been found that the creep characteristics are improved by increasing the heat treatment time after the solid phase diffusion bonding.

[0062]

(Observation of Metal Structure)

The metal structure of the specimens of Examples 1 and 2 and the specimens of Comparative Examples 1 and 2 was observed with an optical microscope. Fig. 6 is a photograph showing the metal structure observation results of the specimen of Comparative Example 1. Fig. 7 is a photograph showing the metal structure observation results of the specimen of Example 1. Fig. 8 is a photograph showing the metal structure observation results of the specimen of Example 2. Fig. 9 is a photograph showing the metal structure observation results of the specimen of Comparative Example 2. Note that the magnification of metal structure observation was 200 times.

[0063]

As shown in Fig. 6, in the specimen of Comparative Example 1, it was confirmed that carbides were present along the bonding interface between the Ni alloy members. Formed at the bonding interface was a layer in which carbides were densely formed. As described above, it has been found that carbides are present along the bonding interface after performing solid phase diffusion bonding without using an insert material. As a result, it is considered that the tensile strength of the specimen of

Comparative Example 1 was reduced.

[0064]

As shown in Fig. 7, in the specimen of Example 1, a bonding portion being a diffusion layer was formed between the Ni alloy members. In the specimen of Example 1, no carbide was found at the bonding interface of the bonding portion. From these results, since the carbides are not precipitated at the bonding interface due to the solid dissolution of the carbides at the bonding interface and in the vicinity thereof, it is possible to prevent the bonding interface from becoming a crack propagation path. As a result, it is considered that the tensile strength of the specimen of Example 1 was improved.

[0065]

As shown in Fig. 8, in the specimen of Example 2, the crystal grains of the bonding portion grew across the bonding interface of the bonding portion. On the other hand, as shown in Fig. 7, in the specimen of Example 1, the crystal grains of the bonding portion did not grow across the bonding interface. From this result, it has been found that, by heat treatment after solid phase diffusion bonding, the crystal grains of the bonding portion grow across the bonding interface, so that the creep characteristics are improved.

[0066]

As shown in Fig. 9, in the specimen of Comparative Example 2, the crystal grains at the bonding interface and in the vicinity thereof did not grow across the bonding interface. From this result, it has been found that, in the case of performing solid phase diffusion bonding without using an insert material, the crystal grains at the bonding interface and in the vicinity thereof hardly grow even in the case of

performing heat treatment after solid phase diffusion bonding.

[Industrial Applicability]

[0067]

The present disclosure can improve the mechanical strength of a metal member joint body, and thus can be applied to turbine blades of aircraft and industrial gas turbines and the like as well as to heat exchangers, reactors, and the like in chemical plants.

[CLAIMS]

[Claim 1]

A method of bonding metal members comprising:

a stacked body forming step of forming a stacked body by putting an insert material between a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys; and

a solid phase diffusion bonding step of forming a metal member joint body by heating and pressurizing the stacked body to perform solid phase diffusion bonding, wherein

the insert material contains Ni having a content higher than an Ni content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Ni alloys, and contains Fe or Ni having a content higher than an Fe content of the first metal member and the second metal member when the first metal member and the second metal member are formed of the carbide-containing Fe alloys.

[Claim 2]

The method of bonding metal members according to claim 1, wherein

the first metal member and the second metal member are formed of the carbide-containing Ni alloys, and

the insert material contains Ni having a content higher than the Ni content of the first metal member and the second metal member.

[Claim 3]

The method of bonding metal members according to claim 2, wherein

the insert material is formed of pure Ni.

[Claim 4]

The method of bonding metal members according to any one of claims 1 to 3, further comprising:

a heat treatment step in which the metal member joint body is heat-treated to grow crystal grains of a bonding portion between the first metal member and the second metal member across a bonding interface of the bonding portion.

[Claim 5]

A metal member joint body comprising:

a first metal member and a second metal member formed of carbide-containing Ni alloys or carbide-containing Fe alloys;
and

a bonding portion provided between the first metal member and the second metal member and formed of a diffusion layer,
wherein

the bonding interface of the bonding portion has no carbides precipitated therein.

[Claim 6]

The metal member joint body according to claim 5, wherein

the first metal member and the second metal member are formed of the carbide-containing Ni alloys.

[Claim 7]

The metal member joint body according to claim 5 or 6,
wherein

the crystal grains of the bonding portion are across the bonding interface.