

Dissolved Nitrogen Concentration Monitoring Method, Substrate Cleaning Method, and Substrate Cleaning Apparatus

Field of the Invention

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The present invention relates to a dissolved nitrogen concentration monitoring method, substrate cleaning method, and substrate cleaning apparatus for a wafer cleaning process. More specifically, the present invention relates to a dissolved
10 nitrogen concentration monitoring method, substrate cleaning method, and substrate cleaning apparatus for monitoring the dissolved nitrogen concentration of a cleaning liquid into which a substrate, such as a wafer, is dipped.

15 Background Art

In general, in a production process of a substrate, such as a wafer, a substrate cleaning process using dipping, single-wafer, or like method is performed to remove factors
20 responsible for defect of semiconductor devices. Such factors include organic substances, metal impurities, particles (fine particles), and chemical oxide films.

A substrate cleaning process employs various types of
25 cleaning methods depending on the purpose. In particular, when the dipping method is employed to remove particles, a substrate is dipped into a cleaning liquid contained in a cleaning bath, and ultrasonic waves are irradiated onto the cleaning liquid where the substrate is dipped. Such ultrasonic waves are
30 called megasonic waves, whose frequency range is around 1 MHz. It is generally recognized that use of ultrasonic waves in a frequency range of around 1 MHz reduces damage to the substrate and increases the effectiveness of cleaning micro particles of submicron sizes on the substrate.

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When megasonic waves are irradiated onto ultrapure water to remove particles from the substrate, the particle removal efficiency is known to be affected by the dissolved nitrogen concentration of a cleaning liquid. Specifically, in a
5 specific range of the dissolved nitrogen concentration of a cleaning liquid, the particle removal efficiency for substrate increases. If the dissolved nitrogen concentration of a cleaning liquid is monitored and controlled to be in a certain range during the cleaning process, effective removal of
10 particles is theoretically possible.

In a hitherto known method, gas components contained in a fluid medium are introduced into a container through a polymer membrane, and the concentration of the gas components are
15 calculated based on changes in the thermal conductivity in the container (Patent Document 1). This method has been employed to monitor the dissolved nitrogen concentration of a cleaning liquid.

20 Alternatively, Irradiation of ultrasonic waves onto sample water containing nitrogen gas generates hydrogen radicals derived from water molecules. The hydrogen radicals react with the nitrogen gas, and nitrogen compounds (NO_x^- , NH_4^+) are produced. A method based on this mechanism has been
25 proposed for calculating the dissolved nitrogen concentration of a sample (Patent Document 2). In this method, after radical treatment is performed for sample water by means of ultrasonic wave irradiation, the ion amount derived from nitrogen atoms is measured by a resistivity meter, and the dissolved nitrogen
30 concentration of the sample is calculated based on the ion amount.

Prior Art Document

35 Patent Document

Patent Document 1: Japanese Laid-open Patent Publication
(Kokai) No. H03-176640

Patent Document 2: Japanese Laid-open Patent Publication
5 (Kokai) No. 2000-131308

Summary of the Invention

Problems to be Solved by the Invention

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In the method according to Patent Document 1, however,
when a gas whose thermal conductivity is close to that of
nitrogen, e.g., oxygen, is contained in gas components, the
thermal conductivity of nitrogen cannot be accurately measured
15 due to effects of the thermal conductivity of oxygen. This
raises the problem that the dissolved nitrogen concentration of
a cleaning liquid cannot be accurately measured.

To address this problem, a different method for
20 calculating the dissolved nitrogen concentration has been
proposed. In this method, the dissolved oxygen concentration
of gas components are measured using the polarography method or
the like, and measurements of the dissolved oxygen
concentration are used to correct the value of the dissolved
25 nitrogen concentration for calculation thereof. However, in
this method, measurement of the dissolved oxygen concentration
needs to be performed in addition to measurement of the
dissolved nitrogen concentration, which requires complicated
operations. There is also a cost problem arising from very
30 expensive dissolved nitrogen concentration meters that have
been conventionally used. In addition, this method requires
more than 10 seconds for each measurement of the thermal
conductivity of gas components. As the dissolved nitrogen
concentration cannot be monitored real-time, the monitoring is
35 not accurate.

Also, in the method according to Patent Document 2, the ion amount derived from nitrogen atoms cannot be accurately measured with presence of another component ionized in sample water, and the dissolved nitrogen concentration of the sample water cannot be accurately calculated. As this method is focused only on changes in the amount of nitrogen compounds due to ultrasonic wave irradiation, but not on changes in the dissolved oxygen concentration.

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It is an object of the present invention to provide a dissolved nitrogen concentration monitoring method, substrate cleaning method, and substrate cleaning apparatus which make it possible to accurately monitor the dissolved nitrogen concentration of a cleaning liquid in real-time without complicated operations and reduce the cost.

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Means for Solving the Problems

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To solve the above problems, according to the present invention, there is provided a dissolved nitrogen concentration monitoring method directed to monitoring a dissolved nitrogen concentration of a cleaning liquid when an ultrasonic wave is irradiated onto the cleaning liquid in which a substrate is dipped. The dissolved nitrogen concentration monitoring method is characterized by comprising the steps of: measuring an increase amount of dissolved oxygen concentration of the cleaning liquid, which is due to an oxygen molecule generated from a water molecule as a result of a radical reaction caused by ultrasonic wave irradiation; and calculating a dissolved nitrogen concentration of the cleaning liquid from the measured increase amount of dissolved oxygen concentration based on a predetermined relationship between a dissolved nitrogen concentration and an increase amount of dissolved oxygen concentration.

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Also, the dissolved nitrogen concentration of the cleaning liquid is calculated from an increase amount of dissolved oxygen concentration measured by a dissolved oxygen concentration meter based on dissolved gas information indicating a relationship between the dissolved nitrogen concentration of the cleaning liquid and the increase amount of dissolved oxygen concentration thereof.

In addition, the dissolved gas information is compiled in advance for each of cleaning conditions of the substrate.

Furthermore, the cleaning conditions of the substrate include an ultrasonic output power level.

The dissolved gas information indicates that as the ultrasonic output power level increases, the increase amount of dissolved oxygen concentration corresponding to a specific dissolved nitrogen concentration increases.

As well, the cleaning conditions of the substrate include an overflow rate of a cleaning liquid.

The dissolved gas information indicates that as the overflow rate decreases, a rate of change in the increase amount of dissolved oxygen concentration increases with respect to the dissolved nitrogen concentration.

Moreover, it is preferable that the cleaning liquid is water.

The substrate cleaning method of the present invention is a method for cleaning a substrate by irradiating an ultrasonic wave onto a cleaning liquid into which the substrate is dipped. In this method, the increase amount of the dissolved oxygen

concentration in the cleaning liquid, which is due to an oxygen molecule generated from a water molecule as a result of a radical reaction caused by ultrasonic wave irradiation, is measured. In turn, the mixture ratio of a cleaning liquid with dissolved nitrogen gas, which is to be introduced into a cleaning bath, is adjusted so that the increase amount of the dissolved oxygen concentration is in a specific range where the cleaning performance is high.

The substrate cleaning apparatus of the present invention is an apparatus for cleaning a substrate by irradiating an ultrasonic wave to a cleaning liquid into which the substrate is dipped. This apparatus measures the increase amount of the dissolved oxygen concentration in the cleaning liquid, which is due to an oxygen molecule generated from a water molecule as a result of a radical reaction caused by ultrasonic wave irradiation. In turn, this apparatus adjusts the mixture ratio of a cleaning liquid with dissolved nitrogen gas, which is to be introduced into a cleaning bath, so that the increase amount of the dissolved oxygen concentration is in a specific range where the cleaning performance is high.

Effects of the Invention

According to the present invention, an increase amount of dissolved oxygen concentration, which is due to oxygen molecules generated from water molecules as a result of a radical reaction caused by ultrasonic wave irradiation, is measured. Then the dissolved nitrogen concentration of a cleaning liquid is calculated from the measured increase amount of dissolved oxygen concentration based on a predetermined relationship between the dissolved nitrogen concentration and the increase amount of dissolved oxygen concentration. As the dissolved nitrogen concentration can be calculated by measuring the dissolved oxygen concentration of a cleaning liquid, no

complicated operation is required. Since the relationship between the dissolved nitrogen concentration and the increase amount of dissolved oxygen concentration is predetermined, the dissolved nitrogen concentration can be accurately calculated using this relationship. Cost reduction is also possible as use of expensive dissolved nitrogen concentration meters is not necessary, and real-time measurement is possible since the dissolved oxygen concentration can be measured using a dissolved oxygen concentration meter of the polarography type or the like. In addition to cost reduction, real-time accurate monitoring of the dissolved nitrogen concentration of a cleaning liquid can be made without complicated operations.

The relationship between the dissolved nitrogen concentration of a cleaning liquid and the increase amount of dissolved oxygen concentration thereof is indicated by dissolved gas information. Based on this information, the dissolved nitrogen concentration of the cleaning liquid is calculated from the increase amount of dissolved oxygen concentration measured by a dissolved oxygen concentration meter. As an inexpensive dissolved oxygen concentration meter can be used for measurement of the dissolved nitrogen concentration, further cost reduction is possible.

Since the dissolved gas information is produced in advance for each of substrate cleaning conditions, even when a cleaning condition is changed, the dissolved nitrogen concentration of a cleaning liquid can be accurately calculated.

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The aforementioned substrate cleaning conditions include the ultrasonic output power level. Even when the output power level of ultrasonic waves irradiated onto a cleaning liquid is changed, the dissolved nitrogen concentration can be accurately

calculated based on the dissolved gas information that corresponds to the changed output power level.

The aforementioned dissolved gas information indicates
5 that as the ultrasonic output power level increases, the increase amount of dissolved oxygen concentration corresponding to a specific dissolved nitrogen concentration increases. By increasing the ultrasonic output power level, the calculatable value of the dissolved nitrogen concentration increases, and
10 the accuracy of measurement thereof increases.

Also, the aforementioned substrate cleaning conditions include the overflow rate of a cleaning liquid. Even when the overflow rate of a cleaning liquid is changed, the dissolved
15 nitrogen concentration can be accurately calculated based on the dissolved gas information that corresponds to the changed overflow rate.

The aforementioned dissolved gas information indicates
20 that as the overflow rate decreases, the rate of change in the increase amount of dissolved oxygen concentration increases with respect to the dissolved nitrogen concentration. By decreasing the overflow rate, the dissolved nitrogen concentration can be accurately calculated.

25 According to the present invention, the mixture ratio of a cleaning liquid with dissolved nitrogen gas, which is to be introduced into a cleaning bath, is adjusted so that the increase amount of the dissolved oxygen concentration is in a
30 specific range where the cleaning performance is high. Substrate cleaning with a high particle removal efficiency can be achieved without using a dissolved nitrogen concentration meter.

Brief Description of the Drawings

FIG. 1 is a diagram schematically showing a configuration of an ultrasonic cleaning apparatus to which a monitoring method according to an embodiment of the present invention is applied.

FIG. 2 is a block diagram showing a configuration of a monitoring unit that performs a monitoring method according a present embodiment.

FIG. 3 is a diagram showing changes in the dissolved oxygen concentration of ultrapure water with a dissolved nitrogen concentration D_{N2} of 0.2 ppm when ultrasonic waves are irradiated onto the ultrapure water.

FIG. 4 is a diagram showing changes in the dissolved oxygen concentration of ultrapure water with a dissolved nitrogen concentration D_{N2} of 13.5 ppm when ultrasonic waves are irradiated onto the ultrapure water.

FIGs. 5 (a) and (b) are diagrams that indicate a relationship between the dissolved nitrogen concentration D_{N2} of ultrapure water and the increase amount of dissolved oxygen concentration thereof ΔD_{O2} for each ultrasonic output power level; FIG. 5 (a) is a diagram plotting each of the ultrasonic output power levels, and FIG. 5 (b) is a diagram depicting approximation equations for each ultrasonic output power level.

FIGs. 6 (a) and (b) are diagrams that indicate a relationship between the dissolved nitrogen concentration D_{N2} of ultrapure water and the increase amount of dissolved oxygen concentration thereof ΔD_{O2} for each overflow rate of ultrapure water; FIG. 6 (a) is a diagram plotting each of the overflow rates, and FIG. 6 (b) is a diagram depicting approximation equations of overflow rates.

FIG. 7 is a flowchart showing a dissolved nitrogen concentration calculation process executed during performance of a monitoring method according an embodiment of the present invention.

FIG. 8 is a diagram showing the relationship between the increase amount of the dissolved oxygen concentration ΔD_{O_2} and the particle removal efficiency.

5 Mode for Carrying out the Invention

The present invention will now be described in detail below with reference to the drawings showing preferred embodiments thereof.

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FIG. 1 is a diagram schematically showing a configuration of an ultrasonic cleaning apparatus to which a monitoring method according to an embodiment of the present invention is applied. FIG. 2 is a block diagram showing a configuration of
15 a monitoring unit that performs the monitoring method according to the present embodiment.

As shown in FIG. 1, an ultrasonic cleaning apparatus 1 is comprised of a supply unit 10, a coupling bath 21, an
20 irradiation unit 30, and a monitoring unit 40. The supply unit 10 supplies a cleaning liquid, such as ultrapure water, to a cleaning bath 20. The coupling bath 21 houses the cleaning bath 20. The irradiation unit 30 is disposed at the bottom of the coupling bath 21 and irradiates ultrasonic waves onto
25 inside the cleaning bath 20. The monitoring unit 40 monitors the dissolved nitrogen concentration of the cleaning liquid supplied to inside the cleaning bath 20.

The supply unit 10 has a first supply valve 11 that
30 supplies ultrapure water with dissolved nitrogen gas to a below-described mixed bath and a second supply valve 12 that supplies degassed ultrapure water to the below-described mixed bath. The ultrapure water with dissolved nitrogen gas and the degassed ultrapure water are mixed at a location downstream
35 from the first supply valve 11 and the second supply valve 12.

The mixed pure water is supplied to a liquid introduction pipe, which will be described below, via a pipe installed inside the cleaning bath 20. By adjusting the amount of the valve opening of the first supply valve 11 and the second supply valve 12,
5 the dissolved nitrogen concentration of the ultrapure water to be supplied to inside the cleaning bath 20 and the flow rate of the supplied water are controlled.

The cleaning bath 20 has a wafer holder 22 that holds
10 inside a wafer W, e.g., a semiconductor wafer, and stores the mixed ultrapure water while the wafer holder 22 is holding a substrate W. The substrate W is thereby dipped into the mixed cleaning liquid in the cleaning bath 20. Liquid introduction pipes 23 are arranged at a lower portion of the cleaning bath
15 20, so that the liquid introduction pipes 23 supply the mixed ultrapure water to the cleaning bath at a predetermined overflow rate. The coupling bath 21 is connected with a supply line (not shown) other than the supply unit 10 and is supplied with water at a predetermined overflow rate.

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By oscillating ultrasonic waves at frequencies of 20 kHz to 2 MHz and at watt densities of 0.05 to 7.0 W/cm², the irradiation unit 30 irradiates the ultrasonic waves onto the mixed ultrapure water in the cleaning bath 20 via the water
25 stored in the coupling bath 21. The wafer W dipped in the mixed ultrapure water is thereby cleaned. It is preferable to use ultrasonic waves whose frequency ranges from 400 kHz to 1 MHz.

30 The monitoring unit 40 includes a sampling pipe 41, a pump 42, a dissolved oxygen concentration meter 43, and a determination unit 44. The sampling pipe 41 extracts the mixed ultrapure water in a predetermined amount. The pump 42 is connected to the sampling pipe 41 and supplies a predetermined
35 amount of mixed ultrapure water to a below-described dissolved

oxygen concentration meter. The dissolved oxygen concentration meter 43, which is connected to the pump 42 at a location downstream thereof, measures the dissolved oxygen concentration of the mixed ultrapure water and sends electric signals
5 corresponding to the measured dissolved oxygen concentration to the below-described determination unit. The determination unit 44 determines the dissolved nitrogen concentration in the cleaning bath 20 based on the electric signals sent from the dissolved oxygen concentration meter 43. The dissolved oxygen
10 concentration meter 43 is, for example, a dissolved oxygen concentration meter using the polarography method. In the polarography method, two types of metals are dipped in an electrolyte solution, and a certain voltage is applied between the two metals to cause an oxidation reduction reaction. Then
15 the current proportional to the dissolved oxygen concentration of the electrolyte solution is measured.

As shown in FIG. 2, the determination unit 44 has a receiving section 45, a storage section 46, a control section
20 47, and a display 48. The receiving section 45 receives electric signals from the dissolved oxygen concentration meter 43. The storage section 46 stores dissolved gas information, which indicates a predetermined relationship between the dissolved nitrogen concentration and the increase amount of
25 dissolved oxygen concentration. The control section 47 calculates the increase amount of dissolved oxygen concentration based on the electric signals received from the receiving section 45 when ultrasonic waves are irradiated. Also, the control section 47 calculates the dissolved nitrogen
30 concentration of a cleaning liquid from the increase amount of dissolved oxygen concentration measured by a dissolved oxygen concentration meter based on the dissolved gas information, which indicates the relationship between the dissolved nitrogen concentration of the cleaning liquid and the increase amount of
35 dissolved oxygen concentration thereof. The display 48

displays the dissolved nitrogen concentration calculated by the control section 47.

The control section 47 performs overall control of each
5 section of the monitoring unit 40 and reads out a program stored in the storage section 46 to execute the below-described dissolved nitrogen concentration calculating process (FIG. 7).

The particle removal efficiency of a cleaning method
10 using ultrasonic waves is affected by the dissolved nitrogen concentration of ultrapure water. Specifically, it is known that the particle removal efficiency for a wafer increases when the dissolved nitrogen concentration of a cleaning liquid is in a specific range. In view of this theory, the present
15 inventors focused on dissolved oxygen concentration, which can be effortlessly measured at low costs, and found out a method for monitoring the dissolved nitrogen concentration of a cleaning liquid. In this method, the dissolved nitrogen concentration is calculated based on the dissolved oxygen
20 concentration during irradiation of ultrasonic waves. The specifics of this monitoring method are explained in the text to follow.

First of all, the principle of this monitoring method is
25 explained in reference to FIGs. 3 and 4. FIG. 3 is a diagram showing changes in the dissolved oxygen concentration of ultrapure water when ultrasonic waves are irradiated onto ultrapure water. In an example shown in FIG. 3, ultrapure water with a dissolved nitrogen concentration D_{N_2} of 0.2 ppm is
30 used to explain changes in the dissolved oxygen concentration. The cleaning bath 20 in FIGs. 3 and 4 is a rectangular water bath made of 3.0 mm-thick plates of quartz glass. The internal dimensions of this bath were 270 mm wide × 69 mm deep × 270 mm high, and its capacity was 5 L. The volume of ultrapure water
35 supplied to the cleaning bath 20 is 5 L/min. The frequency and

output power level of the used ultrasonic waves were 950 kHz and 1200 W (watt density 5.6 W/cm^2), respectively. The irradiated area of a vibration plate was $80 \text{ mm} \times 270 \text{ mm}$, and ultrasonic waves were irradiated onto the whole bottom surface of the cleaning bath 20.

As shown in FIG. 3, irradiation of ultrasonic waves onto ultrapure water with an initial dissolved oxygen concentration D_0 of approximately 0.25 ppm causes the dissolved oxygen concentration to increase to approximately 0.8 ppm. In this case, the value of the dissolved oxygen concentration D_{O2} , which is measured by the monitoring unit 40, minus the initial dissolved oxygen concentration D_0 measured prior to ultrasonic wave irradiation -i.e., the increase amount of dissolved oxygen concentration ΔD_{O2} ($=D_{O2}-D_0$) -is 0.55 ppm. Subsequently, upon termination of ultrasonic wave irradiation, the dissolved oxygen concentration of the ultrapure water decreases to the level of the initial dissolved oxygen concentration. The above trends show that the dissolved oxygen concentration of ultrapure water is increased by ultrasonic wave irradiation.

FIG. 4 is a diagram showing changes in the dissolved oxygen concentration of ultrapure water when ultrasonic waves are irradiated onto ultrapure water. In this case, the dissolved nitrogen concentration D_{N2} is 13.5 ppm.

As shown in FIG. 4, when the dissolved nitrogen concentration D_{N2} of the ultrapure water is 13.5 ppm, irradiation of ultrasonic waves onto the ultrapure water does not cause the dissolved oxygen concentration to change since a reaction to produce oxygen molecules from water molecules is hindered by the presence of dissolved nitrogen. The dissolved oxygen concentration stays at the level of the initial dissolved oxygen concentration where ultrasonic waves are not

irradiated. In this case, the increase amount of dissolved oxygen concentration ΔD_{O_2} is 0 ppm.

It is possible to conclude from FIGs. 3 and 4 that during
5 ultrasonic wave irradiation, as the dissolved nitrogen concentration of ultrapure water decreases, the amount of oxygen produced in the ultrapure water increases, and the dissolved oxygen concentration increases. When a radical
10 reaction by the ultrasonic wave irradiation advances in the ultrapure water and water molecules are decomposed into hydrogen radicals and hydroxyl radicals, the hydroxyl radicals produce oxygen that is responsible for the aforementioned increases.

15 If an equation representing the relationship between the dissolved nitrogen concentration of ultrapure water and the increase amount of dissolved oxygen concentration thereof during ultrasonic wave irradiation is predetermined, this equation can be used to calculate the dissolved nitrogen
20 concentration D_{N_2} . The dissolved nitrogen concentration D_{N_2} corresponds to the increase amount of dissolved oxygen concentration ΔD_{O_2} measured by the dissolved oxygen concentration meter 43. The dissolved nitrogen concentration of the ultrapure water can be monitored by performing the
25 aforementioned calculation. For example, if changes in the increase amount of dissolved oxygen concentration ΔD_{O_2} are monitored, the increase and decrease in the dissolved nitrogen concentration D_{N_2} can be monitored using the above equation. If the increase amount of dissolved oxygen concentration ΔD_{O_2}
30 corresponding to an arbitrary dissolved nitrogen concentration D_{N_2} is calculated and the increase amount of dissolved oxygen concentration of a cleaning liquid ΔD_{O_2} is monitored, it is possible to determine whether the dissolved nitrogen concentration of the cleaning liquid is greater, smaller, or
35 equal to the arbitrary dissolved nitrogen concentration D_{N_2} .

The present inventors conducted a survey to identify factors influencing the relationship between the dissolved nitrogen concentration D_{N2} of ultrapure water and the increase amount of dissolved oxygen concentration thereof ΔD_{O2} . The survey identified that this relationship is influenced by the following factors: (1) the output power level of ultrasonic waves irradiated onto the ultrapure water; and (2) the overflow rate of ultrapure water supplied to the cleaning bath 20. The text to follow explains the relationship between D_{N2} and ΔD_{O2} at different ultrasonic output power levels and at different overflow rates of ultrapure water.

FIGs. 5 (a) and (b) are diagrams that indicate a relationship between the dissolved nitrogen concentration D_{N2} of ultrapure water and the increase amount of dissolved oxygen concentration thereof ΔD_{O2} for each ultrasonic output power level. FIG. 5 (a) is a diagram plotting measurements of the ultrasonic output power levels. FIG. 5 (b) is a diagram depicting approximation equations for each ultrasonic output power levels.

FIG. 5(a) depicts the results of selecting 900 W (watt density: 4.2 W/cm^2), 1000 W (watt density: 4.6 W/cm^2), 1100 W (watt density: 5.1 W/cm^2), and 1200 W (watt density: 5.6 W/cm^2) as ultrasonic output power levels and plotting values indicating the relationship between D_{N2} and ΔD_{O2} at the above output power levels. Approximation equations (calibration curves) determined from the plotted values have the slopes and y-intercepts presented in the drawing (FIG. 5(b)). The plotted values of FIG. 5(a) were obtained from measurement conducted using the cleaning bath 20, which is a rectangular water bath made of 3.0 mm-thick plates of quartz glass. The internal dimensions of this bath were 270 mm wide $\times$ 69 mm deep $\times$ 270 mm high, and its capacity is 5 L. The volume of ultrapure water

supplied to the cleaning bath 20 was 5 L/min. The frequency of the used ultrasonic waves was 950 kHz. The irradiated area of a transducer was 80 mm × 270 mm, and ultrasonic waves were irradiated onto the whole bottom surface of the cleaning bath

5 20.

- When the output power level is 1200 W ... $y = -0.0639x + 0.5667$
 - When the output power level is 1100 W ... $y = -0.0631x + 0.4268$
 - When the output power level is 1000 W ... $y = -0.0606x + 0.2789$
 - 10 • When the output power level is 900 W ... $y = -0.0607x + 0.1763$
- (where y denotes the increase amount of dissolved oxygen concentration ΔD_{O_2} , and x denotes the dissolved nitrogen concentration D_{N_2})

The above results indicate a proportional relationship between the dissolved nitrogen concentration D_{N_2} and the increase amount of dissolved oxygen concentration ΔD_{O_2} . The slopes of the approximation equations are almost equal, and the y-intercept increases with an increase in the ultrasonic output power level. As the ultrasonic output power level increases, the increase amount of dissolved oxygen concentration corresponding to a specific dissolved nitrogen concentration increases. By increasing the ultrasonic output power level, the calculatable value of the dissolved nitrogen concentration increases, and the accuracy of measurement thereof increases.

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FIGs. 6 (a) and (b) are diagrams that indicate the relationship between the dissolved nitrogen concentration D_{N_2} of ultrapure water and the increase amount of dissolved oxygen concentration thereof ΔD_{O_2} for each overflow rate of ultrapure water. FIG. 6 (a) is a diagram plotting each measurement of the overflow rates. FIG. 6 (b) is a diagram depicting approximation equations of overflow rates.

FIG. 6(a) depicts the results of selecting 5 L/min, 2.5 L/min, and 1 L/min as overflow rates of ultrapure water and

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plotting values indicating the relationship between D_{N2} and ΔD_{O2} at the above overflow rates. Approximation equations determined from the plotted values have the slopes and y-intercepts presented in the drawing (FIG. 6(b)). The plotted values of FIG. 6(a) were obtained from measurement conducted using the cleaning bath 20, which is a rectangular water bath made of 3.0 mm-thick plates of quartz glass. The internal dimensions of this bath were 270 mm wide $\times$ 69 mm deep $\times$ 270 mm high, and its capacity is 5 L. The frequency and output power level of the used ultrasonic waves were 950 kHz and 1200 W (watt density: 5.6 W/cm²), respectively. The irradiated area of a transducer was 80 mm $\times$ 270 mm, and ultrasonic waves were irradiated onto the whole bottom surface of the cleaning bath 20.

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- When the overflow rate is 1 L/min ... $y = -0.2222x + 1.956$
 - When the overflow rate is 2.5 L/min ... $y = -0.0971x + 0.868$
 - When the overflow rate is 5 L/min ... $y = -0.069x + 0.5667$
- (where y denotes the increase amount of dissolved oxygen concentration ΔD_{O2} , and x denotes the dissolved nitrogen concentration D_{N2})

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The above approximation equations demonstrate that their slopes and y-intercepts increase with a decrease in the overflow rate of ultrapure water. As the overflow rate of the ultrapure water decreases, the rate of change in the increase amount of dissolved oxygen concentration increases with respect to the dissolved nitrogen concentration. By decreasing the overflow rate, the accuracy of measurement of the dissolved nitrogen concentration increases.

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It is preferable to compile in advance dissolved gas information, as shown in FIGs. 3 and 4, on cleaning conditions, such as ultrasonic output power level and overflow rate, and to store the compiled information in the storage section 46. An approximation equation that corresponds to the ultrasonic

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output power level or overflow rate actually used in a wafer cleaning process can be selected from the dissolved gas information stored in the storage section 46. By substituting the measured increase amount of dissolved oxygen concentration ΔD_{O_2} into the approximation equation, the dissolved nitrogen concentration D_{N_2} of ultrapure water can be accurately calculated.

FIG. 7 is a flowchart of a dissolved nitrogen concentration calculation process executed during performance of the monitoring method according to the embodiment of the present invention.

As shown in FIG. 7, before irradiating ultrasonic waves onto the cleaning bath 20, a predetermined amount of mixed ultrapure water is extracted from the cleaning bath 20 (step S71). Then the dissolved oxygen concentration meter 43 is used to measure the initial dissolved oxygen concentration D_0 prior to ultrasonic wave irradiation (step S72). Next, while ultrasonic waves at a predetermined output power level are irradiated onto the cleaning bath 20, a predetermined amount of mixed ultrapure water is extracted from the cleaning bath 20 (step S73), and the dissolved oxygen concentration D_{O_2} during ultrasonic wave irradiation is measured by the dissolved oxygen concentration meter 43 (step S74). In turn, the increase amount of dissolved oxygen concentration ΔD_{O_2} is calculated by subtracting the initial dissolved oxygen concentration D_0 from the measured dissolved oxygen concentration D_{O_2} (step S75). Subsequently, an approximation equation corresponding to the predetermined overflow rate or ultrasonic output power level is read out from the storage section 46 (step S76), and the approximation equation read out from the storage section 46 is used to calculate the dissolved nitrogen concentration D_{N_2} of the mixed ultrapure water from the increase amount of dissolved oxygen concentration ΔD_{O_2} measured in step S75 (step S77).

Upon completion thereof, the dissolved nitrogen concentration calculation process is terminated.

As described above, according to the embodiment of the present invention, the increase amount of dissolved oxygen concentration ΔD_{O_2} , which is due to a radical reaction in a cleaning liquid irradiated with ultrasonic waves, is measured. In turn, the dissolved nitrogen concentration D_{N_2} of the cleaning liquid is calculated from the measured increase amount of dissolved oxygen concentration ΔD_{O_2} based on a predetermined relationship between the dissolved nitrogen concentration and the increase amount of dissolved oxygen concentration. Namely, as the dissolved nitrogen concentration D_{N_2} can be calculated by measuring the dissolved oxygen concentration D_{O_2} of the cleaning liquid, complicated operations are exempted. Also, since the relationship between the dissolved nitrogen concentration and the increase amount of dissolved oxygen concentration is predetermined, this relationship can be used to accurately calculate the dissolved nitrogen concentration D_{N_2} . In addition, cost reduction is possible as an expensive dissolved nitrogen concentration meter does not need to be used. As well as cost reduction, accurate monitoring of the dissolved nitrogen concentration D_{N_2} of the cleaning liquid can be achieved without complicated operations.

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In the above embodiment, the dissolved oxygen concentration meter 43 is of the polarography type. However, the type of dissolved oxygen concentration meter is not limited to the polarography type. It may be of the galvanic cell type.

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Also, in the above embodiment, the cleaning liquid is ultrapure water, but the type of the cleaning liquid is not limited to ultrapure water. It may be generally used water. Any cleaning liquid whose dissolved oxygen can be accurately measured by a dissolved oxygen concentration meter of the

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polarography type or the like may be used. A mixed solution of hydrogen peroxide and ammonia (SC-1, APM) with a high ability to remove particles and organic contaminant may be used as well.

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Furthermore, in the above embodiment, a wafer W is cleaned as the target substrate of the cleaning process, but it is not limited to the wafer W. Another substrate, such as a glass substrate for liquid crystal display or hard disk drives, may be cleaned as well.

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Moreover, in the above embodiment, the mixture ratio of ultrapure water with dissolved nitrogen gas (the first supply valve 11) to degassed ultrapure water (the second supply valve 12) is adjusted to produce a cleaning liquid with dissolved nitrogen gas. However, the above embodiment is not limited thereto. The dissolved nitrogen concentration of ultrapure water may be directly adjusted by adjusting the pressure of nitrogen gas dissolved in the ultrapure water using a regulator (not shown) or the like.

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For the above embodiment, focus was placed on an increase in the particle removal efficiency of a semiconductor wafer when the dissolved nitrogen concentration of ultrapure water is in a specific range. Accordingly, the dissolved nitrogen concentration was calculated from the increase amount of the dissolved nitrogen concentration ΔD_{O_2} in the ultrapure water. In addition, to survey the relationship between the increase amount of the dissolved oxygen concentration ΔD_{O_2} in ultrapure water and the particle removal efficiency of a semiconductor wafer, the present inventors conducted the following experiment:

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(1) Production of silicon wafer intentionally contaminated for particle removal efficiency measurement

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A p-type silicon wafer with a diameter of 200 mm was dipped in hydrofluoric acid with a concentration of 0.5% for five minutes to remove a native oxide film from a surface thereof so that it is hydrophobic.

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In a silicon nitride powder of Ube Industries, Ltd. (SN-E10, average particle diameter: 0.5 μm) was dispersed in 20 L of an aqueous hydrochloric acid solution (pH = 2) at 50°C so that the concentration is 0.05 ppm. Into the solution, the
10 aforementioned silicon wafer was dipped for one minute.

Thereafter, rinsing was performed in ultrapure water for ten minutes, and drying was performed by a spin drier for two minutes.

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(2) Measurement of particle removal efficiency

Next, the number of particles adhered to a silicon wafer surface was measured using a particle counter (LS-6500 by Hitachi DECO). On the surface of the aforementioned silicon
20 wafer intentionally contaminated for particle removal efficiency measurement produced in (1) above, approximately 8000 particles with a diameter of 0.1 μm or greater were adhered.

25 The number of particles was measured before and after the silicon wafer cleaning experiment described in (3) below. Based on the measurements before and after the experiment, particle removal efficiency was calculated using the following equation:

30 (Particle removal efficiency) = {(Number of particles before cleaning) - (Number of particles after cleaning)} / (Number of particles before cleaning) $\times$ 100 (%)

(3) Silicon wafer cleaning experiment

The silicon wafer cleaning experiment was conducted using
35 the ultrasonic cleaning apparatus shown in Fig. 1.

The cleaning bath 20 is a rectangular water bath made of 3.0 mm-thick plates of quartz glass. The internal dimensions of this bath are 270 mm wide × 69 mm deep × 270 mm high, and its capacity is 5 L. The supply flow rate of ultrapure water supplied to the cleaning bath 20 was 5 L/min. The frequency of the used ultrasonic waves was 950 kHz, and the output was 1200 W (watt density: 5.6 W/cm²). The irradiated area of a transducer was 80 mm × 270 mm, and ultrasonic waves were irradiated onto the whole bottom surface of the cleaning bath 20.

The amount of the valve opening of the first supply valve 11 that supplies ultrapure water with dissolved nitrogen gas and that of the second supply valve 12 that supplies degassed ultrapure water were adjusted. The dissolved nitrogen concentration and flow rate of the ultrapure water to be supplied to inside the cleaning bath 20 were thereby controlled. The flow rate was controlled to be 5 L/min. Ultrasonic waves were irradiated onto the ultrapure water in the cleaning bath 20. The value of ΔD_{O_2} was measured by the monitoring unit 40. A dissolved oxygen concentration meter of the polarography type was used as the dissolved oxygen concentration meter 43. The amount of the valve opening of the first supply valve 11 that supplies ultrapure water with dissolved nitrogen gas and that of the second supply valve 12 that supplies degassed ultrapure water were adjusted so that the ΔD_{O_2} values are 0 ppm, 0.05 ppm, 0.1 ppm, 0.2 ppm, 0.3 ppm, 0.35 ppm, 0.4 ppm, and 0.5 ppm. The cleaning experiment was conducted at these eight ΔD_{O_2} values.

After the ΔD_{O_2} value is stabilized, the silicon wafer intentionally contaminated for particle removal efficiency measurement produced in (1) above was dipped for ten minutes and subsequently dried by a spin drier for two minutes.

(4) Results

Fig. 8 shows the relationship between ΔD_{O_2} and the particle removal efficiency obtained from the results of the cleaning experiment. The particle removal efficiency is found to be high in the ΔD_{O_2} value range between 0.1 and 0.3 ppm.

When the ultrasonic cleaning apparatus of the present invention is used under the conditions of the cleaning experiment, the mixture ratio of ultrapure water with dissolved nitrogen gas (the first supply valve 11) to degassed ultrapure water (the second supply valve 12) was adjusted so that the ΔD_{O_2} value ranges between 0.1 and 0.3 ppm. It is found that by making such an adjustment, cleaning with a high particle removal efficiency is possible without using a dissolved nitrogen concentration meter.

Explanation of Reference Numerals

- 1 ultrasonic cleaning apparatus
- 10 supply unit
- 20 cleaning bath
- 21 coupling bath
- 30 irradiation unit
- 40 monitoring unit
- 41 sampling pipe
- 42 pump
- 43 dissolved oxygen concentration meter
- 44 determination unit
- 45 receiving section
- 46 storage section
- 47 control section
- 48 display

Claims

1. A dissolved nitrogen concentration monitoring method of monitoring a dissolved nitrogen concentration of a cleaning
5 liquid when an ultrasonic wave is irradiated onto the cleaning liquid in which a substrate is dipped, the method characterized by comprising the steps of:

measuring an increase amount of dissolved oxygen concentration of the cleaning liquid, which is due to an oxygen
10 molecule generated from a water molecule as a result of a radical reaction caused by ultrasonic wave irradiation; and

calculating a dissolved nitrogen concentration of the cleaning liquid from said measured increase amount of dissolved oxygen concentration based on a predetermined relationship
15 between a dissolved nitrogen concentration and an increase amount of dissolved oxygen concentration.

2. The dissolved nitrogen concentration monitoring method according to claim 1, wherein:

20 said dissolved nitrogen concentration of the cleaning liquid is calculated from an increase amount of dissolved oxygen concentration measured by a dissolved oxygen concentration meter based on dissolved gas information indicating a relationship between said dissolved nitrogen
25 concentration of the cleaning liquid and said increase amount of dissolved oxygen concentration thereof.

3. The dissolved nitrogen concentration monitoring method according to claim 1 or 2, wherein:

30 said dissolved gas information has been compiled in advance for each of cleaning conditions of said substrate.

4. The dissolved nitrogen concentration monitoring method according to any one of claims 1 to 3, wherein:

said cleaning conditions of said substrate include an ultrasonic output power level.

5 5. The dissolved nitrogen concentration monitoring method according to claim 4, wherein:

said dissolved gas information indicates that as said ultrasonic output power level increases, said increase amount of dissolved oxygen concentration corresponding to a specific dissolved nitrogen concentration increases.

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6. The dissolved nitrogen concentration monitoring method according to any one of claims 1 to 3, wherein:

said cleaning conditions of said substrate includes an overflow rate of a cleaning liquid.

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7. The dissolved nitrogen concentration monitoring method according to claim 6, wherein:

20 said dissolved gas information indicates that as said overflow rate decreases, a rate of change in said increase amount of dissolved oxygen concentration increases with respect to said dissolved nitrogen concentration.

8. The dissolved nitrogen concentration monitoring method according to any one of claims 1 to 7, wherein:

25 said cleaning liquid is water.