

Rotation Type Silicon Wafer Cleaning Equipment

BACKGROUND OF THE INVENTION

5 1. Field of the Invention

 The present invention relates to a rotation type silicon wafer cleaning device to be used with semiconductor fabrication equipment and the like, and more particularly to a rotation type silicon wafer cleaning device making possible substantial quality improvements in the products by stabilizing the
10 outer surface of the silicon wafer through the improved hydrogen treatment of the outer surface of the silicon wafer through the drying process after cleaning is completed.

2. Background of the Invention

15 The fabrication of semiconductor elements generally starts with a cleaning treatment of a silicon wafer, and then various treatments such as the formation of a SiO film and the like on the silicon wafer are applied after the cleaning treatment.

 For cleaning treatment for silicon wafers, the so-called rotation type
20 silicon wafer cleaning device has been broadly employed, in that a silicon wafer placed on the rotation disc installed inside the device body is rotated at high speed (approximately 2000 RPM), and chemical cleaning agents such as hydrofluoric acid and the like are dispersed thereon. After the acid cleaning treatment, a cleaning treatment with pure water is added, and lastly the silicon
25 wafer is dried while rotating at the high speed.

 On the outer surface of a silicon wafer treated for cleaning with the

afore-mentioned conventional rotation type silicon wafer cleaning device, Si on the so-called surface layer is exposed and hydrogen atoms are bonded with the exposed Si atoms, thus putting the outer surface in a condition wherein the so-called hydrogen termination treatment has been performed. The aim is to
5 obtain a highly stable cleaned surface without impure atoms and the like deposited directly onto Si. As the result, it has been said that there will not occur the so-called natural oxidation on the surface layer even when it is left in the air over a long period of time.

10 However, even with a silicon wafer treated for cleaning with this kind of rotation type silicon wafer cleaning device, it is observed that an oxide film is naturally formed on the outer surface with the lapse of time after a cleaning is performed. This makes it difficult to prevent the natural formation of the afore-mentioned oxide film no matter how well environmental conditions are
15 presented for the maintenance of the wafer.

SUMMARY OF THE INVENTION

Object of the Invention

20 It is an object of the present invention to provide a rotation type silicon wafer cleaning device to overcome the afore-mentioned difficulties with this kind of conventional rotation type silicon wafer cleaning device, that is, when the natural formation of an oxide film is made on the outer surface of an wafer with a lapse of time, the formation can not be effectively prevent or delayed.
25 Enhanced stabilization of the outer surface after a cleaning treatment is

performed by means of providing the conventional rotation type wafer cleaning device with a novel wafer drying device.

Disclosure of the Invention

5 Previously, with the conventional rotation type silicon wafer cleaning device, it was assumed that hydrogen atoms were bonded with Si atoms on the exposed wafer through the drying process, thus ensuring stability of the silicon wafer after a cleaning treatment by achieving the so-called hydrogen termination on all the Si atoms on the outer surface of the wafer.

10 However, inventors of the present invention have discerned that either the incomplete treatment of the hydrogen termination of Si on the aforementioned outer surface or the partial mottle of the hydrogen termination would cause relatively low stability of the outer surface of the wafer treated with the conventional rotation type wafer cleaning device, and reached an idea that long-
15 term stability of Si on the outer surface is enhanced by means that the hydrogen termination treatment of Si on the outer surface of the wafer after pure water cleaning is performed in an atmosphere of inert gas(es) (such as N₂) unreactive to hydrogen, including radicalized hydrogen, thus increasing bonding of Si atoms with H atoms, and the number of uncombined Si atoms and the number
20 of Silicon atoms bonded with fluorine atoms are reduced significantly. At the same time, a rotation type silicon wafer cleaning device has been developed to embody the said idea, and a number of stabilization tests have been conducted on the wafers cleaned and dried with the device.

25 The present invention has been a creation based on the aforementioned ideas and tests.

According to a first aspect of the invention there is provided a rotation type silicon wafer cleaning equipment which is provided with a silicon wafer support/rotation driving mechanism (3) inside a case body (2) for cleaning the silicon wafer at the post chemical cleaning with pure water, having a silicon wafer drying device (1) comprising a gas supply panel (5) attached to the afore-mentioned case body (2) to supply a mixed gas of the hydrogen gas and inert gas containing more than 0.05%Vol of the hydrogen, a mixed gas supply pipe (A) coupled with a gas mixer (14) of the afore-mentioned gas supply panel (5) at one end, a mixed gas heating device (B) to heat the mixed gas in the afore-mentioned mixed gas supply pipe (A), and a hydrogen radical formation apparatus (C) equipped with a platinum coating film to form hydrogen radical at the gas contacting part whereto a high temperature gas heated with the afore-mentioned mixed gas heating device (B) touches, thus to gush out the mixed gas containing hydrogen radical formed with the afore-mentioned radical formation apparatus (C) onto the rotating silicon wafer (4) after the cleaning is completed so that drying and hydrogen termination treatments are performed on the outer surface of the silicon wafer (4), wherein the mixed gas supply pipe (A) is formed with a vertical coupling pipe (7) so supported by the case body (2) as to be traveling-free upward and downward and also rotation-free to the direction of the periphery of circle, and a lateral coupling pipe (10) coupled to the other end of the said vertical coupling pipe (7) and supported horizontally and a lift/rotation driving mechanism (8) supports the afore-mentioned vertical coupling pipe (7) and is operated to move the vertical coupling pipe (7) in the upward and downward directions and rotate it to the positive and reverse directions.

25 In a preferred embodiment, a sheathed heater installed at a part in the mixed gas supply pipe A is used as the mixed gas heating device B, thus enabling to heat the mixed gas to more than 150°C by employing the said mixed gas heat device B.

According to another aspect of the present invention there is provided a rotation type silicon wafer cleaning equipment which is provided with a silicon wafer support/rotation driving mechanism (3) inside a case body (2) for cleaning

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the silicon wafer at the post chemical cleaning with pure water, having a silicon wafer drying device (1) comprising a gas supply panel (5) attached to the aforementioned case body (2) to supply a mixed gas of the hydrogen gas and inert gas containing more than 0.05%Vol of the hydrogen, a mixed gas supply pipe (A) coupled with a gas mixer (14) of the afore-mentioned gas supply panel (5) at one end, a mixed gas heating device (B) to heat the mixed gas in the afore-mentioned mixed gas supply pipe (A), and a hydrogen radical formation apparatus (C) equipped with a platinum coating film to form hydrogen radical at the gas contacting part where to a high temperature gas heated with the afore-mentioned mixed gas heating device (B) touches, thus to gush out the mixed gas containing hydrogen radical formed with the afore-mentioned radical formation apparatus (C) onto the rotating silicon wafer (4) after the cleaning is completed so that drying and hydrogen termination treatments are performed on the outer surface of the silicon wafer (4), wherein a hydrogen radical formation/dispersion apparatus (11) equipped with a platinum coating filter fitted to the front end of the mixed gas supply pipe (A) is applied for the hydrogen radical formation apparatus (C).

Preferably, according to either aspect of the invention, the mixing ratio of the hydrogen gas is made to be 0.05Vol% - 5.0Vol%.

In one embodiment, the vertical coupling pipe 7 comprises a coupling body 15 and a sheathed heater 16 inserted and fitted therein and is provided with a vertical coupling pipe 9 which allows a mixed gas to run through the space between the inside wall face of the afore-mentioned coupling pipe 15 and the outside wall face of the sheathed heater 16 to be heated with the sheathed heater.

According to one embodiment, a heater-mounted lateral coupling pipe 10 comprises a stainless-steel-made outer pipe 17, an inner pipe 19 wherein a spacer 18 is installed for its being fixed to allow the mixed gas to run through, a micro sheathed heater 20 wound around the outer perimeter of the inner pipe, and an aluminum-foil-made cover 21 covering the outer perimeter of the outer pipe 19 around which the micro sheathed heater 20 is wound.

In another embodiment the lift/rotation driving mechanism 8 for the vertical coupling pipe 7 lowers the vertical coupling pipe 7 so that the hydrogen radical

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formation/dispersion apparatus 11 is maintained and settled at a place whereat the spacing between the lower surface of a platinum coated filter 26 and the upper surface of the silicon wafer 4 facing the filter will be 0.5mm – 3mm.

In one preferred embodiment the mixed gas temperature to be supplied to the hydrogen radical formation/dispersion apparatus 11 is maintained at 150°C – 300°C.

In another embodiment the hydrogen radical formation/dispersion apparatus 11 comprises a reverse-dish-shaped upper body 23 having a mixed gas inlet opening 23a at the centre of a upper wall, a reflecting plate 25 installed horizontally on the lower face side of the upper body 23 and having a plurality of gas permeating orifices 25a around the outer perimeter, a short cylinder-shaped filter Flange 24 welded onto the lower end surface of the upper body 23, and a platinum coated filter 26 fixed on the lower face side of the filter flange 24 forming a platinum layer on the porous disc made of a stainless-steel-sintered material.

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BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a front view of a wafer cleaning device illustrating an embodiment according to the present invention.

Figure 2 is a right side view of Figure 1.

20 Figure 3 is a schematic illustration taken on line A-A in Figure 2.

Figure 4 is a schematic sectional illustration taken on line B-B in Figure 2.

Figure 5 is a diagram illustrating a composition of a gas supply panel.

Figure 6 is a schematic sectional illustration of a heater-mounted vertical coupling pipe.

Figure 7 is a schematic sectional illustration of a heater-mounted lateral
5 coupling pipe.

Figure 8 is a characteristic curve displaying the relation of a temperature and a reaction ratio at the reaction of hydrogen activated by the platinum catalysis and oxygen.

Figure 9 is a characteristic curve of the infrared absorption of Si-H on
10 the silicon wafer immediately after a hydrogen termination treatment is achieved according to the present invention.

List of Reference Letters and Numerals

- | | |
|----|--|
| 15 | A Mixed gas supply pipe |
| | B Mixed gas heating device |
| | C Hydrogen radical formation apparatus |
| | 1 Silicon wafer drying device |
| | 2 Case body |
| 20 | 3 Wafer support/rotation driving mechanism |
| | 3a Support disc |
| | 3b Rotation driving part |
| | 4 Silicon wafer |
| | 5 Gas supply panel |
| 25 | 6 Flexible coupling pipe |

- 7 Vertical coupling pipe
- 8 Lift/rotation driving mechanism
- 9 Heater-mounted vertical coupling pipe
- 10 Heater-mounted lateral coupling pipe
- 5 11 Hydrogen radical formation/dispersion apparatus
 - 12a Pressure regulator
 - 12b Pressure gauge
 - 12c Mass flow controller
 - 12d□12e Valves
- 10 13a Pressure regulator
 - 13b Pressure gauge
 - 13c Mass flow controller
 - 13d□13e Valves
- 14 Gas mixer
- 15 15 Coupling pipe body
 - 15a Gas inlet opening
 - 16b Gas outlet opening
 - 15c Lead wire dragging-out opening
- 20 16 Sheathed heater
 - 16a Heat generation part
 - 16b Thermoelectric couple
 - 16c Lead for input
 - 16d Lead for thermoelectric couple
- 25 17 Outer pipe
- 18 Spacer

- 19 Inner pipe
- 20 Micro sheathed heater
- 21 Aluminum-foil-made cover
- 22 Union joint
- 5 23 Upper body
- 23a Mixed gas inlet opening
- 24 Filter flange
- 25 Reflecting plate
- 25a Gas permeating orifice
- 10 26 Platinum coated filter

DETAILED DESCRIPTION OF THE INVENTION

The following embodiments in accordance with the present invention are described hereunder with reference to the drawings.

- 15 Figure 1 is a front view of a rotation type silicon wafer cleaning device illustrating an embodiment according to the present invention. Figure 2 is a side view of the device. Figure 3 is a schematic sectional illustration taken on line A-A in Figure 2. Figure 4 is a schematic illustration taken on line B-B in Figure 2. It is to be noted that any type of cleaning devices can be employed as long as it is of a rotation type even though a so-called single wafer processing cleaning device is described in the present invention.
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- Referring to Figures 1-4 inclusive, 1 designates a silicon wafer drying device, 2 a case body, 3 a wafer support/rotation driving mechanism, 4 a silicon wafer, 5 a gas supply panel, 6 a flexible coupling pipe, 7 a vertical coupling pipe, 8 a lift/rotation driving mechanism, 9 a heater-mounted vertical coupling
- 25

pipe, 10 a heater-mounted lateral coupling pipe, and 11 a hydrogen radical formation/dispersion apparatus. And, A designates a mixed gas supply pipe comprising a flexible coupling pipe 6, a vertical coupling pipe 7, heater-mounted vertical coupling pipe 9, a heater-mounted lateral coupling pipe 10 and the like,
5 B a mixed gas heating device installed on a part of the mixed gas supply pipe A, and C a hydrogen radical formation apparatus installed on the down-stream side of the mixed gas heating device B.

The afore-mentioned rotation type silicon wafer cleaning device is formed by arranging a silicon wafer drying device 1 comprising a after-
10 mentioned gas supply panel 5, a mixed gas supply pipe A, a mixed gas heating device B, a hydrogen radical formation apparatus C and the like; a support/rotation driving mechanism 3 for the wafer 4 comprising a support disc 3a, a rotation driving part 3b and the like; an automatic setting/removing device (not illustrated) for the wafer 4; an automatic carry-in/carry-out device (not
15 illustrated) for the wafer 4; a jet-spray device (not illustrated) for chemical cleaning agents such as hydrofluoric acid and the like; a jet-spray device (not illustrated) for cleaning water such as pure water and the like; and the like in the case body 2.

A detailed explanation of a wafer support/rotation driving mechanism 3
20 comprising the afore-mentioned support disc 3a and a rotation driving part 3b, an automatic setting/removing device for a wafer, and automatic carry-in/carry-out device for the wafer, a jet-spraying device for chemical cleaning agents, a jet-spraying device for cleaning water such as pure water and the like is omitted herewith because they are publicly disclosed.

25 The afore-mentioned gas supply panel 5 installed and fixed on the side

part inside a case body 2 supplies a mixed gas G of an inert gas with no reaction with hydrogen (such as N₂ gas) and H₂ as illustrated in Figure 5 to a hydrogen radical formation/dispersion apparatus 11 through a mixed gas supply pipe A comprising an the after-mentioned flexible coupling pipe 6, a vertical coupling pipe 7, a heater-mounted vertical coupling pipe 9, a heater-mounted lateral coupling pipe 10 and the like.

In the embodiment according to the present invention, it is so constructed that a gas supply panel 5 and the like are housed inside the case body 2. However, there is no need to say that they can be installed outside the case body 2. Further, in the embodiment according to the present invention, heating of the after-mentioned mixed gas G is performed at two separate places, that is, a heater-mounted vertical coupling pipe 9 and a heater-mounted lateral coupling pipe 10. However, it is also possible that heating is performed either at the former heater-mounted vertical coupling pipe 9 or at the latter heater-mounted lateral coupling pipe 10.

Furthermore, in the embodiment according to the present invention, a mixed gas heating device B is formed by heaters installed on a vertical coupling pipe 9 and a lateral coupling pipe 10. However, the formation of a mixed gas heating device B can be of any type. Also, either an indirect or direct heating method can be applied to heat the mixed gas G.

Concretely, as illustrated in Figure 5, the afore-mentioned gas supply panel 5 is formed by a N₂ supply line comprising a pressure regulator 12a, a pressure gauge 12b, a mass flow controller 12c and valves 12d and 12e; a H₂ supply line comprising a pressure regulator 13a, a pressure gauge 13b, a mass flow controller 13c and valves 13d and 13e; and a gas mixer 14 for H₂ and N₂.

In the embodiment according to the present invention, it is so arranged that N₂ and H₂ are mixed inside the gas mixer 4, and a mixed gas with N₂ and H₂ containing 0.1Vol% of H₂ is supplied to a hydrogen radical formation/dispersion apparatus 11 at the flow rate of approximately 30SLM (liters per minute under
5 standard conditions).

In the afore-mentioned embodiment according to the present invention, a hydrogen radical formation/dispersion apparatus 11 installed at the front end of the down-stream side of the mixed gas supply pipe A is employed for a hydrogen radical formation apparatus C. However, the said hydrogen radical
10 formation apparatus C can be of any construction as long as the gas contacting part for a mixed gas G is equipped with a platinum film.

There is no need to say that the hydrogen radical formation apparatus C can be installed at any place as long as it is installed down-stream of the mixed gas heating device B.

15 In the afore-mentioned embodiment according to the present invention, a mass flow controller 12c for N₂ and a mass flow controller 13c for H₂ employ one for the flow rate of 50SLM and one for the flow rate of 100SCCM respectively. SLM and SCCM indicate flow rates expressed in l/min and cc/min respectively under the standard conditions.

20 In the embodiment according to the present invention, the mixing ratio of H₂ in the mixed gas G is set at approximately 0.1Vol%. It should be noted that it is desired that the mixing ratio of H₂ is set at around 0.01 - 5.0Vol% for the reasons that the level of a so-called hydrogen termination treatment of Si will not be enhanced due to the fact that it is saturated and the volume loss
25 increases even when the mixing ratio of H₂ is raised to higher than 5.0Vol%,

while the level of a hydrogen termination treatment of Si will be lowered when the mixing ratio of H₂ is lowered below 0.01%, thereby making it difficult to perform the hydrogen termination treatment properly or making the treatment more time-consuming.

5 In the embodiment according to the present invention, it is so arranged that a mixed gas G with a flow rate of 30SML is supplied to a hydrogen radical formation/dispersion apparatus 11 for 2-3 minutes for the drying treatment of a wafer 4 with the outside diameter of approximately 54mm ϕ as explained later. However, the outside diameter of a wafer to be treated is not limited to that in
10 the said embodiment, and the flow rate of the mixed gas to be supplied can be appropriately adjusted depending on the outside diameter of the wafer 4 to be cleaned, the time for the drying treatment, a temperature of the mixing gas and the like.

 In the embodiment according to the present invention, a stainless-steel
15 flexible tube with the outside diameter of 35mm ϕ , which inner surface is electrolytically polished, is employed for the afore-mentioned flexible coupling pipe 6, and, as illustrated in Figure 1, and secured removably between the outlet side of the gas supply panel 5 and the lower end part of the vertical coupling pipe 7.

20 Similarly, a stainless-steel tube with the outside diameter of 6.35mm ϕ , which inner surface is electrolytically polished, is employed for the afore-mentioned vertical coupling pipe 7, and installed in a vertical position inside the case body 1, and supported rotation-free and traveling-free upward and downward thereto.

25 Namely, the outer peripheral surface of the lower end part of the said

vertical coupling pipe 7 engaged with and supported by the after-mentioned lift/rotation driving mechanism 8, thus making the vertical coupling pipe 7 slide upwards and downwards within a prescribed distance (approximately 200mm in the embodiment), and rotate both forwardly and reverse to the peripheral
5 direction within the prescribed range of an angle (approximately 20° in the embodiment) with the operation of the lift/rotation driving mechanism.

The after-mentioned heater-mounted vertical coupling pipe 9 is connected to the upper end part of the said vertical coupling pipe 7, thus forming a passage for the flow of a mixed gas G in the vertical direction with
10 both coupling pipes 7 and 8.

The afore-mentioned lift/rotation driving mechanism 8 allows a vertical coupling pipe 7, a heater-mounted vertical coupling pipe 9 and the like to slide to up and downward directions, and the shaft of a vertical coupling pipe 7 to rotate forwardly and reverse for the angle θ to the peripheral direction
15 (approximately 20° in the embodiment). It is so constituted in the embodiment that a vertical coupling pipe 7 is slid upwards and downwards by means of combining a motor driving part with a rack mechanism, and the vertical coupling pipe 7 rotates forwardly and reverse for the prescribed angle of θ to the peripheral direction by means of combining a motor driving part with a gear
20 mechanism.

The afore-mentioned lift/rotation driving mechanism 8 can be of any construction such as a lift/rotation driving mechanism 8 with an air cylinder type or an oil pressure cylinder type.

As illustrated in Figure 6, the afore-mentioned heater-mounted vertical
25 coupling pipe 9 is formed with a coupling pipe body 15 and a sheathed heater

16 housed in the coupling pipe body 15, and a gas inlet opening 15a, a gas outlet opening 15b and a lead wire dragging-out opening 15c are installed on the coupling pipe body 15 respectively.

In the embodiment according to the present invention, a stainless-steel
5 pipe with an inner surface, which outer diameter is 19.05mm ϕ and inner surface is electrolytically polished, is employed for a coupling pipe body 15, and a space made between the outer peripheral surface of a sheathed heater 16 inserted and fitted to the inside thereof and the inner wall surface of a coupling pipe body 15 forms a flow passage. Also, a stainless-steel pipe with the outer diameter of
10 6.35mm ϕ , which inner wall surface is electrolytically polished, is employed for a gas inlet opening 15a and a gas outlet opening 15b.

The afore-mentioned sheathed heater 16 is formed with a heat generation part 16a, a thermoelectric couple 16b, a lead for input 16c, a lead for the thermoelectric couple 16d, and the like. In the embodiment according to the
15 present invention, the one having a heat generation part 16a with capacity of 20V and 200W inserted in and fitted to the inside of the stainless-steel pipe with the outer diameter of 12mm ϕ is employed for the sheathed heater 16.

The capacity of a sheathed heater 16 and the effective sectional area of a flow passage inside a coupling pipe body 15 are determined appropriately
20 depending on the flow rate of the gas passing through inside a heater-mounted vertical coupling pipe 9 and the degree and velocity of temperature rise and the like of the mixed gas G.

In the embodiment according to the present invention, two pieces of a sheathed heater 16 equipped with a heat generation part 16a with capacity of
25 200W are employed to heat and raise the mixed gas of approximately 30SLM

(H₂ 0.1% and N₂ 99.9%) to 100°C - 150°C within 5 - 20 seconds. Of course, any gas can be employed instead of N₂ to form the mixed gas as long as it does not react with hydrogen.

In the embodiment according to the present invention, a gas inlet opening 15a is installed on the lower part of the outer peripheral surface of the coupling pipe body 15 used for a heater-mounted vertical coupling pipe 9. Therefore, axes of the vertical coupling pipe 7 and the heater-mounted vertical coupling pipe 9 are not lined linearly. However, it is possible that both axes of the vertical coupling pipe 7 and the heater-mounted vertical coupling pipe 9 can be positioned linearly by replacing the position of a lead wire dragging-out opening 15c with the position of a gas inlet opening 15a.

The afore-mentioned heater-mounted lateral coupling pipe 10 is coupled in a horizontal position with the upper end part of the heater-mounted vertical coupling pipe 9. At the front end part, the after-mentioned hydrogen radical formation/dispersion apparatus 11 is installed and fixed. Of course, it is possible that a heater is installed inside the hydrogen radical formation/dispersion apparatus 11.

Figure 7 is a schematic sectional illustration of a heater-mounted lateral coupling pipe 10 employed for a rotation type wafer cleaning device in the embodiment according to the present invention. There is formed a heater-mounted lateral coupling pipe 10 in the manner that a stainless-steel-made inner pipe 19 with an outer diameter of 6.35mmφ, which inner wall surface is electrolytically polished, is supported and fixed inside the stainless-steel-made outer pipe 17 with the outer diameter of 19.05mmφ by means of installing a spacer 18, and the outer peripheral surface of the inner pipe 19 is wounded by

a micro sheathed heater 20 at an appropriate pitch and the upper part of which is covered by a aluminum foil 21.

In the embodiment according to the present invention, a mixed gas G of approximately 100°C - 120°C and approximately 30SLM supplied through a heater-mounted vertical coupling pipe 9 is heated to approximately 200°C - 250°C while passing through an inner pipe 19 by means of 6 pieces of micro sheathed heater 20 with capacity of 150W, and then supplied into the after-mentioned hydrogen radical formation/dispersion apparatus 11 from its front end part.

In the embodiment according to the present invention, the length of a heater-mounted lateral coupling pipe 10 is made approximately 400 - 500mm. Furthermore, as illustrated in Figures 3 and 4, the said heater-mounted lateral coupling pipe 10 travels in the range of approximately 200mm to the up and down directions and also approximately 20° at the angle to the horizontal direction respectively by means of the operation of a lift/rotation driving mechanism.

There is no need to say that heat-insulation materials not illustrated in the afore-mentioned Figures 6 and 7 are applied around the outer peripheral part of the coupling pipe body 15 of the heater-mounted vertical coupling pipe 9 and also around the outer peripheral part of the outer pipe 17 of the heater-mounted lateral coupling pipe 10.

A hydrogen radical formation/dispersion apparatus 11 is welded to the front end part of the afore-mentioned heater-mounted lateral coupling pipe 10. A radicalized hydrogen-contained nitrogen gas is gushed out from the said hydrogen radical formation/dispersion apparatus 11 toward the outer surface of

a silicon wafer 4 positioned thereunder.

As illustrated in Figure 7, the afore-mentioned hydrogen radical formation/dispersion apparatus 11 comprises a stainless-steel-made and reversed-dish-shaped upper body 23, a disc-shaped reflecting plate 25 welded
5 to the lower end edge of the upper body 23 and the upper end part of the cylinder-shaped filter flange 24, and a disc-shaped platinum coated filter 26 fixed to the lower end edge of the filter flange 24.

Namely, there is formed a mixed gas inlet opening 23a on the center of the upper wall surface of the afore-mentioned reverse-dish-shaped upper body
10 23, and a mixed gas G heated to approximately 150°C - 250°C is led to the inside of the upper body 23 through the said gas inlet opening 23a.

The afore-mentioned disc-shaped reflecting plate 25 is made of stainless-steel, and there are made a plurality of gas permeating orifices 25a on its outer peripheral part. The outer peripheral edge of the said reflecting plate is
15 welded to the upper body 23 in such a state as it being held between the upper end surface of a short cylinder-shaped filter flange 24 and the lower end surface of the upper body 23.

Furthermore, the afore-mentioned platinum coated filter 26 is formed by coating platinum on the outer surface of the stainless-steel-made filter material.
20 In the embodiment according to the present invention, pieces of a net-shaped body of approximately 8 mesh formed with the stainless-steel-made wire with the outer diameter of 1μm are stacked and sintered to make a disc-shaped filtration material with the thickness of approximately 2 - 3mm, the outer diameter of approximately 60mm and the average pore size of 20μm, and to
25 form a platinum layer with the thickness of approximately 0.3μm on the outer

surface of a pore of the said filtration material by means of vapor deposition.

There is no need to say that the method to form a platinum layer on the stainless-steel-made filtration material is not limited to the afore-mentioned method of vapor deposition, but any other methods such as an ion plating
5 method can be applied as long as a platinum layer is formed on the outer surface of the stainless steel.

In the embodiment according to the present invention, a sintered material is employed as the stainless-steel-made filtration material, and the average pore size, the thickness, and the thickness of a platinum layer are set
10 at 20 μ m, approximately 2 - 3mm and approximately 0.3 μ m respectively. However, the method of forming a filtration material, the thickness, the external dimensions and the average pore size of the material as well as the thickness of a platinum layer and the like are not limited to values on the embodiment according to the
15 present invention, but they can be appropriately determined depending on the flow rate and the duration of gushing-out of the gas G, the external dimensions of a silicon wafer 4 and the like.

A platinum coated filter 26 for the afore-mentioned hydrogen radical formation/dispersion apparatus 11 is horizontally maintained at and fitted to the
20 lower end part of the short cylinder-shaped filter flange 24 by means of a screw stopping mechanism.

As a hydrogen radical formation/dispersion apparatus 11 is lowered by means of a lift/rotation driving mechanism 8, the lower face side of the said platinum coated filter 26 goes down in the neighborhood of the outer surface of
25 the wafer 4 set on the wafer support disc 3a.

Even though the smaller is the better for the spacing between the lower surface side of the afore-mentioned platinum coated filter 26 and the outer surface of the wafer 4, it is normally set at approximately 0.5 - 1.5mm from the view point of durability and the like of the activity of hydrogen radical formed by the after-mentioned catalytic action of platinum.

Now, the operation of a rotation type silicon wafer cleaning device in accordance with the present invention is explained.

Referring to Figures 1-4 inclusive, a wafer 4 to be treated for cleaning is automatically set and fitted on a support disc 3a of the wafer cleaning device, and the wafer 4 starts rotating at the high speed (approximately 2000 - 2500RPM) by the operation of the wafer support/rotation driving mechanism 3.

Next, so-called acid cleaning is performed by a chemical cleaning agent such as hydrofluoric acid and the like being jet-sprayed onto the wafer 4 rotating at the high speed. Furthermore, upon completion of the said acid cleaning, pure water cleaning is performed by pure water being jet-sprayed onto the outer surface of the wafer 4.

Detailed explanation on the afore-mentioned chemical cleaning and pure water cleaning treatments is omitted herewith due to the reason that these treatments are well disclosed.

Upon completion of the pure water cleaning treatment, draining is performed while the wafer 4 rotates at the high speed, and at the same time, by having a lift/rotation driving mechanism 8 work to lower and rotate a vertical coupling pipe 7, a heater-mounted vertical coupling pipe 9 and a heater-mounted lateral coupling pipe 10 integrally, a hydrogen radical formation/dispersion apparatus 11 at the front end of the heater-mounted lateral

coupling pipe 10 travels from the retreat position (a dotted line) to the operation position (a solid line) in Figures 3 and 4.

Immediately after the operation of the afore-mentioned lift/rotation driving mechanism 8 gets started (or after an appropriate lapse of time), the gas supply panel 5 starts operating to supply a mixed gas G with H₂ and N₂ containing H₂ of 0.1% at the flow rate of 30SLM from a gas mixer 14 to a vertical coupling pipe 7. It is desirable that a hydrogen radical formation/dispersion apparatus 11 has completed its traveling to the operational position before starting the supply of the said mixed gas G.

10 The mixed gas G supplied to a vertical coupling pipe 7 is heated to approximately 80°C - 150°C with a sheathed heater 16 while passing through a heater-mounted vertical coupling pipe 9. And, the mixed gas G heated inside the vertical coupling pipe 9 is continuously heated while passing inside a heater-mounted lateral coupling pipe 10 to approximately 150°C - 300°C, thus
15 being led to the inside of the hydrogen radical formation/dispersion apparatus 11.

Referring to Figure 7, the mixed gas that gushes in to the inside of the upper body 23 of the hydrogen radical formation/dispersion apparatus 11 through a mixed gas inlet opening 23a is dispersed by colliding with a reflecting
20 plate 25, and is let to the upper surface side of a platinum coated filter 26 through gas permeating orifices 25a. After the hydrogen gas is converted to hydrogen radical by the catalytic action of platinum while passing through a filter 26, it is then gushed out together with N₂ onto the wafer 4.

A mixed gas G gushed out onto the afore-mentioned filter 26 is heated
25 to the high temperature of 150°C - 300°C (approximately 250°C in the

embodiment according to the present invention).

As the result, a mixing gas G turn to hydrogen radical when the hydrogen in the mixed gas is activated by means of contacting with a platinum catalyst while passing through the filter 26, thus the binding of Hydrogen with Si
5 atoms is remarkably enhanced.

Namely, gushing out a mixed gas G dominantly composed of N₂ containing hydrogen radical onto the wafer 4 rotating at the high speed from the lower face of the filter 26 hydrogen atoms are firmly and easily bonded with Si atoms exposed through the pure water cleaning, and thus, a hydrogen
10 termination is thoroughly completed for Si atoms on the outer surface of the wafer without any mottles.

The radicalization of hydrogen in the afore-mentioned mixed gas G by means of employing platinum catalyst can be sufficiently performed when the temperature of the mixed gas reaches higher than 150°C. In the embodiment
15 according to the present invention, the temperature of the mixed gas has been raised to 250°C taking some margin into consideration.

It is evident that the limiting temperature to form hydrogen radical is approximately 150°C as illustrated in Figure 8 wherein the relation curve between the reaction rate and the temperature is shown in case that water is
20 produced by the reaction of radicalized hydrogen with oxygen employing platinum as a catalyst. The fact that the reaction rate reaches closely 100% when the temperature exceeds approximately 150°C indicates that hydrogen is almost completely radicalized at the temperature of approximately 150°C.

In the embodiment according to the present invention, the spacing of a
25 hydrogen radical formation/dispersion apparatus 11 and a wafer 4 is set for

approximately 1mm. It should be noted that the smaller spacing is the better. Accordingly, sufficient hydrogen termination treatment cannot be expected when the afore-mentioned spacing becomes wider than approximately 3mm because hydrogen radical vanishes between the outer surface of the filter 26
5 and the outer surface of the wafer 4.

At the same time, contrary to this fact, when the afore-mentioned spacing is made smaller than 0.5mm, it becomes inappropriate because of the possible danger of the wafer 4 rotating at the high speed being contacted with the filter 26. Due to this reasons, the afore-mentioned spacing is set at 1mm in
10 the embodiment according to the present invention.

It would be sufficient if the release of the mixed gas G is performed through the afore-mentioned hydrogen radical formation/dispersion apparatus 11 for approximately 2-3 minutes. In the embodiment according to the present invention, the drying of the Si wafer with the outer diameter of 60mm ϕ rotating
15 at the speed of 2000RPM is perfectly achieved by releasing the mixed gas G which temperature and flow rate are 250°C and 30SLM respectively, and at the same time nearly perfect hydrogen termination treatment of Si atoms on its outer surface is performed.

20 Embodiment

A Si wafer 4 having an outer diameter of 60mm ϕ is treated for cleaning with hydrofluoric acid and pure water, and rotates at the speed of 2000RPM while its Si surface is completely exposed. And, then a mixed gas with H₂ and N₂
25 Containing H₂ of 0.1% is supplied to a hydrogen radical formation/dispersion

apparatus 11 at the speed of 30SLM. The spacing between the filter 26 and the Si wafer is made 1mm, thus making the mixed gas G gushed out for 2 minutes continuously through the space.

5 A filter 26 having the outer diameter of 54mm ϕ , the thickness of 2.5mm is formed in the shape of a disc comprising a sintered body made of a stainless-steel-made meshed net body having a pore with an average size of 20 μ m and the temperature of the mixed gas at an inlet opening of the filter is set at 250°C.

10 When a wafer 4 dried and treated for the hydrogen termination with the silicon wafer drying device 1 in the afore-mentioned embodiment is left in the cleaned air for natural oxidation, it was found that no significant change in appearance such as discoloration is noticed on the outer surface of the silicon wafer even after the lapse of approximately 48 hours.

A test was conducted for comparison. In the test, a Si wafer 4 processed for the same pre-cleaning with hydrofluoric acid and pure water was made to rotate at the speed of 2000RPM, and a N₂ gas of the temperature of 250°C was jet-sprayed onto the outer surface of the Si wafer 4 continuously for 2 minutes using a dispersion apparatus equipped with the identical filter with no platinum coating being done at the flow rate of 30SLM.

20 The Si wafer 4 treated for drying was left in the cleaned air for natural oxidation in the comparison test, and discoloration due to the formation of an oxide film was noticed on the outer surface of the silicon wafer after the lapse of approximately 48 hours.

As evident from the result of the afore-mentioned observation in appearance, when a drying treatment is performed employing a rotation type silicon wafer cleaning device according to the present invention, it is clear that

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Si atoms on the outer surface of the Si wafer reach a high degree of hydrogen termination. This enables the outer surface of the silicon wafer processed for the post-cleaning to be maintained in stable conditions for a long period of time.

Generally, the degree of hydrogen termination on the silicon outer
5 surface is judged by observing the peak of infrared absorption of Si-H (in the neighborhood of 2200Cm^{-1}) by means of the so-called FT-IR (the ATR method).

Referring to Figure 9, there is shown a result of measuring infrared absorption of Si-H on the silicon wafer using the FT-IR-ATR method immediately after cleaning and drying treatments are conducted by means of
10 the method shown in the afore-mentioned embodiment employing a rotation type silicon wafer cleaning device in accordance with the present invention. It has been confirmed that in the case that when a drying treatment (a hydrogen termination treatment) is performed with the mixed gas G containing hydrogen radical (as shown in the curve A), the peak of infrared absorption of Si-H
15 becomes higher compared with the peak in the case without that hydrogen radical (as shown in the curve B).

Effects of the Invention

According to the present invention, a silicon wafer drying device
20 comprising a hydrogen radical formation apparatus C equipped with a platinum film on the gas contacting part, a mixed gas heating device B, a mixed gas supply pipe A, a gas supply panel and the like is installed inside the case body of a rotation type silicon wafer cleaning apparatus, thus drying the wafer by gushing out the mixed gas of hydrogen and inert gas heated to more than
25 150°C through the afore-mentioned hydrogen radical formation apparatus C to

make hydrogen radical by means of the catalytic action with the aforementioned platinum coated film, and jet-spraying the mixed gas containing the said hydrogen radical onto the wafer.

As the result, a high degree of the hydrogen termination treatment can
5 be achieved because Si atoms on the outer surface of the silicon wafer wherein Si is exposed after the pure water cleaning, are perfectly bonded with H atoms so that the outer surface of the Si wafer can be maintained in stable conditions for a long period of time.

As explained above, the present invention achieves excellent, practical
10 effects.

What is claimed is:

1. A rotation type silicon wafer cleaning equipment which is provided with a silicon wafer support/rotation driving mechanism (3) inside a case body (2) for cleaning the silicon wafer at the post chemical cleaning with pure water, having a
5 silicon wafer drying device (1) comprising a gas supply panel (5) attached to the afore-mentioned case body (2) to supply a mixed gas of the hydrogen gas and inert gas containing more than 0.05%Vol of the hydrogen, a mixed gas supply pipe (A) coupled with a gas mixer (14) of the afore-mentioned gas supply panel (5) at one end, a mixed gas heating device (B) to heat the mixed gas in the afore-
10 mentioned mixed gas supply pipe (A), and a hydrogen radical formation apparatus (C) equipped with a platinum coating film to form hydrogen radical at the gas contacting part whereto a high temperature gas heated with the afore-mentioned mixed gas heating device (B) touches, thus to gush out the mixed gas containing hydrogen radical formed with the afore-mentioned radical formation apparatus (C)
15 onto the rotating silicon wafer (4) after the cleaning is completed so that drying and hydrogen termination treatments are performed on the outer surface of the silicon wafer (4), WHEREIN the mixed gas supply pipe (A) is formed with a vertical coupling pipe (7) so supported by the case body (2) as to be traveling-free upward and downward and also rotation-free to the direction of the periphery of circle, and
20 a lateral coupling pipe (10) coupled to the other end of the said vertical coupling pipe (7) and supported horizontally and a lift/rotation driving mechanism (8) supports the afore-mentioned vertical coupling pipe (7) and is operated to move the vertical coupling pipe (7) in the upward and downward directions and rotate it to the positive and reverse directions.
- 25 2. A rotation type silicon wafer cleaning equipment as claimed in Claim 1 wherein a sheathed heater installed at a part of the mixed gas supply pipe (A) is applied for the mixed gas heating device (B), thus heating the mixed gas to higher than 150°C with the afore-mentioned mixed gas heating device (B).
3. A rotation type silicon wafer cleaning equipment which is provided with a
30 silicon wafer support/rotation driving mechanism (3) inside a case body (2) for cleaning the silicon wafer at the post chemical cleaning with pure water, having a

- silicon wafer drying device (1) comprising a gas supply panel (5) attached to the afore-mentioned case body (2) to supply a mixed gas of the hydrogen gas and inert gas containing more than 0.05%Vol of the hydrogen, a mixed gas supply pipe (A) coupled with a gas mixer (14) of the afore-mentioned gas supply panel (5) at one end, a mixed gas heating device (B) to heat the mixed gas in the afore-mentioned mixed gas supply pipe (A), and a hydrogen radical formation apparatus (C) equipped with a platinum coating film to form hydrogen radical at the gas contacting part whereto a high temperature gas heated with the afore-mentioned mixed gas heating device (B) touches, thus to gush out the mixed gas containing hydrogen radical formed with the afore-mentioned radical formation apparatus (C) onto the rotating silicon wafer (4) after the cleaning is completed so that drying and hydrogen termination treatments are performed on the outer surface of the silicon wafer (4), WHEREIN a hydrogen radical formation/dispersion apparatus (11) equipped with a platinum coating filter fitted to the front end of the mixed gas supply pipe (A) is applied for the hydrogen radical formation apparatus (C).
4. A rotation type silicon wafer cleaning equipment as claimed in Claim 1 or 3 wherein the mixing ratio of the hydrogen gas is set at 0.05Vol%-5.0Vol%.
5. A rotation type silicon wafer cleaning equipment as claimed in Claim 1 wherein the vertical coupling pipe (7) comprises a coupling pipe body (15) and a sheathed heater (16) inserted and fitted therein, and the vertical coupling pipe (7) is equipped with a heater-mounted vertical pipe (9) to heat by the sheathed heater (16) a mixed gas passing through between the inner wall face of the afore-mentioned vertical coupling pipe body (15) and the outer wall face of the sheathed heater (16).
6. A rotation type silicon wafer cleaning equipment as claimed in Claim 1 wherein a heater-mounted lateral coupling pipe comprising a stainless-steel-made outer pipe (17), an inner pipe (19) inserted and fitted to the inside thereof by means of installing a spacer (18) for the mixed gas to pass through, a micro sheathed heater (20) wound around the outer peripheral face of the inner pipe (19), and an aluminum-foil-made cover (21) surrounding the outer peripheral face of the inner pipe (19) around which the micro sheathed heater (20) is wound is

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applied for a heater-mounted lateral coupling pipe (10).

7. A rotation type silicon wafer cleaning equipment as claimed in Claim 1 wherein the lift/rotation driving mechanism (8) for the vertical coupling pipe (7) is so constructed that the hydrogen radical formation/dispersion apparatus (11) is
5 maintained and fitted at the position where the spacing between the lower face of a platinum coating filter (26) and the upper face of a silicon wafer (4) placed in the opposite position thereof becomes 0.5mm-3mm when the vertical coupling pipe (7) is lowered.

8. A rotation type silicon wafer cleaning equipment as claimed in Claim 3
10 wherein the temperature of the mixed gas to be supplied to the hydrogen radical formation/dispersion apparatus (11) reaches 150°C – 300°C.

9. A rotation type silicon wafer cleaning equipment as claimed in Claim 3 wherein the hydrogen radical formation/dispersion apparatus (11) is so constructed that the hydrogen radical formation/dispersion apparatus comprises a
15 reverse-dish-shaped upper body (23) having a mixed gas inlet opening (23a) at the centre of the upper wall, a reflecting plate (25) installed horizontally on the lower face side of the upper body (23) and equipped with a plurality of gas permeating orifices (25a), a short cylinder-shaped filter flange (24) welded to the lower end face of the upper body (23), and a platinum coating filter (26) fixed on
20 the lower face side of the filter flange (24) to form a platinum coating layer on the porous disc made of the stainless-steel-sintered material.