

APPARATUS FOR CORRECTING DISTORTED SYNC IN A COMPOSITE VIDEO SIGNAL

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Field of the Invention

The present invention relates to apparatus for correcting the synchronizing (sync) pulse portion of a composite luminance signal after the sync portion has been corrupted by a non-linear processing circuit which is used to process the composite luminance signal.

Background of the Invention

15 In a television receiver, it is often desirable to use non-linear signal processing in order to improve the subjective appeal of displayed images. So called "black stretch" and "white stretch" circuits are used to improve the image contrast ratio by adaptively altering the shape of a signal transfer function in the dark and bright image areas, respectively. So called gamma
20 correcting circuits also alter a signal transfer function in a non-linear manner, either statically or dynamically, to compensate for differences between the non-linear characteristics of television cameras utilized in broadcast studios and the non-linear characteristic of the display device of a receiver. So-called "auto-pedestal" circuits are also used to adaptively adjust the brightness
25 of a displayed image by inserting a "blacker-than-black" variable amplitude pulse during the back-porch region of the luminance signal. The brightness of a displayed image is altered because the "auto-pedestal" function changes the relationship between the
30 clamping level of a "back-porch" clamp and the level of the video signal which is clamped. If the synchronization component and the image component of a video signal are processed together, each of these "picture enhancement" circuit techniques may
35 impact the ability of a synchronizing pulse separator to distinguish between the "blacker-than-black" sync pulses and the image portion.

Figure 1 shows a typical application of a non-linear "picture enhancement" circuit. In this example, a television signal
40 received by an antenna 60 is tuned by a tuner 65 and



demodulated by IF section 70 to produce a baseband video signal 75. This signal is separated into a composite luminance (luma) signal 104, containing both image and sync pulse components, and a chrominance (chroma) signal 85 by a luma-chroma separator 90.

5 The chroma signal is processed by processing circuits 80 to produce color difference signals 86. Color difference signals 86 are matrixed with a luma signal 87 produced by a luma processor 81 in luma-chroma chroma matrix 82 to produce primary color signals 88 suitable for application to a picture tube 83. A non-
10 linear "picture enhancement" circuit 110 precedes luma processing circuit 81 and supplies to it a non-linearly processed luma signal 105. Composite luma signal 104 produced by luma-chroma separator 90 is coupled in parallel fashion to picture enhancement circuit 110 and a sync separator 100. Separated
15 sync signal 115 is applied to horizontal and vertical scan processing circuit 120, which in turn provide deflection signals 89 to a deflection unit 84.

The arrangement shown in Figure 1 has the desirable feature that sync separator 100 derives the composite sync signal
20 from composite luma signal 104 before it is processed by non-linear picture enhancement circuit 110. A similar arrangement is disclosed with respect to Figure 12 of U.S. patent 4,489,349 issued to Okada on December 18, 1984 and assigned to the Sony Corporation.

25 As shown in Figure 2A, the use of a picture enhancement circuit in conjunction with a combined television processor integrated circuit (IC), often called a "one-chip" television IC, such as the Toshiba TA8680 necessitates that the input signal to sync separator 100 be derived from the output
30 signal of picture enhancement circuit 110. This is due to the fact that in ICs such as the TA8680, the inputs to sync separator 100 and luma processing circuit 81 are connected together within the IC and are not accessible separately.

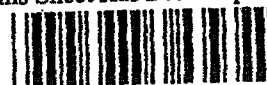
35 An example of an IC providing "black-stretch" and "auto-pedestal" functions, which may be used in the arrangements shown in Figures 1 and 2A is the Sony CX20125 dynamic picture IC. As shown in Figure 2B, the CX20125 IC receives a composite luminance signal 104, a composite horizontal and vertical retrace



blanking signal 101 and a horizontal "back-porch" clamping pulse signal 102 at respective inputs. In response, it provides a composite luminance signal 105 which has been non-linearly processed in accordance with a "black-stretch" function. In addition, an "auto-pedestal" pulse is added to the "back-porch" of the composite luminance signal. The clamping pulse signal is used to provide back-porch clamping for its own signal processing as well as to aid in generation of the "auto-pedestal" pulse. The CX20125 IC uses the composite retrace blanking signal to inhibit black-stretch during horizontal and vertical blanking intervals. Such retrace blanking interval inhibiting provisions for a non-linear processing system are also disclosed with respect to Figure 11 of the aforementioned Okada patent.

To understand how a problem in deriving the composite sync signal arises when the arrangement of Figure 2B is used, it will be helpful to review the operation of separating the composite sync pulses from the composite luminance signal. Reference will be made to Figure 3 during this description. The typical sync separator arrangement includes a clamp 103 to restore the DC level of the composite luma signal, after it is AC coupled through a capacitor (not shown), by clamping the peaks of the sync pulses to a reference voltage 106. The signal 107 so restored is applied to a level comparator 108 having a reference voltage 109 which is related to reference voltage 106 of clamp 103. By choosing reference voltage 109 of comparator 108 to be at an intermediate level between the "back-porch" level and the expected sync tip level, a composite horizontal and vertical sync pulse signal without any artifacts of the image related video signal will be produced at an output 115 of comparator 108.

The horizontal and vertical portions of a typical composite luminance signal are shown in Figures 4a and 4b, respectively. Image portion 280 of the composite luminance signal extends from blanking level 204 to peak white level 205, while horizontal sync pulses 206 and the vertical sync pulses 207 extend below blanking level 204 to sync tip level 208. The NTSC television standard specifies that the amplitude between blanking level 204 and sync tip level 208 should be 40% of the amplitude between blanking level 204 and peak white level 205. This sync



amplitude relationship provides adequate margin for any inaccuracy of the sync separator and allows the sync component to be reliably separated from the image component.

5 The horizontal and vertical portions of a composite
luminance signal which has been processed by a non-linear
processing IC such which has been the CX20125 are shown in
Figures 6a and 6b, respectively. In contrast to the waveform of
Figure 4a, note that the waveform of Figure 6a has a pulse 211
10 inserted during the back-porch interval following horizontal sync
pulse 206. This inserted pulse is a variable amplitude "auto-
pedestal" pulse. The amplitude of the auto-pedestal pulse
typically varies from blanking level 204 to a maximum level 212.
Level 212 is about 50% of the amplitude between sync tip level
208 and blanking level 204. The waveform shown in Figure 4a
15 includes a dark portion 210 during active scan time. This dark
image region extends to a level 209, which is "whiter" than the
"blacker-than-black" blanking level 204. If the total time duration
of dark image regions is relatively large during a field, "black-
stretch" processing will extend level 209 to a black level or even
20 to blacker-than-black blanking level 204. For relatively short
durations, "black-stretch" processing will extend dark level 209 to
a level 213 below blanking level 204 as shown in Figure 6a.

The horizontal and vertical retrace blanking intervals
are shown in Figures 5a and 5b, respectively. Comparing the
25 waveforms of Figures 4a and 5a, it will be noted that the
horizontal blanking interval 214 of the received signal and the
retrace blanking interval 216 are approximately coincident.
However, comparing the waveforms of Figures 4b and 5b, it will
be noted that vertical retrace blanking interval 217 is
30 considerably shorter than the vertical blanking interval 215 of the
received signal. This is a common result of typical receiver design
practice since it allows for a more economical structure and
usually causes no problem. However, in receivers using IC such as
the CX20125 ICs, the short vertical retrace blanking interval
35 results in the response shown in Figure 6b because "black-stretch"
processing is not inhibited during interval 218 between the
beginning of blanking interval 215 of the received signal and the
beginning of retrace blanking interval 217. As shown in Figure



6b, the horizontal trace portions which occur during interval 218 may be stretched from their normal level 204 to the blacker-than-black level 213. In a similar manner, the vertical equalizing pulses 282 which occur during interval 218 may be stretched
5 from level 208 to level 281. In this regard, it is noted that while the equalizing pulses are stretched, the horizontal pulses occurring during interval 218 are not stretched because "black-stretch" processing is inhibited during horizontal blanking intervals. Just as black region 210 shown in Figure 4a is sometimes stretched
10 depending on the total duty cycle of black image regions, the horizontal trace regions which occur during interval 218 may be kept at blanking level 204 or extended towards maximum extension levels 213 or 281 depending upon variations of scene content. Thus, the margin for setting the sync separator
15 comparator reference level is between sync tip level 208 and the lower of levels 212 or 213 for horizontal sync pulses, and is not predictable for vertical sync pulses. It is thus difficult to set a reliable comparator reference.

20 Summary of the Invention

The present invention partially resides in the recognition of the problem of the corruption of the sync pulse component of a composite video signal which has been processed
25 by a non-linear picture enhancement circuit.

According to an aspect of the invention, a composite signal is coupled in parallel fashion to the non-linear video processing circuit and to an auxiliary sync separator circuit. The composite horizontal and vertical sync pulses produced by the
30 auxiliary sync separator are used, according to various other aspects of the invention, to either augment or replace the corrupted sync pulses of the non-linearly processed composite video signal. The resulting composite video signal, having had its synchronizing component corrected, is coupled to a "one-chip"
35 television IC. Accordingly, horizontal and vertical synchronizing pulses can now be reliably separated from the image component.

Brief Description of the Drawing



For a detailed understanding of the invention, reference should be made to the accompanying Drawing. In the Drawing, the same reference numbers have been assigned to the same or similar elements. Figures 1, 2a, 2b, 3, 4a, 4b, 5a, 5b, 6a and 6b have already been described in detail above.

In Summary:

Figure 1 shows a block diagram of a television receiver arranged so that sync separation occurs prior to non-linear processing as is known in the prior art.

Figure 2a shows a configuration of a receiver using a picture enhancement circuit with a "one-chip" television IC and is useful in understanding the problem to which the present invention is directed.

Figure 2b shows the connection of the Sony CX20125 non-linear picture enhancement IC.

Figure 3 shows a block diagram of a sync separator.

Figures 4a and 4b show waveforms of horizontal and vertical portions, respectively, of a composite luminance signal before it is processed by a picture enhancement circuit, such as the Sony CX20125.

Figures 5a and 5b show waveforms of horizontal and vertical retrace blanking signals, respectively.

Figures 6a and 6b show waveforms of horizontal and vertical portions, respectively, of a composite luminance signal after it has been processed by the CX20125 IC.

Figure 7 shows a block diagram of an embodiment of the invention in which a sync correction circuit is interposed between the output of a non-linear signal processing IC and the combined luminance/sync input of a "one-chip" television IC.

Figures 8a, 8b and 8c show block diagrams of various embodiments of the sync corrector shown in Figure 7.

Figures 8d, 8e and 8f show circuit implementations of the embodiments shown in block form in Figures 8a, 8b and 8c, respectively.

Figures 9a and 9b show waveforms of horizontal and vertical sync pulses, respectively, produced by the auxiliary sync separator shown in the arrangement of Figure 7.



Figures 10a and 10b show waveforms of horizontal and vertical portions, respectively, of a composite luminance signal which is produced at an intermediate point of the embodiments shown in Figures 8a and 8b.

Figures 11a and 11b show waveforms of horizontal and vertical pulses, respectively, of a composite luminance signal which is produced at the output of the sync correction circuit shown in Figure 7.

Detailed Description of the Preferred Embodiment

Referring to Figure 7, composite luma signal 104, derived by chroma-luma separator 90, is applied to the input of non-linear processing circuit 110, e.g., comprising the Sony CX20125 IC, and in parallel fashion to a sync correction circuit 111. Sync correction circuit 111 also receives non-linearly processed composite luma signal 105 produced at the output of non-linear processing circuit 110. Composite luma signal 105 contains the corrupted sync portions as is shown in Figures 6a and 6b referred to above. Composite luma signal 112 produced at the output of sync corrector 111 has its sync portions corrected as is shown in Figures 11a and 11b. As a result, sync separator 100 of "one-chip" television IC 200, e.g., comprising the Toshiba TA8680 or a similar IC, can reliably separate the composite sync pulses from composite luma signal 112. The separated sync pulses are coupled to scan processing circuits 120.

Figures 8a, 8b and 8c show alternative forms of the sync corrector 111. Each version includes an auxiliary sync separator 113 which receives composite luma signal 104 which has not been processed by non-linear processing circuit 110. Auxiliary sync separator 113 operates in the manner described above with reference to Figure 3 to produce an uncorrupted composite sync signal 117, as is indicated in Figures 9a and 9b.

Composite sync signal 117 derived by auxiliary sync separator 113 is used in the embodiment shown in Figure 8a to increase the gain of an amplifier 114 during the time intervals in which the horizontal sync and equalizing pulses occur. The input signal of amplifier 114 is non-linearly processed composite luma signal 105 having corrupted sync pulses. Output signal 116 of



amplifier 114 is a composite luma signal which has its horizontal sync and equalizing pulses amplified, as is indicated in Figures 10a and 10b. A negative peak limiter 118 coupled to the output of amplifier 114 causes all of the horizontal sync and equalizing pulses to have equal amplitudes, as is indicated in Figures 11a and 11b.

In the embodiment of Figure 8b, composite sync signal 117 is added to non-linearly processed composite luma signal 105 by an adder 170. Resultant signal 116 is a composite luma signal with its horizontal and equalizing pulses extended as is indicated in Figures 10a and 10b. Composite luma signal 116 is negative peak limited by negative peak limiter 118 which provides sync corrected composite luma signal 112.

In the embodiments shown in Figures 8a and 8b, negative peak limiter 118 is desirable because composite sync signal 116 produced by gain controlled amplifier 114 of the embodiment of Figure 8a and adder 170 of the embodiment shown in Figure 8b, respectively, contains pulses with different amplitudes. This is indicated in Figures 10a and 10b. Since DC restoring clamp 103 preceding the threshold comparator 108 of sync separator 100 of IC 200 (see Figure 3) is operated to clamp the peaks of the input signal, the amplitude region or margin in which the comparison is made is a function of the peak amplitude of the input signal. This may cause unreliable operation of sync separator 100. Negative peak limiter causes all of the pulses of composite luma signal 112 to have the same amplitude and therefore eliminates that problem.

In the embodiment shown in Figure 8c, the sync pulses of composite sync signal 117 is used to operate a switch 171 which replaces the corrupted sync pulses of non-linearly processed composite luma signal 105 with a reference voltage 172. Reference voltage 172 may be chosen to provide extended amplitude sync pulses. Since all the pulses are replaced with the reference voltage, output signal 112 has pulses of equal amplitude, without the need for negative peak limiter.

In each of the above embodiments, the resulting amplitude of the pulses of composite sync signal 112 is made sufficiently large, in fact larger than the NTSC standard sync, so



that sync separator comparator reference voltage can be set to produce reliable switching at a level within the margin between the maximum black extension level 212 or 213 and the extended sync tip levels 284 of composite luma signal 112, as is indicated in
5 Figures 11a and 11b.

Figure 8d shows a circuit implementation of the embodiment shown in block form in Figure 8a. Gain controlled amplifier 114 comprises transistors 220 and 222 operating as a feedback voltage follower with gain greater than unity. The closed
10 loop gain (A) of amplifier 114 is determined by the feedback ratio set by resistors 223, 224 and 225 and is mathematically expressed as:

$$A=1 + R223/(R224 + R225)$$

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The pulses of the output signal of auxiliary sync separator 113 effectively act to short resistor 225 thereby increasing the gain of amplifier 114. Comparator configured transistors 229 and 230, along with an emitter resistor 231 and a
20 bias network comprising resistors 232 and 233, form negative peak limiter 118.

A circuit implementation of the embodiment shown in block diagram form in Figure 8b is shown in Figure 8e. As is shown in Figure 8e, composite luma signal 104 is applied in
25 parallel fashion to auxiliary sync separator 113 and to a non-linear processing circuit 110, which in the implementation shown in Figure 8e comprises the CX20125 IC. A capacitor 142 serves as a DC blocking and a clamping storage element for an input clamp within IC 110. A resistor 147 and a capacitor 148 provide a time
30 constant for the "black-stretch" function of the CX20125 IC. A resistor 144 and a capacitor 145 comprise an averaging filter for the "auto-pedestal" function of the CX20125 IC. A resistor 143 provides current limiting for the "back-porch" clamp pulse input signal required by the CX20125 and a resistor 146 provides the
35 same function for the composite blanking pulse input.

Resistors 130, 131, 132 and 133 along with a transistor 160 form an amplifier of auxiliary sync separator 113. A resistor 134 and a capacitor 138 form a low-pass filter for



improving the noise immunity of auxiliary sync separator 113. Auxiliary sync separator 113 is of conventional design having a dual time constant for optimizing both horizontal and vertical sync separation. The horizontal time constant is determined by a
5 resistor 140 and a capacitor 139, and the vertical time constant is determined by a resistor 135 and resistor 140 in combination with a capacitor 136 and a diode 137. The base-emitter junction of transistor 141 acts as a comparator for separating the
10 composite sync pulses from composite luma signal 104. Composite sync signal 117 appears at the collector of transistor 141.

Summing amplifier 170 includes a transistor 154 configured as a common base stage. Base bias voltage is provided by a bias network comprising resistors 150 and 153 and a filter capacitor 152 coupled to the Vcc supply line. The emitter of
15 transistor 154 forms a virtual ground summing node for non-linear processed composite luma signal 105 produced by IC 110 and composite sync signal 117 produced by auxiliary sync separator 113. Signals 105 and 117 are converted to currents by resistors 149 and 155, respectively. The currents are summed in
20 the emitter of transistor 154. The output voltage of the common base amplifier is developed at the collector of transistor 154 across a load resistor 159 and is buffered by emitter follower configured transistor 156. Output composite luminance signal 112 with corrected sync pulses appears at the emitter of transistor
25 156 across a load resistor 157.

The function of peak limiter 118 mentioned with regard to Figure 8b is accomplished by setting the bias of the base of transistor 154 so that transistor 154 is cutoff at a desired level of the sync pulses 117. The base bias is determined by resistors
30 150 and 153. The gain of amplifier 170 is set to ensure that cutoff is reached in response to sync pulse 117. The gain is set by resistors 155 and 159.

Figure 8f shows a circuit implementation of the embodiment shown in block form in Figure 8c. Switch 171
35 includes a series-shunt switch comprising transistors 236 and 240 and resistor 237, and an emitter follower amplifier comprising a transistor 238 and a resistor 239. The switch is coupled between the output of non-linear processing circuit 110 and output 112 of



the sync correction circuit. The switch is controlled by composite sync signal 117 produced by auxiliary sync separator 113.

Composite sync signal 117 is coupled to an amplifier including a transistor 226 and a load resistor 241 through a network

5 including resistors 227 and 228. Transistor 226 inverts composite sync signal 117. The inverted signal is coupled to the base of transistor 240 through a network including a resistor 234 and a diode 235. Reference voltage 172 is applied to the emitter of transistor 236. Between sync pulses, composite sync signal 117

10 produced auxiliary sync separator 113 has a voltage level near supply voltage V_{CC} . As a result, transistor 240 is non-conductive and transistor 236 is conductive, causing the image portions of

non-linearly processed luma signal 105 to be coupled to output 112. When negative-going pulses are present at output 117 of

15 auxiliary sync separator 113, transistor 240 conducts causing transistor 236 to be reverse biased because its base voltage is higher than reference voltage 172 coupled to its emitter through conductive transistor 240. Thus, composite luma signal 112 is

20 made equal to voltage 172 minus the base-emitter potential of transistor 238 during the pulse intervals of composite sync signal 117.

The present invention has been described in terms of a non-linear picture enhancement circuit, such as the Sony CX20125 IC, which provides both "black-stretch" non-linear

25 processing and "auto-pedestal" non-linear processing functions.

However, it will be appreciated by those skilled in the art, that the invention is useful even when only one of these non-linear

processing functions or when another non-linear processing function which affect sync pulses is used. In addition, while the

30 present invention has been described in terms of a composite luminance signal including a sync component, it is applicable to

any other composite video signal including a sync component, such as a composite video signal including a chrominance

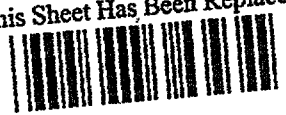
component. These and other modifications are intended to be

35 included within the scope of the invention defined by the following claims.

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CLAIMS:

1. In a television system, apparatus comprising:
means (90) for providing an input composite video
5 signal including an image component and a synchronization pulse
component;
means (110) for non-linearly processing said
composite video signal (104) including both of said image and
synchronization pulse components to produce a non-linearly
10 processed composite video signal (105) including a non-linearly
processed image component and a non-linearly processed
synchronization pulse component; said non-linearly processed
synchronization component being subject to distortion due to the
non-linear processing; characterized by
15 means (113) for separating said synchronization pulse
component of said input composite video signal before it is
processed by said non-linear processing means to produce an
undistorted synchronization pulse signal; and
means (111) responsive to both said non-linearly
20 processed composite video signal, including said non-linearly
processed synchronization component, and said undistorted
synchronization pulse signal for producing a further composite
video signal including a non-linearly processed image component
and an undistorted synchronization pulse component.
25
2. The apparatus recited in Claim 1, further
characterized by:
means (200) for further processing said further
composite video signal, including means for separating said non-
30 linearly processed image component and said undistorted
synchronization component of said further composite signal.
3. The apparatus recited in Claim 2, characterized in
that:
35 said further processing means (200) comprises an
integrated circuit having an input terminal (112) for receiving
said further composite video signal and which is coupled to the



inputs of a video signal processing section (81) and a synchronization pulse separator (100).

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4. The apparatus (111) recited in Claim 1,
5 characterized in that:

said means for producing said further composite video signal includes means for combining said non-linearly processed composite video signal and said undistorted synchronization signal to produce an output signal.

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5. The apparatus recited in Claim 4, characterized in that:

said means (114) for producing said further composite video signal includes means (118) for limiting the peak amplitude
15 of the output signal to produce said further composite video signal.

6. The apparatus (111) recited in Claim 1, characterized in that:

20 said means for producing said further composite video signal includes means (114) for amplifying pulses of said non-linearly processed synchronization pulse component of said non-linearly processed composite video signal to produce an output signal (112).

25

7. The apparatus recited in Claim 6, characterized in that:

said means (111) for producing said further composite video signal includes means (118) for limiting the peak amplitude
30 of the output signal to produce said further composite video signal.

8. The apparatus recited in Claim 1, characterized in that: ✓

35 said means (111) for producing said further composite video signal includes means (113) for replacing pulses of said non-linearly processed synchronization pulse component of said non-linearly processed composite video signal.

