

Description

This invention relates to an electrical circuit breaker, and in particular to an operating mechanism for such a circuit breaker, and generally to molded case circuit breakers with a trip-free linkage system.

Circuit breakers and, more particularly molded case circuit breakers, are old and well known in the prior art. Examples of such devices are disclosed in the specification of United States Patents Nos. 2,186,251; 2,492,009; 3,239,638; 3,525,959; 3,590,325; 3,614,685; 3,775,713; 3,783,423; 3,805,199; 3,815,059; 3,863,042; 3,959,695; 4,077,025; 4,166,205; 4,258,403; and 4,295,025. Such molded case circuit breakers have been provided with movable contact arrangements and operating mechanisms designed to provide protection for an electrical circuit or system against electrical faults, specifically, electrical overload conditions, low-level short circuit or fault current conditions, and in some cases, high level short circuit or fault current conditions. Prior art devices have utilized an operating mechanism having a trip mechanism for controlling the movement of an over-center toggle mechanism to separate a pair of electrical contacts upon an overload condition or upon a short circuit or fault current conditions. At least some prior art devices use contacts that "blow open", i.e., separate prior to the sequencing of the operating mechanism through a trip operation, to rapidly interrupts the flow of high level short circuit or fault current.

While many prior art devices have provided adequate protection against fault conditions in electrical circuits, a need exists for dimensionally small molded case circuit breakers capable of fast, effective and reliable operation. Many operating mechanisms used to control the mechanical operation of such circuit breakers require relatively large amounts of operating space. A need exists for an operating mechanism for molded case circuit breakers that utilizes a relatively small amount of space yet provides fast, effective and reliable operations for protecting an electrical circuit against overload or fault current conditions.

GB-A-1 523 407 discloses an electric circuit breaker comprising an over-center toggle mechanism having two pivotally connected toggle links and a toggle spring together with a releasable cradle. During a trip operation, when the cradle is released and initiates collapse of said toggle links one of said toggle links engages a curved abutment member disposed adjacent thereto so as to cause said toggle link to tilt around said abutment member, so as to collapse said toggle linkage and to lift the contact arm into its open position.

It is an object of the invention to provide a

molded case circuit breaker which, while designed dimensionally small and compact capable of providing faster contact separation during a trip operation.

The invention accordingly resides in an electrical circuit breaker as characterized in claim 1.

Advantageously, the present invention relates to a molded case circuit breaker having an operating mechanism that occupies a small amount of space while providing fast, effective and reliable operation in protecting an electrical circuit or system from electrical overload and fault current conditions. The operating mechanism includes trip-free, over-center toggle mechanism to achieve the opening and closing of a pair of electrical contacts in response to overload and short circuit or fault current conditions. The over-center toggle mechanism includes a pair of stationary links having a recess formed in a lower portion thereof for receiving a rotatable cradle support pin and having an elongated surface formed at the lower portion thereof.

The over-center toggle mechanism includes a pair of upper toggle links and a pair of lower toggle links interconnected by a toggle spring pin. The over-center toggle mechanism further includes a pivotable, one-piece, rigid cradle having a first aperture formed therethrough for receiving the rotatable cradle support pin and a second aperture formed therethrough at a location spaced by a predetermined distance from the first aperture for receiving an upper toggle link follower pin. The upper toggle links include a recess for receipt in and retention by a pair of spaced apart journals formed along the length of the upper toggle link follower pin such that rotational movement of the cradle effects a corresponding movement of the upper toggle links. The lower toggle links are secured to a movable electrical contact by a toggle contact pin. Each of the upper toggle links includes a first or initial pivot point for engaging the elongated, lower surface of one of the stationary links. Each of the stationary links includes a second pivot point for engaging an upper surface of one of the upper toggle links.

The stationary, upper and lower, links enable a trip operation of the operating mechanism when a manually engageable operating handle is physically restricted in its ON or CLOSED position. The upper toggle links move about their first pivot points during an initial trip movement of the over-center toggle mechanism to effect a rapid separation of the electrical contacts during a trip operation of the circuit breaker. Subsequently, the pivoting of the upper toggle links is transferred from the first pivot points to the second pivot points to rapidly accelerate the movement of the movable electrical contacts in the circuit breaker, thereby rapidly length-

ening any electrical arc between the electrical contacts to increase the arc voltage and rapidly extinguish any electrical arcs.

The invention will now be described, by way of example, with reference to the following description illustrated in the accompanying drawing wherein:

Fig. 1 is a top plan view of a molded case circuit breaker;

Fig. 2 is a side elevational view of the device of Fig. 1, portions being deleted to show interior details;

Fig. 3 is an enlarged, fragmentary, cross sectional view of the device of Fig. 1 taken along line 3-3 of Fig. 1;

Fig. 4 is an enlarged, perspective view of a pair of electrically insulating barrier indicator cards of the device of Fig. 1;

Fig. 5 is an enlarged, cross sectional view of the device of Fig. 1 taken along the line 5-5 of Fig. 1, depicting the device in its CLOSED and BLOWN-OPEN positions;

Fig. 6 is an enlarged, fragmentary, cross sectional view of the device of Fig. 1 taken along line 6-6 of Fig. 5;

Fig. 7 is an enlarged fragmentary, cross sectional view of the device of Fig. 1 taken along line 7-7 of Fig. 5;

Fig. 8 is an enlarged, fragmentary, cross sectional view of the device of Fig. 1 taken along line 8-8 of Fig. 5;

Fig. 9 is an enlarged, fragmentary, cross sectional view of the cross-bar assembly of the device of Fig. 1 taken along line 9-9 of Fig. 8;

Fig. 10 is an enlarged fragmentary, cross sectional view of the cross-bar assembly of the device of Fig. 1 taken along line 10-10 of Fig. 8;

Fig. 11 is an enlarged, fragmentary, cross sectional view of the cross-bar and upper contact assembly of the device of Fig. 1 taken along the line 11-11 of Fig. 5;

Fig. 12 is an enlarged, fragmentary, cross sectional view of the cross-bar and upper contact assembly of the device of Fig. 1 taken along the line 12-12 of Fig. 11;

Figs. 12A and 12B are enlarged, fragmentary, cross sectional views of a portion of the upper contact assembly of the device of Fig. 1, depicting sequential positions of the upper contact assembly during a BLOWN-OPEN operation;

Fig. 13 is an enlarged, exploded, perspective view of portions of the operating mechanism of the device of Fig. 1;

Fig. 14 is an enlarged, fragmentary, cross sectional view of the center pole or phase of the device of Fig. 1, depicting the device in its OPEN position;

Fig. 15 is an enlarged, fragmentary, cross sectional view of the center pole or phase of the

device of Fig. 1, depicting the device in its TRIPPED position;

Figs. 16 and 17 are enlarged, fragmentary, cross sectional views of the device of Fig. 1 depicting sequential positions of the operating mechanism of the device of Fig. 1 during a trip occurrence;

Fig. 18 is a force diagram illustrating the amount of handle force required to reset the device of Fig. 1 as a function of handle travel;

Figs. 19, 20 and 21 are each enlarged, fragmentary, cross sectional views, similar to the view of Fig. 12, depicting alternative embodiments of the cross-bar and upper contact assembly for the device of Fig. 1;

Fig. 22 is an enlarged, fragmentary, cross sectional view of the assembly of Fig. 21 taken along line 22-22 of Fig. 21;

Fig. 23 is an enlarged, fragmentary, cross sectional view of an alternative embodiment of a lower contact for the device of Fig. 1; and

Fig. 24 is an enlarged, fragmentary, cross sectional view of the lower contact of Fig. 23 taken along line 24-24 of Fig. 23.

Figs. 1-17 illustrate molded case circuit breaker 30 depicted and described herein as a three phase or three pole circuit breaker, the principles of the present invention are equally applicable to single phase or other polyphase circuit breakers.

The circuit breaker 30 includes a molded, electrically insulating, top cover 32 mechanically secured to a molded, electrically insulating, bottom cover or base 34 by a plurality of fasteners 36. A plurality of first electrical terminals or line terminals 38A, 38B and 38C are provided, one for each pole or phase, as are a plurality of second electrical terminals or load terminals 40A, 40B and 40C. These terminals are used to serially electrically connect the circuit breaker 30 into a three phase electrical circuit for protecting a three phase electrical system.

The circuit breaker 30 further includes an electrically insulating, rigid, manually engageable handle 42 extending through an opening 44 in the top cover 32 for setting the circuit breaker 30 to its CLOSED position (Fig. 5) or to its OPEN position (Fig. 14). The circuit breaker 30 also may assume a BLOWN-OPEN position (Fig. 5, dotted line position) or a TRIPPED position (Fig. 15). Subsequently moving to its TRIPPED position, the circuit breaker 30 may be reset for further protective operation by moving the handle 42 from its TRIPPED position (Fig. 15) to and past its OPEN position (Fig. 14). The handle 42 may then be left in its OPEN position (Fig. 14) or moved to its CLOSED position (Fig. 5), in which case the circuit breaker 30 is ready for further protective operation. The movement of the handle 42 may be achieved either

manually or automatically by a mechanical actuator. A position indicator 46 provides an externally visually discernible indication of the condition or position of the circuit breaker 30. The position indicator 46 is disposed about the handle 42 and covers the bottom of the opening 44 to function as a mechanical and electrical barrier between the interior and exterior of the circuit breaker 30.

As its major internal components (Fig. 5), the circuit breaker 30 includes a lower electrical contact assembly 50, a pair of upper electrical contact members 52, an electrical arc chute 54, a slot motor 56, and an operating mechanism 58. The arc chute 54 and the slot motor 56 are conventional, per se, and thus are not discussed in detail hereinafter. Briefly, the arc chute 54 is used to divide a single electrical arc formed between separating electrical contacts 72 and 238 upon a fault condition into a series of smaller electrical arcs, increasing the total arc voltage and resulting in extinguishing of the electrical arc. The slot motor 56, consisting either of a series of U-shaped steel laminations encased in electrical insulation or of a U-shaped, electrically insulated, solid steel bar, is disposed about the contact arms 66 and 240 to concentrate the magnetic field generated upon a high level short circuit or fault current condition, thereby greatly increasing the magnetic repulsion forces between the separating electrical contact arms 66 and 240 to rapidly accelerate the separation of the electrical contacts 72 and 238. The rapid separation of the electrical contacts 72 and 238 results in a relatively high arc resistance to limit the magnitude of the fault current. Reference may be had to the specification of United States Patent No. 3,815,059 for a more detailed description of the arc chute 54 and the slot motor 56.

The lower electrical contact assembly 50 (Figs. 14 and 15) includes a lower, formed, stationary member 62 secured to the base 34 by a fastener 64, a lower movable contact arm 66, a limit or stop pin 68 fixedly secured to and movable with the movable contact arm 66, a lower contact biasing means or compression spring 70, a contact 72 for physically and electrically contacting the upper electrical contacts 238 and an electrically insulating strip 74 to reduce the possibility of arcing between the upper electrical contact members 52 and portions of the lower electrical contact assembly 50. The line terminal 38B extending exteriorly of the base 34 comprises an integral end portion of the member 62 (Fig. 2). The base 34 includes an upwardly protuberant portion 34A having an upper, inclined surface 34B that serves as a lower limit or stop for the moving contact arm 66 during rapid separation of the upper contact members 52 from the lower contact assembly 50. The lower, formed stationary member 62 includes a lower portion 62A

that engages the base 34. An aperture 62B is formed through the lower portion 62A for receiving the upwardly extending base portion 34A and for seating the compression spring 70. The lower portion 62A may also include a threaded aperture 62C formed therethrough for receiving the fastener 64 to secure the stationary member 62 and thus the lower electrical contact assembly 50 to the base 34. The stationary member 62 includes an upstanding, contacting portion 62D that may be integrally formed with or fixedly secured to the lower portion 62A. The stop pin 68 (FIG. 5) is provided for limiting the upward movement of the movable contact arm 66 upon physical engagement with the upstanding contacting portion 62D.

The contact arm 66 is fixedly secured to a rotatable pin 78 for rotation therewith on the upstanding contacting portion 62D about the longitudinal axis of the rotatable pin 78. Effective conductive contact and current transfer is achieved between the lower formed stationary member 62 and the lower movable contact arm 66 through the rotatable pin 78. The lower movable contact arm 66 includes an elongated rigid lever arm 66A extending between the rotatable pin 78 and the contact 72 and a downwardly protuberant portion or spring locator 66B for receipt within the upper end of the compression spring 70 for maintaining effective physical interconnection between the lower movable arm 66 and the compression spring 70. Finally, the lower movable contact arm 66 includes an integrally formed, flat surface 66C formed at its lower end for physically engaging the stop 34B to limit the downward movement of the lower movable contact arm 66 and the contact 72 fixedly secured thereto.

Each upper electrical contact member 52 has a current contact 238 for physically and electrically contacting the contact 72 of the lower electrical contact assembly 50 disposed at the end of an upper movable elongated contact arm 240. It is the passage of high level short circuit or fault current through the generally parallel contact arms 66 and 240 that causes very high magnetic repulsion forces between the contact arms 66 and 240, effecting the extremely rapid separation of the contacts 72 and 238. The electrically insulating strip 74 is used to electrically insulate the upper contact arms 240 from the lower contact arm 66.

The lower electrical contact assembly 50 utilizes the high magnetic repulsion forces generated by high level short circuit or fault current flowing through the elongated parallel portions of the electrical contact arms 66 and 240 to cause the rapid downward movement of the contact arm 66 against the bias of the compression spring 70 (Fig. 5). An extremely rapid separation of the electrical contacts 72 and 238 and a resultant rapid increase in the

resistance across the electrical arc formed between the electrical contacts 72 and 238 is thereby achieved, providing effective fault current limitation within the confines of relatively small physical dimensions. The lower electrical contact assembly 50 further eliminates the necessity for utilizing flexible copper shunts used in many prior art molded case circuit breakers for providing a current carrying conductive path between a terminal of the circuit breaker and a lower movable contact arm of a lower electrical contact.

The operating mechanism 58 (Figs. 5, 13 and 16) includes an over-center toggle mechanism 80; an electronic or thermal-magnetic trip mechanism 82 (not shown in detail); an integral or one-piece molded cross-bar 84 (Fig. 13); a pair of rigid, opposed or spaced apart, metal side plates 86; a rigid, pivotable, metal handle yoke 88; a rigid stop pin 90; and a pair of operating tension springs 92.

The over-center toggle mechanism 80 includes a rigid, one-piece metal cradle 96 that is rotatable about the longitudinal axis of a cradle support pin 98. The opposite longitudinal ends of the cradle support pin 98 in an assembled condition are retained in a pair of apertures 100 formed through the side plates 86.

The toggle mechanism 80 further includes a pair of upper toggle or kicker links 102, a pair of lower toggle links 104, a toggle spring pin 106 and an upper toggle link follower pin 108. The lower toggle links 104 are secured to the upper electrical contact members 52 by a toggle contact pin 110. Each of the lower toggle links 104 includes a lower aperture 112 for receipt therethrough of the toggle contact pin 110. The toggle contact pin 110 also passes through an aperture 114 formed through each of the upper electrical contact members 52 enabling the upper electrical contact members 52 to freely rotate about the central longitudinal axis of the pin 110. The opposite longitudinal ends of the pin 110 are received and retained in the cross-bar 84 (Fig. 6). The movement of the lower toggle links 104 causes the movement of the cross-bar 84 and the corresponding movement of the upper electrical contact members 52 under other than high level short circuit or fault current conditions. In this manner, movement of the upper electrical contact members 52 in the center pole or phase of the circuit breaker 30 by the operating mechanism 58, simultaneously, through the rigid cross-bar 84, causes the same movement in the upper electrical contact members 52 associated with the other poles or phases of the circuit breaker 30.

Each of the lower toggle links 104 also includes an upper aperture 116; and each of the upper toggle links 102 includes an aperture 118. The toggle spring pin 106 is received through the apertures 116 and 118, thereby interconnecting the

upper and lower toggle links 102 and 104 and allowing rotational movement therebetween. The opposite longitudinal ends of the pin 106 include journals 120 for the receipt and retention of the lower, hooked or curved ends 122 of the springs 92. The upper, hooked or curved ends 124 of the springs 92 are received through and positioned in slots 126 formed through an upper, planar or flat surface 128 of the handle yoke 88. A locating pin 130 is transversely disposed across the slots 126 for retaining the curved ends 124 of the springs 92 in engagement with the handle yoke 88 (Fig. 7).

In an assembled condition, the disposition of the curved ends 124 within the slots 126 and the disposition of the curved ends 122 in the journals 120 retain the links 102 and 104 in engagement with the pin 106 and also maintain the springs 92 under tension, enabling the operation of the over-center toggle mechanism 80 to be controlled by and responsive to external movements of the handle 42.

The upper links 102 (Fig. 13) also include a recess or groove 132 which mates with a pair of spaced apart journals 134 formed along the length of the pin 108. The center portion of the pin 108 is configured to be fixedly received in an aperture 136 formed through the cradle 96 at a location spaced by a predetermined distance from the axis of rotation of the cradle 96 coincident with the longitudinal axis of the pin 98. The spring tension from the springs 92 retains the upper toggle links 102 in engagement with the pin 108. The rotational movement of the cradle 96 effects a corresponding movement or displacement of the upper portions of the links 102 as is described hereinafter.

The cradle 96 includes an elongated surface 140 having a generally flat latch surface 142 formed therein. The surface 142 is configured to engage a pivotable lever or trip arm 144 (Figs. 5, 16 and 17) of the trip mechanism 82. The trip arm 144 pivots about a stationary pin 145 of the trip mechanism 82 upon a trip operation initiated by the trip mechanism 82. The trip mechanism 82 is an electronic or thermal-magnetic trip mechanism that is capable of detecting both low level short circuit or overload current conditions and high level short circuit or fault current conditions. Upon the detection of any such condition the trip mechanism 82 rotates the trip arm 144 about the pivot pin 145 to initiate a trip operation of the operating mechanism 58 (Figs. 16 and 17).

The cradle 96 also includes a curved, elongated cam surface 148 for contacting a cradle cam or limit pin 150. The opposite longitudinal ends of the cam pin 150 are received and retained in a pair of grooves 152 formed in the handle yoke 88, to enable, in the preferred embodiment, the rotation of the pin 150 within the handle yoke 88. The cradle

96 further includes a generally flat stop surface 154 for contacting a central portion of rigid stop 156 of the stop pin 90. The engagement of the surface 154 with the rigid stop 156 limits the movement of the cradle 96 in a counterclockwise direction subsequent to a trip operation (Figs. 15 and 17).

During a trip operation, the lines of action of the operating springs 92 are changed, resulting in the movement of the handle 42 to a TRIPPED position (Fig. 15), intermediate the CLOSED position (Fig. 5) and the OPEN position (Fig. 14) of the handle 42, to indicate that the circuit breaker 30 has tripped. The engagement of the stop surface 154 and rigid stop 156 limits the movement of the cradle 96 and thereby locates the handle 42 in the TRIPPED position (Fig. 15) through the engagement of the pin 150 with the cam surface 148 of the cradle 96. In addition, the camming engagement of the cam surface 148 and rotatable pin 150 resets the operating mechanism 58 subsequent to a trip operation as the cradle 96 moves in a clockwise direction against the bias of the operating springs 92 from its TRIPPED position (Fig. 15) to and past its OPEN position (Fig. 14), thereby relatching the latch surface 142 and the trip arm 144. The cam surface 148 is configured to increase the mechanical advantage of the handle 42 in a predetermined manner in accordance with the specific design or contour of the cam surface 148 as the springs 92 are extended during a reset operation. In this manner only a comparatively low and substantially constant reset force applied to the handle 42 is required to achieve the resetting of the operating mechanism 58 after a trip operation and to move the handle 42 between its TRIPPED and OPEN positions.

The force diagram of FIG. 18 illustrates handle travel during a reset operation from a TRIPPED (0) position to a RESET (1) position relative to the reset force required to move the handle 42. The NORMAL RESET line illustrates the force required in conventional or prior art circuit breakers having cradles without the contoured cam surface 148 in the cradle 96 to overcome the increasing bias of one or more operating springs as a handle is moved during a reset operation. The CONSTANT FORCE RESET line illustrates the substantially constant reset force required to be applied through the handle 42 to the pin 150 and the cam surface 148 of the cradle 96 to achieve a reset operation. As is apparent, the peak force required during such a reset operation of the operating mechanism 58 having the cradle 96 with the contoured cam surface 148 is substantially reduced from the peak force required in circuit breakers having conventional cradles. The work done during such reset operations corresponds to the areas under the NORMAL RESET line and the CONSTANT FORCE

RESET line. The total work done during the reset operation is the same for both the NORMAL RESET line and the CONSTANT FORCE RESET line. However, the reduction in the peak force required for a reset operation by the use of a cradle 96 having a cam surface 148 contoured in a predetermined manner as described hereinabove and as depicted in the drawing enables the use of a motor operator or actuator with a peak power rating corresponding to the comparatively low constant force depicted in Fig. 18 required to move the handle 42.

The engagement of the cam surface 148 of cradle 96 and pin 150 during a reset operation occurs as follows. During a reset operation subsequent to a trip operation, as the handle 42 is moved clockwise from the TRIPPED position (Fig. 15) to and past the OPEN position (Fig. 14), a moment about the longitudinal axis of the cradle support pin 98 occurs due to the application of handle force through the cam pin 150 to the cam surface 148 that substantially counteracts the bias of the operating springs 92. The moment about the longitudinal axis of the pin 98 increases as the pin 150 moves along the surface 148 proportionally to the increase in the distance between the longitudinal axis of the pin 98 and the location of engagement of the pin 150 on the surface 148 that is, the moment arm. Additionally, cam surface 148 is contoured in a predetermined manner to further increase the mechanical advantage of the handle 42 as the handle 42 is moved during the reset operation. During the initial movement of the handle 42, the surface 148 is contoured at a relatively steep angle with respect to the distance between the cam pin 150 and the rotatable cradle support pin 98 since a relatively small force is required to overcome the bias of the springs 92. As the handle 42 is moved further during the reset operation the cam surface 148 is comparatively less steeply contoured providing increased mechanical advantage to the handle 42 to overcome the increased bias of the extended springs 92. This increased mechanical advantage enables a substantially constant reset force to be applied through the handle 42 throughout the reset operation (Fig. 18).

The toggle mechanism 80 includes a pair of rigid, spaced-apart, stationary, pivot-transfer links 158 (Figs. 5, 13, 16 and 17) that are fixedly secured to the stop pin 90. The stationary links 158 include an elongated, lower surface 160 spaced from an elongated surface 162 formed on the upper toggle links 102. Each stationary link 158 further includes a recess or groove 164 configured for receiving the rotatable cradle support pin 98. The metal side plates 86 include apertures 166 for receiving and retaining the opposite longitudinal ends of the stop pin 90.

The stationary links 158 and the links 102 and

104 enable the "trip-free" operation of the operating mechanism 58 even with the handle 42 physically restricted or obstructed in the CLOSED position, ensuring that the upper electrical contacts 238 are moved out of engagement with the lower electrical contacts 72 upon the initiation of a trip operation by the trip mechanism 82. When the handle 42 is in a CLOSED position (Fig. 16), a pair of first or initial pivot points 163 at the ends of the surfaces 162 of the upper links 102 engage the surfaces 160 of the links 158 near the grooves 164 of the links 158. During a trip operation, the cradle 96 is unlatched by the clockwise rotational movement of the trip arm 144, resulting in the counterclockwise rotation of the cradle 96. The upper links 102 are rotated counterclockwise by the springs 92 about the first pivot point 163. The springs 92 also move the toggle spring pin 106 in a clockwise direction about the pin 110, resulting in corresponding movements of the links 104, the upper contact members 52 and the cross-bar 84. Subsequently, the surfaces 162 of the links 102 physically engage the surfaces 160 of the links 158 and, thereafter, the pivot points are transferred from the initial pivot points 163 to a pair of second pivot points 168, resulting in the increased rotational velocity of the upper contact members 52.

The pivot-transfer system as disclosed herein exhibits a significant mechanical advantage to move the upper links 102 about the first or initial pivot points 163 during the initial counterclockwise rotation of the upper links 102 upon the occurrence of a trip condition and thereby to overcome inertia and to cause the rapid separation of the upper and lower contacts 238 and 72. The pivot transfer from the pivot points 163 to the pivot points 168 accelerates the movements of the upper electrical contact members 52 to rapidly lengthen the electrical arc between contacts 72 and 238 and thus to increase the arc voltage to rapidly extinguish the electrical arc.

The handle yoke 88 includes a pair of downwardly depending support arms 176 (FIG. 13). A pair of bearing surfaces or rounded tabs 178 are formed at the lowermost extremities of the downwardly depending support arms 176 of the handle yoke 88 for engagement with bearing or pivot surfaces 180 formed in the side plates 86. The handle yoke 88 is thus controllably pivotable about the bearing surfaces 178 and 180. The side plates 86 also include bearing surfaces 182 for contacting round bearing surfaces 186 of the cross-bar 84 and for retaining the cross-bar 84 securely in position within the base 34. Each of the side plates 86 includes a pair of downwardly depending support arms 188 that terminate in elongate, downwardly projecting stakes or tabs 190 for securely retaining the side plates 86 in the circuit breaker 30. In

assembling the support plate 86 in the circuit breaker 30, the tabs 190 are passed through apertures 191 formed through the base 34 (Fig. 6). The tabs 190 may then be mechanically deformed, for example, by peening, to lock the tabs 190 in engagement with the base 34. A pair of formed electrically insulating barriers 192 (FIG. 7) is used to electrically insulate conductive components and surfaces in one pole or phase of the circuit breaker 30 from conductive components or surfaces in adjacent poles or phases of the circuit breaker 30.

The integral or one-piece molded cross-bar 84 includes three enlarged sections 194 separated by the round bearing surfaces 186. A pair of peripherally disposed, outwardly projecting locators 196 are provided to retain the cross-bar 84 properly located within the base 34. The base 34 includes a plurality of bearing surfaces 198 (FIG. 7) complementarily shaped to the bearing surfaces 186 for seating the cross-bar 84 for rotational movement in the base 34. The locators 196 are received within arcuate recesses or grooves 200 formed along the surfaces 198. Each enlarged section 194 further includes a pair of spaced-apart apertures 202 (FIG. 13) for receiving the toggle contact pin 110. The pin 110 may be retained within the apertures 202 by any suitable means, for example, by an interference fit therebetween. Each enlarged section 194 also includes an opening 204 formed therein for receipt of one longitudinal end or base portion 206 of each of the upper electrical contact members 52.

The opening 204 also permits the receipt and retention of a pair of contact arm compression springs 208 (FIGS. 11 and 13) and an associated, formed, spring clip 210. The compression springs 208 are retained in position by being disposed within a pair of spaced-apart recesses 212 formed therein. The spring clip 210 is configured to be disposed between the compression springs 208 and the base portions 206 of the upper electrical contact members 52 to transfer the compressive force from the springs 208 to the base portions 206, thereby ensuring that the upper electrical contact members 52 and the cross-bar 84 move in unison in response to the operation of the operating mechanism 58 during a normal trip operation. However, upon the occurrence of a high level short circuit or fault current condition, the upper electrical contact members 52, responding to the repulsion forces generated between the parallel contact arms 66 and 240, can individually rotate about the pin 110, overcoming the bias forces of the spring 208 and the spring clip 210, thus enabling the electrical contacts 72 and 238 to rapidly separate and move to their BLOWN-OPEN positions (Figs. 5 and 12, as depicted in dotted lines) without waiting for the operating mechanism 58 to sequence. This independent movement of each of the upper electrical

contact members 52 under the above high fault condition is possible in any pole or phase of the circuit breaker 30.

The spring clip 210 (Fig. 12) includes a lower formed portion 214 having an upper tab portion 215 (Fig. 13) and an upstanding end portion 217 for engagement with a complementarily shaped portion 216 of the enlarged section 194 of the cross-bar 84 to properly locate and retain the spring clip 210 in engagement with the enlarged section 194. The spring clip 210 includes a pair of upwardly extending legs 218 for engagement with the compression springs 208. Each upwardly extending leg 218 includes an outwardly projecting surface 220. The terminal portion 206 of each upper contact arm 240 includes a generally C-shaped slot or detent 222 formed in an arcuately shaped surface 224 thereof. The detent 222 and the surface 220 are configured to provide a predetermined, variable amount of compressive force therebetween.

During normal operating conditions, the surfaces 220 of the spring clip 210 contact the surface 224 of the upper contact arms 240 at the detents or steep cam surfaces 222 thereof to retain the cross-bar 84 in engagement with the upper electrical contact members 52 (Figs. 5 and 12). Upon the occurrence of a high level short circuit or fault current condition, as each upper contact arm 240 rotates in a clockwise direction about the longitudinal axis of the pin 110, each surface 224 moves along the surface 220. The resultant line of force of the spring 208 through the engaging surfaces 220 and 224 passes substantially through the longitudinal axis of the pin 110 as the upper electrical contact members 52 rotate to their BLOWN-OPEN position (Figs. 5 and 12), thereby substantially decreasing the compression moment of the springs 208 about the longitudinal axis of the pin 110. Subsequently, when the circuit breaker 30 is reset to its CLOSED position, the arcuate cam surface 224 is moved against the surface 220 to the latch point at the detent 222. By changing the configuration of the detent 222 or the configuration of the cam surface 220 of the spring clip 210, the compression moment arm of springs 208 can be increased or decreased as desired.

Referring to Figs. 12A and 12B, the base portion 206 of the upper electrical contact members 52 is shown in its CLOSED position (Fig. 12A) and in a sequential position (Fig. 12B) during a BLOWN-OPEN operation. The compressive force of the spring 208 is illustrated in Figs. 12A and 12B by an arrow at the point of engagement of the surfaces 220 (Fig. 12) and 224 and is designated with a reference character F. In the CLOSED position, a component force F1 is directed along a line normal to the tangent of the surface 224 at the

point of engagement of the surfaces 220 and 224. The line of action of the force F1 is separated from the longitudinal axis of the pin 110 by a distance shown as L1. The compression moment of the component spring force F1 with the moment arm L1 is provided to ensure that the upper electrical contact members 52 and the cross-bar 84 move in unison in response to the operation of the operating mechanism 58 during a normal trip operation. During a BLOWN-OPEN operation as the upper electrical contact members 52 rotate about the longitudinal axis of the pin 110 (Fig. 12B), the surface 224 is configured to provide a component force F2 of the springs 208 that passes substantially through or close to the pivot of members 52 or the longitudinal axis of the pin 110 to reduce the moment arm to substantially zero. The compression moment of the spring 208 about the longitudinal axis of the pin 110 is substantially reduced thereby ensuring that the upper electrical contact members 52 move independently of the cross-bar 84 to rapidly separate the electrical contacts 72 and 238 during a BLOWN-OPEN operation. The component force F2 is essentially a friction force and the magnitude of force F2 is significantly less than the component force F1. In such manner, the compression springs 208 releasably bias the base portions 206 into driving engagement with the cross-bar 84 for enabling rotational movement of the upper contact members 52 in unison with the rotational movement of the cross bar 84 and for enabling rotational movement of the upper electrical contact member 52 substantially independently of the cross bar 84 upon the occurrence of a fault current condition during a BLOWN-OPEN operation.

Two pairs of flexible current shunts 234, as illustrated in Fig. 13, are used to provide a current carrying electrical path through the circuit breaker 30. Each pair of flexible shunts 234 is connected by any suitable means, for example, by brazing, to the opposite sides of the longitudinal end portion 206 of each upper electrical contact member 52 and to a lower conductive plate 236 in the trip mechanism 82. The flexible shunts 234 provide the current carrying electrical path between the upper electrical contact members 52 and the trip mechanism 82 and thereby through the circuit breaker 30 between the terminals 38B and 40B via the lower electrical contact assembly 50, the upper electrical contact members 52, the flexible shunts 234 and the trip mechanism 82.

In operation, the circuit breaker 30 may be interconnected in a three phase electrical circuit via line and load connections to the terminals 38A, B and C and 40A, B and C. The operating mechanism 58 may be set by moving the handle 42 from its TRIPPED position (Fig. 15) as far as possible

past its OPEN position (Fig. 14) to ensure the resetting of the latch surface 142 of the cradle 96 and the pivotable trip arm 144.

Subsequent to a trip operation, a force is applied to the handle 42 to move the handle 42 clockwise from its TRIPPED position (Fig. 15) to and past its OPEN position (Fig. 14) to enable relatching of the latch surface 142 of the cradle 96 with the trip arm 144. During such movement of the handle 42, the cam pin 150 engages the cam surface 148 of the cradle 96 and moves the cradle 96 clockwise about the rotatable cradle support pin 98. The clockwise rotation of the cradle 96 results in a corresponding movement of the toggle link follower pin 108 that is fixedly retained within the cradle 96. During such movement, the operating springs 92 rotate clockwise about the toggle spring pin 106 and exert an upward force on the toggle spring pin 106; the kicker links 102 rotate counterclockwise about the upper toggle link follower pin 108 and the lower toggle links 104 are rotated clockwise about the pin 110 that is held in a stationary position within the cross-bar 84. The upward spring force exerted on the toggle spring pin 106 is also applied through the kicker links 102 to the pin 108, thereby providing a counterclockwise biasing force to the cradle 96 about the longitudinal axis of the cradle support pin 98. The handle 42 is moved clockwise past the OPEN position shown in Fig. 14 until the latch surface 142 relatches with the trip arm 144. The handle 42 may then be moved from its OPEN position (Fig. 14) to its CLOSED position (Fig. 5) causing the operating mechanism 58 to close the contacts 72 and 238; and the circuit breaker 30 is then ready for operation in protecting a three phase electrical circuit.

The handle 42 is moved from its OPEN position to its CLOSED position by applying a force to the handle 42 to cause the counterclockwise movement thereof. In the OPEN position, the cradle 96 is provided in its latched position with the latch surface 142 engaging the pivotal trip arm 144 and the grooves 132 of the upper toggle links 102 are retained in engagement with the upper toggle link follower pin 108 that is fixedly received within the cradle 96. During the initial counterclockwise movement of handle 42, the lines of action of the operating springs 92 are to the right to the upper toggle link follower pin 108; the kicker links 102, the lower toggle links 104 and the toggle spring pin 106 are then stationary. As the line of action of the operating springs 92 is moved past the upper toggle link follower pin 108, the kicker links 102 rotate clockwise until the pivot 163 engages the surface 160 of the stationary links 158. Additionally, as a result of the change in the line of action of the operating springs 92 moving past the pin 108, the toggle spring pin 106 rotates clockwise about the upper

toggle link follower pin 108 and moves to the left, resulting in the movement of the lower toggle link 104 which rotates counterclockwise about the toggle spring pin 106. Thereby, the cross-bar 84 is rotated counterclockwise and the corresponding movement of the electrical contact members 52 effects the closing of the contacts 72 and 238 with the operating mechanism 58 in the CLOSED position.

Upon the occurrence of a sustained overload condition, the pivotable trip arm 144 pivots about the stationary pin 145 to unlatch the latch surface 142 of the cradle 96. The cradle 96 is immediately accelerated by the operating springs 92 through the kicker links 102 for rotation in the counterclockwise direction resulting in the substantially instantaneous movement of the upper toggle links 102, the toggle spring pin 106 and the lower toggle links 104, as illustrated in dotted line in Fig. 16. The upward movement of the pin 106 results in a corresponding upward movement of the toggle contact pin 110 through the movement of the lower toggle links 104, and the immediate, upward movement of the rotatable cross-bar 84 effecting the upward movement of the upper electrical contact members 52 to their TRIPPED position (Fig. 15). Since the base portions 206 of the upper electrical contact members 52 are biased into engagement with the cross-bar 84 through the springs 208, the upper electrical contact members 52 move in unison with the cross-bar 84, resulting in the simultaneous or synchronous separation of all three of the pairs of upper electrical contacts 72 from the lower electrical contacts 238 in the circuit breaker 30. During this trip operation, any electrical arc that may have been present across the contacts 72 and 238 is lengthened, subdivided, and in the normal course of events, extinguished.

Upon the occurrence of a high level short circuit or fault current condition and as a result of the large magnetic repulsion forces generated by the flow of fault current through the generally parallel contact arms 66 and 240, the electrical contacts 72 and 238 rapidly separate and move to their BLOWN-OPEN positions (depicted in dotted line form in Fig. 5). Movement of the contact arm 66 of the lower electrical contact assembly 50 is limited by the stop surface 34B, and movement of each contact arm 240 of each upper electrical contact member 52 is limited by the engagement of a lower contacting surface 242 (Fig. 12) of the terminal portion 206 of the contact arm member 52 and a stop surface 244 formed in the base. Each contact arm 240 is held in its BLOWN-OPEN position by the engagement of the surfaces 220 and 224. The separation of the electrical contacts 72 and 238 may thus be achieved without the necessity of the operating mechanism 58 sequencing through a

trip operation.

The position indicator 46 (Figs. 1, 3-5 and 14-17) of the circuit breaker 30 provides an externally visually discernible indication of the condition or position of the operating mechanism 58 of the circuit breaker. The position indicator 46 includes a plurality of insulating cards, strips or barriers, for example, as specifically illustrated, a first or upper electrically insulating card, strip or barrier 246 and a second or lower electrically insulating card, strip or barrier 248 that cooperate to provide an external, clear indication of the position or condition of the operating mechanism 58. The barriers 246 and 248 are disposed about the handle 42 and cover the bottom of the opening 44 to function as a mechanical and electrical barrier between the interior and exterior of the circuit breaker 30. Preferably, the top cover 32 includes a pair of spaced apart, laterally aligned openings or viewing slots 250 formed therethrough to provide external visual access to either a pair of spaced apart, laterally aligned position indicia or red markings 252 (Fig. 4) fixedly secured to, or on, the barrier 246 or a pair of spaced apart, laterally aligned position indicia or white markings 254 fixedly secured to, or on, the barrier 246 or a pair of spaced apart, laterally aligned position indicia or green markings 256 fixedly secured to, or on, the upper surface of the barrier 248.

The barrier 246 has a relatively small slot 258 that fits securely about the handle 42. The barrier 248 has, comparatively, a much larger slot 260 that enables relative movement between the barriers 246 and 248 and also between the barrier 248 and the handle 42. The barrier 248 also is dimensionally longer along the longitudinal axis of the opening 44 than the barrier 246 in order to ensure that the green markings 256 may be externally visually discerned when aligned with the viewing slots 250 and to ensure that the opening 44 is covered in all positions of the handle 42.

When the handle 42 is moved in the opening 44 to its ON or CLOSED position, the red markings 252 are positioned in the viewing slots 250 to provide an externally visually discernible indication that the operating mechanism 58 of the circuit breaker 30 is in its CLOSED position (Fig. 5). Upon a trip operation of the circuit breaker 30, the handle 42 moves to the load side of the circuit breaker 30 (Fig. 15). The barrier 246, captured about the handle 42, moves with the handle 42 to position the white markings 254 in the viewing slots 250, providing an externally visible indication that the operating mechanism of the circuit breaker 30 is in its TRIPPED position (Fig. 15). During this movement of the handle 42 the lower barrier 248 is not moved as the handle 42 moves within the slot 260. When the handle 42 is moved to its OFF or OPEN

position in the opening 44, the barrier 246 is moved beyond the viewing slots 250 and the green markings 256 on the barrier 248 are positioned in the viewing slots 250 to provide an external visually discernible indication that the operating mechanism 58 is in its OPEN position.

A plurality of spaced apart insulating support members 262 (Figs. 3 and 5), preferably integrally formed portions of the top cover 32, is used to provide lateral support of the longitudinal end of the barrier 248 when the handle 42 is in its OPEN position in order to prevent substantial internal deflection of the barrier 248 upon the application of an external force. The use of the two barriers 246 and 248 with the colored markings 252, 254 and 256 disposed thereon is particularly advantageous in applications where maximum movement is required in a limited amount of space, since the lost motion connection between the handle 42 and the barrier 248 enables a shorter barrier 248 to be used than would be required in the absence of the lost motion connection.

In accordance with an alternative embodiment (Fig. 19) of the circuit breaker 30, identical reference characters as used hereinabove with respect to Figs. 1-17 are employed hereinafter to describe unchanged portions and common components of the circuit breaker 30, each of a pair of upper electrical contact members 264 includes a longitudinal end or base portion 266. The terminal portions 266 include a lower groove or detent 268 and an upper groove or detent 270 formed along an arcuate surface 272 thereof. A spring clip 274 is disposed between a pair of compression springs 276 and the base portions 266 of the upper electrical contact members 264 to transfer to transfer the compressive force from the springs 276 to the base portions 266, thereby ensuring that the upper electrical contact members 264 and the cross-bar 84 move in unison in response to movement of the handle 42 or the operation of the operating mechanism 58 during a normal trip operation. The spring clip 274 includes an outwardly projecting surface 278 formed in each of the upstanding legs 218 for engaging the arcuate surfaces 272 of the base portions 266 of the upper electrical contact members 264. As described hereinbefore with respect to Figs. 12A and 12B, the lower detents 268 and the surfaces 278 are configured to provide a compression moment of the component force F_1 about the longitudinal axis of the pin 110 proportional to the distance L_1 between the longitudinal axis of the pin 110 and the resultant line of force of the spring 212 through the engaging surfaces 278 and 272. That moment may be varied as desired by appropriately contouring the surface 272. The springs 212 releasably bias the base portions 242 of the upper contact members 264 into driving engage-

ment with the cross-bar 84 enabling rotational movement of members 264, in unison with the cross-bar 84 and enabling rotational movement of the members 264 substantially independently of the cross-bar 84 upon the occurrence of a fault current condition during a BLOWN-OPEN operation. The frictional force F_2 (Fig. 12B) passes substantially through the longitudinal axis of the pin 110 and is significantly less than F_1 (Fig. 12A), as is described hereinbefore.

During normal operating conditions, the surface 278 of the spring clip 274 contacts the lower detent 268 of the upper electrical contact members 264 to retain the cross-bar 84 in driving engagement with the upper electrical contact members 264. Upon the occurrence of a high level short circuit or fault current condition, as the upper electrical contact members 264 rotate in a clockwise direction about the longitudinal axis of pin 110, the arcuate surface 272 of the base portion 266 is moved against the surface 278. The resultant line of force of the spring 212 through the engaging cam surfaces 278 and 272 passes substantially through the longitudinal axis of the pin 110 as the upper electrical contacts 264 rotate to their BLOWN-OPEN position (Fig. 19, in dotted line), thereby substantially reducing the moment imparted by the springs 276 about the longitudinal axis of the pin 110. The upper detent 270 engages the outwardly projecting surface 278 of the spring clip 274 in the BLOWN-OPEN position to retain the upper electrical contact members 264 in their BLOWN-OPEN position, thereby eliminating or minimizing the possibility of contact restrike.

In accordance with a further alternative embodiment (Fig. 20) of the circuit breaker 30, each of a pair of upper electrical contact members 280 includes a longitudinal end or base portion 282. The portion 282 includes a lower groove or detent 284 and an upper groove or detent 286 formed along an arcuate surface 288 thereof.

A ball 290 is disposed between the arcuate surface 288 of each base portion 282 and one of a pair of compression springs 292 that are retained within a cross-bar 294. An adjusting screw or threaded plug 296 engages the compression spring 292 to provide a desired spring force on the ball 290. The balls 290 transfer the compressive force from the springs 292 to the base portions 282, thereby ensuring that the upper electrical contact members 280 and the cross-bar 294 move in unison in response to movement of the handle 42 or the operation of the operating mechanism 58 during a normal trip operation. During normal operating conditions, the ball 290 engages the lower detent 284 of the upper electrical contact members 280 and transfers the compressive spring force thereto.

Upon the occurrence of a high level short circuit or fault current condition, as the upper electrical contact members 280 rotate in a clockwise direction about the longitudinal axis of pin 110, the arcuate surfaces 288 of the base portions 282 are moved against the balls 290. As described hereinbefore with respect to Figs. 12A and 12B, the component force of the springs 292 is significantly reduced from F_1 with the moment arm L_1 in the CLOSED position to frictional force F_2 that passes substantially through the pivot of members 280 or the longitudinal axis of pin 110 in the subsequent position as the upper electrical contact members 280 rotate about the longitudinal axis of the pin 110 during a BLOWN-OPEN operation. The upper detents 286 engage the balls 290 in the BLOWN-OPEN position, holding the contact members 280 in their BLOWN-OPEN position, thereby eliminating or minimizing the possibility of contact restrike. Subsequently, when the circuit breaker 30 is reset to its CLOSED position, the arcuate surfaces 288 are moved against the balls 290 until the balls 290 are disposed in the lower detents 284.

In accordance with another alternative embodiment (Figs. 21 and 22) of the circuit breaker 30, each of a pair of upper electrical contact members 298 includes a longitudinal end or base portion 300 having a lower groove or detent 302 and an upper groove or detent 304 formed along an arcuate surface 306. A metal leaf spring 308 is secured to a molded cross-bar 310 by a fastener 312 and is disposed between the base portions 300 of the upper electrical contact members 298 and the cross-bar 310. The leaf spring 308 includes an upper, generally flat portion 314 that engages the cross-bar 310 and that has an aperture (not illustrated) formed therethrough for receiving the fastener 312 to secure the leaf spring 308 to the cross-bar 310. The leaf spring 308 further includes a pair of downwardly depending arms 316 with lower, integrally formed, laterally extending portions 318 thereof. Each lower portion 318 includes an outwardly projecting surface 320 formed thereon. The leaf spring 308 is configured to be disposed about the cross-bar 310 with the cam surfaces 320 thereof provided in contacting engagement with the arcuate surfaces 306 of the base portions 300 of the upper electrical contact members 298. The leaf spring 308 is formed to provide a predetermined spring force to the base portions 300 to ensure that the upper electrical contact members 298 and the cross-bar 310 move in unison in response to movements of the handle 42 and of the operating mechanism 58 during a normal trip operation.

During normal operation, the surfaces 320 of the leaf spring 308 engage the lower detents 302 of the base portions 300. Upon the occurrence of a high level short circuit or fault current condition, the

upper electrical contact members 298 rotate about the pin 110 and the surfaces 306 move along the surfaces 320 of the leaf spring 308 enabling the electrical contacts 72 and 238 to rapidly separate and to move to their BLOWN-OPEN positions (Fig. 21, in dotted line) without waiting for the operating mechanism 58 to sequence. As described hereinbefore with respect to Figs. 12A and 12B, the component force of the leaf spring 308 is significantly reduced from F1 with the moment arm L1 in the CLOSED position to the frictional force F2 that passes substantially through the pivot of members 298 or the longitudinal axis pin 110 in the subsequent position as the upper electrical contact members 298 rotate about the longitudinal axis of the pin 110 during a BLOWN-OPEN operation. The upper detents 304 engage the surfaces 320 to retain the upper electrical contacts 298 in their BLOWN-OPEN position, thereby eliminating or minimizing the possibility of contact restrike. The leaf spring 308 provides sufficient spring force to ensure proper contacting engagement between the upper electrical contact members 298 and the cross-bar 310 without the necessity for one or more compression springs.

In accordance with a further alternative embodiment (Figs. 23 and 24) of the circuit breaker 30, a lower electrical contact assembly 322 includes a lower, formed, stationary member 324 that engages the base 34, an upstanding contacting portion 326, a lower movable contact arm 328, a lower contact biasing means or torsion spring 330, a contact 332 for physically and electrically contacting the upper electrical contact 238 and an electrically insulating strip 334 to reduce the possibility of arcing between the upper electrical contact member 52 and portions of the lower electrical contact assembly 322. The movable contact arm 328 is fixedly secured to the rotatable pin 78 for rotation therewith on the upstanding contacting portion 326 about the longitudinal axis of the rotatable pin 78. The movable contact arm 328 includes an inclined, elongated surface 336 having a recess or groove 338 formed at one end thereof. The movable contact arm 328 further includes an integrally formed, generally flat, limit surface 340 formed at one end for contacting the stop 34B to limit the downward movement of the movable contact arm 328 and the contact 332 fixedly secured thereto.

The torsion spring 330 includes an upper elongated spring arm 342 for engaging the surface 336 and a pair of spaced-apart, elongated, downwardly extending support arms 337 terminating in a pair of coil extensions 344 for securely retaining the contact spring 330 in the circuit breaker 30. In assembling the lower electrical contact assembly 322 in the circuit breaker 30, the extensions 344 are passed through a pair of apertures 346 formed

through the lower formed stationary member 324; and the legs 344 may then be mechanically deformed to lock the spring 330 in engagement with the stationary contact member 324. The torsion spring 330 is configured as described herein and as depicted in the drawing to provide the required spring force to ensure that the lower electrical contact 322 is properly biased into engagement with the upper electrical contact 52 and to provide reliable operation over an extended period of time.

As described hereinabove with respect to the lower electrical contact assembly 50, the contact assembly 322 utilizes the high magnetic repulsion forces generated by high level short circuit or fault current flowing through the elongated parallel portions of the electrical contact arms 240 and 328 to cause the rapid downward movement of the contact arm 328 against the bias of the contact spring 330.

Upon the occurrence of a high level short circuit or fault current condition, the movable contact arm 328 rotates in a counterclockwise direction about the longitudinal axis of the pin 78 and is downwardly deflected; and the spring arm 342 of the spring 330 moves along the surface 336 of the movable contact arm 328. The downward deflection of the movable contact arm 328 is limited by the engagement of the flat surface 340 of the contact arm 328 with the stop 34B. The angle of inclination of the inclined surface 336 effectively reduces the spring force applied to the movable contact arm 328 after the upper and lower contacts 238 and 332 separate, to minimize the spring force opposing the downward movement of the contact 322 during a fault current condition. In addition, the moment arm of the spring force, applied by the spring arm 342, about the axis of the pin 78 is reduced while, simultaneously, the mechanical advantage of the above-mentioned high magnetic repulsion forces increases as the spring arm 342 moves along the surface 336 in the direction of the pin 78. Consequently, the resultant force opposing the downward movement of the contact 322 during a fault current condition is substantially reduced.

Claims

1. An electrical circuit breaker (30) having cooperating contacts (72, 238) and operating means (42, 96, 102, 104) for operating said contacts, said operating means comprising an over-center toggle mechanism having a first toggle link (102) and a second toggle link (104) pivotally connected by a toggle pin (106) and a toggle spring (92) connected to said toggle pin, said second toggle link being pivotally connected to a contact arm (240) carrying one (238) of said contacts, and said first toggle link being oper-



upper electrical contact members 298 rotate about the pin 110 and the surfaces 306 move along the surfaces 320 of the leaf spring 308 enabling the electrical contacts 72 and 238 to rapidly separate and to move to their BLOWN-OPEN positions (Fig. 21, in dotted line) without waiting for the operating mechanism 58 to sequence. As described hereinbefore with respect to Figs. 12A and 12B, the component force of the leaf spring 308 is significantly reduced from F1 with the moment arm L1 in the CLOSED position to the frictional force F2 that passes substantially through the pivot of members 298 or the longitudinal axis pin 110 in the subsequent position as the upper electrical contact members 298 rotate about the longitudinal axis of the pin 110 during a BLOWN-OPEN operation. The upper detents 304 engage the surfaces 320 to retain the upper electrical contacts 298 in their BLOWN-OPEN position, thereby eliminating or minimizing the possibility of contact restrike. The leaf spring 308 provides sufficient spring force to ensure proper contacting engagement between the upper electrical contact members 298 and the cross-bar 310 without the necessity for one or more compression springs.

In accordance with a further alternative embodiment (Figs. 23 and 24) of the circuit breaker 30, a lower electrical contact assembly 322 includes a lower, formed, stationary member 324 that engages the base 34, an upstanding contacting portion 326, a lower movable contact arm 328, a lower contact biasing means or torsion spring 330, a contact 332 for physically and electrically contacting the upper electrical contact 238 and an electrically insulating strip 334 to reduce the possibility of arcing between the upper electrical contact member 52 and portions of the lower electrical contact assembly 322. The movable contact arm 328 is fixedly secured to the rotatable pin 78 for rotation therewith on the upstanding contacting portion 326 about the longitudinal axis of the rotatable pin 78. The movable contact arm 328 includes an inclined, elongated surface 336 having a recess or groove 338 formed at one end thereof. The movable contact arm 328 further includes an integrally formed, generally flat, limit surface 340 formed at one end for contacting the stop 34B to limit the downward movement of the movable contact arm 328 and the contact 332 fixedly secured thereto.

The torsion spring 330 includes an upper elongated spring arm 342 for engaging the surface 336 and a pair of spaced-apart, elongated, downwardly extending support arms 337 terminating in a pair of coil extensions 344 for securely retaining the contact spring 330 in the circuit breaker 30. In assembling the lower electrical contact assembly 322 in the circuit breaker 30, the extensions 344 are passed through a pair of apertures 346 formed

through the lower formed stationary member 324; and the legs 344 may then be mechanically deformed to lock the spring 330 in engagement with the stationary contact member 324. The torsion spring 330 is configured as described herein and as depicted in the drawing to provide the required spring force to ensure that the lower electrical contact 322 is properly biased into engagement with the upper electrical contact 52 and to provide reliable operation over an extended period of time.

As described hereinabove with respect to the lower electrical contact assembly 50, the contact assembly 322 utilizes the high magnetic repulsion forces generated by high level short circuit or fault current flowing through the elongated parallel portions of the electrical contact arms 240 and 328 to cause the rapid downward movement of the contact arm 328 against the bias of the contact spring 330.

Upon the occurrence of a high level short circuit or fault current condition, the movable contact arm 328 rotates in a counterclockwise direction about the longitudinal axis of the pin 78 and is downwardly deflected; and the spring arm 342 of the spring 330 moves along the surface 336 of the movable contact arm 328. The downward deflection of the movable contact arm 328 is limited by the engagement of the flat surface 340 of the contact arm 328 with the stop 34B. The angle of inclination of the inclined surface 336 effectively reduces the spring force applied to the movable contact arm 328 after the upper and lower contacts 238 and 332 separate, to minimize the spring force opposing the downward movement of the contact 322 during a fault current condition. In addition, the moment arm of the spring force, applied by the spring arm 342, about the axis of the pin 78 is reduced while, simultaneously, the mechanical advantage of the above-mentioned high magnetic repulsion forces increases as the spring arm 342 moves along the surface 336 in the direction of the pin 78. Consequently, the resultant force opposing the downward movement of the contact 322 during a fault current condition is substantially reduced.

Claims

1. An electrical circuit breaker (30) having cooperating contacts (72, 238) and operating means (42, 96, 102, 104) for operating said contacts, said operating means comprising an over-center toggle mechanism having a first toggle link (102) and a second toggle link (104) pivotally connected by a toggle pin (106) and a toggle spring (92) connected to said toggle pin, said second toggle link being pivotally connected to a contact arm (240) carrying one (238) of said contacts, and said first toggle link being oper-



atively connected to a cradle (96), said cradle having a free end releasably engaged by a trip member (144) and, when released, acting to initiate collapse of said toggle links (102, 104), said first toggle link coacting with a stationary abutment member (158) when collapse of said toggle links occurs, characterized in that cooperating edges (160, 162) of said first toggle link (102) and said stationary abutment member (158) are configured and relatively disposed so as to engage each other upon release of the cradle after an initial rotational movement of said cradle (96), the engagement creating a first pivot point (163) about which said first toggle link (102) rotates and after some further rotational movement of said cradle, the engagement creating a second pivot point (168) about which said first toggle link rotates, said second pivot point (168) being laterally offset from the toggle linkage center line by a shorter distance than said first pivot point (163).

2. The circuit breaker of claim 1, characterized in that said cradle (96) has a first aperture formed therethrough for receiving a cradle support pin (98) and a second aperture (136) formed therethrough for receiving a movable link follower pin (108).
3. The circuit breaker of claim 2, characterized in that said first link (102) includes a recess (132) formed therein for engagement with said movable link follower pin (108), the rotational movement of said cradle (96) effecting a corresponding movement of said first link.

Revendications

1. Disjoncteur électrique (30) ayant des contacts coopérants (72, 238) et un moyen de manoeuvre (42, 96, 102, 104) pour manoeuvrer lesdits contacts, ledit moyen de manoeuvre comprenant un mécanisme de basculement rapide ayant une première biellette de basculement (102) et une seconde biellette de basculement (104) reliées d'une manière articulée par un axe de basculement (106) et un ressort de basculement (92) relié audit axe de basculement, ladite seconde biellette de basculement étant reliée d'une façon articulée à un bras de contact (240) portant un (238) desdits contacts, et ladite première biellette de basculement coopérant avec un berceau (96), ledit berceau ayant une extrémité libre étant retenu d'une façon libérable par un organe de déclenchement (144), et, lorsqu'il est libéré, servant à déclencher le basculement desdites biellettes de basculement (102, 104), ladite première

biellette de basculement coopérant avec une pièce de butée fixe (158) lorsque survient le basculement desdites biellettes de basculement, caractérisé en ce que les bords coopérants (160, 162) de ladite première biellette de basculement (102) et de ladite pièce de butée fixe (158) ont une configuration et une disposition mutuelle qui leur permettent de s'engager l'un contre l'autre au moment de le basculement du berceau après un mouvement de rotation initial dudit berceau (96), l'engagement créant un premier point de pivotement (163) autour duquel tourne ladite première biellette de basculement (102), et, après une certaine continuation du mouvement de rotation dudit berceau, l'engagement créant un second point de pivotement (168) autour duquel tourne ladite première biellette de basculement, ledit second point de pivotement (168) étant décalé latéralement, par rapport à l'axe central des biellettes de basculement, d'une distance plus courte que ledit premier point de pivotement (163).

2. Disjoncteur selon la revendication 1, caractérisé en ce qu'à travers ledit berceau (96) sont formées une première ouverture pour recevoir un axe (98) de support de berceau et une seconde ouverture (136) pour recevoir un doigt mobile (108) d'accompagnement de biellettes.
3. Disjoncteur selon la revendication 2, caractérisé en ce que ladite première biellette (102) comporte un évidement (132) formé dans celle-ci pour l'engagement avec ledit doigt mobile (108) d'accompagnement de biellettes, le mouvement de rotation dudit berceau (96) provoquant un mouvement correspondant de ladite première biellette.

Patentansprüche

1. Elektrischer Schalter (30) mit miteinander zusammenwirkenden Kontakten (72, 238) und Betätigungsmitteln (42, 96, 102, 104) zur Betätigung dieser Kontakte, wobei die Betätigungsmittel ein Kniehebelsprungwerk mit einem ersten Kniehebelglied (102) und einem zweiten Kniehebelglied (104), die durch einen Kniegelenkzapfen (106) gelenkig verbunden sind, und eine Sprungwerkfeder (92) aufweisen, die mit dem Kniegelenkzapfen verbunden ist, wobei das zweite Kniehebelglied gelenkig mit einem Kontaktarm (240) verbunden ist, der einen (238) der genannten Kontakte trägt, und wobei das erste Kniehebelglied wirkungsmäßig mit einem Spannhebel (96) verbunden ist, mit dessen freiem Ende ein Auslöseglied (144) lösbar



- in Eingriff steht und der, wenn er gelöst wird, das Zusammenklappen der Kniehebelglieder (102, 104) einleitet, und wobei das erste Kniehebelglied mit einem feststehenden Anschlagteil (158) zusammenwirkt, wenn das Zusammenklappen der Kniehebelglieder erfolgt, dadurch gekennzeichnet, daß miteinander zusammenwirkende Kanten (160, 162) des ersten Kniehebelglieds (102) und des feststehenden Anschlagteils (158) so ausgebildet und relativ zueinander angeordnet sind, daß sie beim Lösen des Spannhebels nach einer anfänglichen Schwenkbewegung des Spannhebels (96) miteinander in Zusammenwirkung kommen, wobei durch die Zusammenwirkung ein erster Gelenkpunkt (163) geschaffen wird, um welchen das erste Kniehebelglied (102) schwenkt, und wobei nach einer weiteren Schwenkbewegung des Spannhebels die Zusammenwirkung einen zweiten Gelenkpunkt (168) erzeugt, um welchen das erste Kniehebelglied schwenkt, wobei der zweite Gelenkpunkt (168) seitlich um eine kürzere Distanz als der erste Gelenkpunkt (163) mit Bezug auf die Kniehebelwerk-Mittellinie versetzt ist.
2. Schalter nach Anspruch 1, dadurch gekennzeichnet, daß der Spannhebel (96) eine erste darin gebildete Öffnung zur Aufnahme eines Spannhebeltragzapfens (98) und eine zweite darin gebildete Öffnung (136) zur Aufnahme eines beweglichen Hebelglied-Gleitzapfens (108) aufweist.
3. Schalter nach Anspruch 2, dadurch gekennzeichnet, daß das erste Kniehebelglied (102) eine darin gebildete Ausnehmung aufweist, in welche der bewegliche Gleitzapfen (108) eingreift, wobei die Schwenkbewegung des Spannhebels (96) eine entsprechende Bewegung des ersten Kniehebelglieds bewirkt.

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