

Description**Background of the Invention****a) Field of the Invention**

The present invention relates to a conductive polysulfone resin composition which has improved electrical conductivity and is excellent in heat resistance, processability and mechanical strength, and a high-heat-resistant, conductive semi-conductor article molded from the composition.

b) Description of the Related Art

As a technique for providing electrical conductivity to an aromatic polysulfone resin, it has been disclosed, for example, in Japanese Laid-Open Patent 61670 (1978) a process for preparing an electrically conductive composite by the addition of conductive materials such as conductive carbon to the aromatic polysulfone resin. The invention describes that the composite having an electrical resistance of $10^{10} \Omega$ or less can be prepared. In practice, however, the semi-conductor material thus obtained has a resistance of $10^7 - 10^{10} \Omega$. According to the information of the present inventors, formulation of conductive carbon for providing conductivity to the aromatic polysulfone resin causes increase in melt viscosity corresponding to the amount of addition. Consequently, kneading and molding of the molten composition becomes difficult or impossible in a formulating region capable of providing sufficient conductivity.

On the other hand, an injection molding resin composition containing conductive carbon dispersed in a polyphenylene sulfide resin has been known. Japanese Laid-Open Patent 8335 (1985) and 81450 (1987) disclose compositions containing conductive carbon having high oil absorption. However, the specific polyphenylene sulfide resin employed in the former patent is difficult to obtain uniform dispersion of conductive carbon and is not effective for furnishing electrical conductivity. Consequently, a remarkably increased amount of conductive carbon must be added in some uses. On the other hand, the latter patent describes that the amount of conductive carbon added can be decreased by using a polyphenylene sulfide resin having lower viscosity than that of the resin in the former patent. The latter patent, however, illustrates that the effect on conductivity improvement indicated by resistance is only $10^1 \Omega$ or at most $10^2 \Omega$, value which is smaller than the addition effect of conventional conductive carbon.

Japanese Laid-Open Patent 98632 (1983) discloses a molding resin composition containing 100 parts by weight of a resin blend composed of 99 to 50% by weight of an aromatic polysulfone resin and 1 to 50% by weight of a polyphenylene sulfide resin and from 10 to 200 parts by weight, most preferably from 80 to 180 parts by weight of a filler. The filler which can be employed in the invention includes, for example, reinforcements such as glass fiber and carbon fiber, impact strength improvers such as graphite, heat resistance improvers such as antimony trioxide, electrical property improvers such as clay and mica, acid resistance improvers such as barium sulfate, and thermal conductivity improvers such as iron. Practical cases described in the examples are only single use of glass fiber or carbon fiber and combined use of 80 parts of carbon fiber and 20 parts of graphite. No consideration is taken in the invention on the solution of a specific problem related to processing methods such as injection molding. Further, no disclosure is found at all on providing a molded article having excellent electrical conductivity.

Accompanied by high density packaging of electronic equipment, semi-conductors are mounted on a through-hole substrate in order to increase density. When moisture is adsorbed on semi-conductor parts, water vapor generates in the interior of the semi-conductor parts by heating with flow solder, leads to blister or crack and damages the semi-conductor. As a countermeasure, it has been required in the mounting to furnish a step for previously drying the semi-conductor at temperature of above 100°C to remove moisture. Conventionally, the semi-conductor drying step is carried out after once transferring the semi-conductor from a tray of conductive vinyl chloride resin or styrene base resin to a die-cast aluminum tray. The dried semi-conductor is delivered after transferring again to the above resin tray. Thus a complex step has been required. In order to simplify the step and to replace the expensive die-cast aluminum tray, application of a resin tray having excellent heat resistance is now under investigation.

Another mounting technique of the semi-conductor is a packaging method using a tape automated bonding (TAB) in order to meet the demand for density increase and thickness reduction. Application of resin parts called "carrier" is also under investigation for the transfer of the semi-conductor.

A heat resistant carrier composed of polypropylene resin has been used as a resin carrier having heat resistance of above 100°C which is suitable for the object. Drying temperature is, however, liable to increase in order to reduce drying time of the semi-conductor. Drying is carried out at 130 to 150°C , sometimes at a high temperature of 175°C . Such a high temperature causes defective phenomena such as warpage and deformation and makes the semi-conductor useless. Nylon resin is also used due to higher heat resistance than polypropylene resin. A carrier composed of nylon resin has a high heat-shrinkage and leads to problems such as

dimensional change of the carrier which renders automatic transfer with a robot to impossible. Polyphenylene sulfide is a resin having a high heat resistance. Molding of carriers composed of the resin has, however, a problem of so-called "flash" in those who are skilled in the art. Flash is a problem of generating on a molded article a surplus portion formed by squeezing-out and solidifying the resin through a parting line of the mold.

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Object and Summary of the Invention

An object of the present invention is to provide a conductive polysulfone resin composition which has an improved electrical conductivity and is excellent in heat resistance, processability and mechanical strength.

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Another object of the present invention is to provide a conductive polysulfone resin composition which has a good molding ability to give a molded article having particularly small warpage and deformation at high temperatures, is excellent in the mechanical strength indicated by drop strength, and has a dominant geometric accuracy of moldings, that is, scarce generation of flash.

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A further object of the present invention is to provide a high-heat-resistant, conductive article for semiconductor by using the above conductive polysulfone resin composition.

The above objects of the present invention can be accomplished by providing a resin composition obtained by formulating an aromatic polysulfone resin, polyphenylene sulfide resin and conductive carbon in a specific proportion and melt-kneading the resultant mixture.

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That is, one aspect of the invention is to provide a conductive resin composition obtained by mixing (A) 100 parts by weight of a composition essentially consisting of from 5 to 95% by weight of an aromatic polysulfone resin and from 95 to 5% by weight of a polyphenylene sulfide resin with (B) from 3 to 40 parts by weight of conductive carbon selected from the group consisting of furnace black, channel black, lamp black, acetylene black and thermal black.

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Detailed Description of the Invention

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The above conductive polysulfone resin composition of the present invention can be processed by various methods such as injection molding, extrusion and transfer molding. A preparation example of the high-heat-resistant, conductive semi-conductor-chip-carrier will hereinafter be illustrated as an application example by injection molding and as an example of the articles.

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Particularly surprising matter in the invention is that the aromatic polysulfone resin composition of the invention is found to have a remarkably improved conductivity and additionally have a stabilized surface resistance as compared with an aromatic polysulfone resin composition or a polyphenylene sulfide resin composition individually obtained by adding the same amount of the conductive carbon as in the present invention.

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The polyphenylene sulfide resin is assumed to have a much higher concentration of conductive carbon in the resin composition and to cause such characteristic. The resin composition of the invention can hence decrease the minimum amount of the conductive carbon required for obtaining electrical conductivity, can also depress viscosity increase of the resin composition and has a characteristic of little flash in the molding step as compared with the polyphenylene sulfide resin.

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The high-heat-resistant, conductive semi-conductor-articles molded by using the conductive polysulfone resin composition is suitable for parts, for example, IC-tray and chip-carrier for use in drying, transporting and inspection steps of semi-conductor production.

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The term "high-heat-resistant, conductive semi-conductor article" in the present invention refers to container, magazine, magazine-tube, socket for burn-in, rack, carriers, trays and other parts which are used in drying, transporting and inspection steps of semi-conductor production. The conductive chip-carrier in the articles is required to have surface resistance of from 10^5 to $10^4 \Omega$ or less in order to inhibit static charge or to use in the inspection step.

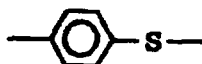
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The aromatic polysulfone resin which constitutes the conductive polysulfone resin composition of the invention is a polymer obtained by condensation reaction of an alkali phenolate group in an aprotic solvent with an aromatic halogen group which is activated by an electron attractive sulfonyl group and is a linear polymer having three required unit linkage of an arylene bond (aromatic bond), ether bond and sulfonyl bond.

The aromatic polysulfone resin can be prepared by the processes described in, for example, Japanese Patent Publication 10067 (1965), 7799 (1967) and 617 (1972). A representative commercial product is VIC-TREX (Trade mark of Imperial Chemical Industries).

The aromatic polysulfone resin used in the invention has an inherent viscosity in a 1% dimethylformamide solution at 25°C of preferably 0.38 dl/g or less, more preferably from 0.25 to 0.38 dl/g.

The polyphenylene sulfide resin (hereinafter referred to as PPS resin) for use in the invention is required to have 90% by mole or more of structural unit represented by the formula:

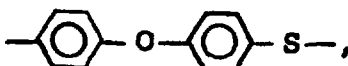


5 when the above structural unit is less than 90% by mole, excellent properties suitable for the object of the invention are difficult to obtain. Copolymerization components including a meta bond such as



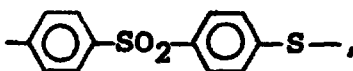
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ether bond such as



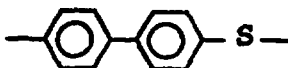
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sulfonyl bond such as



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25 and biphenyl bond such as



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may be present in less than 10% by mole unless giving remarkably adverse effect on the crystallinity and stretch orientation of the polymer. Amount of the copolymerization components is preferably 5% by mole or less.

35 Polymerization of PPS can be carried out by reacting a halogen substituted aromatic compound with alkali metal sulfide [USP 2513188 and Japanese Patent Publication 3368 (1970)], by condensation reaction of thiophenols in the presence of an alkali catalyst [USP 3274165], and by condensation reaction of aromatic compounds with sulfur chloride in the presence of a Lewis acid catalyst [Japanese Patent Publication 27255 (1971)]. These processes can difficultly provide PPS of high polymerization degree and high polymer formation accompanied by crosslinking is usually carried out after polymerization. Consequently, these PPS are generally called crosslinking type PPS. The crosslinking type PPS which is available in the market includes RYTON P-6 (Trade mark of Phillips Petroleum).

40 Polymerization of PPS can also be carried out in the presence of oxide or hydroxide of alkaline earth metals to obtain straight chain polymers of high molecular weight [Japanese Laid-Open Patent 55029 (1985) and 55030 (1985)]. PPS prepared by these processes is generally called straight chain PPS. Marketed straight chain PPS includes FORTRON W-205 (Trade mark of Kureha Chemical Industry). Both crosslinking type and straight chain type PPS resins can be used for the PPS resin of the invention.

The conductive carbon used for the invention is filled into the resin, provides a high electrical conductivity for the resin and remarkably reduces surface resistance of the resin.

50 The conductive carbon employed is selected from furnace black, channel black, lamp black, acetylene black and thermal black; in particular, acetylene black and furnace black are preferably used. Graphite and carbon fiber are unsuitable for the conductive carbon of the invention. The conductive carbon may be used singly or as a mixture. Marketed furnace black includes, for example, KETCHEN BLACK EC (Trade mark of Akzo in Holland) and VULKAN XC-72 (Trade mark of Cabot in USA).

55 Electrical conductivity can be sufficiently provided in the invention by formulating conductive carbon in the resin composition. Other conductive fillers can also be added depending upon the object of conductivity increase. Other conductive fillers include, for example, a single material or a mixture of the material selected from silver, copper, gold, aluminum, nickel, palladium, iron, stainless steel, tin oxide, indium oxide, lead oxide,

silicon carbide, zirconium carbide, titanium carbide, graphite carbon fiber or metallic fiber; or powder, flake, bead, fiber or other various materials obtained by coating these conductive fillers.

In the present invention, the formulating ratio of the aromatic polysulfone resin to the polyphenylene sulfide resin is from 5 to 95% by weight of the aromatic polysulfone resin to from 95 to 5% by weight of the polyphenylene sulfide resin. The formulating ratio of the resin which provides very excellent heat resistance and electrical conductivity is preferably from 60 to 95% by weight of the aromatic polysulfone resin to from 40 to 5% by weight of the polyphenylene sulfide resin, more preferably from 70 to 90% by weight of the aromatic polysulfone resin to from 30 to 10% by weight of the polyphenylene sulfide resin. The formulating ratio of the resin which provides very excellent processability is preferably from 5 to 60% by weight of the aromatic polysulfone resin to from 95 to 40% by weight of the polyphenylene sulfide resin, more preferably from 10 to 50% by weight of the aromatic polysulfone resin to from 90 to 50% by weight of the polyphenylene sulfide resin. To 100 parts by weight of the resin composition (A), the conductive carbon (B) is added in an amount of from 3 to 40 parts by weight, preferably from 3 to 25 parts by weight. If the amount of aromatic polysulfone resin is less than 5% by weight causes marked reduction of heat resistance and is additionally liable to generate flash on conductive articles. If the amount of aromatic polysulfone resin exceeds 95% by weight the processing ability is decreased and further leads to unstable surface resistivity. The conductive carbon less than 3 parts by weight results in insufficient electrical conductivity. On the other hand, amount of the carbon exceeding 40 parts by weight lowers flowability and mechanical strengths of the composition and good molded articles become difficult to obtain.

No particular restriction is imposed and usually known processes can be used on the preparation process of the high-heat-resistant, conductive semi-conductor-articles of the invention. In the preparation process, the aromatic polysulfone resin, polyphenylene sulfide resin, conductive carbon and, if desired, other materials and additives are uniformly mixed with a high speed stirrer. The resulting mixture is melt-kneaded with a single or multi screw extruder having sufficient capacity, pelletized and then injection molded to obtain the articles.

Various elastomers can be added to further improve mechanical strengths of the resin composition and the high-heat-resistant, conductive semi-conductor-articles.

The elastomers which can be used are A-B-A' type block copolymer elastomers. A and A' are polymerized vinyl aromatic hydrocarbon blocks and B is a polymerized, conjugated diene block or a block obtained by hydrogenating the polymerized, conjugated diene block. A glycidyl group containing copolymer composed of α -olefin and α,β -unsaturated carboxylic acid glycidyl ester, a core-shell type elastomer and a polyester elastomer can also be added for the same object. The elastomers may be used singly or as a mixture. The elastomers can be added in an amount which causes no remarkable reduction in heat resistance of the conductive polysulfone resin composition. The amount is preferably from 0.5 to 30 parts by weight, more preferably from 1 to 20 parts by weight per 100 parts by weight of the composition (A).

Additives which can be incorporated depending upon the object are pigments and dyes, fillers such as glass fiber, talc and calcium carbonate, stabilizers such as calcium stearate, bleaching agents such as hydro-sulfite, antioxidants, ultraviolet absorbers, lubricants, release agents such as fluoro resin and silicon resin, flame retardants, and antistatics. Amount of additives except fillers and other elastomers is preferably from 3 to 50 parts by weight, more preferably from 5 to 30 parts by weight per 100 parts by weight of the composition (A).

The conductive polysulfone resin composition of the invention is excellent in electrical conductivity, has good processability, heat resistance and mechanical strengths and consequently is high in practical value. The high-heat-resistant, conductive semi-conductor-articles molded from the conductive polysulfone resin composition has large value in practical use due to excellent electrical conductivity, little flash in molding step, and additionally excellent heat resistance and mechanical strength.

The present invention will hereinafter be illustrated further in detail by way of examples. The resin compositions and molded articles in the examples and comparative examples were evaluated their properties by the following methods.

(1) Tensile strength

In accordance with JIS-K 7113.

(2) Heat distortion temperature

In accordance with JIS-K 7207 at a bending stress of 18.56 kg/cm².

(3) Melt flow index (processability)

In accordance with JIS K-7210, under 10 kg load at 320°C.

(4) Surface resistivity

A two terminal type surface resistivity tester (RESISTAT; manufactured by Mitsubishi Petrochemical) was used.

A dumbbell specimen used for the tensile strength test and a specimen cut from the molded carrier

(molded article) were respectively used for measuring surface resistivity at 23°C in 50% relative humidity.

(5) Warpage and deformation of molded article (carrier)

A tray having dimensions of 300 x 150 x 6 mm, an average thickness in flat portion of 2.5 mm and a total weight of 80 g was injection molded, allowed to stand in a drying oven at 175°C for 2 hours, placed on a flat plate and then presence of warpage and deformation was visually observed.

(6) Mechanical strength of molded article

A molded article was gravity-dropped from a height of 2 m on a concrete floor and damage was visually observed.

(7) Flash of molded articles

A molded article was observed with a magnifier and presence of flash was observed.

Examples 1 - 5

An aromatic polysulfone resin VICTREX 3600P (manufactured by Imperial Chemical Industries), a polyphenylene sulfide resin RYTON P-6 (manufactured by Phillips Petroleum) and conductive carbon KETCHEN BLACK EC (manufactured by Akzo in Holland) having dibutyl phthalate oil absorption of 360 ml/100 g were formulated in a proportion illustrated in Table 1, kneaded in a temperature range of 270 to 330°C to prepare pellets. The pellets thus obtained was injection molded to form specimens and chip carriers. The evaluation results of properties are illustrated in Table 1.

Injection molding was carried out under mold clamping force of 150 ton at a cylinder temperature of 360°C and a mold temperature of 150°C.

Example 6

The same procedures as described in Example 1 were carried out except that methyl methacrylate/butadiene/styrene graft copolymer KM653 (Trade mark of Rohm & Haas Company) was used as a core-shell type elastomer and formulated in a proportion illustrated in Table 1.

Example 7

The same procedures as described in Example 6 were carried out except that ethylene/glycidyl methacrylate copolymer BONDFAST 2B (Trade mark of Sumitomo Chemical Industry) (illustrated as EGMA in Table 1) was used as an elastomer and formulated in a proportion illustrated in Table 1.

Example 8

The same procedures as described in Example 3 were carried out except that glass fiber ESC T-24 (Trade mark of Nippon Electric Glass) (illustrated as GF in Table 1) was used and formulated in a proportion illustrated in Table 1.

Comparative Examples 1-4

The same procedures as described in Examples 1-4 were carried out except that proportion of components in the formulations were changed as illustrated in Table 2.

When the proportion of components deviates from the specified formulating ratio, the resin compositions cause a remarkable decrease in some of heat distortion temperature, melt flow index, tensile strength and surface resistivity, and the molded articles lead to generation of warpage or flash and marked lowering of mechanical strength and surface resistivity. Thus the molded articles were found to be unsatisfactory for practical use.

Comparative Example 5

The same procedures as described in Example 3 were carried out except that graphite was used in place of KETCHEN black EC. The composition obtained had insufficient physical properties. The molded article is also inferior in mechanical strengths and surface resistivity. Thus the composition was unsuitable for practical use.

Table 1

Example No.	1	2	3	4	5	6	7	8
<u>Formulation</u>								
(A) Aromatic polysulfone resin (% by weight)	20	40	70	70	90	70	90	70
Polypheylene sulfide resin (% by weight)	80	60	30	30	10	30	10	30
(B) Conductive carbon (parts by weight)	8	8	8	20	8	5	10	4
Elastomer (parts by weight)						Core shell 5	EGMA 10	
Glass fiber (parts by weight)								GF 10
<u>Property of composition</u>								
Tensile strength (kg/cm ²)	430	440	510	460	550	570	550	810
Heat distortion temperature (°C)	183	189	203	209	209	192	201	214
Melt flow index (g/10 min)	42	38	33	28	28	31	27	27
Surface resistivity (Ω)	1x10 ³	3x10 ³	3x10 ³	7x10 ²	2x10 ³	5x10 ³	4x10 ³	1x10 ⁴
<u>Property of molded article</u>								
Warpage and deformation	no	no	no	no	no	no	no	no
Mechanical strength	good	good	good	good	good	good	good	good
Surface resistivity (Ω)	1x10 ⁴	8x10 ³	7x10 ³	1x10 ³	8x10 ³	9x10 ³	7x10 ³	5x10 ⁴
Flash (Geometrical accuracy)	no	no	no	no	no	no	no	no

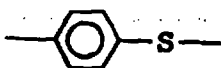
Table 2

Comparative Example No.	1	2	3	4	5
<u>Formulation</u>					
(A) Aromatic polysulfone resin (% by weight)	100	2	70	70	70
Polyphenylene sulfide resin (% by weight)	0	98	30	30	30
(B) Conductive carbon (parts by weight)	8	8	1	50	Graphite 8
Elastomer (parts by weight)					
Glass fiber (parts by weight)					
<u>Property of composition</u>					
Tensile strength (kg/cm ²)	550	480	620	430	480
Heat distortion temperature (°C)	212	117	201	210	204
Melt flow index (g/10 min)	16	31	23	13	25
Surface resistivity (Ω)	1×10^8	3×10^7	$> 10^{14}$	6×10^3	4×10^7
<u>Property of molded article</u>					
Warpage and deformation	no	found	no	no	no
Mechanical strength	good	good	good	crack	good
Surface resistivity (Ω)	2×10^8	5×10^7	$> 10^{14}$	7×10^3	8×10^7
Flash (Geometrical accuracy)	no	found	no	no	no



Claims

1. A conductive polysulfone resin composition comprising mixing (A) 100 parts by weight of a composition essentially consisting of from 5 to 95% by weight of an aromatic polysulfone resin and from 95 to 5% by weight of a polyphenylene sulfide resin with (B) from 3 to 40 parts by weight of conductive carbon selected from the group consisting of furnace black, channel black, lamp black, acetylene black and thermal black.
2. The resin composition of claim 1 wherein (A) 100 parts by weight of the composition essentially consisting of from 20 to 95% by weight of the aromatic polysulfone resin and 80 to 5% by weight of the polyphenylene sulfide resin are mixed with (B) from 3 to 25 parts by weight of the conductive carbon.
3. The resin composition of claim 1 wherein (A) 100 parts by weight of the composition essentially consisting of from 60 to 95% by weight of the aromatic polysulfone resin and from 40 to 5% by weight of the polyphenylene sulfide resin are mixed with (B) from 3 to 25 parts by weight of the conductive carbon.
4. The resin composition of claim 1 wherein (A) 100 parts by weight of the composition essentially consisting of from 5 to 60% by weight of the aromatic polysulfone resin and from 95 to 40% by weight of the polyphenylene sulfide resin are mixed with (B) from 3 to 25 parts by weight of the conductive carbon.
5. The resin composition of claim 1 wherein the aromatic polysulfone resin has an inherent viscosity of 0.38 dl/g or less at 25°C in a 1% dimethylformamide solution.
6. The resin composition of claim 1 wherein the polyphenylene sulfide resin comprises 90% by mole or more of the structural units represented by the formula:



7. The resin composition of claim 1 wherein the polyphenylene sulfide is a straight chain type polyphenylene sulfide resin.
8. The resin composition of claim 1 wherein the conductive carbon is acetylene black or furnace black.
9. The resin composition of claim 1 wherein an elastomer is added in an amount of from 0.5 to 30 parts by weight per 100 parts by weight of the resin composition (A).
10. The resin composition of claim 9 wherein the elastomer is a core-shell type elastomer.
11. The resin composition of claim 9 wherein the elastomer is a glycidyl group containing copolymer composed of α -olefin and α,β -unsaturated glycidyl ester.
12. The resin composition of claim 1 wherein the amount of a filler and other additives excluding the elastomer is in the range of from 5 to 30 parts by weight per 100 parts by weight of the resin composition (A).
13. A molded article obtained by molding a conductive polysulfone resin composition comprising mixing (A) 100 parts by weight of a composition essentially consisting of from 5 to 95% by weight of an aromatic polysulfone resin and from 95 to 5% by weight of a polyphenylene sulfide resin with (B) from 3 to 40 parts by weight of conductive carbon selected from the group consisting of furnace black, channel black, lamp black, acetylene black and thermal black.
14. A molded article of high-heat-resistant, conductive semi-conductor-chip-carrier of claim 13.

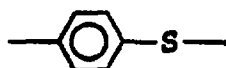
Patentansprüche

1. Leitfähige Polysulfonharzzusammensetzung umfassend das Mischen von
(A) 100 Gewichtsteilen einer Zusammensetzung bestehend im wesentlichen aus 5 bis 95 Gew.-% ei-



nes aromatischen Polysulfonharzes und 95 bis 5 Gew.-% eines Polyphenylensulfidharzes mit (B) 3 bis 40 Gewichtsteilen leitfähigem Harz ausgewählt aus der Gruppe bestehend aus Ofenruß, Kanalruß, Lampenruß, Acetylenruß und thermischem Ruß.

- 5 2. Harzzusammensetzung nach Anspruch 1, worin
 (A) 100 Gewichtsteile der Zusammensetzung im wesentlichen bestehend aus 20 bis 95 Gew.-% des aromatischen Polysulfonharzes und 80 bis 5 Gew.-% des Polyphenylensulfidharzes mit
 (B) 3 bis 25 Gewichtsteilen des leitfähigen Kohlenstoffs gemischt sind.
- 10 3. Harzzusammensetzung nach Anspruch 1, worin
 (A) 100 Gewichtsteile der Zusammensetzung im wesentlichen bestehend aus 60 bis 95 Gew.-% des aromatischen Polysulfonharzes und 40 bis 5 Gew.-% des Polyphenylensulfidharzes mit
 (B) 3 bis 25 Gewichtsteilen des leitfähigen Kohlenstoffs gemischt sind.
- 15 4. Harzzusammensetzung nach Anspruch 1, worin
 (A) 100 Gewichtsteile der Zusammensetzung im wesentlichen bestehend aus 5 bis 60 Gew.-% des aromatischen Polysulfonharzes und 95 bis 40 Gew.-% des Polyphenylensulfidharzes mit
 (B) 3 bis 25 Gewichtsteilen des leitfähigen Kohlenstoffs gemischt sind.
- 20 5. Harzzusammensetzung nach Anspruch 1, worin das aromatische Polysulfonharz eine grundmolare Viskosität von 0,38 dl/g oder weniger bei 25°C in einer 1-prozentigen Dimethylformamidlösung aufweist.
6. Harzzusammensetzung nach Anspruch 1, worin das Polyphenylensulfidharz 90 Mol-% oder mehr der Struktureinheiten umfaßt, die durch die Formel

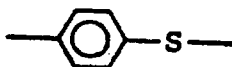


- 30 repräsentiert werden.
7. Harzzusammensetzung nach Anspruch 1, worin das Polyphenylensulfid ein geradkettiger Typ von Polyphenylensulfidharz ist.
- 35 8. Harzzusammensetzung nach Anspruch 1, worin der leitfähige Kohlenstoff Acetylenruß oder Ofenruß ist.
9. Harzzusammensetzung nach Anspruch 1, worin ein Elastomer in einer Menge von 0,5 bis 30 Gewichtsteilen pro 100 Gewichtsteile der Harzzusammensetzung (A) zugegeben ist.
- 40 10. Harzzusammensetzung nach Anspruch 9, worin das Elastomer ein Elastomer vom Kern-Mantel-Typ ist.
11. Harzzusammensetzung nach Anspruch 9, worin das Elastomer ein Glycidylgruppe enthaltendes Copolymer ist, das aus α -Olefin und α,β -ungesättigtem Glycidylester zusammengesetzt ist.
- 45 12. Harzzusammensetzung nach Anspruch 1, worin die Menge eines Füllstoffes und anderer Additive, ausgeschlossen das Elastomer, im Bereich von 5 bis 30 Gewichtsteilen pro 100 Gewichtsteile der Harzzusammensetzung (A) vorliegt.
- 50 13. Ausgeformter Gegenstand erhalten durch Ausformen einer leitfähigen Polysulfonharzzusammensetzung enthaltend eine Mischung aus
 (A) 100 Gewichtsteilen einer Zusammensetzung im wesentlichen bestehend aus 5 bis 95 Gew.-% eines aromatischen Polysulfonharzes und 95 bis 5 Gew.-% eines Polyphenylensulfidharzes mit
 (B) 3 bis 40 Gewichtsteilen leitfähigem Kohlenstoff, ausgewählt aus der Gruppe bestehend aus Ofenruß, Kanalruß, Lampenruß, Acetylenruß und thermischem Ruß.
- 55 14. Ausgeformter Gegenstand aus hochhitzebeständigem, leitfähigem Halbleiterchipträgermaterial nach Anspruch 13.



Revendications

1. Composition de résine polysulfone conductrice comprenant le mélange (A) de 100 parties en poids d'une composition constituée sensiblement par 5 à 95 % en poids d'une résine polysulfone aromatique et de 95 à 5 % en poids d'une résine de sulfure de polyphénylène avec (B) de 3 à 40 parties en poids de carbone conducteur choisi dans le groupe constitué par du noir de fourneau, du noir de tunnel, du noir de fumée, du noir d'acétylène et du noir thermique.
2. Composition de résine selon la revendication 1, dans laquelle (A) 100 parties en poids de la composition constituée essentiellement par 20 à 95 % en poids de la résine de polysulfone aromatique et 80 à 5 % en poids de la résine de sulfure de polyphénylène sont mélangées avec (B) de 3 à 25 parties en poids du carbone conducteur.
3. Composition de résine selon la revendication 1, dans laquelle (A) 100 parties en poids de la composition constituée essentiellement par 60 à 95 % en poids de la résine polysulfone aromatique et de 40 à 5 % en poids de la résine de sulfure de polyphénylène sont mélangées avec (B) de 3 à 25 parties en poids du carbone conducteur.
4. Composition de résine selon la revendication 1, dans laquelle (A) 100 parties en poids de la composition essentiellement constituée par 5 à 60 % en poids de la résine polysulfone aromatique et de 95 à 40 % en poids de la résine de sulfure de polyphénylène sont mélangées avec (B) de 3 à 25 parties en poids du carbone conducteur.
5. Composition de résine selon la revendication 1, dans laquelle la résine polysulfone aromatique possède une viscosité inhérente de 0,38 dl/g ou moins à 25°C dans une solution de diméthylformamide à 1 %.
6. Composition de résine selon la revendication 1, dans laquelle la résine de sulfure de polyphénylène comprend 90 % en mole ou davantage des motifs structuraux représentés par la formule :



7. Composition de résine selon la revendication 1, dans laquelle le sulfure de polyphénylène est une résine de sulfure de polyphénylène à chaîne linéaire.
8. Composition de résine selon la revendication 1, dans laquelle le carbone conducteur est du noir d'acétylène ou du noir de fourneau.
9. Composition de résine selon la revendication 1, dans laquelle on ajoute un élastomère dans une quantité de 0,5 à 30 parties en poids pour 100 parties en poids de la composition de résine (A).
10. Composition de résine selon la revendication 9, dans laquelle l'élastomère est un élastomère de type noyau-enveloppe.
11. Composition de résine selon la revendication 9, dans laquelle l'élastomère est un groupe glycidyle contenant un copolymère d' α -oléfine et d'ester α,β -glycidyle non saturé.
12. Composition de résine selon la revendication 1, dans laquelle la quantité de l'agent de charge et d'autres additifs excluant l'élastomère se situe dans la plage de 5 à 30 parties en poids pour 100 parties en poids de la composition de résine (A).
13. Produit moulé obtenu par moulage d'une composition de résine polysulfone conductrice comprenant le mélange (A) de 100 parties en poids d'une composition constituée essentiellement de 5 à 95 % en poids d'une résine polysulfone aromatique et de 95 à 5 % en poids d'une résine de sulfure de polyphénylène avec (B) de 3 à 40 parties en poids de carbone conducteur, choisi dans le groupe constitué par le noir de fourneau, le noir de tunnel, le noir de fumée, le noir d'acétylène et le noir thermique.



14. Produit moulé présentant une résistance élevée à la chaleur, support conducteur pour puce de semi-conducteur selon la revendication 13.

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