

Description

The present invention relates to the manufacture of drill screws, and more particularly to novel methods and apparatus for repeatably making high performance drill screws.

This invention can be considered to be an improvement of the arrangements disclosed in US-A-3280412, which describes the nearest prior art, and GB-A-2063731, GB-A-2100157, GB-A-2101019 and GB-A-2101022, to which the reader is invited to refer.

The art of forming milled drill points on drill screws has generally involved a frame structure which carries a conveyor or turret which is adapted to convey successive screw blanks to various work stations. The screw blanks have elongate shanks exposed beneath the turret. It is upon these exposed shanks that various operations have been performed involving the use of milling saws. Such operations have been generally successful and have enabled commercially acceptable drill screws to be produced in an efficient manner.

In accordance with one aspect of the present invention an apparatus, for consistently producing within exacting tolerances drill screws having drilling tips with at least two flutes, comprises: an indexable turret for intermittently conveying successive screw blanks having exposed axially extending shanks along a path of travel; a cam operated milling station adjacent said path including a motor driven spindle for mounting a pointing cutter with its axis of rotation inclined to the axis of a screw blank at the milling station, the pointing cutter having a concave profile and forming one of a plurality of form relieved rotary milling cutters used to form said drilling tips; and means for firmly holding said screw blanks against uplift and rotational forces resulting from interaction between said screw blanks and said cutters; characterised by

(a) means for adjusting the position of the pointing cutter in a direction along the axis of rotation of the pointing cutter, in order precisely to control the size and orientation of heel portions of said drilling tips,

b) means for rotating said cutters at a rate of approximately 304.8 surface meters (1000 surface feet) per minute, and

c) said holding means being capable of exerting a downward axial force on said screw blanks of between 889.64 and 1556.87 N (200 and 350 pounds) inclusive.

In accordance with another aspect of the present invention a method, for producing drill screws having drilling tips, comprises the steps of: using an indexable turret for intermittently conveying successive screw blanks having head portions and axially extending shank portions along a path of travel with tips of said shanks exposed; shaping the drilling tips of said screw blanks with a plurality of form relieved rotary milling cutters mountable on motor driven spindles which are pivotable into engagement

with said screw shanks at cam operated milling stations, one milling station including a pointing cutter having a concave profile to be mounted with its axis of rotation inclined to the axis of a screw blank at said one milling station; and applying an axially downward load to said successive screw blanks in order to prevent rotational and axial movement thereof; characterised by

a) adjusting the position of the pointing cutter in a direction along the axis of rotation of the pointing cutter, in order precisely to control the size and orientation of heel portions of said drilling tips,

b) variably adjusting the cut per tooth of said cutters, and

c) applying the axially downward load to between 889.64 and 1556.87 N (200 and 350 pounds) inclusive,

whereby the life of said cutters may be maximized and the size and shape of burrs resulting from the formation of said tips can be precisely controlled.

The present invention thus envisages that form relieved rotary milling cutters may be rotated at unusually high speeds to produce high performance drill screws at improved rates of production. The cutters may be adjusted in a simple manner to achieve variations in the geometry of the drill point, and the speed of the cutters may be controlled carefully to maintain the quality of the products and maximize the life of the cutters. The screw blanks may be held down by unusually high forces during cutting to prevent rotational and axial movement of the screw blanks.

An apparatus and a method, in accordance with the present invention, will now be described by way of reference to the accompanying drawings, in which:—

Figures 1 and 2 are elevational views of a portion of an apparatus incorporating some of the features of the present invention;

Figures 3 and 4 are enlarged elevational views showing a screw blank and a rotary milling cutter adjusted to form drilling tips in accordance with the present invention;

Figure 5 is an elevational view showing milling cutters used to form flutes in a screw blank;

Figure 6 is a sectional view taken along line 6—6 of Figure 5;

Figures 7 and 8 are elevational views of a milling cutter used to form the tips of drill screws;

Figures 9 and 10 are elevational views of a milling cutter used to form the flutes of drill screws;

Figures 11 and 12 are enlarged elevational views of alternative embodiments of milling cutters used to form drilling tips in screw blanks; and

Figure 13 is a view in partial section taken along line 13—13 in Figure 5 showing an alternative embodiment of a milling cutter used to form flutes in a screw blank.

Detailed Description of the Invention

Referring now to the drawings wherein like parts are designated by the same numerals throughout the various figures, Fig. 1 shows a portion of a drill pointing machine with a pointing unit assembly 10 mounted on a base 12 adjacent an indexable turret 14. The assembly 10 comprises an axially adjustable spindle cartridge 16 which carries a milling cutter 18. An electric motor 20 is adapted to drive the cutter 18 by means of a roller chain 22. The assembly 10 is adapted to pivot about a point 24 so as to cause the cutter 18 to engage a screw blank 26 mounted in the turret 14. The assembly 10 further includes a vertical adjusting nut 28 adapted to raise and lower the height of the cutter 18. The position of the cutter 18 along its axis is controllable by means of the spindle adjusting rings 32. The pointing unit assembly 10 preferably includes a variable control 30 which is used to vary the speed at which the motor 20 rotates the cutter 18. It should also be noted that the pivoting movement of the assembly 10 is controlled by a cam member X (not shown) beneath the support 12. The movement of the unit 10 and the resulting lateral movement of the cutter 18 is timed such that the cutter 18 strikes the bottom portion of the blank 26 between indexing movements of the turret 14. Since the movement of the unit is cam operated the rate at which the cutter engages the blank 26 varies depending upon the desired output of the entire pointing machine.

By controlling the rotational speed of the cutter 18 with the control 30, and by controlling the rate at which the assembly 10 pivots into engagement with the blank 26 an operator can maintain virtually complete control over the cut per tooth of the milling cutter 18. This is significant because variations in the quality of the material comprising the blank 26 often result in variations in the way burrs are formed. It has been found that strategically locating the burrs which result from the milling operation can result in improved performance depending upon the extent to which the screw is plated and the material used in the plating. Another significant feature which is the result of having the ability to control the cut per tooth of the milling cutters 18 is the ability to maximize the life of the cutter, while at the same time maximizing output. Since the hardness of raw materials may vary, it may be desirable to lower or increase the cut per tooth of the cutters at the expense of output in order to make the best use of the cutters.

Fig. 2 more clearly shows the cutter holding spindle cartridge 16. The axial position of the cutter 18 can be adjusted along the axis of the cutter by rotating the spindle adjusting rings 32. The vertical position of the cutter 18 can be adjusted by rotating the nut 28, because movement of the nut vertically raises or lowers the entire cartridge 16.

Figs. 3 and 4 show the significance of the ability to vary the axial location of the cutter 18, particularly in connection with the use of a concave

milling cutter. By forming a drilling point 17 on the blank 26 with the upper portion of the concave milling cutter 18, the length of the heel portion 34 is maximized and the included angle "A" formed by tangents to the heel portion at the tip 36 of the point 17 is minimized. In contrast, Fig. 4 shows the formation of the point 17 with the lower portion of the concave milling cutter 18. In this case the length of the heel portion 34 is minimized and the included angle "B" of the point 17 is maximized. It should be noted that this is easily achieved by simply moving the cutter 18 along its axis in the directions of the arrows in Figs. 3 and 4, by adjusting the spindle adjusting rings 32 and in some cases adjusting the vertical positions of the cutter with the adjusting nut 28. It should be noted that the term "drilling point" as used in this specification is intended to include the combination of fluting and heel surfaces.

Figs. 5 and 6 show portions of an apparatus used to form the flute portions of drill screws in accordance with the present invention. In these figures convex milling cutters 19 are used to form curved surfaces in the screw blank 26. By using cutters with a convex profile the geometry of the point 17 is comprised of compound surfaces 38 comprised of curved portions 39 and straight portions 40. The formation of flutes in drilling screws in the past was accomplished by substantially flat profiled milling saws. By using convex milling cutters the discontinuities in the cross-sectional configuration of flutes of the prior art can be avoided. As a result a drill point of significantly stronger geometry can be achieved by using milling cutters in accordance with the present invention. It should be noted however that the use of milling cutters necessitates significantly greater hold down forces to avoid movement of the blank during the milling operation. Both of the fluting cutters 19 contact the blank with generally downward force, but since they are angled at about 15 degrees with respect to vertical and since they contact opposite sides of the blank their horizontal components combine to impart significant rotational force to the blank. And since there are relatively few teeth on the cutters compared to the saws used in the prior art, it has been found that more than twice the amount of hold down force is required. It has been discovered that hold down forces of between 889.64 and 1555.87 N (200 and 350 pounds (90.7 and 158.8 Kg) inclusive) may be required, depending upon the speed of rotation of the cutters and the number of cutting teeth on the cutter. In the preferred embodiment a hold down pin 29 actuated by air pressure is used to hold the screw blank in a collet. The pin is part of a piston mounted in a cylinder which is connected to a pressure line capable of selectively exerting the required hold down forces. Alternatively, mechanical or hydraulic holding means could be used in place of the pneumatic means discussed above.

Figs. 7 and 8 show the preferred form of milling cutter 18 used to form the heel portions of screw

blanks while Figs. 9 and 10 show the preferred form of milling cutters used to form flutes in screw blanks. The teeth 50 have relieved portions 51 to prevent friction, curved cutting edges 52 to create the desired forms in the screw blanks, and significant spaces 53 between the teeth to prevent build-up of removed material. It has been found that by using cutters between 20 and 32 teeth and diameters between 2.0 and 3.5 inches (5.08 and 8.89 cm) inclusive, and by carefully controlling the rotational speed and thereby the cut per tooth of the milling cutters, the life of the cutters can be maximized; while at the same time the quality of the end product can be improved in terms of accuracy, repeatability of performance, and the output of the drill pointing machine can be improved. This is a result, at least in part, because, as the output of the machine is increased, the speed at which the cutters are moved into engagement with the blank and the resulting cut per tooth of the cutters would be excessive without the ability to increase the rotational speed of the cutters to compensate for the increased amount of material cut by the tooth. By having relatively few teeth on the perimeter of the cutter the extent to which each tooth may be sharpened will be increased because the sharpening of the cutters is accomplished by grinding the faces of the teeth rather than by profile grinding.

It has also been found that potential interference between the fluting cutters 19 and the turret 14 makes the use of small diameter cutters desirable, especially when milling short screw blanks because in those cases only a small amount of the screw blank is exposed. It has been determined that the cutters described above as having diameters as small as 5.21 cm (2.05 inches) can be used with satisfactory results in terms of cutter life and burr formation as well as output rate and quality control with screws as short as $\frac{1}{8}$ inches (0.79 cm).

By using small diameter form relieved milling cutters with relatively few teeth, and by rotating such cutters at unusually high rates which approach 304.8 surface meters (1000 surface feet) per minute, optimum use can be made of the cutters and increased rates of production can be achieved without sacrificing quality.

It should also be noted that in some cases it may be desirable to include a chip breaking feature on either the pointing cutter 18 or the fluting cutter 19. Figs. 11 and 12 show pointing cutters 18 with ribs 41 formed on each tooth thereof. The ribs are aligned on the cutter to form a single trough 42 on each heel portion 34 of the tip 17 of the blank 26. However, in the preferred embodiment of a screw incorporating a chip breaking feature on the heel portions, the troughs on opposite heel portions are not equidistant from the center of the blank so that in a workpiece the cutting edge on one side of the screw will remove the rib formed by the trough on the opposite side of the screw. It should be noted that by placing a rib in an off-center position on the pointing cutter and by using cutters in the manner shown in Figs. 11 and 12 where the rib 41 is on the

upper portion when forming one heel portion and the rib 41 is on the lower portion when forming the other heel portion, a single form of cutter can be used without the need for right and left hand forms.

Fig. 13 shows a cutter 19 used to form a chip breaking feature in the flutes 40 of a blank 26. A rib 43 is used to form a trough 44 in the flute 40. The rib 43 is comprised of a plurality of segments in alignment on the teeth of the cutter 19. Alternatively a trough could be formed on the cutter in order to form a rib in the flute. Similarly such an alternative technique could be used in forming the chip breaking feature on the heel.

By using milling cutters, drill pointing apparatus and methods in accordance with the present invention it is possible to produce high performance drill screws within exacting tolerances at rates of production which are significantly greater than were previously obtainable.

While the preferred embodiment of the present invention has been shown and described, it is to be understood that variations in structure, obvious to those having ordinary skill in the art, and are intended to fall within the scope of the appended claims.

Claims

1. An apparatus, for consistently producing within exacting tolerances drill screws having drilling tips (17) with at least two flutes (38, 40), comprising: an indexable turret (14) for intermittently conveying successive screw blanks (26) having exposed axially extending shanks along a path of travel; a cam operated milling station (10) adjacent said path including a motor driven spindle (16) for mounting a pointing cutter (18) with its axis of rotation inclined to the axis of a screw blank at the milling station, the pointing cutter (18) having a concave profile and forming one of a plurality of form relieved rotary milling cutters (18, 19) used to form said drilling tips; and means (29) for firmly holding said screw blanks (26) against uplift and rotational forces resulting from interaction between said screw blanks (26) and said cutters (18, 19); characterised by

a) means (32) for adjusting the position of the pointing cutter (18) in a direction along the axis of rotation of the pointing cutter (18), in order precisely to control the size and orientation of heel portions (34) of said drilling tips,

b) means (20) for rotating said cutters at a rate of approximately 304.8 surface meters (1000 surface feet) per minute, and

c) said holding means (29) being capable of exerting a downward axial force on said screw blanks (26) of between 889.64 and 1556.87 N (200 and 350 pounds) inclusive.

2. An apparatus according to claim 1, including means (30, X) for controlling the cut per tooth of said cutters whereby the life of said cutters can be maximized despite variations in stock material and whereby the size and shape of burrs resulting from the formation of said tips can be controlled.

blanks while Figs. 9 and 10 show the preferred form of milling cutters used to form flutes in screw blanks. The teeth 50 have relieved portions 51 to prevent friction, curved cutting edges 52 to create the desired forms in the screw blanks, and significant spaces 53 between the teeth to prevent build-up of removed material. It has been found that by using cutters between 20 and 32 teeth and diameters between 2.0 and 3.5 inches (5.08 and 8.89 cm) inclusive, and by carefully controlling the rotational speed and thereby the cut per tooth of the milling cutters, the life of the cutters can be maximized; while at the same time the quality of the end product can be improved in terms of accuracy, repeatability of performance, and the output of the drill pointing machine can be improved. This is a result, at least in part, because, as the output of the machine is increased, the speed at which the cutters are moved into engagement with the blank and the resulting cut per tooth of the cutters would be excessive without the ability to increase the rotational speed of the cutters to compensate for the increased amount of material cut by the tooth. By having relatively few teeth on the perimeter of the cutter the extent to which each tooth may be sharpened will be increased because the sharpening of the cutters is accomplished by grinding the faces of the teeth rather than by profile grinding.

It has also been found that potential interference between the fluting cutters 19 and the turret 14 makes the use of small diameter cutters desirable, especially when milling short screw blanks because in those cases only a small amount of the screw blank is exposed. It has been determined that the cutters described above as having diameters as small as 5.21 cm (2.05 inches) can be used with satisfactory results in terms of cutter life and burr formation as well as output rate and quality control with screws as short as $\frac{5}{16}$ inches (0.79 cm).

By using small diameter form relieved milling cutters with relatively few teeth, and by rotating such cutters at unusually high rates which approach 304.8 surface meters (1000 surface feet) per minute, optimum use can be made of the cutters and increased rates of production can be achieved without sacrificing quality.

It should also be noted that in some cases it may be desirable to include a chip breaking feature on either the pointing cutter 18 or the fluting cutter 19. Figs. 11 and 12 show pointing cutters 18 with ribs 41 formed on each tooth thereof. The ribs are aligned on the cutter to form a single trough 42 on each heel portion 34 of the tip 17 of the blank 26. However, in the preferred embodiment of a screw incorporating a chip breaking feature on the heel portions, the troughs on opposite heel portions are not equidistant from the center of the blank so that in a workpiece the cutting edge on one side of the screw will remove the rib formed by the trough on the opposite side of the screw. It should be noted that by placing a rib in an off-center position on the pointing cutter and by using cutters in the manner shown in Figs. 11 and 12 where the rib 41 is on the

upper portion when forming one heel portion and the rib 41 is on the lower portion when forming the other heel portion, a single form of cutter can be used without the need for right and left hand forms.

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While the preferred embodiment of the present invention has been shown and described, it is to be understood that variations in structure, obvious to those having ordinary skill in the art, and are intended to fall within the scope of the appended claims.

Claims

1. An apparatus, for consistently producing within exacting tolerances drill screws having drilling tips (17) with at least two flutes (38, 40), comprising: an indexable turret (14) for intermittently conveying successive screw blanks (26) having exposed axially extending shanks along a path of travel; a cam operated milling station (10) adjacent said path including a motor driven spindle (16) for mounting a pointing cutter (18) with its axis of rotation inclined to the axis of a screw blank at the milling station, the pointing cutter (18) having a concave profile and forming one of a plurality of form relieved rotary milling cutters (18, 19) used to form said drilling tips; and means (29) for firmly holding said screw blanks (26) against uplift and rotational forces resulting from interaction between said screw blanks (26) and said cutters (18, 19); characterised by

a) means (32) for adjusting the position of the pointing cutter (18) in a direction along the axis of rotation of the pointing cutter (18), in order precisely to control the size and orientation of heel portions (34) of said drilling tips,

b) means (20) for rotating said cutters at a rate of approximately 304.8 surface meters (1000 surface feet) per minute, and

c) said holding means (29) being capable of exerting a downward axial force on said screw blanks (26) of between 889.64 and 1556.87 N (200 and 350 pounds) inclusive.

2. An apparatus according to claim 1, including means (30, X) for controlling the cut per tooth of said cutters whereby the life of said cutters can be maximized despite variations in stock material and whereby the size and shape of burrs resulting from the formation of said tips can be controlled.



3. An apparatus according to claim 2, wherein the means for controlling the cut per tooth of said cutters includes means (30) for adjusting the rotational speed thereof.

4. An apparatus according to any preceding claim, wherein said cutters (18, 19) have approximately between 20 and 32 teeth (50) each and are between 5.08 and 8.89 cm (2.0 and 3.5 inches) diameter inclusive.

5. A method, for producing drill screws having drilling tips, comprising the steps of: using an indexable turret (14) for intermittently conveying successive screw blanks (26) having head portions and axially extending shank portions along a path of travel with tips of said shanks exposed; shaping the drilling tips (17) of said screw blanks with a plurality of form relieved rotary milling cutters (18, 19) mountable on motor driven spindles (16) which are pivotable into engagement with said screw shanks at cam operated milling stations, one milling station (10) including a pointing cutter (18) having a concave profile to be mounted with its axis of rotation inclined to the axis of a screw blank at said one milling station; and applying an axially downward load to said successive screw blanks (26) in order to prevent rotational and axial movement thereof; characterised by

a) adjusting the position of the pointing cutter (18) in a direction along the axis of rotation of the pointing cutter (18), in order precisely to control the size and orientation of heel portions (34) of said drilling tips,

b) variably adjusting the cut per tooth of said cutters, and

c) applying the axially downward load to between 889.64 and 1556.87 N (200 and 350 pounds) inclusive,

whereby the life of said cutters (18, 19) may be maximized and the size and shape of burrs resulting from the formation of said tips can be precisely controlled.

6. A method according to claim 5, wherein adjusting the cut per tooth is achieved by controlling the rotational speed of said cutters.

Patentansprüche

1. Gerät zur reproduzierbaren Erzeugung von Bohrschrauben innerhalb einer Toleranzen, wobei die Bohrschrauben Bohrspitzen (17) mit mindestens zwei Nuten (38, 40) aufweisen, mit einem schaltbaren Revolverkopf (14) zum intermittierenden Fördern aufeinanderfolgender Schraubenrohlinge (26) mit exponierten, sich axial erstreckenden Schäften entlang einem Bewegungspfad, einer nockenbetätigten Frässtation (10) nahe dem Pfad mit einer motorgetriebenen Welle (16) zur Montage eines Schärf-schneidwerkzeuges (18), dessen Drehachse zur Achse eines Schraubenrohlings in der Frässtation geneigt ist, wobei das Schärf-schneidwerkzeug (18) eine konkaves Profil aufweist und eines aus einer Vielzahl von hinterdrehten Drehfrässhneidwerkzeugen (18, 19) bildet, die zur

Ausformung der Bohrspitzen benutzt werden, und Mitteln (29) zum sicheren Halten der Schraubenrohlinge (26) gegen Heben und Drehkräfte, die durch die Interaktion zwischen den Schraubenrohlingen (26) und den Schneidwerkzeugen (18, 19) entstehen, gekennzeichnet durch:

a) Mittel (32) zum Einstellen der Stellung des Schärf-schneidwerkzeuges (18) in Richtung der Drehachse des Schärf-schneidwerkzeuges (18), um die Größe und Ausrichtung der Schneidrückenabschnitte (34) der Bohrspitzen genau zu steuern,

b) Mittel (20) zum Drehen des Schneidwerkzeuges mit einer Umfangsgeschwindigkeit von etwa 304,8 m pro Minute (1000 Fuß pro Minute) und

c) Haltemittel (29), die eine axiale, nach unten gerichtete Kraft von zwischen 889,64 und inklusive 1556,87 N (200 und 350 Pfund) auf die Schraubenrohlinge (26) ausüben.

2. Gerät nach Anspruch 1, gekennzeichnet durch Mittel (30, X) zum Steuern des Schnitts pro Zahn des Schneidwerkzeugs, wodurch die Lebensdauer des Schneidwerkzeugs trotz Veränderungen des Werkstückwerkstoffes maximiert werden kann, und wodurch die Größe und Gestalt des Grats aus der Bildung der Spitzen gesteuert werden können.

3. Gerät nach Anspruch 2, dadurch gekennzeichnet, daß die Mittel zum Steuern des Schnitts pro Zahn des Schneidwerkzeugs Mittel (30) zur Einstellung von dessen Drehgeschwindigkeit aufweisen.

4. Gerät nach einem der vorangegangenen Ansprüche, dadurch gekennzeichnet, daß die Schneidwerkzeuge (18, 19) jeweils etwa zwischen 20 und 32 Zähne (50) aufweisen und einen Durchmesser zwischen 5,08 und 8,89 cm (2,0 und 3,5 Zoll) inklusive aufweisen.

5. Verfahren zum Erzeugen von Bohrschrauben mit Bohrspitzen mit dem Schritten: Einsatz eines schaltbaren Revolverkopfes (14) zum intermittierenden Fördern aufeinanderfolgender Schraubenrohlinge (26) mit Köpfschnitten und sich axial erstreckenden Schaftabschnitte entlang einem Bewegungspfad, wobei die Spitzen der Schäfte exponiert sind, Formen der Bohrspitzen (17) der Schraubenrohlinge mit einer Vielzahl von hinterdrehten Drehfrässhneidwerkzeugen (18, 19), die auf motorgetriebenen Wellen (16) montierbar sind, die in Eingriff mit den Schraubenrohlingen in nockenbetätigten Frässtationen schwenkbar sind, wobei eine Frässtation (10) ein Schärf-schneidwerkzeug (18) mit einem konkaven Profil aufweist, das mit seiner Drehachse zur Achse eines Schraubenrohlings in der einen Frässtation geneigt angeordnet ist, und Aufbringen einer axial gerichteten Kraft auf die aufeinanderfolgenden Schraubenrohlinge (26), um deren Dreh- und Axialbewegung zu verhindern, gekennzeichnet durch:

a) Einstellen der Stellung des Schärf-schneidwerkzeuges (18) in einer Richtung entlang der Drehachse des Schärf-schneidwerkzeuges (18),



um die Größe und Ausrichtung der Schneidrückenabschnitte (34) der Bohrspitzen genau zu steuern,

b) veränderbares Einstellen des Schnittes per Zahn des Schneidwerkzeuges, und

c) Aufbringen der axial nach unten gerichteten Kraft von zwischen 889,64 und 1556,87 N (200 und 350 Pfund) inklusive,

wodurch die Lebensdauer des Schneidwerkzeuges (18, 19) maximiert werden und die Größe und Gestalt des Grats aus der Bildung der Spitzen genau gesteuert werden kann.

6. Verfahren nach Anspruch 5, dadurch gekennzeichnet, daß das Einstellen des Schnittes per Zahn durch Steuern der Drehgeschwindigkeit des Schneidwerkzeuges erreicht wird.

Revendications

1. Appareil pour produire de façon uniforme, dans des tolérances rigoureuses, des vis perceuses comportant des pointes de perçage (17) ayant au moins deux cannelures (38, 40), comprenant: une tourelle diviseuse (14) pour transporter par intermittence des ébauches de vis successives (26) comportant des tiges exposées, s'étendant axialement, suivant une trajectoire de course; un poste (10) de fraisage actionné par came, adjacent à ladite trajectoire, comprenant une broche (16) entraînée par un moteur pour le montage d'une fraise (18) à tailler en pointe dont l'axe de rotation est incliné par rapport à l'axe d'une ébauche de vis dans le poste de fraisage, la fraise (18) à tailler en pointe ayant un profil concave et formant l'une de plusieurs fraises rotatives détalonnées (18, 19) utilisées pour former lesdites pointes de perçage; et des moyens (29) pour maintenir fermement lesdites ébauches de vis (26) contre des forces de soulèvement et de rotation résultant d'une interaction entre lesdites ébauches des vis (26) et lesdites fraises (18, 19); caractérisé par

a) des moyens (32) destinés à régler la position de la fraise (18) à tailler en pointe dans une direction le long de l'axe de rotation de la fraise (18) à tailler en pointe, afin de commander avec précision la dimension et l'orientation de parties de talon (34) desdites pointes de perçage,

b) des moyens (20) destinés à faire tourner lesdites fraises à une vitesse d'environ 304,8 mètres de surface (1000 feet de surface) par minute, et

c) lesdits moyens de maintien (29) étant capables d'exercer une force axiale vers le bas sur lesdites ébauches de vis (26) comprise entre 889,64 et 1556,87 N (200 et 350 pounds), inclus.

2. Appareil selon la revendication 1, comprenant des moyens (30, X) destinés à commander la coupe par dent desdites fraises afin que la durée

de vie desdites fraises puisse être maximisée malgré des variations de la matière première et de manière que la dimension et la forme des bavures résultant de la formation desdites pointes puissent être maîtrisées.

3. Appareil selon la revendication 2, dans lequel les moyens destinés à commander la coupe par dent desdites fraises comprennent des moyens (30) destinés à régler leur vitesse de rotation.

4. Appareil selon l'une quelconque des revendications précédentes, dans lequel lesdites fraises (18, 19) ont approximativement entre 20 et 32 dents (50) chacune et ont un diamètre compris entre 5,08 et 8,89 cm (2,0 et 3,5 inches) inclus.

5. Procédé pour la production de vis perceuses comportant des pointes de perçage, comprenant les étapes qui consistent: à utiliser une tourelle diviseuse (14) pour transporter par intermittence des ébauches de vis successives (26) ayant des parties de tête et des parties de tige s'étendant axialement le long d'une trajectoire de course, les pointes desdites tiges étant exposées; à façonner les pointes de perçage (17) desdites ébauches de vis au moyen de plusieurs fraises rotatives détalonnées (18, 19) pouvant être montées sur des broches (16) entraînées par moteur qui peuvent être amenées par pivotement en contact avec lesdites tiges de vis dans des postes de fraisage actionnés par came, un poste de fraisage (10) comprenant une fraise (18) à tailler en pointe ayant un profil concave, destinée à être montée de façon que son axe de rotation soit incliné par rapport à l'axe d'une ébauche de vis dans ledit poste de fraisage; et à appliquer une charge axialement vers le bas sur lesdites ébauches de vis successives (26) pour en empêcher un mouvement de rotation et un mouvement axial; caractérisé par

a) un réglage de la position de la fraise (18) à tailler en pointe dans une direction suivant l'axe de rotation de la fraise (18) à tailler en pointe, afin de commander avec précision la dimension et l'orientation de parties de talon (34) desdites pointes de perçage,

b) à régler de façon variable la coupe par dent desdites fraises, et

c) à appliquer la charge axialement vers le bas entre 889,64 et 1556,87 N (200 et 350 pounds), inclus,

de manière que la durée de vie desdites fraises (18, 19) puisse être maximisée et que la dimension et la forme des bavures résultant de la formation desdites pointes puissent être maîtrisées avec précision.

6. Procédé selon la revendication 5, caractérisé en ce que le réglage de la coupe par dent est réalisé par une commande de la vitesse de rotation desdites fraises.

